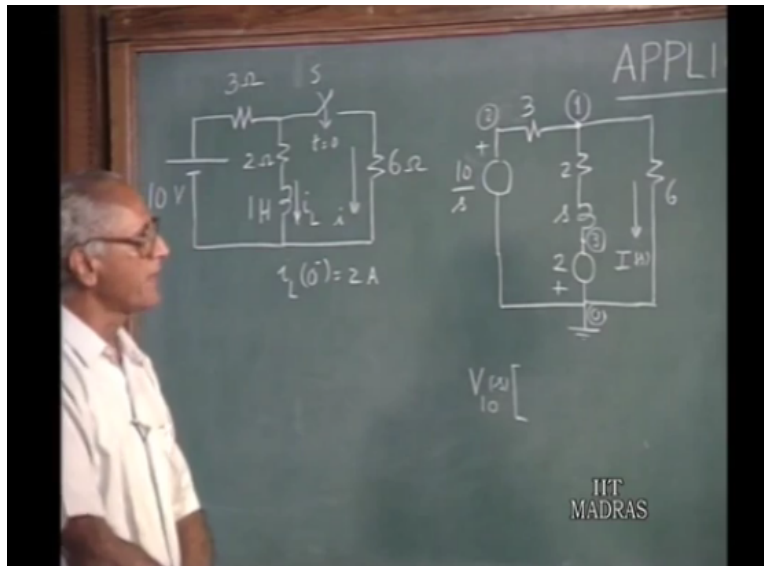


Networks and Systems
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Lecture-61
Laplace Transform Method for Mutual Inductance

In the last lecture, we acquainted ourselves with concept of transform diagrams, and how they help us in writing down the equation of performance of a network, the Laplace transform domain.

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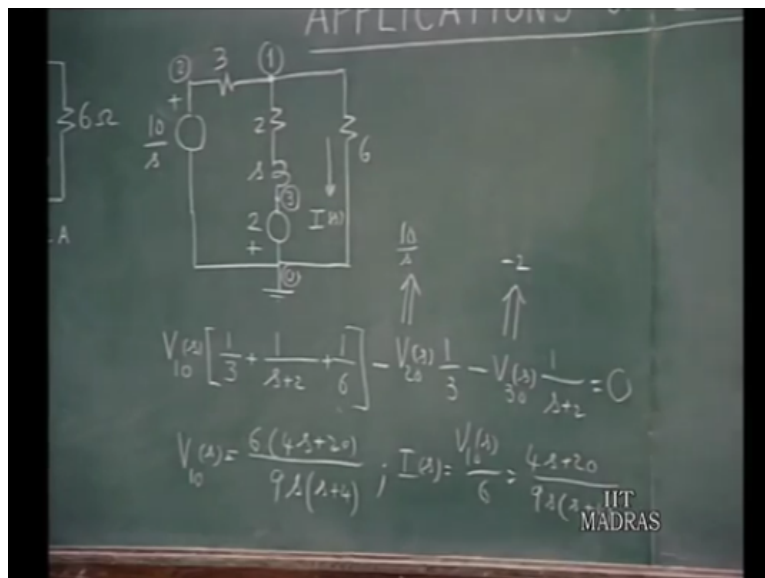
We took up this particular example, where the switch s is closed t equals 0, and you are asked to find out this current i . And then taking note of the current of the initial the 2 amperes. We replace that initial condition in the current by equivalent voltage source in the transform diagram, and we establish this transform diagram.

As I mentioned in the last class, once we have the transform diagram that can be analyzed in almost the same lines, as what you would observe in the case of dc circuits. Writing down the various equations, we took up in the last class; the loop current method for the solution of this network. We may as well the node voltage method. We can use superposition technique.

We can use thevenin's theorem, whatever, all the, the whole gamete of techniques that is available, for solution of dc circuits or ac circuits can be applied to the transforms diagrams as well. Just for the sake of illustration, let me solve this same circuit by the node voltage method.

Suppose I take this at the datum node, and if I solve for this node voltage, then you can find out the current in the 6 ohm resistor, by dividing that voltage 6. Therefore, I would like to use it node to datum voltage method. This is the node voltage to be solved for. Suppose this is node 2; the value of the node voltage with reference to the datum is 10 by s this is already known, and suppose I call this node 3, the voltage of node 3 the datum is already known.

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So, our aim is, to write the node equations to solve for v 1. So, there is only 1 unknown node voltage; therefore, let us say v 1 0 of s times the sum of the impedances connecting that node. One admittance this is generalized admittance I am talking about. The impedance is 3 therefore; the admittance is 1 by 3. The admittance of this combination for entire branch; the impedance has s plus 2; therefore, the admittance is 1 over s plus 2.

The impedance of 6 generalize impedance, the impedance is 1 by 6; that is the self node admittance that node 1. Therefore, the mutual terms you have to take v_{20} of s , and admittance connecting node 1 in 2 is 3. Therefore, 1 by 3 therefore, that is the coupling term that we are having.

Further you also have coupling term with reference to 3 0 of s . So, the admittance joining node is 1 and 3 is, $1 \text{ over } s \text{ plus } 2$. This must be the sum of the currents entering node 1, to the various currents of sources. In this particular example there is no such current source; therefore, is 0.

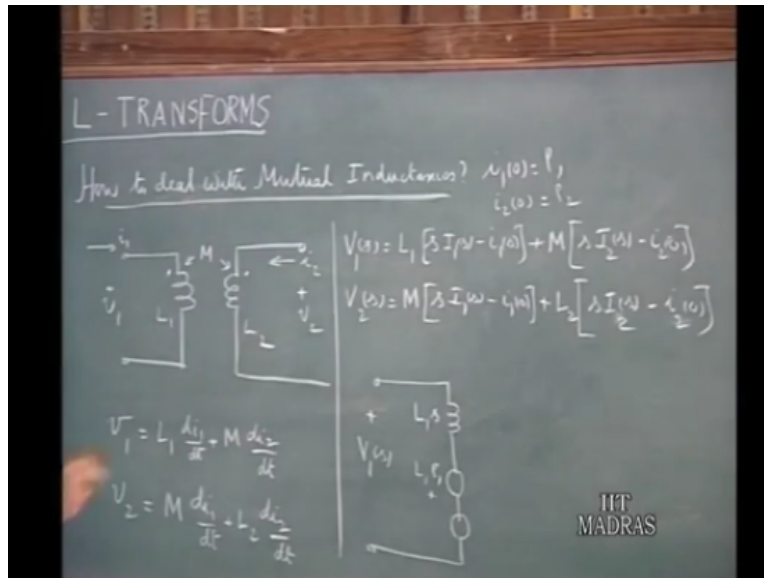
Now, in this equation the only unknown is v_{10} of s , because v_{20} of is known; that is equal to $10 \text{ by } s$. v_{30} of s is also known, since the polarity is plus with, the 0 as positive polarity reference to 3, v_{30} can be written as minus 2. On substitution of this values per v_{20} and v_{30} , we can get v_{10} of s . v_{10} of s can be calculated and shown to be, $6 \text{ times } 4 \text{ s plus } 20 \text{ divided by } 9 \text{ s times } s \text{ plus } 4$.

But we are interested not v_{10} of s , but the current in this 6 ohm resistance/ therefore, i of s obtained by dividing the v_{10} of s by 6. And when you do that this becomes $4 \text{ s plus } 20 \text{ divided by } 9 \text{ s time } s \text{ plus } 4$. This exactly the same expression that we got for the current i of s , if the loop current methods, and once we got a this point further work is the same, as what we have done in the case of loop current method.

So I will not do that, so from this you can get i of t . The point is that once we have the transform diagram, you can analyze the transform diagram, by any one of the known techniques that is available to you, in the whatever you do in the case of dc circuits can be applied to this transform diagram as well, except in terms of resistances.

We have generalize impedances, except in terms of tight dc voltage sources, we have transform voltage sources instead of dc current sources you transformed current sources. So, everything is in terms of s , but otherwise the principle, the technique is the same.

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Now, next question that you like to ask ourselves is how to deal with mutual inductance. We have so far addressed ourselves, to finding out the generalized impedances r and l and c elements. What we do when we encounter mutual inductances. So, suppose I have two couple coils, having self inductance l_1 and l_2 .

These are the dot points, and I have a mutual inductance m between them, and let me say the voltages and the currents, are the 2 coils are indicated as follows, as given here. Then in time domain the equations are performance of this mutually coupled pair of coils is v_1 equals $l_1 \frac{di_1}{dt}$ plus $m \frac{di_2}{dt}$, because the two currents, both the currents enter the dot points.

Therefore, beside of the mutually induced m is the same as the self induce m ; therefore, this is plus that is also plus v_2 likewise, is m times $\frac{di_1}{dt}$ plus l_2 times $\frac{di_2}{dt}$. These are straight forward standard equations, governing the behavior of the pair of couple coils which we know. When we transform this equations, in term by term we transform. So, v_1 will have Laplace transform v_1 of s .

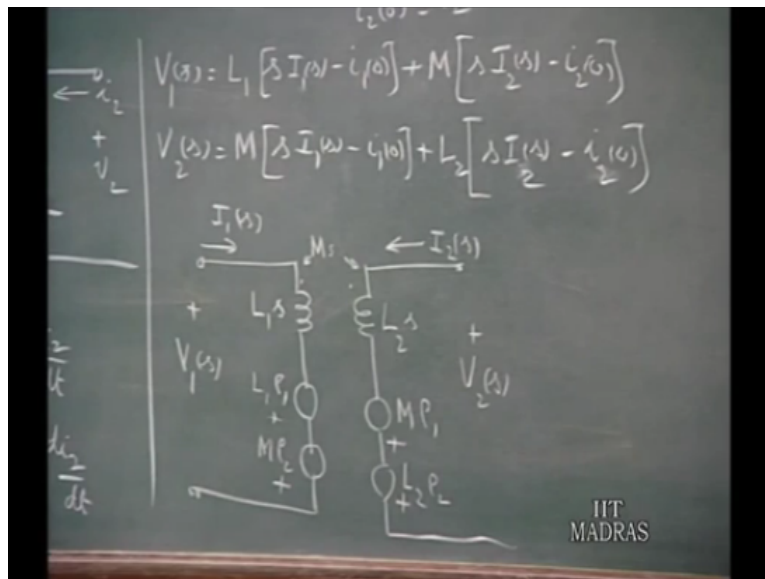
When you transform this, this will be l_1 times s times i_1 of s minus $i_1(0)$; that is the Laplace transform of $l_1 \frac{di_1}{dt}$. Similarly, the Laplace transform of $m \frac{di_1}{dt}$ be m times

s times i_2 of s minus $i_2(0)$. Second equation will be v_2 of s m times s times i_1 of s minus $i_1(0)$ plus L_2 times s times i_2 of s minus $i_2(0)$.

So, this is straight forward application of the transforming this equations. Now we have to draw a transform diagram, which repeats these equations. So, what you have now is, v_1 of s is $L_1 s$ times i_1 plus $M s$ of i_2 of s plus minus $i_1(0)$ minus $i_1(0)$. Therefore, if I have in the transform diagram; for the first coil v_1 of s is the transformed voltage, terminal voltage the coil, and the coil has the self inductance L_1 and it has got a generalized impedance L_1 of s ; this is self impedance of the first coil.

And you have 2 sources voltage sources represents the initial currents in the inductors therefore, this is $i_1(0)$. Suppose $i_1(0)$ write; as ρ_1 as $i_2(0)$ as ρ_2 to simplify my notation.

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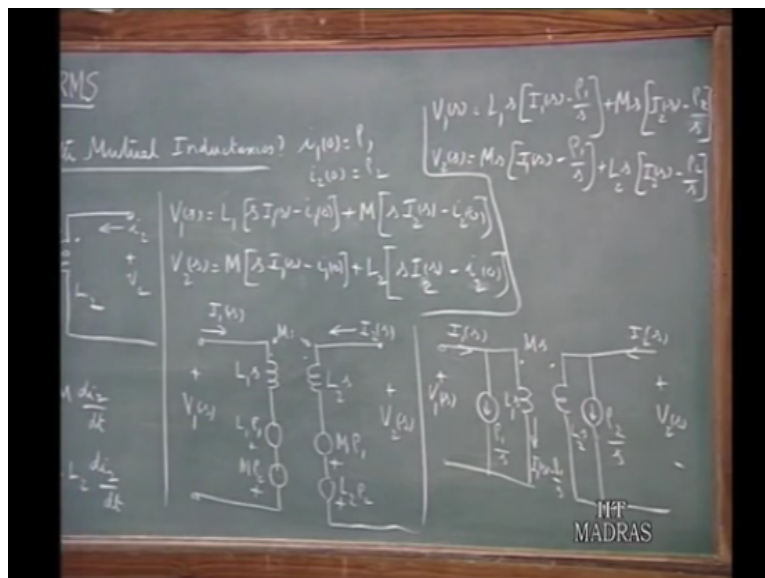
So, $L_1 \rho_1$ and minus $M i_2(0)$ therefore, you have another term $M \rho_2$. So, you have 2 voltage sources, representing the initial currents in the inductor, and the second coil likewise we have a representation like this. Where v_2 of s is the terminal voltage and the current is i_2 of s , and the Laplace transform of the current here is i_1 of s , L_2 of s and then here you have once again minus $M i_1(0)$, L_1 of s minus $i_1(0)$ that is M times ρ_1 and here you have L_2 times ρ_2 .

In addition we have a coupling impedance $m s$. so; that means, once you have write down this equation, the transform diagram in this fashion. We say the voltage terminal voltage v_1 of s are this coil is i_1 of s passing through l_1 of s we create a l_1 of s times i_1 of s . In addition i_2 flowing to this coil will have a mutually induced voltage here, whose Laplace transform is $m s$ times i_2 of s .

So, you have not only l_1 of s l_1 s times i_1 of s plus also $m s$ times i_2 of s . L_1 of s i_1 of s plus $m s$ times i_2 of s . In addition representing the initial current in inductors we have 2 voltage sources. Likewise the same situation is there in the second coil also. This is very similar to what you do in the case of study state circuit analysis ac circuit analysis, where instead of self inductance is represents as impedance $j \omega l_1$.

The mutual impedance is $j \omega m$. So, instead of $j \omega m$ we have s ; otherwise it is exactly the same, that the situation that we have in the case of ac circuits. Now, you may as well think of v plus in the initial currents, through current sources. So, if you do that, you can write this equation in this form.

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You can write v_1 of s , you can write as $l_1 s$ times i_1 of s minus ρ_1 by s . So, instead of writing minus $l_1 \rho_1$, I can write l_1 of s times minus ρ_1 by s . So, this term here, is

put in this form plus $m s$ times i_2 of s minus ρ_2 by s . and you can write v_2 of s exactly going to the same method; $m s$ times i_1 of s minus ρ_1 by s plus l_1 of s time i_2 of s minus ρ_2 by s ; that is what we handle.

So, if you look at these two equations, you can represent them in this fashion. You can have a current source here. So, let the current source be of strength ρ_1 by s . So, the current in the actual inductor here, is i_1 of s minus ρ_1 by s , and that current passing through l_1 of s will set up a voltage drop l_1 of s times i_1 of s minus ρ_1 by s . In addition you will have a mutually induced voltage $m s$ times, the current in this coil, and what is the current in that coil, in a symmetrical way you have i_2 of s here this is v_2 of s , and you have another current source here, which is ρ_2 by s .

So, the current in this coil is i_1 of s minus ρ_1 by s , and the current here is i_2 of s minus ρ_2 by s . So, now you see that this voltage v_1 of s is obtained as the drop in this inductor. What is the drop in this inductor to self induced $v_m f i_1$ of s minus ρ_1 of s times l_1 of s . and the mutually induced voltage is $m s$ times the current here, which is i_2 of s minus ρ_2 by s .

So, this exactly the term that you have having here. Similarly the voltage induced in this which is equal to v_2 of s , is the self induced voltage i_2 of s minus ρ_2 by s by l_2 of s , and the mutual induced voltage this is $m s$ times i_1 of s minus ρ_1 by s . So, these are 2 alternative representations of the initial conditions the mutual inductor, if you work with the voltage sources use this diagram.

If you like to use the current sources you can use this diagram. The advantage of the current source representation is, that on one side you have only ρ_1 only figures here, when you put the voltage source both ρ_1 and ρ_2 come on both sides; that is the minor advantage. So, this is the way in which we can analyze the transient problem, involved in mutual inductances. Let us work out an example to clarify these ideas.