

Course on Momentum Transfer in Process Engineering
Prof. Tridib Kumar Goswami
Department of Agricultural & Food Engineering IIT Kharagpur
Mod 02 Lecture 06
Equation of motion (Part-2) or Navier Stokes equations

A small recapitulation of the previous class that we have done that is the momentum transfer, how that is being done for a particular component that is a velocity component that is x component of the velocity, V_x acting on the x, y and z directions by the bulk transport as well by the molecular transport, you remember we said that the molecular transport is being done by the molecules of the layers, which are vibrating in staying in the layer, but they are giving the energy or they are exchanging the energy with the adjacent layer molecules, right. This way the two ways of transport of momentum occurring we have done for the one component that is x component. Now we will do for y and z and then sum up all of them and derive the basic equation of motion that is the NAVIER stokes, okay.


(Refer Slide Time: 1:47)

By molecular transport -:

Rate of x component of momentum on face x and $x+\Delta x$
= $\tau_{xx}|_x \Delta y \Delta z$ and $\tau_{xx}|_{x+\Delta x} \Delta y \Delta z$ respectively.

Rate of x component of momentum on face y and $y+\Delta y$
= $\tau_{yx}|_y \Delta x \Delta z$ and $\tau_{yx}|_{y+\Delta y} \Delta x \Delta z$ respectively.

Rate of x component of momentum on face z and $z+\Delta z$
= $\tau_{zx}|_z \Delta x \Delta y$ and $\tau_{zx}|_{z+\Delta z} \Delta x \Delta y$ respectively.



∴ Sum of the convective and molecular transport terms:

$$(\rho v_x v_x|_x - \rho v_x v_x|_{x+\Delta x}) \Delta y \Delta z + (\rho v_y v_x|_y - \rho v_y v_x|_{y+\Delta y}) \Delta x \Delta z + (\rho v_z v_x|_z - \rho v_z v_x|_{z+\Delta z}) \Delta y \Delta x - (\tau_{xx}|_x - \tau_{xx}|_{x+\Delta x}) \Delta y \Delta z + (\tau_{yx}|_y - \tau_{yx}|_{y+\Delta y}) \Delta x \Delta z + (\tau_{zx}|_z - \tau_{zx}|_{z+\Delta z}) \Delta x \Delta y$$

Other terms,
 Pressure force:- $(p|_x - p|_{x+\Delta x}) \Delta y \Delta z$
 Gravity force- $\rho g_x \Delta x \Delta y \Delta z$
 Accumulation -:
 Rate of accumulation of x component of momentum
 $= (\partial(\rho v_x) / \partial t) \Delta x \Delta y \Delta z$

Equating and dividing by $\Delta x \Delta y \Delta z$

$$(\rho v_x v_x|_x - \rho v_x v_x|_{x+\Delta x}) / \Delta x + (\rho v_y v_x|_y - \rho v_y v_x|_{y+\Delta y}) / \Delta y + (\rho v_z v_x|_z - \rho v_z v_x|_{z+\Delta z}) / \Delta z + (\tau_{xx}|_x - \tau_{xx}|_{x+\Delta x}) / \Delta x + (\tau_{yx}|_y - \tau_{yx}|_{y+\Delta y}) / \Delta y + (\tau_{zx}|_z - \tau_{zx}|_{z+\Delta z}) / \Delta z + (p|_x - p|_{x+\Delta x}) / \Delta x + \rho g_x = \partial(\rho v_x) / \partial t$$

or,

$$\partial(\rho v_x) / \partial t = - [\partial(\rho v_x v_x) / \partial x + \partial(\rho v_y v_x) / \partial y + \partial(\rho v_z v_x) / \partial z] - [\partial \tau_{xx} / \partial x + \partial \tau_{yx} / \partial y + \partial \tau_{zx} / \partial z - \partial p / \partial x + \rho g_x]$$

..... (1)

By molecular transport. ✓ ✓

z-comp. x & $x+\Delta x = \tau_{xz}|_x \Delta y \Delta z + \tau_{xz}|_{x+\Delta x} \Delta y \Delta z$

x-comp. y & $y+\Delta y = \tau_{yx}|_y \Delta x \Delta z + \tau_{yx}|_{y+\Delta y} \Delta x \Delta z$

x-comp. z & $z+\Delta z = \tau_{zx}|_z \Delta x \Delta y + \tau_{zx}|_{z+\Delta z} \Delta x \Delta y$

$(\rho u_x u_x|_x - \rho u_x u_x|_{x+\Delta x}) \Delta y \Delta z + \rho u_y u_x|_y - (\rho u_y u_x|_{y+\Delta y}) \Delta x \Delta z$
 $+ (\rho u_z u_x|_z - \rho u_z u_x|_{z+\Delta z}) \Delta x \Delta y - (\tau_{xx}|_x - \tau_{xx}|_{x+\Delta x}) \Delta y \Delta z +$
 $(\tau_{yx}|_y - \tau_{yx}|_{y+\Delta y}) \Delta x \Delta z + (\tau_{zx}|_z - \tau_{zx}|_{z+\Delta z}) \Delta x \Delta y$ ✓

other terms

Pressure: $(p|_x - p|_{x+\Delta x}) \Delta y \Delta z$ ✓

gravity $(\rho g_x \Delta x \Delta y \Delta z)$ ✓

Accumulation: $\frac{\partial (\rho u_x)}{\partial t} \Delta x \Delta y \Delta z$ ✓

So let us follow. So then we had come if you remember we had come up to this that accumulation, right where the volume element was there $\Delta x \Delta y \Delta z$ and we also had taken that by molecular transport by the bulk transport this was for molecular transport, this was for bulk transport we had done, right and then pressure term and the gravity term that is sum of the other forces, right.

(Refer Slide Time: 2:45)

By molecular transport. ✓ ✓

z-comp. x & $x+\Delta x = \tau_{xz}|_x \Delta y \Delta z + \tau_{xz}|_{x+\Delta x} \Delta y \Delta z$

x-comp. y & $y+\Delta y = \tau_{yx}|_y \Delta x \Delta z + \tau_{yx}|_{y+\Delta y} \Delta x \Delta z$

x-comp. z & $z+\Delta z = \tau_{zx}|_z \Delta x \Delta y + \tau_{zx}|_{z+\Delta z} \Delta x \Delta y$

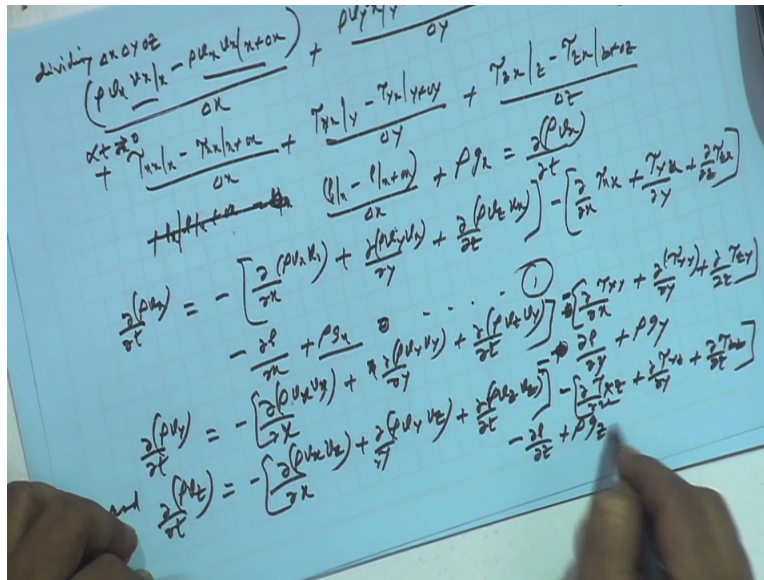
$(\rho u_x u_x|_x - \rho u_x u_x|_{x+\Delta x}) \Delta y \Delta z + \rho u_y u_x|_y - (\rho u_y u_x|_{y+\Delta y}) \Delta x \Delta z$
 $+ (\rho u_z u_x|_z - \rho u_z u_x|_{z+\Delta z}) \Delta x \Delta y - (\tau_{xx}|_x - \tau_{xx}|_{x+\Delta x}) \Delta y \Delta z +$
 $(\tau_{yx}|_y - \tau_{yx}|_{y+\Delta y}) \Delta x \Delta z + (\tau_{zx}|_z - \tau_{zx}|_{z+\Delta z}) \Delta x \Delta y$ ✓

other terms

Pressure: $(p|_x - p|_{x+\Delta x}) \Delta y \Delta z$ ✓

gravity $(\rho g_x \Delta x \Delta y \Delta z)$ ✓

Accumulation: $\frac{\partial (\rho u_x)}{\partial t} \Delta x \Delta y \Delta z$ ✓



From (1)

$$\frac{\partial(\rho v_x)}{\partial t} = \rho \frac{\partial v_x}{\partial t} + v_x \frac{\partial \rho}{\partial t}$$

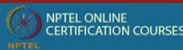
From equation of continuity

$$\frac{\partial \rho}{\partial t} = - \left[\frac{\partial(\rho v_x)}{\partial x} + \frac{\partial(\rho v_y)}{\partial y} + \frac{\partial(\rho v_z)}{\partial z} \right]$$

$$\therefore \frac{\partial(\rho v_x)}{\partial t} = \rho \frac{\partial v_x}{\partial t} - v_x \left[\frac{\partial(\rho v_x)}{\partial x} + \frac{\partial(\rho v_y)}{\partial y} + \frac{\partial(\rho v_z)}{\partial z} \right]$$

The right hand side of eqⁿ (1) can be written as,

$$- \left[\frac{\partial(\rho v_x v_x)}{\partial x} + \frac{\partial(\rho v_y v_x)}{\partial y} + \frac{\partial(\rho v_z v_x)}{\partial z} \right] - \left[\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right] - \frac{\partial p}{\partial x} + \rho g_x$$



So now if we divide in both the sides with del x del y del z, right. If we divide with del x del y del z dividing both the sides, we can write that Rho Vx into Vx at x minus Rho Vx into Vx at x plus delta x, right. This divided by del divided by del x del y del z and we had the on the top this if you remember that this was del y del z. So dividing it to with del x del y del z we take of del y del z it remains del x, right.

Similarly here also del x del y del z we take of del y del z or rather del x del z del y remains and in this case also del x del y del z. So we take of del y del x del z remains, right. Similarly, here also, so dividing all with del x del y del z we get respective terms like that divide by del x right plus Rho Vy Vx at the face y minus Rho Vy Vx at the face y plus delta y over del y plus Rho Vz

at V_x at the face z minus $\rho V_x \rho V_z$ into V_x at the face z plus Δz over Δz , right plus τ_{xx} at the face x minus τ_{xx} at the face x plus Δx over Δx plus τ_{yx} , right τ_{yx} at the face y minus τ_{yx} at the face y plus Δy over Δy plus τ_{zx} at the face z minus τ_{zx} at the face z plus Δz over Δz , right.

So this is equals to and the pressure terms that is p at x plus Δx minus V at x plus Δx minus p at rather sorry, p at x minus p at x plus Δx , it should be p at the written $(\)$ (5:45) p at x minus p at x plus Δx into or divided by Δx was also, we had $\Delta x \Delta y \Delta z$, so here it is Δx . So this plus in ρg rather we had $\Delta x \Delta y \Delta z$ if you remember so that goes off, so ρg_x remains and this is equal to nothing but $\frac{\partial}{\partial t} \rho V_x$ that is the accumulation term, right.

So this applying the theory of limit $\Delta x \Delta y \Delta z$ tends to zero and from the definition of applying this limit $\Delta x \Delta y \Delta z$ tends to zero and applying the definition of derivative, right you know derivative that is out minus in over the Δ . So this is a derivative, so we can write then this is nothing, but $\frac{\partial}{\partial t} \rho V_x$ right. This is equals to minus $\frac{\partial}{\partial x} \rho V_x$ into V_x , right plus $\frac{\partial}{\partial y} \rho V_y$ into V_x , right plus $\frac{\partial}{\partial z} \rho V_z$ into V_x , right. This minus $\frac{\partial}{\partial x} \tau_{xx}$ plus $\frac{\partial}{\partial y} \tau_{yx}$ plus $\frac{\partial}{\partial z} \tau_{zx}$, right. This minus $\frac{\partial p}{\partial x}$ plus ρg_x over this ρg_x this is equals to rather already we have made it equal. So this we can say to be equation number 1, right.

In this case, here you remember that we have applied this concept that limit $\Delta x \Delta y \Delta z$ that tends to zero number 1 and number 2 when limit tends to zero and by the definition of the derivative this out minus in over Δ that is nothing but the derivative that is $\frac{\partial}{\partial x} \rho V_x$ V_x $\frac{\partial}{\partial y} \rho V_y$ V_x $\frac{\partial}{\partial z} \rho V_z$ V_x , right. Similarly $\frac{\partial}{\partial x} \tau_{xx}$ $\frac{\partial}{\partial y} \tau_{yx}$ $\frac{\partial}{\partial z} \tau_{zx}$, right. Here in this case also minus this that is why negative is coming, so $\frac{\partial p}{\partial x}$ and here, we had ρg_x all x, y, z was out. So only ρg_x remaining, right.

So this we can say that equation number 1 and subsequently we can write for the other two components that is for the y component and z component we can also write that in similar to this $\frac{\partial}{\partial t} \rho V_y$ this is equals to minus $\frac{\partial}{\partial y} \rho V_y$ V_y , right ρV_y V_y or rather ρV_x V_y , right and this plus this is $\frac{\partial}{\partial t} \rho V_y$, so $\frac{\partial}{\partial x} \rho V_x$ V_y plus $\frac{\partial}{\partial y} \rho V_y$

$\rho v_x v_x$, right plus $\frac{\partial}{\partial z} \rho v_z v_x$, right. This is for the bulk transport and for molecular transport we can write τ_{xy} , right plus $\frac{\partial}{\partial y} \tau_{yy}$ right plus $\frac{\partial}{\partial z} \tau_{zy}$, right. This plus that $\frac{\partial p}{\partial x}$ or rather here would be minus, because by definition.

So minus $\frac{\partial p}{\partial x}$ plus ρg_x and in the same way we can write the z one right. We are not writing then we will okay, it will take only just a little time $\frac{\partial}{\partial t} \rho v_z$, this is equals to minus $\frac{\partial}{\partial x} \rho v_x v_z$ plus $\frac{\partial}{\partial y} \rho v_y v_z$ plus $\frac{\partial}{\partial z} \rho v_z v_z$, right. So this was like this plus or this plus of course that will come minus ultimately, right. Here you should have been minus; here also it is minus, right. So $\frac{\partial}{\partial x} \tau_{xy}$ or in this case it will be τ_{xz} , right plus $\frac{\partial}{\partial y} \tau_{yz}$ plus $\frac{\partial}{\partial z} \tau_{zz}$, right this minus $\frac{\partial p}{\partial z}$ plus ρg_z , these are the three equations for the three co-ordinates systems, right.

(Refer Slide Time: 12:54)

The image shows handwritten mathematical derivations on a blue notepad. The equations are as follows:

$$\frac{\partial(\rho v_x)}{\partial t} = - \left[\frac{\partial(\rho v_x v_x)}{\partial x} + \frac{\partial(\rho v_x v_y)}{\partial y} + \frac{\partial(\rho v_x v_z)}{\partial z} \right] - \left[\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + \frac{\partial \tau_{xz}}{\partial z} \right] - \frac{\partial p}{\partial x} + \rho g_x$$

$$\frac{\partial(\rho v_y)}{\partial t} = - \left[\frac{\partial(\rho v_x v_y)}{\partial x} + \frac{\partial(\rho v_y v_y)}{\partial y} + \frac{\partial(\rho v_z v_y)}{\partial z} \right] - \left[\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} + \frac{\partial \tau_{yz}}{\partial z} \right] - \frac{\partial p}{\partial y} + \rho g_y$$

$$\frac{\partial(\rho v_z)}{\partial t} = - \left[\frac{\partial(\rho v_x v_z)}{\partial x} + \frac{\partial(\rho v_y v_z)}{\partial y} + \frac{\partial(\rho v_z v_z)}{\partial z} \right] - \left[\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z} \right] - \frac{\partial p}{\partial z} + \rho g_z$$

$$\frac{d(pv_x)}{dt} = \rho \left(\frac{dv_x}{dt} \right) + v_x \left(\frac{dp}{dt} \right)$$
 from equation continuity

$$\frac{dp}{dt} = - \left[\rho \frac{dv_x}{dx} + \rho \frac{dv_y}{dy} + \rho \frac{dv_z}{dz} \right]$$

$$\therefore \frac{d(pv_x)}{dt} = \rho \left(\frac{dv_x}{dt} \right) - v_x \left[\rho \frac{dv_x}{dx} + \rho \frac{dv_y}{dy} + \rho \frac{dv_z}{dz} \right]$$

$$= \rho \left(\frac{dv_x}{dt} \right) + \frac{d(\rho v_x v_x)}{dt} - \left[\rho v_x \frac{dv_x}{dx} + \rho v_x \frac{dv_y}{dy} + \rho v_x \frac{dv_z}{dz} \right]$$

$$= \rho \left(\frac{dv_x}{dt} \right) + \rho v_x \frac{dv_x}{dx} + \rho v_y \frac{dv_x}{dy} + \rho v_z \frac{dv_x}{dz} - \left[\rho v_x \frac{dv_x}{dx} + \rho v_x \frac{dv_y}{dy} + \rho v_x \frac{dv_z}{dz} \right]$$

Now if we remember we had given this was the equation 1, right. So keep in mind that this equation then from that equation we can write $\frac{d}{dt}(\rho v_x)$, right. This is again nothing but $\rho \frac{d}{dt} v_x$ or $\frac{d}{dt}(\rho v_x) + v_x \frac{d}{dt} \rho$, right again this is on x function uv we can write, right. So this from equation of continuity we can write that $\frac{d}{dt} \rho$, this is equals to $-\left[\frac{d}{dx}(\rho v_x) + \frac{d}{dy}(\rho v_y) + \frac{d}{dz}(\rho v_z) \right]$, right. This was taken in the equation of continuity and we can write it here.

So we can write then $\frac{d}{dt}(\rho v_x)$ or rather $\rho \frac{d}{dt} v_x$ is equal to $\rho \frac{d}{dt} v_x + v_x \frac{d}{dt} \rho$, right. So this we can write and if you remember the right of the equation which was this was equation 1 and the right side was this big $-\left[\frac{d}{dx}(\rho v_x) + \frac{d}{dy}(\rho v_y) + \frac{d}{dz}(\rho v_z) \right]$, right.




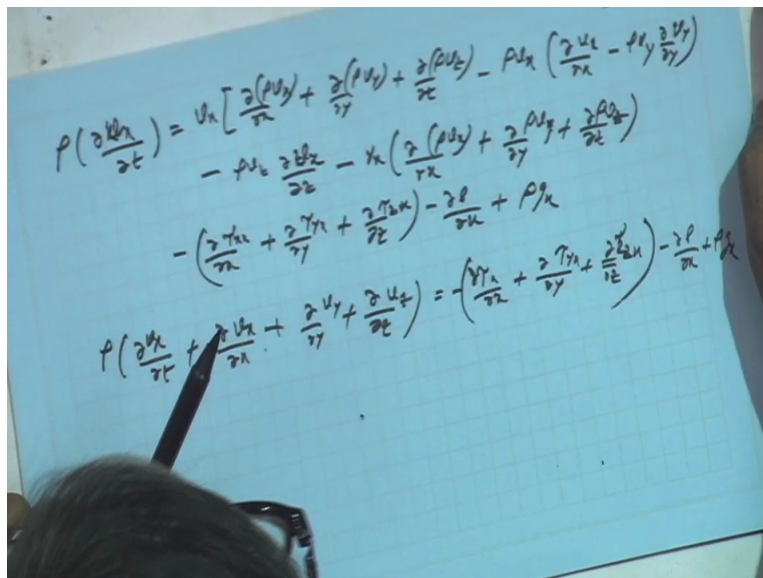
So one term if we take then we can write $-\left[\frac{d}{dx}(\rho v_x) + \frac{d}{dy}(\rho v_y) + \frac{d}{dz}(\rho v_z) \right]$, right. This was like that $-\left[\frac{d}{dx}(\rho v_x) + \frac{d}{dy}(\rho v_y) + \frac{d}{dz}(\rho v_z) \right]$, right. This minus we also had $\frac{d}{dt} \rho$ plus ρg_x , right. So this on further expansion we can write, so this first term can be expanded like this that $-\rho v_x \frac{d}{dx} v_x$ if we take this as u and this as v the minus ρv_x into $\frac{d}{dx} v_x$, right minus $\rho v_y \frac{d}{dy} v_x$ plus minus rather minus since, we have not given in a bracket if you were have given a bracket then we could have written like this, then $\rho v_z \frac{d}{dz} v_x$ rather $\frac{d}{dx}(\rho v_x)$, this is $\frac{d}{dx}(\rho v_x)$ plus $\rho v_x \frac{d}{dx} \rho$, right. This we could have written and this minus v_x times $\frac{d}{dx}(\rho v_x)$

plus del del y of Rho Vy plus Del del z of Rho Vz, right. This term on expansion we can write like this, right as U and V.

(Refer Slide Time: 17:47)

Eq. (1) can be written as

$$\rho \left(\frac{\partial v_x}{\partial t} \right) = -v_x \left[\frac{\partial(\rho v_x)}{\partial x} + \frac{\partial(\rho v_y)}{\partial y} + \frac{\partial(\rho v_z)}{\partial z} \right] - \rho v_x \left(\frac{\partial v_x}{\partial x} \right) - \rho v_y \left(\frac{\partial v_y}{\partial y} \right) - \rho v_z \left(\frac{\partial v_z}{\partial z} \right) - v_x \left[\frac{\partial(\rho v_x)}{\partial x} + \frac{\partial(\rho v_y)}{\partial y} + \frac{\partial(\rho v_z)}{\partial z} \right] - [\partial\tau_{xx} / \partial x + \partial\tau_{yx} / \partial y + \partial\tau_{zx} / \partial z] - \partial p / \partial x + \rho g_x$$

$$\rho \left[\frac{\partial v_x}{\partial t} + \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} \right] = -[\partial\tau_{xx} / \partial x + \partial\tau_{yx} / \partial y + \partial\tau_{zx} / \partial z] - \partial p / \partial x + \rho g_x$$





So if we do like that then we can rewrite this equation one which we have shown you earlier as Rho del Vx del t, this is equals to Vx into del del x of Rho Vx, right plus del del y of Rho Vy plus del del z of Rho Vz minus Rho Vx times del del x of Vx, right minus Rho Vy del del y of Rho Vy, right and also minus Rho Vz del del z of Rho del del z of Vz, right. So this minus Vx del del x of Rho Vx plus del del y of Rho Vy plus del del z of Rho Vz Rho Vx okay Rho Vx. So this also will be Rho Vx. So we can write, so del del Rho Vx del del x, sorry (())(19:30). This is y and this

is z, right ρV_z . This if we write then minus del del x of τ_{xx} plus del del y of τ_{yx} plus del del z of τ_{zx} , right. So this minus del p del x plus ρg_x , right. So this we can write further that we can say that $\rho \frac{Dv_x}{Dt}$ plus del del x of v_x plus del del y of v_y plus del del z of v_z , this is nothing but τ_{xx} plus del del x of τ_{yx} plus del del y of τ_{yx} plus del del z of τ_{zx} , right. So this we can write and of course here, we can with a if we remember that earlier we had taken this and of course (21:09) minus del p del x plus ρg_x was also there, right.



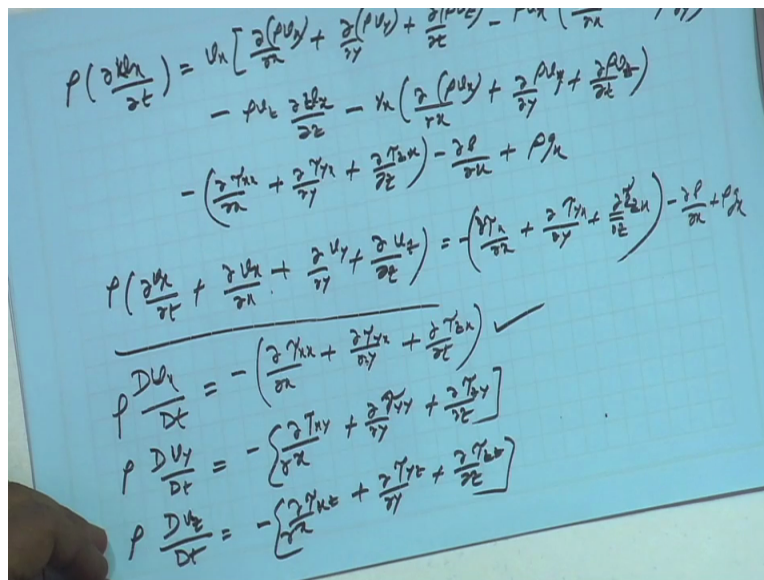
(Refer Slide Time: 21:20)

Or, $\rho \frac{Dv_x}{Dt} = -[\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z}] - \frac{\partial p}{\partial x} + \rho g_x$

Similarly

$\rho \frac{Dv_y}{Dt} = -[\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} + \frac{\partial \tau_{zy}}{\partial z}] - \frac{\partial p}{\partial y} + \rho g_y$

$\rho \frac{Dv_z}{Dt} = -[\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z}] - \frac{\partial p}{\partial z} + \rho g_z$

Handwritten derivation of the x-momentum equation:

$$\rho \left(\frac{\partial v_x}{\partial t} + \frac{\partial v_x}{\partial x} v_x + \frac{\partial v_x}{\partial y} v_y + \frac{\partial v_x}{\partial z} v_z \right) = - \left(\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right) - \frac{\partial p}{\partial x} + \rho g_x$$

$$\rho \frac{Dv_x}{Dt} = - \left(\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right) - \frac{\partial p}{\partial x} + \rho g_x$$

$$\rho \frac{Dv_y}{Dt} = - \left(\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} \right) - \frac{\partial p}{\partial y} + \rho g_y$$

$$\rho \frac{Dv_z}{Dt} = - \left(\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z} \right) - \frac{\partial p}{\partial z} + \rho g_z$$

Using $\tau_{xx} = -\mu \partial v_x / \partial x$, $\tau_{yx} = -\mu \partial v_x / \partial y$, $\tau_{zx} = -\mu \partial v_x / \partial z$
 $\tau_{xy} = -\mu \partial v_y / \partial x$, $\tau_{yy} = -\mu \partial v_y / \partial y$, $\tau_{zy} = -\mu \partial v_y / \partial z$
 $\tau_{xz} = -\mu \partial v_z / \partial x$, $\tau_{yz} = -\mu \partial v_z / \partial y$, $\tau_{zz} = -\mu \partial v_z / \partial z$
 $\partial \tau_{xx} / \partial x = (-\mu) \partial^2 v_x / \partial x^2$, $\partial \tau_{yx} / \partial y = \partial^2 v_x / \partial y^2$, $\partial \tau_{zx} / \partial z = \partial^2 v_x / \partial z^2$
 $\partial \tau_{xy} / \partial x = \partial^2 v_y / \partial x^2$, $\partial \tau_{yy} / \partial y = \partial^2 v_y / \partial y^2$, $\partial \tau_{zy} / \partial z = \partial^2 v_y / \partial z^2$
 $\partial \tau_{xz} / \partial x = \partial^2 v_z / \partial x^2$, $\partial \tau_{yz} / \partial y = \partial^2 v_z / \partial y^2$, $\partial \tau_{zz} / \partial z = \partial^2 v_z / \partial z^2$

IIT KHARAGPUR | NPTEL ONLINE CERTIFICATION COURSES

Then we can say that this to be nothing g but the operant (())(21:24) capital D. So we can write that capital DVx the into D t times Rho this is nothing but minus del del x of Tau xx plus del del y of Tau yx plus del del z of Tau zx, right. So this is so this is for the x component. Similarly for the y and z component we can write Rho capital D operand del Vy del t, right. This is equals to minus del del x of Tau xy plus del del y of Tau yy plus del del z of Tau zy, right. So this and similarly for the z component Rho D of V D Vz Dt this is equals to again minus del del x of Tau zx or in this case xz, right plus del del y of Tau yz plus del del z of Tau zz, right. So this three can be written easily, right.

(Ref Slide Time: 23:17)

Navier Stokes equation in cartesian coordinate

$$\rho [\partial v_x / \partial t + v_x \partial v_x / \partial x + v_y \partial v_x / \partial y + v_z \partial v_x / \partial z] = \mu [\partial^2 v_x / \partial x^2 + \partial^2 v_x / \partial y^2 + \partial^2 v_x / \partial z^2] - \partial p / \partial x + \rho g_x$$

$$\rho [\partial v_y / \partial t + v_x \partial v_y / \partial x + v_y \partial v_y / \partial y + v_z \partial v_y / \partial z] = \mu [\partial^2 v_y / \partial x^2 + \partial^2 v_y / \partial y^2 + \partial^2 v_y / \partial z^2] - \partial p / \partial y + \rho g_y$$

$$\rho [\partial v_z / \partial t + v_x \partial v_z / \partial x + v_y \partial v_z / \partial y + v_z \partial v_z / \partial z] = \mu [\partial^2 v_z / \partial x^2 + \partial^2 v_z / \partial y^2 + \partial^2 v_z / \partial z^2] - \partial p / \partial z + \rho g_z$$

Using $\tau_{xx} = -\mu \partial v_x / \partial x$, $\tau_{yx} = -\mu \partial v_x / \partial y$,

$\tau_{zx} = -\mu \partial v_x / \partial z$

$\tau_{xy} = -\mu \partial v_y / \partial x$, $\tau_{yy} = -\mu \partial v_y / \partial y$,

$\tau_{zy} = -\mu \partial v_y / \partial z$

$\tau_{xz} = -\mu \partial v_z / \partial x$, $\tau_{yz} = -\mu \partial v_z / \partial y$,

$\tau_{zz} = -\mu \partial v_z / \partial z$

$\partial \tau_{xx} / \partial x = (-\mu) \partial^2 v_x / \partial x^2$, $\partial \tau_{yx} / \partial y = \partial^2 v_x / \partial y^2$,

$\partial \tau_{zx} / \partial z = \partial^2 v_x / \partial z^2$

$\partial \tau_{xy} / \partial x = \partial^2 v_y / \partial x^2$, $\partial \tau_{yy} / \partial y = \partial^2 v_y / \partial y^2$,

$\partial \tau_{zy} / \partial z = \partial^2 v_y / \partial z^2$

$\partial \tau_{xz} / \partial x = \partial^2 v_z / \partial x^2$, $\partial \tau_{yz} / \partial y = \partial^2 v_z / \partial y^2$,

$\partial \tau_{zz} / \partial z = \partial^2 v_z / \partial z^2$

Handwritten mathematical derivation on a grid background. The text "NAVIER STOKES EQUATION" is written in the center. The equations show the relationship between shear stress components and velocity gradients:

$$\tau_{xx} = -\mu \frac{\partial^2 v_x}{\partial x^2}$$

$$\tau_{yx} = -\mu \left(\frac{\partial^2 v_x}{\partial y^2} + \frac{\partial^2 v_y}{\partial x^2} \right)$$

The derivation shows the substitution of these stress terms into the momentum equations. The final equations shown are:

$$\rho \left(\frac{\partial v_x}{\partial t} + v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} + v_z \frac{\partial v_x}{\partial z} \right) - \frac{\partial p}{\partial x} + \rho g_x = \mu \left(\frac{\partial^2 v_x}{\partial x^2} + \frac{\partial^2 v_x}{\partial y^2} + \frac{\partial^2 v_x}{\partial z^2} \right)$$

$$\rho \left(\frac{\partial v_y}{\partial t} + v_x \frac{\partial v_y}{\partial x} + v_y \frac{\partial v_y}{\partial y} + v_z \frac{\partial v_y}{\partial z} \right) - \frac{\partial p}{\partial y} + \rho g_y = \mu \left(\frac{\partial^2 v_x}{\partial x^2} + \frac{\partial^2 v_y}{\partial x^2} + \frac{\partial^2 v_y}{\partial y^2} + \frac{\partial^2 v_y}{\partial z^2} \right)$$

$$\rho \left(\frac{\partial v_z}{\partial t} + v_x \frac{\partial v_z}{\partial x} + v_y \frac{\partial v_z}{\partial y} + v_z \frac{\partial v_z}{\partial z} \right) - \frac{\partial p}{\partial z} + \rho g_z = \mu \left(\frac{\partial^2 v_x}{\partial x^2} + \frac{\partial^2 v_x}{\partial y^2} + \frac{\partial^2 v_z}{\partial x^2} + \frac{\partial^2 v_z}{\partial y^2} + \frac{\partial^2 v_z}{\partial z^2} \right)$$

Now if we substitute that by using the value Tau xx is nothing but minus Mu del del x of Vx is Tau yx. Similarly we can also write Tau yx is equals to minus Mu del del y of Vx, right and using the similar way all others they (())(23:51), right you remember that this one and this one, okay I have given two, okay let me also give the third one Tau zx yz Tau zx, this is equals to minus Mu del Vx del z, right. So this is for the velocity component, this is for the direction, this is for the velocity component this is for the direction, this is for the velocity component this is for the direction, if we keep in mind, this simple thing then we will be able to expand it in terms of V, right.

All this Tau terms that is your shear stress terms we can expand in terms of the velocity terms if there in Tau xx, first x is the direction, second x is the velocity component, Tau yx, y is the direction x is the velocity component. So that means (())(25:04) will be del Vy del x right. Del Vx del x then similarly, Tau yz will be del Vz del y, right. So keeping all these in term in mind if we substitute then in this equation, because okay some more if we show that, for example this we can write okay, Tau this minus Mu this, therefore we can write del del x of Tau xx Tau xx is defined as this, right. So del del x of Tau xx we can write, this is nothing but del 2 Vy del xx square, right, del 2 v this is Tau not xx Tau xx will be del del x of Tau xx will be minus, okay minus Mu right minus Mu into del 2Vx del xx square, right del 2Vx del xx square.

So keeping all minus Mu similarly we can write del del y of Tau yx right is equals to again del 2 Vx del y square like that all the terms we can write with of course minus mu(26:48), right and in

that case if we substitute them in the equation what we have shown as equation 1 if we substitute all these Tau values in terms of velocity and viscosity then we can say that Rho times del del t of Vx plus Vx del del x of del Vx del del x of Vx plus del Vy del del y of Vy plus Vz del del z of Vz, this is equals to that Mu now it has come to the right side.

So negative has gone out Mu del 2 Vx del X square, right plus del 2 Vx del y square plus del 2 Vx del z square, right minus del p del x plus Rho gx, right. This is for x component for y component we can write Rho del del t of Vy, right plus Vx del del x of Vy plus Vy del del y of Vy plus Vz del del z of Vz, right or rather this will be y Vy , this is equals to Mu del 2 Vy del x square plus del 2 Vy del y square plus del 2 Vy del z square, right minus del p del y plus Rho gy and for the z component similarly, del Vz del t plus Vz del Vz del x plus Vz plus, this is Vx then Vy sorry, Vx del Vz del y plus Vz del Vz del z right. This is equals to Mu del 2 Vz del x square plus del 2 Vz del y square plus del 2 Vz del z square minus Rho no rather del p del z minus del p del z plus Rho gz.

So these are known as NAVIER stokes equation. When NAVIER stokes equation. So when and this is for the Cartesian co-ordinate x, y, z right. Now when you will be doing it you have to identify from the problem given or from the situation which term corresponds to what.



(Refer Slide Time: 31:25)

Navier stokes eqⁿ in cylindrical coordinate

$$\rho \left[\frac{\partial v_r}{\partial t} + v_r \left(\frac{\partial v_r}{\partial r} \right) + \left(\frac{v_\theta}{r} \right) \frac{\partial v_r}{\partial \theta} - \frac{v_\theta^2}{r} + v_z \left(\frac{\partial v_r}{\partial z} \right) \right] = \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (r v_r) \right) + \frac{1}{r^2} \frac{\partial^2 v_r}{\partial \theta^2} - \frac{2}{r^2} \frac{\partial v_\theta}{\partial \theta} + \frac{\partial^2 v_r}{\partial z^2} \right] - \frac{\partial p}{\partial r} + \rho g_r$$

$$\rho \left[\frac{\partial v_\theta}{\partial t} + v_r \left(\frac{\partial v_\theta}{\partial r} \right) + \left(\frac{v_\theta}{r} \right) \frac{\partial v_\theta}{\partial \theta} - \frac{v_r v_\theta}{r} + v_z \frac{\partial v_\theta}{\partial z} \right] = \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (r v_\theta) \right) + \frac{1}{r^2} \left(\frac{\partial^2 v_\theta}{\partial \theta^2} \right) + \frac{2}{r^2} \left(\frac{\partial v_r}{\partial \theta} \right) + \frac{\partial^2 v_\theta}{\partial z^2} \right] - \frac{1}{r} \frac{\partial p}{\partial \theta} + \rho g_\theta$$

$$\rho \left[\frac{\partial v_z}{\partial t} + v_r \left(\frac{\partial v_z}{\partial r} \right) + \left(\frac{v_\theta}{r} \right) \frac{\partial v_z}{\partial \theta} + v_z \left(\frac{\partial v_z}{\partial z} \right) \right] = \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (r v_z) \right) + \frac{1}{r^2} \frac{\partial^2 v_z}{\partial \theta^2} + \frac{\partial^2 v_z}{\partial z^2} \right] - \frac{\partial p}{\partial z} + \rho g_z$$

R-component

$$\begin{aligned} & \rho \left[\frac{\partial v_r}{\partial t} + v_r \frac{\partial v_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_r}{\partial \theta} - \frac{v_\theta^2}{r} + v_z \frac{\partial v_r}{\partial z} \right] \\ &= \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_r}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_r}{\partial \theta^2} - \frac{2}{r^2} \frac{\partial v_\theta}{\partial \theta} - \frac{2}{r^2} \frac{\partial v_r}{\partial \theta} + \frac{\partial^2 v_r}{\partial z^2} \right] \\ & \quad - \frac{\partial p}{\partial r} + \rho g_r \end{aligned}$$



IIT KHARAGPUR



NPTEL ONLINE
CERTIFICATION COURSES

θ -component

$$\begin{aligned} & \rho \left[\frac{\partial v_\theta}{\partial t} + v_r \frac{\partial v_\theta}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_\theta}{\partial \theta} + \frac{v_r v_\theta}{r} + v_z \frac{\partial v_\theta}{\partial z} \right] \\ &= \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_\theta}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_\theta}{\partial \theta^2} + \frac{2}{r^2} \frac{\partial v_r}{\partial \theta} + \frac{\partial^2 v_\theta}{\partial z^2} \right] \\ & \quad - \frac{1}{r} \frac{\partial p}{\partial \theta} + \rho g_\theta \end{aligned}$$



IIT KHARAGPUR



NPTEL ONLINE
CERTIFICATION COURSES

17

Z-component

$$\rho \left[\frac{\partial v_z}{\partial t} + v_r \frac{\partial v_z}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_z}{\partial \theta} + v_z \frac{\partial v_z}{\partial z} \right]$$
$$= \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_z}{\partial \theta^2} + \frac{\partial^2 v_z}{\partial z^2} \right] - \frac{\partial p}{\partial z} + \rho g_r$$

So if you can identify you can solve any problem on the momentum transfer with the help of this NAVIER stokes equation, right we will do some problems next time and then identify and understand this individual terms, okay. So that is what here we do, so NAVIER stokes equation in a cylindrical co-ordinate I have given, in the slide you can check and also this of course not coming proper way in there R component, theta component like that. So thank you.