

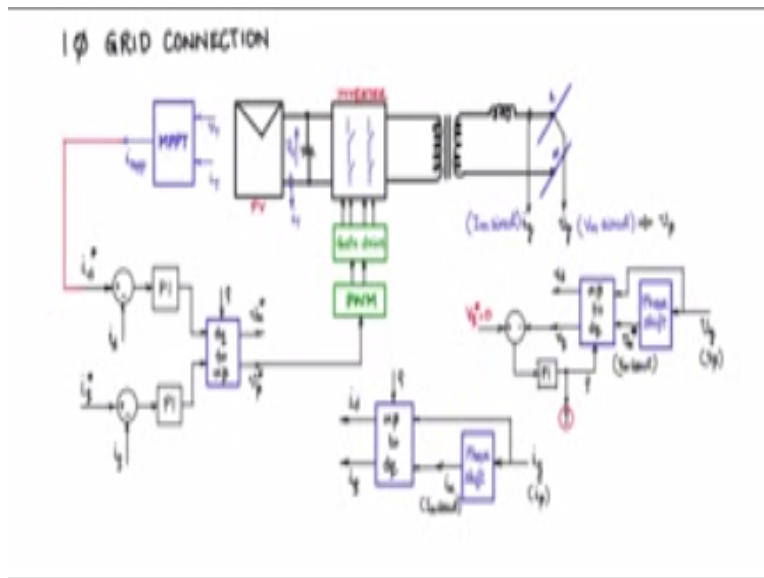
Indian Institute of Science

Design of Photovoltaic Systems

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NPTEL Online Certification Course

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Let us now discuss the single phase grid connection as the PV module is being interface to a single phase grid, let us first draw the topology of the PV module being connected to a single phase grid. The PV module terminals being buffered is connected to a single phase inverter which is consisting of a bridge having four switches full bridge having four switches and from this center of this bridge arms we will connected to a single phase transformer like this and the secondary side of the transformer is connected to an inductor and through the inductor is connected to the line neutral of the grid for single phase grid.

So this is the basic topology of the single phase grid which we have discussed earlier, this PV and this is the inverter let us name this parts, now the gate drive here unlike the three phase case we need to drive only four switches so let us have four gear drives and the signals for then gear drive or coming from a PWM module. The PWM module will give two signals depending upon the type of the PWM which will be used for driving these four switches.

Let us now sense the current that is flowing through the inductor into the grid that we are pumping into the grid we will call it as i_g and let us also measure the phase voltage have a line and neutral and I will call that one as v_g that is the grid voltage, grid voltage v_g is $v_m \sin \omega t$ it of course contains lot of harmonics but let us say that v_g is $v_m \sin \omega t$ and i_g we wanted to the $i_m \sin \omega t$ that is we would like to inject the current into the grid at unity power factor.

So the moment you say this is $v_m \sin \omega t$ this is $i_m \sin \omega t$ this is actually i_β , this is v_β there is no v_α or i_α so we have to generate it, we have to create the α component so that it will fit into the α, β co-ordinate axis. Let me consider a phase shifter block, so let us say this phase shifter block does the job of taking the input signal and shifting the phase by 90° we will see how we can realize that but that is the objective of this phase shifter block.

So to the input of the phase shifter block I will give i_g , i_g which is considered as i_β because it is a $\sin \omega t$ and the output of the phase shifter block will give you i_α so after this $i_m \sin \omega t$ is pass through the phase shifter block it will become $i_m \cos \omega t$ shifted by 90° . Now I have i_α and I have i_β also so which I can pass it to a transformation this is α, β to dq which will give me i_d and i_q , so now I have this i_d and i_q which are dc quantities due to this $\alpha\beta$ to dq transformation there is a ρ input which has to be given so we will provide that ρ input.

Now what is that ρ , ρ is the angle between the $\alpha\beta$ co-ordinate axis in the dq co-ordinate axis I will come to I will come and discuss later on how we will generate this ρ . Now that I have let us say i_d and i_q the dc quantities of the current I will now have a control mechanism like this so I have i_d^* , i_d just like in the case of three phase and the error is passed through a PI controller. Similarly, I will have another control mechanism for i_q^* , i_q is fed back and I will have a PI controller.

So we will see what we have to set for i_d^* and i_q^* i_d is basically this transformed current which is given here i_q is this transformed current which is given here, coming ultimately from any input measurement. Now this PI these two PI outputs will be passed through a transformation this PI controller outputs will represent voltages which need to given to the PWM to control their inverter, so this would be a dq to $\alpha\beta$ transformation it also needs ρ information ρ which is the angle between the dq axis and the $\alpha\beta$ axis.

The output of this will be v_{α}^* or reference v_{β}^* and these two will act as a reference for the PWM generation it means this, this will be given as the signal for comparing with a triangle and generate the pulses for giving it to the gate drive. Now we do not need to use both v_{α}^* and v_{β}^* see that v_g here is $v_m \sin \omega t$ which is v_{β} , now i_g is also i_{β} v_g is v_{β} that is a β axis components we have, we generated the α axis components by this phase shift, we generated i_{α} and then the i_d and i_q where obtained. So we need to use only the β axis components α axis components where created just to provide us the transformation, so that we could go into the dq domain that is the dc domain so that you could so set point control.

So here we will use only one of this which is v_{β} here for now because we are taking this as $v_m \sin \omega t$. $v_m \cos \omega t$ so we will use that. Now this will go to the PWM it will generate the PWM signals gate drive and then it will drive the current pump the current into the grid, now this current i_g which is being pumped into the grid is the one which is actually being controlled because these are current controllers and we are doing current control, we need to set these references before we set these references let us see how we are going to get this row these two rows.

Let me use another phase shifter the input to that is v_g which is v_{β} and I will use $\alpha\beta$ to dq transformer, the phase shift output is going to give me v_{α} because it has shifted it by 90° which is $v_m \cos \omega t$ this was $v_m \sin \omega t$ and I can use v_g here so this will give me v_{β} and v_{α} and I will pass it through $\alpha\beta$ to dq which will give me v_d and v_q and this will have a row input, so how do I get this row input I will setup a control system here, I will have a reference and the feedback point is v_q the converted transformed v_q , the output of that the error is given to a PI block the output of the PI block is given as ρ to this $\alpha\beta$ to dq transformation just like as we did in the three phase system.

Now this v_q^* here I am setting it to 0 then eventually this control mechanism will operate in such a way that this PI controller being high gain controller will make this error 0 which means v_q will become 0 match with the v_q^* and therefore we can say that the ρ is at such an angle that the dq axis is aligned along the v_d which is the voltage space vector. So once it is aligned along v_g then I can set commands to the current set points or the current references.

So I would not like to have any quadrature component of the current I would like to inject only active current which means in phase current so therefore i_q has to set to 0 there should not be any

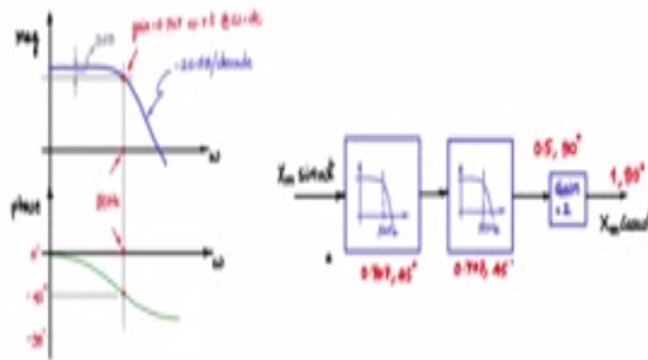
quadrature component then the current space phaser will become in line with the voltage space vector which will be in line with the dq axis of the rotating dq axis co-ordinate system just like in a three phase system.

So we will set i_q^* to be 0 and i_d^* whatever value that is being set here will be the amplitude of the current that will be actually pumped in here which is directly proportional to the power being pumped into the grid because the voltage is fixed by the grid. So therefore, i_d^* set point should actually have the output of the MPPT control algorithm.

So therefore, I will set up this MPPT block now this is v_d the terminal voltage of the PV I will measure also i_d the current through the PV we will have a MPPT block the inputs are v_t and it power will be calculated and a MPPT algorithm can be used to obtain an output which will be proportional to i_{mpV} current at maximum power point and that will be given as a set point to i_d^* , so output of the MPPT will determine i_d^* and i_d will try to match that meaning the current that is flowing here could corresponds to the, will correspond to the maximum power point of the PV panel.

Thereby achieving MPPT integrated MPPT control and grid connection, so this would be the entire block diagram for a single phase grid connected inverter. Now what about this two phase shift blocks, how will you make the phase shift I will just tell that now right now.

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Let us now see how we obtain the 90° phase shift, so consider this graph where the x-axis is ω frequency not time. Now this graph has magnitude as the y axis and this graph has phase as the y axis, now consider a first order filter now first order filter will have a magnitude verses ω plot something like this, this slope is -20dp/decade and find out the 3dp point below the flat portion of the magnitude curve that is 3dp below the magnitude at ω which is dc.

So this is the 3dp below point, now at this point the gain is 0.707 with respect to the flat portion. Now that the frequency, take this vertical line which cuts the frequency and look at the phase curve the phase at that 3dp point will be 45° so this is 0° - 45° eventually this phase curve will reach 90° . So for us the grid frequency is very stable it varies between 49.5 to 50.5 Hz which is a very small margin it is more or less 50Hz.

So this line should be add frequency which is 50 Hz, the we can say now at this point the gain is 0.707 with respect to ω_{dc} or the flat portion of this magnitude curve. Now we can say that if I have this first order filter and at 50Hz it is so designed that it is having a gain of 0.707 or an angle of 45° then I will use two such first order filters each providing 45° if I am biasing in that fashion designing in that fashion where the 3dp point is at 50Hz then this first order filter will give gain of 0.707 and 45° shift another first order filter will give again a 0.707 45° shift overall I will have a 0.5, 0.707 into 0.707 will be 0.5 gain and 90° shift.

Now pass this through a gain block, gain of 2 and I will get 1 gain same as the input and with the 90° shift, so if I am having $x_m \sin \omega t$ they format the input it pass through and at the output here you will get $x_m \cos \omega t$, so this is how you will generate a 90° phase shift the one that I had indicated here this and this, so with this, this entire single phase grid connected inverter topology can be implemented.