

Course on Momentum Transfer in Process Engineering
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Lecture 48
Module 10
Ergun's equation-derivation (Part-1)


Hello, we are doing packed bed, okay. So in the packed bed we have already said what is the utility of the packed bed? What is the application? Particularly in process engineering, but we also have shown there were some definitions a or many others like hydraulic radius or sphericity this things we have already defined we have also found out Reynolds number, right? So now we will go from that packed bed Reynolds number, then yeah.

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From Hagen Poiseulle Eq. for laminar flow

$$\Delta p = \frac{32\mu v \Delta L}{D^2} = \frac{32\mu v \Delta L}{\varepsilon (4r_{11})^2} = \frac{32\mu v \Delta L}{\left(\frac{\varepsilon \phi_s D_p}{6(1-\varepsilon)}\right)^2}$$
$$= \frac{72\mu v \Delta L (1-\varepsilon)^2}{\varepsilon^3 \phi_s^2 D_p^2}$$
$$\approx \frac{150\mu v \Delta L (1-\varepsilon)^2}{\varepsilon^3 \phi_s^2 D_p^2}$$

This is called Blake – Kozeny equation and is valid for $N_{Re} < 10$.



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Hagen Poiseuille eqn. for laminar flow

$$\Delta P = \frac{32 \mu u \Delta L}{D^2} = \frac{32 \mu v' \Delta L}{\epsilon (4r_h)^2} \quad v' = \epsilon v$$

$$= \frac{32 \mu v' \Delta L}{\left(\frac{4 \epsilon \phi_s D_p}{6(1-\epsilon)}\right)^2} = \frac{72 \mu v' \Delta L (1-\epsilon)^2}{\epsilon^3 \phi_s^2 D_p^2}$$

$$\approx \frac{150 \mu v' \Delta L (1-\epsilon)^2}{\epsilon^3 \phi_s^2 D_p^2}$$

Blake-Kozeny ✓ Valid for $Re \leq 10$

Now from the Hagen Poiseuille equation for laminar flow we have seen that ΔP was equal to $32 \mu v \Delta L$ or $\mu v L$ since it is L so we can take it as ΔP for ΔL for ΔP over D square, right? Now this we can rewrite as $32 \mu v' \Delta L$ over ϵ into $4 r_h$ where r_h is hydraulic radius square, right? This we have substituted D , right? v as v' and v' by ϵv and D as $4 r_h$ whole square, right? Because your v' was equals to ϵv , right? So this v' is the flow through the packed bed.

So if that be true, then we can also write this is equal to $32 \mu v' \Delta L$ over this we can rewrite as $4 \epsilon \phi_s D_p$ over 6 into $1 - \epsilon$ this square, right? This r_h we have done it earlier in the previous class, right? r_h hydraulic radius and then to from there to hydraulic diameter that we have done. So it is $4 \epsilon \phi_s D_p$ by 6 into $1 - \epsilon$ square, right? This on rearrangement we can write this is equals to $72 \mu v' \Delta L$ to $1 - \epsilon$ whole square over ϵ^3 into ϕ_s^2 into D_p^2 , right?

Now this can roughly be written as equals to $150 \mu v' \Delta L$ into $1 - \epsilon$ square divided by $\epsilon^3 \phi_s^2$ into D_p^2 , right? Why? Because this has been seen this has been found out that whenever the value of ΔP predicted this is a relation, so that means you can predict the ΔP for a laminar flow using Hagen Poiseuille's equation this you can at (5:20) at this state using $\epsilon \phi_s$ everything, right? So this is for packed bed that what is the ΔP when your there is a sphericity of ϕ_s or there is a void space of ϵ .

So when all these are known, then you can write it in terms of $72 \mu v' \Delta L / (1 - \epsilon)^2 \phi_s^2 D_p^2$. So that means if you know all these terms then you can tell that what is the ΔP , but the problem is that when you do this the actual case the it has been found that the actual case will be much better if this 72 is replaced by 150 that is the prediction is much closer to the actual ΔP that is why this 72 has been replaced with 150, right?

This was done by Blake and Kozeny and according to their name this equation is known as Blake Kozeny equation for flow through packed bed and this is for the laminar part, so for laminar flow we have started with Hagen Poiseuille equation from there the ΔP relation whatever we had we have taken that and we have modified that only in terms of putting the actual parameters like ϵ , ϕ_s , D_p and the velocity v' , right? So these by rearranging we have now got one relation where ΔP is instead of 72 it is 150, then $\mu v' \Delta L / (1 - \epsilon)^2 \phi_s^2 D_p^2$, this we call it to be the Blake Kozeny equation, right?

And this is valid for $N_{re} < 10$, this is valid for $N_{re} < 10$, right? Now let us look into the other that is the other part when the flow is not laminar.

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for turbulent flow

$$\Delta P_f = 4f\rho \frac{\Delta L}{D} \frac{v'^2}{2}$$

$$= 4f\rho \frac{\Delta L}{\frac{4\epsilon\phi_s D_p}{6(1-\epsilon)}} \cdot \frac{v'^2}{2\epsilon^2}$$

$$= 3f\rho \frac{\Delta L}{\phi_s D_p} \frac{v'^2(1-\epsilon)}{\epsilon^3}$$

$$\approx 1.75\rho \frac{\Delta L}{\phi_s D_p} \frac{v'^2(1-\epsilon)}{\epsilon^3} \quad 3f = 1.75$$

$$\Delta P_f = 1.75\rho \frac{\Delta L}{\phi_s D_p} \frac{v'^2(1-\epsilon)}{\epsilon^3}$$

Bunker-Plummer equation

$N_{re} > 1000$

For turbulent flow we can use that ΔP_f is equal to $4 f \rho \Delta L / D \text{ into } v^2$ by 2 this we know for turbulent flow for laminar flow it was there using fanning friction factor we have reduced it that ΔP_f is $4 f \rho \Delta L / D$ or $L / D \text{ to } v^2$ by 2, right?

This we have established long back. Now if we start from that point and rewrite, right? Now this we can also write as $4 f$, right? ρ then this ΔL remains there, this D we can write 4 by 6 $\epsilon \phi \text{ s } D_p$ over $1 - \epsilon$, right? Times that v has now become v' square divided by $2 \epsilon^2$ so v^2 by 2 so v'^2 by $2 \epsilon^2$ again the same thing that v' is equal to v , right?

From that relation we got this v'^2 by $2 \epsilon^2$, right? This D we have replaced with D_p and that we have shown earlier that this is equal to that 4 by $6 \epsilon \phi \text{ s } D_p$ by $1 - \epsilon$, right? This we can rearrange rewrite as equal to $3 f \rho \Delta L / \phi \text{ s } D_p$ times v'^2 times $1 - \epsilon$ over ϵ^3 , right? This we can rewrite like this because this 4 that 4 goes up this 2 and this 6 goes up and 3 remains so 3 comes $4 \rho \Delta L \phi \text{ s}$ remains there D_p remains there $1 - \epsilon$ goes up v'^2 and this remains ϵ and 1ϵ so ϵ^3 , right? This ϵ^2 ϵ remains and it becomes ϵ^3 , right?

So here also the researchers have seen that the ΔP which is predicted with this equation with this relation the ΔP which is ΔP_f for turbulent flow for turbulent flow the pressure drop under friction factor ΔP_f that can be predicted through this relation where we also have the particle size as D_p we also have the void space as ϵ and we also have this velocity through that packed bed that is v' I think we had said that v' is empty cross section and v is through that packed bed, right?

So if there is ϵ void space, then that v that becomes equal to v' / ϵ , right? That we have earlier established and shown. Now so that is what that ΔP_f when it is equal to this $3 f \rho \Delta L / \phi \text{ s } \text{ into } D_p v'^2$ into $1 - \epsilon$ by ϵ^3 this has been seen that the prediction of ΔP with this relation is not so close. So it was changed to roughly equal to $1.75 \rho \Delta L / \phi \text{ s } D_p v'^2$ into $1 - \epsilon$ divided by ϵ^3 , right?

So roughly 3 f is equals to 1.75 sorry 1.75, right? So 3 f is 1.75 we have substituted, right? Like the previous one we had substituted 150 72 with 150, right? Here we have substituted 3 f with 1.75, right? Then delta P f that is equals to 1.75 rho delta L by phi s Dp v prime square into 1 minus epsilon by epsilon cube, right? So this is called this was proposed or this relation was derived by the another pair of scientist or another pair of researchers there name is Burker Plummer and this equation is known as Burker Plummer equation, right?

So this like the previous one that was valid for Nre less than 10, this is valid for Nre greater than 1000, right? So in one case we have seen that we can predict delta P for flow through packed bed when Nre is less than 10 and in another case for turbulent flow when Nre is greater than 1000. Than the question automatically comes that what about if Nre is between 10 and 1000, is not it.

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Blake-Kozeny Kozeny

$$\Delta P = \frac{150 \mu v' \Delta L (1-\epsilon)^2}{\epsilon^3 \phi_s^2 D_p^2}$$

$$= \frac{150 \mu v' \Delta L (1-\epsilon)^2}{\epsilon^3 \phi_s^2 D_p^2} \frac{v'^2 \rho^2}{v'^2 \rho^2}$$

$$= \frac{150 \mu v' \Delta L (1-\epsilon)^2 (\rho v')^2}{\epsilon^3 \phi_s^2 D_p^2 v'^2 \rho^2}$$

$G = \rho v$
 $G' = \rho v'$

$$= 150 (G')^2 \frac{\Delta L}{\phi_s D_p \rho v'} \frac{(1-\epsilon)}{\epsilon^3} \frac{1}{\rho}$$

So for that another scientist who did a clumbing I mean punching of these two that he has predicted he has used both of these two relations and then what it did it from the Burker Plummer equation or Blake Kozeny equation first was Blake Kozeny, right? It was Blake Kozeny equation from Blake Kozeny equation we have seen delta P was 150 mu v prime delta L 1 minus epsilon whole square divided by epsilon cube phi s square Dp square, right?

So this can be rearranged as 150 mu v prime delta L 1 minus epsilon whole square by epsilon cube phi s square Dp square. Now if we multiply both numerator and denominator with v prime rho square by v prime rho square, then we can rewrite and rearrange it as 150 mu v prime, right?

mu v prime, v prime we can use afterwards, okay 150 mu say delta L mu delta L because this v prime we can use inside. So 150 mu delta L into 1 minus epsilon whole square now this v prime we can take there and write rho v prime square, right?

And in denominator we have epsilon cube phi s square, right? And Dp square and this side it was v prime rho square, right? So this again we can rewrite as equals to 150 G prime square, right? Because G is rho v so G prime is equals to rho v prime, right? So if that be true then we can write 150 G prime square delta L by phi s Dp, right? Over phi s Dp rho v prime over 1 minus epsilon into mu times 1 minus epsilon over epsilon cube times 1 by rho because we have taken 1 additional rho and that rho came out here, right?

So this we can rearrange rewrite 150 G prime square delta L by phi s Dp into 1 minus epsilon by epsilon cube into 1 by rho, right? Into phi s into Dp into rho v prime over 1 minus epsilon into mu, right? This v prime was there and this rho is taken only here it was rho square so 1 rho is taken here and 1 rho remains here, right? So this rearrangement is required because we would like to proceed to one relation because this was developed by the scientist we will name him afterwards and during that process he has done all these.

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Burke - Plummer

$$\Delta \rho = 1.75 \rho \frac{\Delta L}{\phi_s D_p} \frac{v'^2 (1-\epsilon)}{\epsilon^3}$$

$$= 1.75 \rho \frac{\Delta L}{\phi_s D_p} \frac{v'^2 (1-\epsilon) \rho}{\epsilon^3 \rho}$$

$$= 1.75 (\rho v')^2 \frac{\Delta L}{\phi_s D_p} \frac{(1-\epsilon)}{\epsilon^3} \frac{1}{\rho}$$

$$= 1.75 (G')^2 \frac{\Delta L}{\phi_s D_p} \frac{(1-\epsilon)}{\epsilon^3} \frac{1}{\rho} \dots \textcircled{2}$$

So this equation we name it to be say equation 1, right? So let us keep it aside and now from the other one that is Burke Plummer I think the previous one where we so far remember it was Burke not er BURKE only, right? B, U, R, K, E Burke Plummer P, L, U, M, M, E, R, right? Burke

Plummer, okay. So next form the equation Burke Plummer we can write ΔP is 1.75ρ into ΔL over $\phi^5 D_p^5$ rather into $v' \text{ into } 1 - \epsilon$ over ϵ^3 this was the original equation which was Burke Plummer, right? This we just have done here, it was like that $1.75 \rho \Delta L$ over $\phi^5 D_p v' \text{ into } 1 - \epsilon$ by ϵ^3 , right?

So this if we know, then we can rewrite it as 1.75ρ , right? ΔL by $\phi^5 D_p$ into $v' \text{ into } 1 - \epsilon$ by ϵ^3 into both numerator and denominator let us multiply and divide with ρ . So in that case we can rewrite it as 1.75 , right? This as ρ into v' this as ρ into v' , right? $\rho v'$ and we also can write this ΔL by $\phi^5 D_p$, right? Into $1 - \epsilon$ by ϵ^3 , right? Divided by into 1 by ρ because this $\rho v'$ we have gathered together, so 1 by ρ remains. So this we can write that this is equals to 1.75 , right? G' , right? And this was $v' \text{ into } 1 - \epsilon$, right? So it was $v' \text{ into } 1 - \epsilon$ so it should be square here this ρ this ρ is this $\rho v' \text{ into } 1 - \epsilon$.

So this is $\rho v' \text{ into } 1 - \epsilon$ so we can write $G' \text{ into } \Delta L$ by $\phi^5 D_p$, right? Into $1 - \epsilon$ by ϵ^3 into 1 by ρ , right? So this is if we tell that this is equation number 2 so that means till now what we have done we have taken in one hand that Blake Kozeny equation that we have taken and we have come to equation number 1 with a relation, right? So ΔP is equals to this this this this with a relation we have found out what is the ΔP .

And in another with the Burke Plummer equation which was for the turbulent flow we have taken that equation and we have come to this relation that $1.75 G' \text{ into } \Delta L$ by $\phi^5 D_p$ into $1 - \epsilon$ by ϵ^3 to 1 by ρ , right? This we have done purposefully so that we can utilize ultimately our target is we have said we have gotten 1 equation that is Blake Kozeny which is valid for N_{re} less than 10, right? And we have also taken another equation which was and that we started with laminar flow, right? And now in this case we have taken for turbulent flow and in turbulent flow we have said that this is valid for N_{re} greater than 1000, right?

And in both the cases in terms of G' that is mass velocity we have taken that okay now in terms of G' and $\epsilon D_p \rho$ all these terms we have done in one form as ΔP for

prediction in terms of G prime and we named them as say equation 1 and equation 2, right? So perhaps this class we cannot proceed further, when we again come to the next class then we will see how beautifully that scientist has utilized and made another what I should say another relation by which you can use both the for laminar as well turbulent flow you can use the generalized equation and for the intermediate also, okay thank you let us go for the next class thank you.