

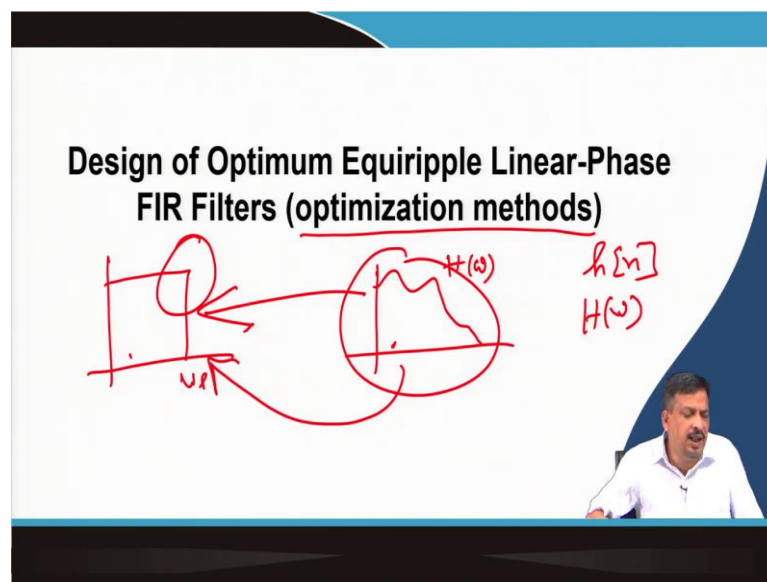
Signal Processing Techniques and its Applications
Dr. Shyamal Kumar Das Mandal
Advanced Technology Development Centre
Indian Institute of Technology, Kharagpur

Lecture - 40

Design Optimum Equiripple Linear-Phase FIR Filters (optimization methods)

So, last week, we talked about the design of FIR filters, mainly using two methods: one is called Windowing Methods, and one is called Frequency Sampling Methods. So, in the last week, I discussed how to design an FIR filter using windowing methods and frequency sampling methods. So, this week, let us start with the design of FIR filter using approximation methods.

(Refer Slide Time: 00:50)



So, what is the name? The name is called Design of Optimum Equiripple Linear-Phase FIR Filter using optimization methods. What is the meaning? This is that let I have a given and desired frequency response; let us this is my desired frequency response, which is ω_p , ok. So, I want to design an ideal low-pass filter. And then, I have designed a filter. Let us say I have designed an $h[n]$ I have designed an $h[n]$, and I calculate $H(\omega)$. So, I get the design $H(\omega)$.

Now, what I want to know is how close my desired frequency is to the designed frequency response. So, are there errors between those two things? So, if I say this one minus this one, it is an error in my design. So, I have to optimize the error to get that as

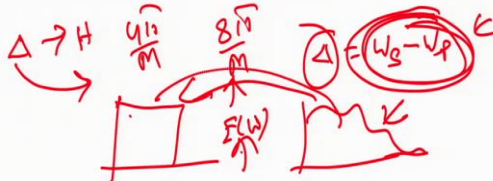
close as possible to the desired frequency response. So, that is the main motto of these methods.

So, what I said? Design of an optimum equiripple linear-phase FIR filter using optimization methods. So, why do we go for these methods?

(Refer Slide Time: 02:12)

The window method and the frequency-sampling method are relatively simple techniques of designing linear-phase FIR filters but they also possess some minor disadvantages, which may render them undesirable for some applications

Lack of precise control of the critical frequencies such as ω_p and ω_s



The diagram shows a rectangular pulse response $h[n]$ of length M . The frequency response $F(\omega)$ is a sinc function. A transition band is indicated with a width of $8\pi/M$. A specific frequency difference is circled and labeled $\Delta = \omega_s - \omega_p$.

Let us talk about how the window method and frequency sampling method are relatively simple techniques, as you say, simple techniques to design linear-phase FIR filters. But there is a certain limitation. What are those limitations? Now, if you see that if I use windowing methods, I know that the transition bandwidth δ depends on what type of window I use.

So, if I use a rectangular window, then the transition bandwidth is 4π by a , and I think 4π by M , but the present bandwidth is less. But what is there that in the case of the rectangular window, the problem is pass band, stop band ripple, and stopband ripple is very high? Now, if I want to reduce the ripple, then I have to go to the other window.

Once I use the hamming window, hamming window, I know the transition bandwidth increases from 8π by M . So, in the same order why, my transition bandwidth is larger. So, what is the problem with windowing methods? That lack of precise control over the critical frequency ω_p pass band edge frequency, ω_s the pass the stop band edge frequency.

So, the transition bandwidth δ is nothing but a, you know, stop band edge frequency minus pass band edge frequency. So, in this part, I have a lack of control that depends on the window, if I want to reduce the ripple, the transition bandwidth increases; if I want to increase the ripple, the transition bandwidth decreases, and that is ok. However, there is a lack of control over the windowing method.

Similarly, the frequency sampling method also means that I have a sample with a frequency of either type 1 or type 2 in both cases. I have designed using sampling frequency sampling methods, but these frequency responses may not be as controlled as there is no control over this transition bandwidth. So, that is the main drawback in the design of FIR filters using window methods and frequency sampling methods.

Now, I want a method that has the desired control over transition bandwidth. So, what do I want? I want to design an FIR filter using methods that can give me control over the transition bandwidth and the ripple in the pass band and stop band. That is why I said I want to design an FIR filter, which is an equiripple FIR filter linear-phase FIR filter, using optimization methods.

So, optimization is nothing but a graph of; let us say that suppose I want this filter, now I design this filter. Now, I know this is my design part, and this is my desired part; I know the error. Now, I say I want to minimize the error so that my design response is as close as possible to the desired response. That I want. So, that is nothing but an approximation.

(Refer Slide Time: 05:41)

Design of Optimum Equiripple Linear-Phase FIR Filters is formulated as a Chebyshev approximate problem

- Weighted approximated error between the desired frequency response and the actual frequency response is spread evenly across the pass-band and stop-band of the filter
- Resulting filter have ripples in both the pass-band and the stop-band

The slide includes two hand-drawn diagrams in red ink. The first diagram on the left shows a rectangular pulse representing an ideal filter response. The second diagram on the right shows a similar pulse but with ripples (oscillations) in both the pass-band and the stop-band, illustrating the behavior of an equiripple filter. A small video inset of a speaker is visible in the bottom right corner of the slide.

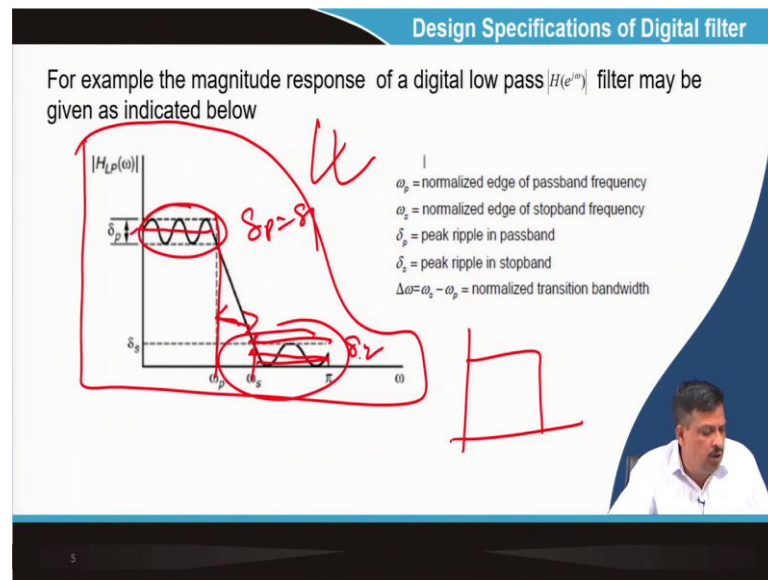
So, that approximation is done using the Chebyshev approximation problem. That is used in mathematics. Do you know the Chebyshev approximation problem in mathematics? We have studied it to optimize that distribution approximation. So, I have a desired distribution; I have a given distribution, and then I change the parameter so that it is close to the desired one. So, that approximation is called the Chebyshev approximation problem. The same method is used to design this kind of filter.

How do you use it? We design and introduce a weighted approximation in error between the desired and actual frequency responses. So, I derived a weighted approximation error function and weighted approximation error between them, so what I want is that, ok, there may be an error between the desired one and the desired frequency and the actual frequency response. But that error should eventually be spread across the pass band and stop band.

So, when I say there is an error, and that error is eventually distributed over the pass band and stop band, I can say the pass band and stop band both the way there is a ripple is there. So, I may want this kind of frequency response, but I can lead down to this kind of frequency response. So, there will be an error that ripples in both the pass band and stop band.

So, I desire to use a weighted approximation error function, which will allow whatever kind of error I desire. So, instead of depending on the window and depending on the methods of frequency sampling, I can say I approx, this is an approximation problem, and I define an error function in which error is eventually evenly distributed among the pass band and stop band, and that error is I have control, I want to minimize that error. So, that is the acceptable design. So, how do I do that? That method.

(Refer Slide Time: 08:10)



So, let us say again that you already know that. So, this is the given frequency response of a low-pass filter. So, you know this is called passband ripple. This is called stop band ripple. This is pass band edge frequency and stopband edge frequency, and this difference is called transition bandwidth. So, I have already known all those things. That is the same for all kinds of filter designs. So, this is the desired frequency response. The frequency response is provided per the specifications.

So, the ideal low pass filter is this one, but we cannot design the ideal one. So, people said, ok, I require a low pass filter whose stop band attenuation is 60 dB, pass band is this dB, and transition bandwidth is this one so that I know.

(Refer Slide Time: 09:05)

In the **pass band** $0 \leq \omega \leq \omega_p$ we require that $|H(e^{j\omega})| \approx 1$ with a deviation $\pm \delta_1$

$1 - \delta_1 \leq |H_r(e^{j\omega})| \leq 1 + \delta_1, \quad |\omega| \leq \omega_p$

In the **stop band** $\omega_s \leq \omega \leq \pi$ we require that $|H(e^{j\omega})| \approx 0$ with a deviation $\pm \delta_2$

$-\delta_2 \leq |H_r(e^{j\omega})| \leq \delta_2, \quad \omega_s \leq |\omega| \leq \pi$

Handwritten annotations include: a red circle around the pass band deviation equation, a red circle around the stop band deviation equation, a red line connecting the two equations, and two sine wave diagrams labeled δ_1 and δ_2 representing ripple.

So, now, since the ripple is distributed evenly among this pass band and stop band, I can say that I required this frequency response in the pass band. The magnitude of the frequency response is one of the filters. δ_1 is the deviation in the pass band. So, I can say this one is let us δ_p is equal to δ_1 .

And instead of δ_s , I said peak to peak δ_2 . So, here also δ_1 is peak to peak, and here also δ_2 is also a have a peak to peak. So, it is minus δ to plus δ . So, the stop band ripple will vary from one idea to another. So, one plus δ and one minus δ_1 . So, that is the stop band ripple variation.

Pass band ripple variation instead of δ_s , I said pass band has a ripple, then I said in the middle there is a line, so there is an δ_2 plus and δ_2 minus. So, δ_2 plus and δ_2 minus that is a ripple condition. Instead of 0 to δ_s , I said minus δ_2 to δ minus δ_2 to plus δ_2 . So, that is the deviation in the stop band, and that is the deviation in the passband, ok. So, that I have known.

(Refer Slide Time: 10:36)

Case 1: Symmetric unit response order of the filter is Odd

$h(n) = h(N-1-n)$ The order of the filter N is Odd

$H_r(\omega) = h\left(\frac{N-1}{2}\right) + \sum_{n=1}^{(N-1)/2} 2h(n) \cos\left(\omega\left(\frac{N-1}{2} - n\right)\right)$

$k = (N-1)/2 - n$

$a(k) = \begin{cases} h\left(\frac{N-1}{2}\right) & \text{for } k=0 \\ 2h\left(\frac{N-1}{2} - n\right) & \text{for } k=1, 2, \dots, (N-1)/2 \end{cases}$

$H_r(\omega) = \sum_{k=0}^{(N-1)/2} a(k) \cos \omega k$

$\delta(\omega) = 1$

$N-1-n=k$

$h(n)$

$a(k)$

$\delta(\omega) = 1$

Now, I know that there are 4 methods for the design of linear-phase FIR filters. So, in the case of case 1, which is a symmetric unit response, an order N is odd. So, the order of the filter N is odd, and the impulse response is symmetric. So, that is the requirement for the linear phase. So, this is my linear-phase requirement plus-minus. So, I know this is a requirement. So, if it is symmetric, then I know $h[n]$ is equal to $h(N-1-n)$. That is my symmetric requirement.

And now small capital N is odd; that means the order of the filter is odd, ok. Now, I know if the order is odd already, we have derived for linear-phase condition what is the frequency response; that we have already known that that is my (Refer Time: 11:37). So, H_r is the design if $h[n]$ is my impulse response, then this will be my H_r for my design frequency response. So, H_r is nothing but a frequency response of the design filter.

So, if $h[n]$ is my impulse response, which is symmetric, and the order of N is odd, then this will be my frequency response. Now, in this equation, if I pick, make k equal to this one. So, this part is equal to k , then I can say that I can define

$$a(k) = \begin{cases} h\left(\frac{N-1}{2}\right), & \text{for } k = 0 \\ 2h\left(\frac{N-1}{2} - n\right), & \text{for } k = 1, 2, \dots, \frac{N-1}{2} \end{cases}$$

Then, I can say:

So, this is my first one, and this is my second one. The difference between the two equations is nothing but a relationship between the $b(k)$ and $b \text{ cap } k$. So, this is a $b \text{ cap } k$,

ok. So, the relations will come like this: if I 1 and 2 are equalized and do the relationship, you can derive this sequence relationship. So, now, you can see that $H_r(\omega)$ is written in one kind of format: $b(k)$ into $\cos \omega k$.

So, in the case of the first one, it is 1 into this one. In the case of this one, this is convolution where this is the coefficient, which is related to the $h[n]$; $b(k)$ is related to the $h[n]$ because if you see the $b(k)$, I define it in terms of $h[n]$. So, there is a linear relationship between the $b(k)$ and $h[n]$.

So, $b(k)$ is related to $h[n]$, and $a(k)$ is related to $h[n]$, so all $h[n]$ basically define the filter coefficient. Here also, $b(k)$ defines the filter coefficient and $\cos \omega k$; only one \cos constant term is there, which is $\cos(\omega/2)$; instead of 1 in the case of symmetric even, it is $\cos(\omega/2)$.

(Refer Slide Time: 16:05)

Case 3: Anti-symmetric unit response order of the filter is Odd

$h(n) = -h(N-1-n)$ The order of the filter N is Odd

$H_r(\omega) = \sum_{n=0}^{(N-1)/2} 2h[n] \sin\left(\omega\left(\frac{N-1}{2} - n\right)\right)$

$k = (N-1)/2 - n$

$c(k) = 2h\left(\frac{N-1}{2} - k\right)$ for $k=1, 2, \dots, N/2$

$H_r(\omega) = \sum_{k=1}^{(N-1)/2} c(k) \sin \omega k$

$H_r(\omega) = \sin \omega \sum_{k=0}^{(N-1)/2} c(k) \cos \omega k$

Handwritten notes: $c(k) = h(n)$, $Q(\omega) = \sin \omega$

Similarly, for anti-symmetric, again, you take this one, and again, k is equal to this one. Again, the approximation is you can get the same kind of equation; this part is the same: $c(k)$ is related to c cap k is related to $h[n]$, linearly related to $h[n]$. Again, it has a multiplication factor $\sin \omega$, ok.

(Refer Slide Time: 16:34)

Case 3: Anti-symmetric unit response order of the filter is Even

$h(n) = -h(N-1-n)$ The order of the filter N is even

$H_r(\omega) = \sum_{n=0}^{N/2-1} 2h(n) \sin\left(\omega\left(\frac{N-1}{2} - n\right)\right)$

$k = N/2 - n$


$d(k) = 2h\left(\frac{N}{2} - k\right)$ for $k=1, 2, \dots, N/2$

$H_r(\omega) = \sum_{k=1}^{N/2} d(k) \sin\left(\omega\left(k - \frac{1}{2}\right)\right)$

$H_r(\omega) = \sin\left(\frac{\omega}{2}\right) \sum_{k=0}^{N/2-1} d(k) \cos \omega k$

$H_r(\omega) = Q(\omega) \cdot P(\omega)$

$Q(\omega) = \sin \frac{\omega}{2}$



Now, again, if I say that N is even in the case of anti-symmetric, I can get the same things. Only the multiplication factor is $\sin(\omega/2)$ and the rest are the same.

(Refer Slide Time: 16:59)

Real-Valued Frequency Response Functions for all 4 types Linear-Phase FIR Filters can be expressed as

$H_r(\omega) = Q(\omega)P(\omega)$

$Q(\omega) = \begin{cases} 1 & \text{for Type 1} \\ \cos(\omega/2) & \text{for Type 2} \\ \sin(\omega) & \text{for Type 3} \\ \sin(\omega/2) & \text{for Type 4} \end{cases}$

$P(\omega) = \begin{cases} \sum_{k=0}^{(N-1)/2} a(k) \cos \omega k & \text{for Type 1} \\ \sum_{k=0}^{N/2-1} b(k) \cos \omega k & \text{for Type 2} \\ \sum_{k=0}^{(N-1)/2-1} c(k) \cos \omega k & \text{for Type 3} \\ \sum_{k=0}^{N/2-1} d(k) \cos \omega k & \text{for Type 4} \end{cases}$

$Q(\omega) \leftarrow h(n)$

$a(k) \leftarrow h(n)$


$b(k) \leftarrow h(n)$

$c(k) \leftarrow h(n)$

$d(k) \leftarrow h(n)$

$L = (N-1)/2$

$N/2 - 1 + 1$



So, if I write all the 4, 4 equation, this equation, this equation, this equation and this equation in a summarized format, I can say $H_r(\omega)$; $H_r(\omega)$ is nothing but a I can say it is a $Q(\omega)$ multiplied by $P(\omega)$, where $Q(\omega)$ in this case $Q(\omega)$ is equal to $\sin(\omega/2)$. In this case, $Q(\omega)$ is equal to $\sin(\omega)$. In this case, $Q(\omega)$ is equal to \cos , $Q(\omega)$ is equal to $\cos(\omega/2)$ and in here it is nothing but a $Q(\omega)$ is equal to 1.

So, if I want to write down these 4 equations in a generalized form, which $H_r(\omega)$ is equal to $Q(\omega)$ and multiplied by $P(\omega)$. So, $Q(\omega)$ in the case of type 1 or case 1, is 1. In case of case 2, it is ω by 2. In case of case 3, it is $\sin(\omega)$. In case of case 4, it is nothing but a $\sin(\omega/2)$.

What is $P(\omega)$? $P(\omega)$ type 1 k equal to 0 to this one, type 2 this one, type 3 this one, type 4 this one. Now, if you see $Q(\omega)$ does not depend on $h[n]$. because no component of $h[n]$ is here; it is nothing, but a 1 is a constant. $\cos(\omega/2)$ is nothing but a function of ω . $\sin(\omega)$ is nothing but a function of ω . $\sin(\omega/2)$, it is nothing but a function of ω .

But here, all are $a(k)$, $b(k)$, and $c(k)$, which are all related to $h[n]$. So, I can control $H_r(\omega)$ by controlling $P(\omega)$. How can I control $P(\omega)$? My controlling of $P(\omega)$ depends on $a(k)$, $b(k)$, $c(k)$ or $d(k)$ and all are related to $h[n]$. So, if I find out the filter coefficient precisely and if I want to find out the filter coefficient precisely, such that I can design a perfect $H_r(\omega)$ which is as close as to desired frequency response.

(Refer Slide Time: 19:16)

$P(\omega)$ has the common form

$$P(\omega) = \sum_{k=0}^{L-1} \alpha(k) \cdot \cos \omega k$$

$L = (N-1)/2$ N is odd
 $L = N/2 - 1$ N is even

$\alpha(k)$ representing the parameters of the filter, which are linearly related to the units sample response $h[n]$ of the FIR filter

- Let the real-valued desired frequency response $H_d(\omega)$ and weighting function on the approximation error is $W(\omega)$.
- $W(\omega)$ is used to choose the relative size of the errors in the different frequency bands
- For convenience to normalization $W(\omega)$ is unity in the stopband and set $W(\omega) = \frac{\delta_s}{\delta_p}$ in the passband

weighted approximation error

$$E(\omega) = W(\omega)[H_d(\omega) - H_r(\omega)]$$

$$E(\omega) = W(\omega)[H_d(\omega) - Q(\omega)P(\omega)]$$

$$= W(\omega)Q(\omega)\left[\frac{H_d(\omega)}{Q(\omega)} - P(\omega)\right]$$

So, how do you do that? So, the problem is, if you see the $P(\omega)$ in a common form, I can write down, let us say all are $b(k) \cos \omega k$, $c(k) \cos \omega k$ Sorry, there is $\cos \omega k$ $d(k) \cos \omega k$. I can write it down. So, all are the same kinds of things. So, I can say

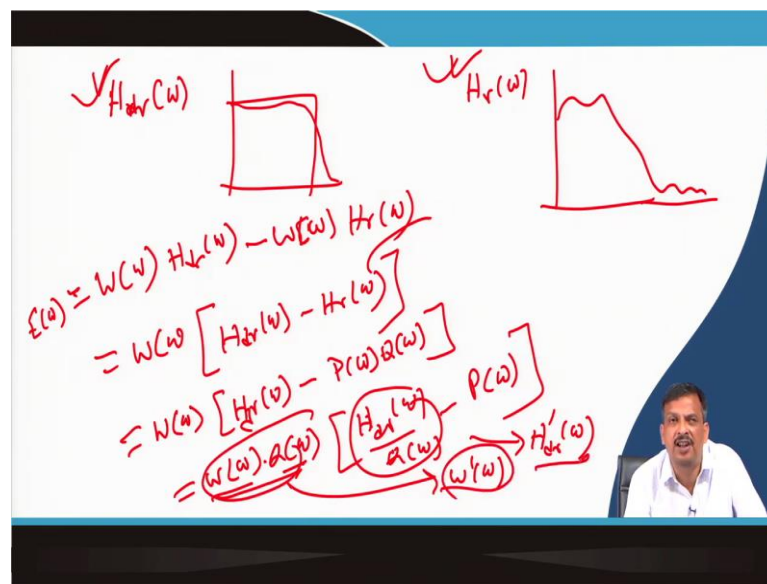
$$P(\omega) = \sum_{k=0}^N \alpha(k) \cdot \cos(\omega k)$$

Let us say here L only varies. L is equal to N minus 1 divided by 2 in case of odd and N by 2 minus 1 in case of N is even.

So, I can say only L will vary; L will be N minus 1 by 2 if N is odd. L will be N by 2 minus 1 if N is even. Otherwise, this is the same. Otherwise, all are the same; $\alpha(k)$ is a variable that is $\alpha(k)$, which may be $a(k)$, which may be $b(k)$, which may be $c(k)$, which may be $d(k)$. So, this $\alpha(k)$ represents the parameters of the filter, which are linearly related to the impulse response of the filter.

So, if I say $H_r(\omega)$, $H_r(\omega)$ is nothing but a combination of $Q(\omega)$ and $P(\omega)$. I have only control on $P(\omega)$, $Q(\omega)$ is a constant. So, how do I control $P(\omega)$? By controlling $h[n]$, which depends on $\alpha(k)$. So, $\alpha(k)$ is called the filter parameter. So, let us say the real value desired frequency response is $H_{dr}(\omega)$; that means I want this frequency response. So, I will take a slide here.

(Refer Slide Time: 21:22)



Let us say I want a frequency response, which is my desired frequency response, which is $H_{dr}(\omega)$, which is this one. Now, I design $H_r(\omega)$, which may be this one. Then, I want to compute the error between the desired one and the design one. Let us say I define a function $W(\omega)$, which relatively sizes the error in the different frequency bands. So, I can say I want to monitor the error by using $W(\omega)$. So, let us say I said, instead of this kind of error is sufficient for me.

So, if you see here, only I can minimize the error with respect to $\mathbf{a}(k)$ or α I can say $\alpha(k)$, not a cap, $\alpha(k)$ with respect to $\alpha(k)$. So, this is $\alpha(k)$. So, $\alpha(k)$ is the filter parameter with

respect to which I want to minimize the $E(\omega)$. So, it is a minimization problem, so take the derivative. So, I want to find a set of $\alpha(k)$ that minimizes the maximum absolute value of $E(\omega)$. Minimize the $E(\omega)$ with respect to $\alpha(k)$, is nothing but a taking derivative with $dE(\omega)/d\alpha(k)$.

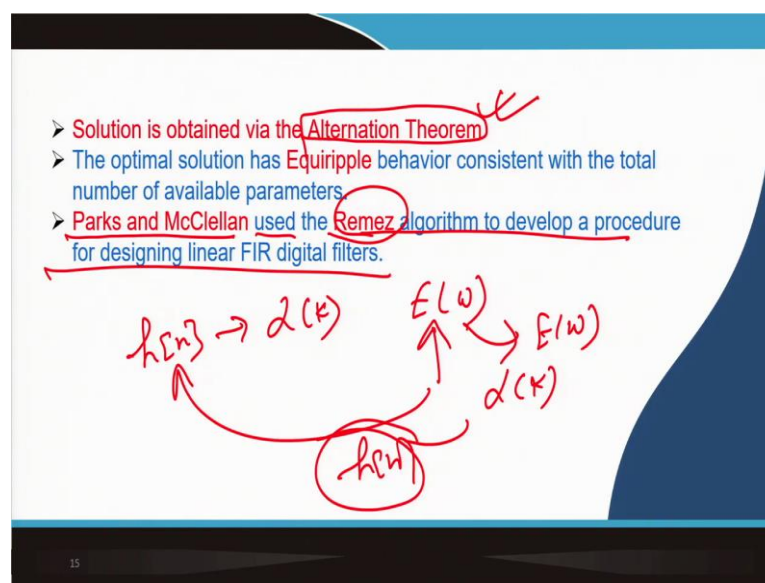
So, with respect to $\alpha(k)$, if I take the derivative and if I minimize this one. So, what do I want? I want to determine the desired $\alpha(k)$, which is related to the impulse response of the filter design filter so that $E(\omega)$ becomes minimum. So, what is $E(\omega)$? It is the difference between the desired response and the design response.

So, that is, maximize the approximation problem, or I can say optimization problem, I want to optimize the error. So, that optimization is done using the Chebyshev approximation problem. So, that is a method by which I do this optimization. So, if you have a mathematical background, you can do that optimization, and you can do that. I am not covering it purposefully because if I cover it for a B.Tech engineer, it will be huge because it can take another 1-week course for this whole optimization problem description.

So, what is my job? Our job has to $\alpha(k)$ has been determined to construct the original frequency response and hence $h[n]$. So, once I minimize the $E(\omega)$, for that set of $\alpha(k)$ for which the error is minima, from that $\alpha(k)$ value, if I say the $h[n]$, I can design $h[n]$. So, $h[n]$ is given, $\alpha(k)$ is derived, calculate the error, minimize the error and modify that $h[n]$.

So, once I do an approximation problem then I get the desired, once I go close to the desired frequency response, I can say that set of $h[n]$ is my optimal set of impulse response which is close to the desired frequency response. So, that is the optimization problem.

(Refer Slide Time: 27:52)



So, what is the solution to this optimization problem? So, the solution is obtained via the alternation theorem. There is another theorem called the alternation theorem or alternation theorem. This alternation theorem is used to solve this. Now, there is one method Parks and McClellan used, the Remez algorithm, to develop the procedure for design. So, what is the procedure? I have to design a set of $h[n]$, derive $\alpha(k)$, and find out the error; then, I want to minimize this error by changing this $h[n]$.

Once I said this is optimum, $E(w)$ is optimum, that set of $\alpha(k)$ for that set of $h[n]$ is my desired impulse response of the filter. So, that approximation is made using an algorithm, which is the remaining algorithm. You can see that book, or you can go to any standard DSP book and get it. If you are interested, you can raise a question after covering the course. So, send an email, then I can take another class for this one, so that optimization problem, you know, ok.

So, that is the design method for FIR filters using optimization methods. So, if I summarize the FIR filter, you have to know the FIR filter finite impulse response filter, the property it may be linear symmetric or anti-symmetric if the order of the filter is even and odd. So, we know what kind of frequency response will be there for the linear-phase requirement. So, that is common for all kinds of design.

Then, I go for the design of 3 methods; one is called window methods, and I can design an FIR filter using window methods. So, using algebra, I can calculate $h[n]$ multiplied by

the W_n and then convolve it with the input signal, and I get the desired output. Similarly, I can go for the frequency sampling methods; there is a type 1 sampling and type 2 sampling, and those equations are there. Using that method, I can also design the FIR filter for a given specification.

Then, I go for the optimization methods, which are computer-based design methods that can be optimization algorithms that can be done on a computer to find out a desired set of $h[n]$ for which the difference between the desired frequency response and the design frequency response is minimal. So, that is the summary of the FIR filter.

So, from the next lecture, I will go for the IIR filter design, ok.

Thank you.