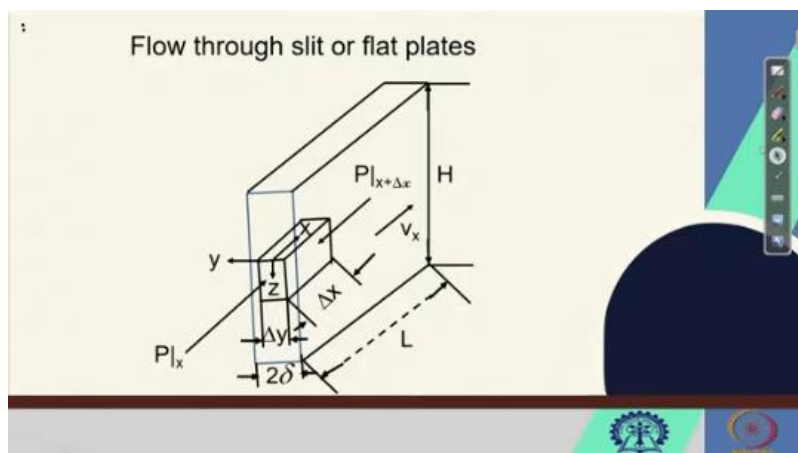


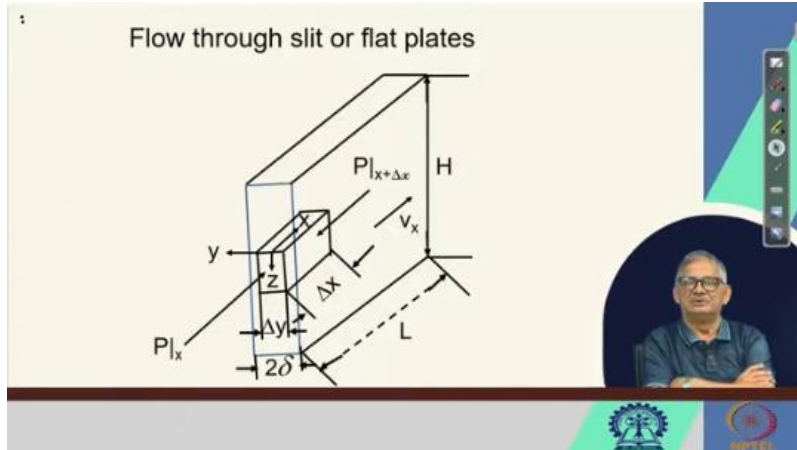
IMPACT OF FLOW OF FLUIDS IN FOOD PROCESSING AND PRESERVATION

Lecture27

LECTURE 27 : FLOW BEHAVIOUR THROUGH NARROW SLIT

Good morning, my dear friends, students, boys, and girls. We are handling the course: flow through pipes, flow through annulus, flow through some slits or flat plates. Some of them we have already done, right? Maybe flow through a slit or a similar thing we have done earlier also. But why am I inclined to repeat here?

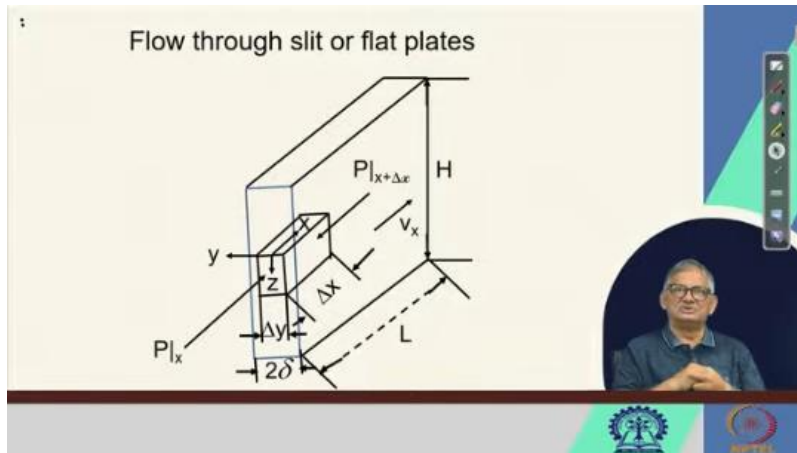




It is because, as I said earlier, if you know these flow behaviors, then you can find out. What is happening during homogenization. If you know how homogenization is made, that fluid at high pressure is passed through a very narrow slit, and then the size of the fat globules, which may be 2 to 30 microns in size or even more. They are shattered and disintegrated into smaller uniform sizes.

This helps to preserve the milk for a longer period, right? That is why homogenization is I gave an example of milk; it could be some other many things. So, that is why I do not know whether it was done earlier, but maybe in a different way. So, we are doing flow through a slit, and after this, we will quickly go through because we may have some points which are already handled; we will do some problems and solutions.

So, that is the fundamental or prime reason why I am bringing this here also. So, as you see from the pictorial view, we have taken a small volume element. Right, and this is in the x and y axis, and the third dimension is H, right. delta y, delta z, and the third dimension is x. So, we have taken the volume element and that the thickness of the volume element is 2δ , and we have to find out the pressure, more than pressure, velocity distribution, and shear stress distribution.



Right. So, similar to the pipe flow or falling film, we can use force balance on an infinitesimally small volume element of size Δx by Δy , w by Δx by Δy , and this is 2δ , sorry again, that cut and paste problem. So, Δx by Δy . OK, and W . So, like previous cases, the net convective volume or convective momentum flux is 0, since the flow is fully developed and in steady state.

Similar to pipe flow or falling film, we can use force balance on an infinitesimally small volume element of size Δx , Δy , w . Like previous cases, the net convective momentum flux is zero since the flow is fully developed and steady.

Net rate of momentum efflux due to molecular transport
 $= \tau_{yx}|_{y+\Delta y} \Delta x W - \tau_{yx}|_y \Delta x W$

Net Pressure forces = $p|_{x+\Delta x} \Delta y W - p|_x \Delta y W$

Sum of the forces = $(\tau_{yx}|_{y+\Delta y} - \tau_{yx}|_y) \Delta x W$
 $+ (p|_{x+\Delta x} - p|_x) \Delta y W = 0$, or,

$$\frac{(\tau_{yx}|_{y+\Delta y} - \tau_{yx}|_y)}{\Delta y} = - \frac{(p|_{x+\Delta x} - p|_x)}{\Delta x}$$

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$$\frac{(\tau_{yx}|_{y+\Delta y} - \tau_{yx}|_y)}{\Delta y} = - \frac{(p|_{x+\Delta x} - p|_x)}{\Delta x}$$

So, we can also write that the rate of momentum efflux due to molecular transport could be τ_{yx} at $y + \Delta y$ into area Δx into w minus τ_{yx} at y into $\Delta x w$, that is net, OK, mind it. And net pressure forces are P at $x + \Delta x$ minus P at x , obviously, into the area that is Δy into w . Then, if we take the sum of the forces, that is τ_{yx} at $y + \Delta y$ minus τ_{yx} at y times the area $\Delta x w$ plus P at $x + \Delta x$ minus P at x into area Δy into w . So, this is equal to 0. So, we can write

τ_{yx} at $y + \Delta y$ minus τ_{yx} at y over Δy is equal to p at $x + \Delta x$ minus p at x over Δx , ok. Now, putting the limit and then according to the definition of derivative, we can write $\Delta y \Delta y$ is equal to minus $\Delta P / \Delta x$ or $\Delta P / \Delta x$ is equal to minus $\Delta P / L$, as pressure decreases with increase in L , the negative sign is there. So, the negative sign is because the pressure is decreasing due to the increase in length.

or, $\frac{\partial \tau_{yx}}{\partial y} = -\frac{\partial p}{\partial x}$

$\frac{\partial p}{\partial x} = -\frac{\Delta p}{L}$ As pressure decreases with increase in L .

$\therefore \frac{\partial \tau_{yx}}{\partial y} = \frac{\Delta p}{L}$

Integrating we get, $\tau_{yx} = \frac{\Delta p}{L} y + C_1$

B.C., at $y = 0, \tau_{yx} = 0; \therefore C_1 = 0; \text{ and } \tau_{yx} = \frac{\Delta p}{L} y$

So, we can write $\Delta \tau_{yx} / \Delta y$ is equal to $\Delta P / L$, and integrating, we can write that τ_{yx} is equal to $\Delta P / L$ into y plus C_1 . So, we have to find out the integral constant. So, that is why the boundary conditions, and the boundary condition is that at y is equal to 0, τ_{yx} is equal to 0, therefore, C_1 is 0, therefore, τ_{yx} is $\Delta P / L$ into y . So, again using the definition of shear stress in terms of viscosity, we can write $\mu \Delta v_x / \Delta y$ is equal to τ_{yx} is equal to $\Delta P / L$ into y .


$$\text{or, } \frac{\partial \tau_{yx}}{\partial y} = -\frac{\partial p}{\partial x}$$

$$\frac{\partial p}{\partial x} = -\frac{\Delta p}{L} \quad \text{As pressure decreases with increase in L.}$$

$$\therefore \frac{\partial \tau_{yx}}{\partial y} = \frac{\Delta p}{L}$$

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And then integrating, we can write v_x is equal to minus delta p by 2 mu L into y square plus C_2 , and the boundary condition is v_x is equal to 0 at y is equal to plus minus del, because we have taken $y, 2 \text{ del}$, you remember 2 del means, one plus del, & one minus del, this is 2 del . So, we get from there the value of the integral constant C_2 as delta p by 2 mu L into del square. Therefore, v_x is equal to delta p by 2 mu L into del square minus y square, and that can be simplified as delta p del (δ) square by 2 mu into $1 - \left(\frac{y}{\delta}\right)^2$ whole square, again this is parabolic in nature. So, now, at y equals to 0, v_x is v_{\max} , and that is delta p del square by 2 mu L. Average velocity is like this $v_{\text{average}} = \frac{1}{A} \int_0^L v_x dx dy$.

$$U \sin g - \mu \frac{\partial v_x}{\partial y} = \tau_{yx} = \frac{\Delta p}{L} y$$

$$\text{Integrating, } v_x = -\frac{\Delta p}{2\mu L} y^2 + C_2$$

B.C., $v_x = 0, \text{ at } y = \pm \delta$

we get $C_2 = \frac{\Delta p}{2\mu L} \delta^2$

$$\therefore v_x = \frac{\Delta p}{2\mu L} (\delta^2 - y^2) = \frac{\Delta p \delta^2}{2\mu L} \left[1 - \left(\frac{y}{\delta}\right)^2 \right]$$


And that is equal to L by del into L into 0 to del $v_x dy$. Substituting the values of v_x and taking out the constants out of the integration, that is, delta P del by 2 mu L, integration between 0 to del of $1 - \left(\frac{y}{\delta}\right)^2$ into dy . So, that is delta P del by 2 mu L into del minus del cube by 3 del square, that is, delta P into del square by 3 mu L. We have already seen that v_{\max} is delta P del square by 2 mu L, here it is delta P del square by

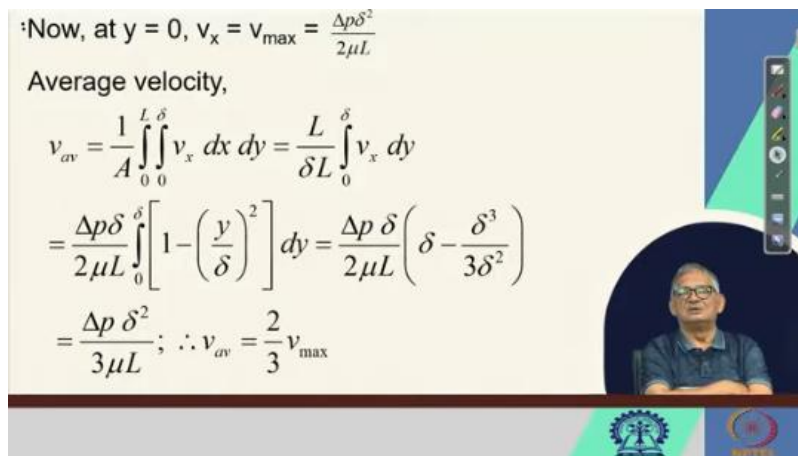
$3 \mu L$. So, average is nothing but $2/3$ of v_{\max} , right. Hence, velocity distribution as it was in the falling film and those in slip flow are analogous.

Now, at $y = 0$, $v_x = v_{\max} = \frac{\Delta p \delta^2}{2\mu L}$

Average velocity,

$$v_{av} = \frac{1}{A} \int_0^L \int_0^\delta v_x dx dy = \frac{L}{\delta L} \int_0^\delta v_x dy$$

$$= \frac{\Delta p \delta}{2\mu L} \int_0^\delta \left[1 - \left(\frac{y}{\delta} \right)^2 \right] dy = \frac{\Delta p \delta}{2\mu L} \left(\delta - \frac{\delta^3}{3\delta^2} \right)$$

$$= \frac{\Delta p \delta^2}{3\mu L}; \therefore v_{av} = \frac{2}{3} v_{\max}$$


So, as H is much much greater than 2δ , the hydraulic diameter of the slit flow becomes 4δ and therefore, the Reynolds number can be written as N_{Re} is 4 average δ ρ by μ . Fanning friction factor, which we have defined earlier as f , equals to τ_w at the wall, shear stress at the wall over product of, product of velocity head and density, right. So, ρv_{av} by 2 or τ_w is $\Delta P \delta$ by capital L , equals to $3 \mu L$ average by δ^2 into δ by L . So, that is 3μ $v_{average}$ over δ .

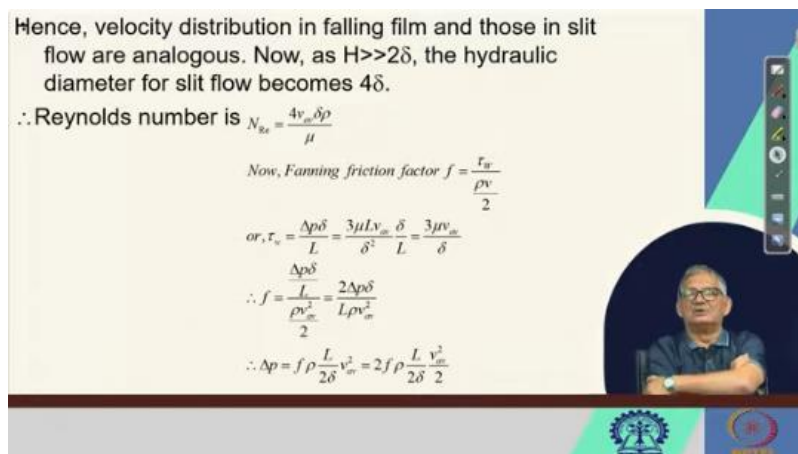
Hence, velocity distribution in falling film and those in slit flow are analogous. Now, as $H \gg 2\delta$, the hydraulic diameter for slit flow becomes 4δ .

\therefore Reynolds number is $N_{Re} = \frac{4v_{av}\delta\rho}{\mu}$

Now, Fanning friction factor $f = \frac{\tau_w}{\rho v}$

$$\text{or, } \tau_w = \frac{\Delta p \delta}{L} = \frac{3\mu L v_{av}}{\delta^2} \cdot \frac{\delta}{L} = \frac{3\mu v_{av}}{\delta}$$

$$\therefore f = \frac{\tau_w}{\rho v_{av}^2} = \frac{2\Delta p \delta}{L \rho v_{av}^2}$$

$$\therefore \Delta p = f \rho \frac{L}{2\delta} v_{av}^2 = 2f \rho \frac{L}{2\delta} \frac{v_{av}^2}{2}$$


Hence, velocity distribution in falling film and those in slit flow are analogous. Now, as $H \gg 2\delta$, the hydraulic diameter for slit flow becomes 4δ .

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$$\text{or, } \tau_w = \frac{\Delta p \delta}{L} = \frac{3\mu L v_{av} \delta}{\delta^2 L} = \frac{3\mu v_{av}}{\delta}$$

$$\therefore f = \frac{\frac{\Delta p \delta}{L}}{\rho v_{av}^2} = \frac{2\Delta p \delta}{L \rho v_{av}^2}$$

$$\therefore \Delta p = f \rho \frac{L}{2\delta} v_{av}^2 = 2f \rho \frac{L}{2\delta} \frac{v_{av}^2}{2}$$

Therefore, f is ΔP del by L over ρv_{average} square by 2 and this is equal to 2 ΔP del by L into ρv_{average} square. Therefore, ΔP is f into ρ into L by 2 del into v_{average} square, that is equal to 2 $f \rho$ rather into L by 2 del into v_{average} square by 2. So, by substituting expressions for v_{average} into Fanning friction factor we can write, f is 2 ΔP del by $L \rho v_{\text{average}}$ square is equal to 2 into 3 $\mu L v_{\text{average}}$ del by del square $L \rho v_{\text{average}}$ square. that is equal to 6 μ by $\Delta P \rho v_{\text{average}}$ is equal to 24 by 4 del ρv_{average} square v_{average} by μ .

Substituting expression for v_{av} into Fanning friction factor

$$f = \frac{2\Delta p \delta}{L \rho v_{av}^2} = \frac{2 \times 3\mu L v_{av} \delta}{\delta^2 L \rho v_{av}^2} = \frac{6\mu}{\delta \rho v_{av}} = \frac{24}{4\delta \rho v_{av}} \frac{v_{av}}{\mu}$$

$$= \frac{24}{N_{Re}} \quad \text{This means } f \text{ value is 50\% more than that of pipe flow}$$

So, Fanning friction factor for Pipe flow in the laminar range is

$$f = \frac{16}{N_{Re}}, \text{ where, } N_{Re} = \frac{D v_{av} \rho}{\mu}$$

$$\text{where as, for slit flow, } f = \frac{24}{N_{Re}}, \text{ where, } N_{Re} = \frac{4\delta v_{av} \rho}{\mu}$$

So, that is nothing but 24 by N_{Re} . This means that the f value is 50 percent more than that of the flow through the pipe. So, finding the friction factor for pipe flow in the laminar range is f equals to 16 by N_{Re} , where N_{Re} is $D v_{\text{average}} \rho$ by μ . Whereas, for slit flow, f is 24 by N_{Re} , where, of course, N_{Re} is 4 del $v_{\text{average}} \rho$ by μ , right? Now, we come to some problem solutions because, most of the time, I, not only me, but many faculties, do say that solving problems makes the subject easier to understand.

So, we are given a problem; here is the problem: A plate heat exchanger is used to sterilize apple juice. The gap between the plates is 10 millimeters and 3 meters long, rather than 20 millimeters. Assuming the density and viscosity of apple juice to be 1060 kg per meter cubed and 1 into 10 to the power of minus 4, respectively. What is the average velocity and pressure drop if the Reynolds number is 1200? So, we have stated the problem. For understanding, we repeat: A plate heat exchanger is used to sterilize the apple juice.

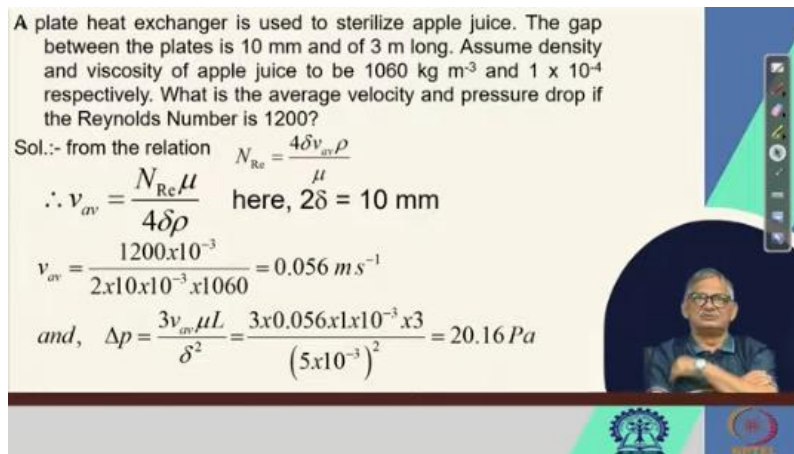
A plate heat exchanger is used to sterilize apple juice. The gap between the plates is 10 mm and of 3 m long. Assume density and viscosity of apple juice to be 1060 kg m⁻³ and 1 x 10⁻⁴ respectively. What is the average velocity and pressure drop if the Reynolds Number is 1200?

Sol.:- from the relation $N_{Re} = \frac{4\delta v_{av} \rho}{\mu}$

$$\therefore v_{av} = \frac{N_{Re} \mu}{4\delta \rho} \quad \text{here, } 2\delta = 10 \text{ mm}$$

$$v_{av} = \frac{1200 \times 10^{-3}}{2 \times 10 \times 10^{-3} \times 1060} = 0.056 \text{ m s}^{-1}$$

and, $\Delta p = \frac{3v_{av} \mu L}{\delta^2} = \frac{3 \times 0.056 \times 1 \times 10^{-3} \times 3}{(5 \times 10^{-3})^2} = 20.16 \text{ Pa}$



The gap between the plates, I hope plate heat exchanger, you have seen, or if you have not seen, let me just show you that this is nothing but this type of plate. So, one plate is here, another similar plate could be here. And the fluid flows through this. There are four holes, right? There are four holes in the plate. So, depending on which flow, which hole is open, the flow is accordingly because the next plate will receive or deliver the fluid.

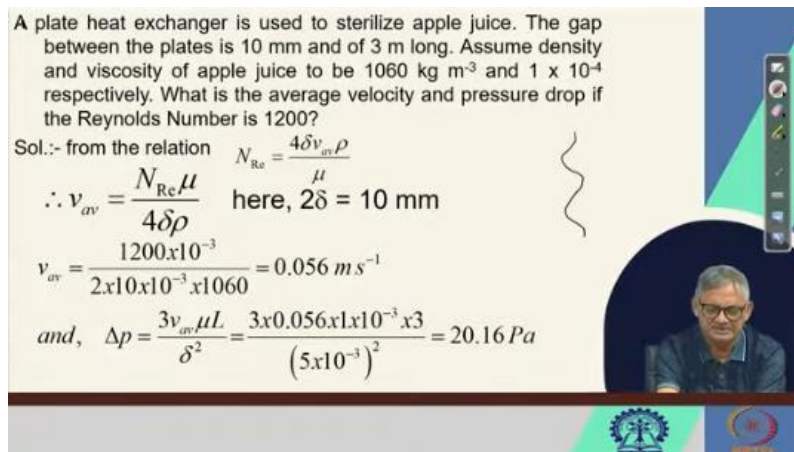
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A plate heat exchanger is used to sterilize apple juice. The gap between the plates is 10 mm and of 3 m long. Assume density and viscosity of apple juice to be 1060 kg m^{-3} and 1×10^{-4} respectively. What is the average velocity and pressure drop if the Reynolds Number is 1200?

Sol:- from the relation $N_{Re} = \frac{4\delta v_{av} \rho}{\mu}$

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So, that is how plate heat exchangers work, and these plate heat exchangers are very useful not only in the food industry but also in many other industries, okay? So, the apple juice is sterilized in a plate heat exchanger, and the gap between the plates is 10 millimeters. And it is 3 meters long, and we are assuming the density and viscosity of the apple juice to be 1060 kg per cubic meter and 1 multiplied by 10 to the power of minus 4, obviously, Pascal second, respectively. What is the average velocity and pressure drop if the Reynolds number is 1200? Now, from the given relation, we know what the value of N_{Re} is.

N_{Re} is 4 del vaverage rho divided by mu. So, vaverage or average velocity is N_{Re} multiplied by mu divided by 4 del rho, right? Here, we are given 2 del, that is, the thickness is 10 millimeters, right? So, if we substitute the values, vaverage is, N_{Re} , given already 1200, right, and mu is 1 Mu, yeah, mu, I think here we have given 10 to the power of minus 4, but we have taken actually 1 multiplied by 10 to the power of minus 3, right?

A plate heat exchanger is used to sterilize apple juice. The gap between the plates is 10 mm and of 3 m long. Assume density and viscosity of apple juice to be 1060 kg m^{-3} and 1×10^{-4} respectively. What is the average velocity and pressure drop if the Reynolds Number is 1200?

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So, there should be a correction. So, instead of 10 to the power of minus 4 here it is 10 to the power of minus 3, right? So, there should be taken, okay?

A plate heat exchanger is used to sterilize apple juice. The gap between the plates is 10 mm and of 3 m long. Assume density and viscosity of apple juice to be 1060 kg m^{-3} and 1×10^{-3} respectively. What is the average velocity and pressure drop if the Reynolds Number is 1200?

Sol:- from the relation $N_{Re} = \frac{4\delta v_{av} \rho}{\mu}$

$\therefore v_{av} = \frac{N_{Re} \mu}{4\delta \rho}$ here, $2\delta = 10 \text{ mm}$

$v_{av} = \frac{1200 \times 10^{-3}}{2 \times 10 \times 10^{-3} \times 1060} = 0.056 \text{ m s}^{-1}$

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So, what we are doing is 2δ is 10 millimeter, v_{average} is 1200 N_{Re} and μ is 1×10^{-3} to the power minus 3 divided by 2δ , that is 2×10 . We have said 2δ is 10 millimeter. So, 4δ means 2×2 . 2×10 , rather, into 10 to the power minus 3, this is in millimeter. So, in meters, it is 10 to the power minus 3 into ρ , ρ is given as 1060. So, this becomes equal to 0.056 meters per second.

A plate heat exchanger is used to sterilize apple juice. The gap between the plates is 10 mm and of 3 m long. Assume density and viscosity of apple juice to be 1060 kg m^{-3} and 1×10^{-3} respectively. What is the average velocity and pressure drop if the Reynolds Number is 1200?

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Right. Therefore, we can find out what is the ΔP ? ΔP is $3 v_{\text{average}} \mu L$ by δ^2 square, or it is 3×0.056 . Right, 3×0.056 into 1×10^{-3} into L , L is 3 meters. So, 3 divided by δ^2 , now 2δ is 10.

So, 1δ is 5, 5×10^{-3} to the power minus 3, all square. So, that becomes 20.16, ΔP , right. What could be the unit? Unit is, of course, Pascal.

So, once we know how much pressure is dropped for such heat exchangers where the apple is getting sterilized, then we can roughly say that around 10 or rather around 20 Pascal is decreased, right, ΔP . Next, another problem we can say is that whole milk is heated in

a tubular heat exchanger having a diameter of 10 millimeters. This is another example of a heat exchanger, right.

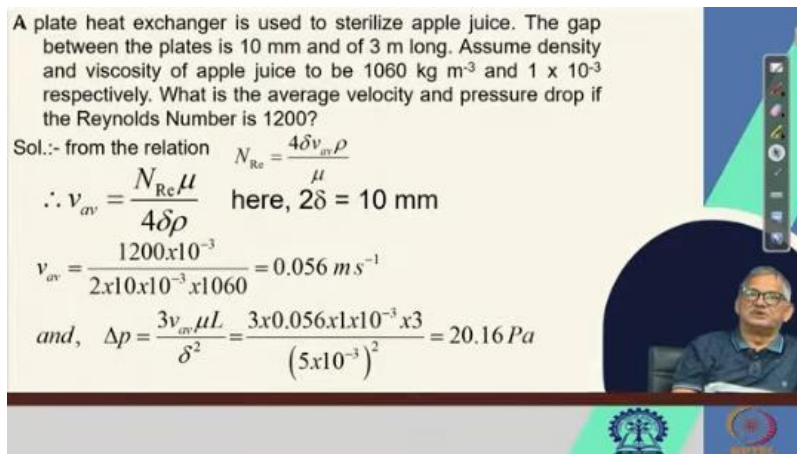
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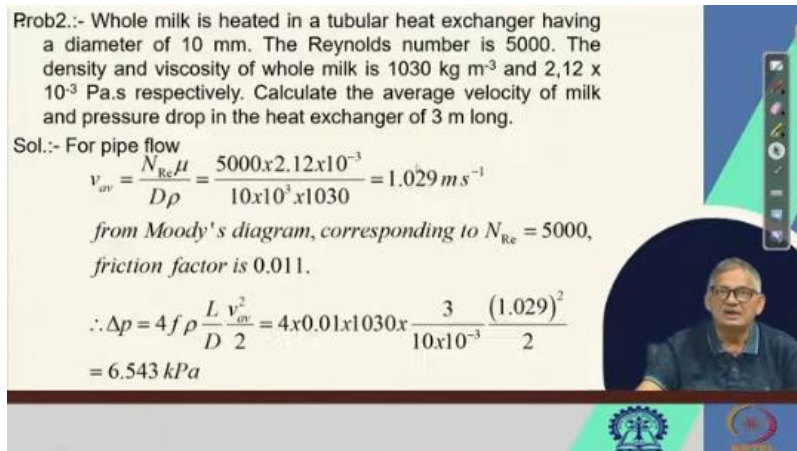
Prob2:- Whole milk is heated in a tubular heat exchanger having a diameter of 10 mm. The Reynolds number is 5000. The density and viscosity of whole milk is 1030 kg m^{-3} and $2.12 \times 10^{-3} \text{ Pa.s}$ respectively. Calculate the average velocity of milk and pressure drop in the heat exchanger of 3 m long.

Sol:- For pipe flow

$$v_{av} = \frac{N_{Re} \mu}{D \rho} = \frac{5000 \times 2.12 \times 10^{-3}}{10 \times 10^{-3} \times 1030} = 1.029 \text{ m s}^{-1}$$

from Moody's diagram, corresponding to $N_{Re} = 5000$, friction factor is 0.011.

$$\therefore \Delta p = 4f \rho \frac{L}{D} \frac{v_{av}^2}{2} = 4 \times 0.011 \times 1030 \times \frac{3}{10 \times 10^{-3}} \times \frac{(1.029)^2}{2}$$

$$= 6.543 \text{ kPa}$$


You see how the flow of fluid is also being used in different parts, different engineering. This is used in the heat exchangers, right. Whole milk is heated in a tubular heat exchanger having a diameter of 10 millimeters, the Reynolds number is 5000, The density and viscosity of whole milk are $1030 \text{ kg per meter cube}$ and $2.12 \times 10^{-3} \text{ Pascal second}$, respectively. Calculate the average velocity of milk and pressure drop in the heat exchanger of 3 meters long.

So, we have read and we can Understand by reading once more that whole milk is heated in a tubular heat exchanger having a diameter of 10 millimeters, the Reynolds number is 5000, density and viscosity of whole milk are $1030 \text{ kg per meter cube}$ and $2.12 \times 10^{-3} \text{ Pascal second}$, respectively. Calculate the average velocity of milk and pressure drop in the heat exchanger of 3 meters long, right. So, all the values are given. So, we can find out differently.

For pipe flow, we have seen that average velocity is N_{Re} general or N_{Re} other μ by $D \rho$. Where N_{Re} is given as 5000, μ is given as 2.12×10^{-3} , and D is given as 10 millimeters. So, $10 \times 10^{-3} \times 1030$. Here also, you see there is a mistake. So, here you mind it is not 10^3 , it is $10^{-3} \times 1030$.

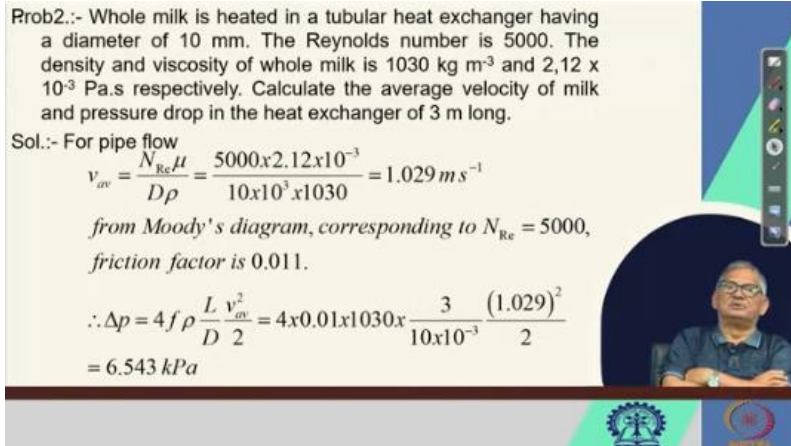
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$$\therefore \Delta p = 4 f \rho \frac{L}{D} \frac{v_{av}^2}{2} = 4 \times 0.011 \times 1030 \times \frac{3}{10 \times 10^{-3}} \frac{(1.029)^2}{2}$$

$$= 6.543 \text{ kPa}$$


So, this becomes equal to 1.029 meters per second, right? As we said earlier, now it is also a heat exchanger. So, earlier we said that the length of the heat exchanger or any such pipe which we consider may not be equal to the one which we are considering. In many cases, it is more than that, and that was established by the great scientist called Moody.

So, based on the Moody's chart, he made a chart based on Moody's chart, we can find out from the Moody's chart corresponding to January 5000, the fanning friction factor is 0.011, right? So, if it is 0.011, then we can say that ΔP is nothing but $4 f \rho L$ by D average square by 2. So, it is $4 f$ is 0.011, you have taken only 1, okay? into 1030 into L 3 meters long. So, 3 divided by D is 10 millimeters.

So, it is 10 into 10 to the power minus 3 into v average is 1.029 whole square over 2. So, this becomes equal to 6.543 kilo Pascal. If you remember, in the previous problem, for apple juice in a plate heat exchanger, we have seen the ΔP is around 20 Pascal. And now, for a tubular heat exchanger with milk,

Prob2:- Whole milk is heated in a tubular heat exchanger having a diameter of 10 mm. The Reynolds number is 5000. The density and viscosity of whole milk is 1030 kg m^{-3} and $2.12 \times 10^{-3} \text{ Pa.s}$ respectively. Calculate the average velocity of milk and pressure drop in the heat exchanger of 3 m long.

Sol:- For pipe flow

$$v_{av} = \frac{N_{Re} \mu}{D \rho} = \frac{5000 \times 2.12 \times 10^{-3}}{10 \times 10^{-3} \times 1030} = 1.029 \text{ m s}^{-1}$$

from Moody's diagram, corresponding to $N_{Re} = 5000$, friction factor is 0.011.

$$\therefore \Delta p = 4 f \rho \frac{L}{D} \frac{v_{av}^2}{2} = 4 \times 0.011 \times 1030 \times \frac{3}{10 \times 10^{-3}} \times \frac{(1.029)^2}{2}$$

$$= 6.543 \text{ kPa}$$

we are finding that the delta P required or obtained is 6.53 kilo Pascal, which was Pascal. So, if it is in Pascal, that was 20 Pascal, here it is 6543 Pascal. So, that means, on the system, depending on the property values, these delta P or any other, that varies, may be widely sometimes, or sometimes may not be widely. So, what I suggest to you is to try to find out from books or the internet or wherever different problems and try to solve them with respect to the profile of the flow of the fluid. Profile, I mean, whether it is with respect to pressure drop or whether it is with respect to velocity distribution or shear transport, shear force distribution, or finding out viscosity, etc., whatever is required, ask for it. So, take that in the spirit of calculating the fluid flow problem. So, you do as many problems as possible, and the more solutions you find, the clearer the subject will become, right?

So, with this, I think we have come to the end of the class, and I thank you all for attending. Obviously, we will move to the next class with a new chapter so that, by this time, you can also bring yourself up to date with the topics we have already covered, okay? Thank you all.

