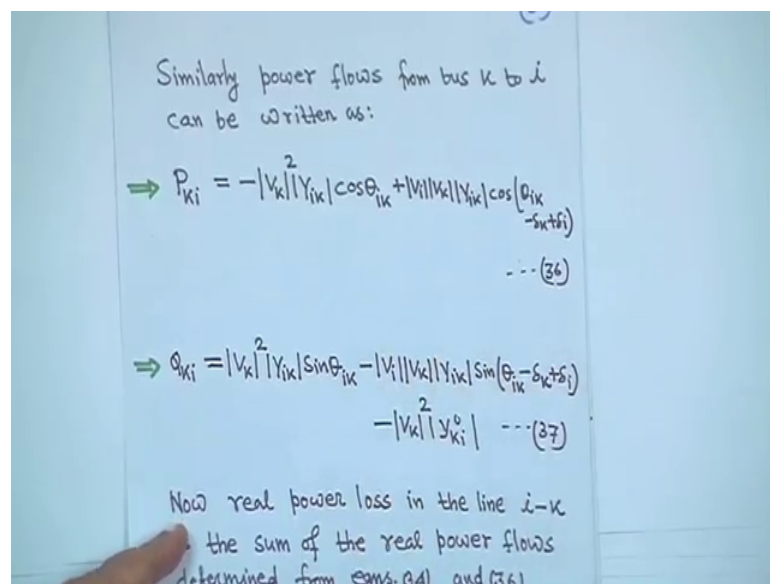


Power System Analysis
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Lecture - 32
Load Flow Studies (Contd.)

Next are from equation 36 right. So, equation 36 it was P_{ki} that was P_{ik} and this is your P_{ki} right.

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So, this is the expression for this thing is. So, here also find out P_{21} also right like k is equal to 2 i is equal to 1 in this expression in substitute.

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From eqn. (36),

$$P_{21} = -|V_2|^2 |Y_{12}| \cos \theta_{12} + |V_1| |V_2| |Y_{12}| \cos(\theta_{12} - \delta_2 + \delta_1)$$

$$\therefore P_{21} = -(0.98265)^2 \times 22.36 \cos(116.56^\circ) + 1.05 \times 0.98265 \times 22.36 \cos(116.56^\circ + 3.046^\circ + 0^\circ)$$

$$\therefore P_{21} = -1.744 \text{ pu MW} = -174.4 \text{ MW}$$

$$P_{31} = -|V_3|^2 |Y_{13}| \cos \theta_{13} + |V_1| |V_3| |Y_{13}| \cos(\theta_{13} - \delta_3 + \delta_1)$$

If you do so, that will be the expression for P 21 that is equation 36 right.

So that means, are all the parameters you put it here, put it here then you will get P 21 is equal to your minus 1.744 per unit megawatt minus 174.45 megawatt right.

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$$+ 1.05 \times 0.98265 \times 22.36 \cos(116.56^\circ + 3.046^\circ + 0^\circ)$$

$$\therefore P_{21} = -1.744 \text{ pu MW} = -174.4 \text{ MW}$$

$$P_{31} = -|V_3|^2 |Y_{13}| \cos \theta_{13} + |V_1| |V_3| |Y_{13}| \cos(\theta_{13} - \delta_3 + \delta_1)$$

$$\therefore P_{31} = -(1.00099)^2 \times 31.62 \cos(108.4^\circ) + 1.05 \times 1.00099 \times 31.62 \cos(108.4^\circ + 2.68^\circ + 0^\circ)$$

$$\therefore P_{31} = -1.95 \text{ pu MW} = -195 \text{ MW}$$

if you see P 12 it P 12 here 181.89 megawatt right and that mean

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$$\begin{aligned} \therefore P_{12} &= -(1.05)^2 \times 22.36 \cos(116.56^\circ) \\ &\quad + 1.05 \times 0.98265 \times 22.36 \cos(116.56^\circ - 0 - 3.048^\circ) \\ \therefore P_{12} &= 1.8189 \text{ pu MW} = 181.89 \text{ MW} \\ P_{13} &= -|V_1|^2 |Y_{13}| \cos(\theta_{13}) + |V_1| |V_3| |Y_{13}| \cos(\theta_{13} - \delta_1 + \delta_3) \\ \therefore P_{13} &= -(1.05)^2 \times 31.62 \cos(108.4^\circ) \\ &\quad + 1.05 \times 1.00099 \times 31.62 \cos(108.4^\circ - 0 - 2.68^\circ) \\ \therefore P_{13} &= 2.0 \text{ pu MW} = 200 \text{ MW} \end{aligned}$$

It is positive means power is flowing 1 to 2 right and here at the P 21 it is minus 174.4 megawatt, then the power actually flowing from why your what to you call one to two, but is P 21 is showing minus right that mean P 2 in one this one, this one is your P 1 to this one is 1 8, this is one is 181.89, it indicate difference indicate that resistive lose in the in the line right that we will see after this.

So, similarly this is P 21 similarly P 31 using the same equation 36 right k is equal to 3 i is equal to 1. If you put it put all the parameters, P 31 will also become minus 1.95 per unit megawatt that is minus 195 megawatt right.

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$$P_{32} = -|V_3|^2 |Y_{23}| \cos \theta_{23} + |V_3| |V_2| |Y_{23}| \cos(\theta_{33} - \theta_3 + \theta_2)$$

$$\Rightarrow P_{32} = -(1.00099)^2 \times 35.77 \cos(116.6^\circ) + 1.00099 \times 0.98265 \times 35.77 \cos(116.6^\circ + 2.68^\circ - 3.046^\circ)$$

$$\therefore P_{32} = 0.496 \text{ pu MW} = 49.6 \text{ MW.}$$

Real power losses in line 1-2, 1-3, and 2-3.

$$\Rightarrow P_{\text{Loss}} = P_{12} + P_{13} = (181.89 - 174.4) = 7.49 \text{ MW}$$

So; that means, power is the power the actual duration of the power flowing is one to 3 because it is minus sign is coming right.

So, next is your P 32 same way you can compute, write this is same equation you can use and put your k 3 i k is equal to 3 i is equal to 2 expand these and you are what you call put this, and there you put all the values you will get P 32 is equal to 49.6 megawatt these all this results are after second iteration only right.

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$$\therefore P_{32} = 0.496 \text{ pu MW} = 49.6 \text{ MW.}$$

Real power losses in line 1-2, 1-3, and 2-3.

$$\Rightarrow P_{\text{Loss}_{12}} = P_{12} + P_{21} = (181.89 - 174.4) = 7.49 \text{ MW}$$

$$\Rightarrow P_{\text{Loss}_{13}} = P_{13} + P_{31} = (200 - 195) = 5 \text{ MW}$$

$$\Rightarrow P_{\text{Loss}_{23}} = P_{23} + P_{32} = (-49.03 + 49.6) = 0.57 \text{ MW}$$

Now real power losses in line 1 2, 1 3, and 2 3; so P Loss 12 actually is equal to the we have showing before know that P your line place P 12 plus P 21 that is 181.89 minus 174.4 that is 7.49 megawatt. Similarly P Loss 13 that is P 13 plus P 31 200 minus 195 that is 5 megawatt and P Loss 23 that is P 23 plus P 32 that is minus 49.03 plus 49.6 is 0.57 megawatt right.

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Reactive line flows can be calculated from eqns (35) and (37).

From eqn. (35), we get,

$$Q_{12} = |V_1|^2 |Y_{12}| \sin \theta_{12} - |V_1| |V_2| |Y_{12}| \sin(\theta_{12} - \delta_1 + \delta_2)$$

$$\therefore Q_{12} = (1.05)^2 \times 22.36 \sin(116.56^\circ) - 1.05 \times 0.98265 \times 22.36 \sin(116.56^\circ - 3.04^\circ)$$

$\therefore Q_{12} = 0.8948 \text{ pu MVAR} = 89.48 \text{ MVAR}$

Similarly,

$$Q_{13} = (1.05)^2 \times 31.62 \sin(108.4^\circ) - 1.05 \times 1.00099 \times 31.62 \sin(108.4^\circ - 3.04^\circ)$$

So, these are the result for the loss is after your what you call that second iteration that is a real power loss right. Similarly your reacting line flows we calculated from equation 35 and 37. So, against like your Q your qik expression is given in equation 35 right.

So, there you just put i is equal to 1, k is equal 2 and this expression and put all these parameters you will get Q 12 actually is equal 0.8948 it power unit megawatt, that is multiply your 100, 100 m is the base. So, 89.48 megawatt right similarly Q13 also you compute put all the values.

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$$\begin{aligned} \therefore Q_{12} &= (1.05)^2 \times 22.36 \sin(116.56^\circ) \\ &\quad - 1.05 \times 0.98265 \times 22.36 \sin(116.56^\circ - 3.04^\circ) \\ \therefore Q_{12} &= 0.8948 \text{ pu MVAR} = 89.48 \text{ MVAR} \end{aligned}$$

Similarly,

$$\begin{aligned} Q_{13} &= (1.05)^2 \times 31.62 \sin(108.4^\circ) \\ &\quad - 1.05 \times 1.00099 \times 31.62 \sin(108.4^\circ - 2.68^\circ) \\ \therefore Q_{13} &= 1.088 \text{ pu MVAR} = 108.8 \text{ MVAR} \end{aligned}$$

So, Q13 will be become 108.8 megawatt right.

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$$\begin{aligned} Q_{23} &= (0.98265)^2 \times 35.77 \sin(116.6^\circ) \\ &\quad - 0.98265 \times 1.00099 \times 35.77 \sin(116.6^\circ + 3.04^\circ - 2.68^\circ) \\ \therefore Q_{23} &= -0.4746 \text{ pu MVAR} = -47.46 \text{ MVAR} \end{aligned}$$

From eqn. (37),

$$\begin{aligned} Q_{21} &= (0.98265)^2 \times 22.36 \sin(116.56^\circ) \\ &\quad - 1.05 \times 0.98265 \times 22.36 \sin(116.56^\circ + 3.04^\circ) \\ \therefore Q_{21} &= -0.746 \text{ pu MVAR} = -74.6 \text{ MVAR} \end{aligned}$$

So, similarly Q23 also you compute Q23 also you compute right. So, all these directly I am not writing the formula for Q23 again just you can do it of your own right. So, all all this things are details I have been explained right. So, you can do it. So, Q23 will be become minus 47.46 megawatt right.

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$$\therefore Q_{23} = -0.4746 \text{ pu MVAR} = -47.46 \text{ MVAR}$$

From eqn. (37),

$$Q_{21} = (0.98265)^2 \times 22.36 \sin(116.56^\circ) - 1.05 \times 0.98265 \times 22.36 \sin(116.56^\circ + 3.046^\circ)$$

$$Q_{21} = -0.746 \text{ pu MVAR} = -74.6 \text{ MVAR}$$

$$Q_{31} = (1.00099)^2 \times 31.62 \sin(108.4^\circ) - 1.05 \times 1.00099 \times 31.62 \sin(108.4^\circ + 2.68^\circ)$$

$$\therefore Q_{31} = -0.946 \text{ pu MVAR} = -94.6 \text{ MVAR}$$

Now similarly from we equation 37 that it that is your that is your Q_{ki} .

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can be written as:

$$\Rightarrow P_{ki} = -|V_k|^2 |Y_{ik}| \cos \theta_{ik} + |V_i| |V_k| |Y_{ik}| \cos(\theta_{ik} - \delta_k + \delta_i) \quad \dots (36)$$

$$\Rightarrow Q_{ki} = |V_k|^2 |Y_{ik}| \sin \theta_{ik} - |V_i| |V_k| |Y_{ik}| \sin(\theta_{ik} - \delta_k + \delta_i) - |V_k|^2 |Y_{ki}^0| \quad \dots (37)$$

Now real power loss in the line $i-k$ is the sum of the real power flows determined from eqns. (34) and (36)

$$\therefore P_{\text{Loss}_{ik}} = P_{ik} + P_{ki}$$

That was your that was Q_{ik} and that is Q_{ki} this expression is given 37 but note that charging admittance is not considered. So, it will be 0, this term will be 0 right and Q_{ki} also for Q_{ik} also for Q_{ik} also charging admittances 0, but you have not considered that right. So, if you calculate Q_{21} then it is coming minus 74.6 megawatt using equation 37.

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Handwritten calculation for Q_{21} on a whiteboard. The calculation is as follows:

$$Q_{21} = (0.98265)^2 \times 22.36 \sin(116.56^\circ) - 1.05 \times 0.98265 \times 22.36 \sin(116.56^\circ + 3.046^\circ)$$
$$Q_{21} = -0.746 \text{ pu MVAR} = -74.6 \text{ MVAR.}$$

Below this, the calculation for Q_{31} is shown:

$$Q_{31} = (1.00099)^2 \times 31.62 \sin(108.4^\circ) - 1.05 \times 1.00099 \times 31.62 \sin(108.4^\circ + 2.68^\circ)$$
$$\therefore Q_{31} = -0.9469 = -94.69 \text{ MVAR}$$

A small circular inset in the bottom right corner shows a man in a pink shirt.

Similarly Q_{31} you compute often substation there all you will get it is minus 94.69 point six nine megawatt right.

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Handwritten calculation for Q_{32} on a whiteboard. The calculation is as follows:

$$Q_{32} = (1.00099)^2 \times 35.77 \sin(116.6^\circ) - 1.00099 \times 0.98265 \times 35.77 \sin(116.6^\circ + 2.68^\circ - 3.046^\circ)$$
$$\therefore Q_{32} = 0.4866 \text{ pu MVAR} = 48.66 \text{ MVAR.}$$

Below this, the text reads: "Reactive power losses in line 1-2, 1-3 and 2-3."

Then, the calculation for reactive power loss in line 1-2 is shown:

$$\Rightarrow Q_{\text{Loss}_{12}} = Q_{12} + Q_{21} = (89.48 - 74.6) = 14.88 \text{ MVAR}$$

And for line 1-3:

$$Q_{\text{Loss}_{13}} = Q_{13} + Q_{31} = (108.8 - 94.69) = 14.11 \text{ MVAR}$$

A hand holding a blue pen is visible at the bottom of the whiteboard. A small circular inset in the bottom right corner shows a man in a pink shirt.

So, then you calculate Q_{32} that is your Q_{32} again the same expression put all the values not writing those expression again and again right understandable now right. So, this is coming Q_{32} is equal to 48.66 megawatt; now reactive power losses in line 1 2, 1 3 and 2 3 same as before, so $Q_{\text{loss}_{12}} = Q_{12} + Q_{21}$.

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Reactive power losses in line 1-2, 1-3 and 2-3.

$$\Rightarrow Q_{Loss_{12}} = Q_{12} + Q_{21} = (89.48 - 74.6) = 14.88 \text{ MVAR}$$
$$\Rightarrow Q_{Loss_{13}} = Q_{13} + Q_{31} = (108.8 - 94.69) = 14.11 \text{ MVAR}$$
$$\Rightarrow Q_{Loss_{23}} = Q_{23} + Q_{32} = (-47.46 + 48.66) = 1.20 \text{ MVAR}$$

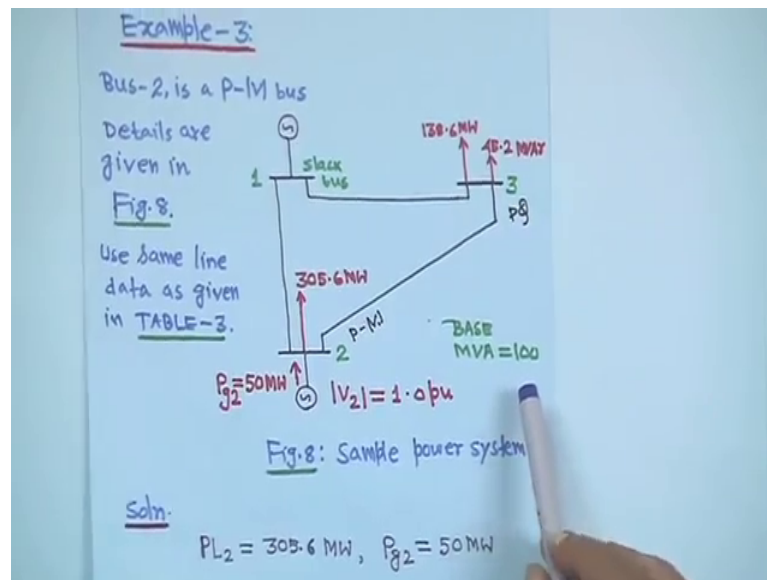
Note that all the results given above are computed after 2nd iteration.

So, you will get 14.88 megawatt. So, Q loss 13 is equal to Q 13 plus Q 31 you will get 14.11 megawatt, and Q loss 23 is equal to Q23 plus Q32 that is coming 1.20 megawatt. Note that all the all the results given above are computed after second iteration only it is not converse result of that convergence you have to make more number of iteration. So, you have to trace the convergence that whatever convergence procedure I have said right next is this example considered for I will all busses are your PQ type busses right.

Now next will take an example that will that I will considered Pv loss also and you can see that have we can accommodate Pv loss in the Gauss-Seidel method. After Gauss-Seidel method we will come to the Newton-Raphson method right and your decouple couple decouple and first decouple right loop loss and then will see that you are for transformer captures in transform representation the pi model, and after that I will tell you that P and pqv your bus accommodation in that loop loss study that how one can do this and what is the your significance of it right.

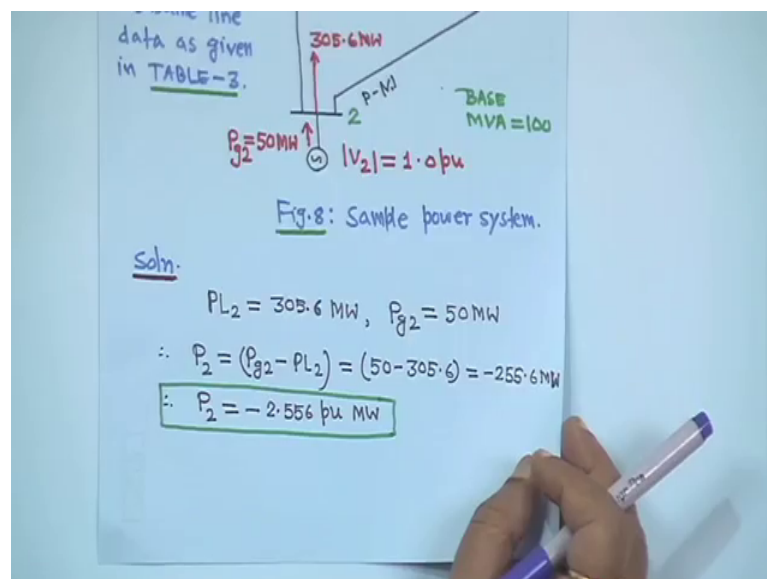
So, next example is

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Next example is that your same data we have taken accept one thing, that this is actually in this case this is a slack bus 3 is a PQ bus that same load data as before 138.6 megawatt.

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And reactive load is 45.2 megawatt right and this bus is a Pv bus, this bus is a Pv bus. So, here for bus 2 voltage magnitude is specified a Pv bus P has to be specified and voltage magnitude has to be specified. So, voltage magnitude V 2 is equal to 1.0 per unit it is specified. And they load that is 305.6 x megawatt Pg 2 is also 50 megawatt, but you

know other thing has been main side right that mean Pv bus means you have to find out that your what you call Q is not given right.

. So, so; that means, in PQ bus b and delta are unknown for this bus V3 and delta 3 have to find out and for this busses your Q and delta 2 has to obtained because voltage magnitude specified we all for also specified right. So, in this case we will show only your what you call that couple of iterations right I have to check either are made it 2 iterations or 3 iterations right, but how to make it, but no queue limit nothing will be considered here just to show you that how things can happen right. So, same has V 4 pl t PL 2 is given 305.6 megawatt, Pg 2 is 50 megawatt right your put P 2 is equal to Pg 2 minus PL 2 that minus 255.6 megawatt there put P 2 is equal to minus 2.556 power unit megawatt same as before right and similarly. So, this is again 3 bus problem know.

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(55)

$$P_3 = P_{g3} - PL_3 = (0 - 138.6) \text{ MW} = -138.6 \text{ MW}$$

$$\therefore P_3 = -1.386 \text{ pu MW}$$

$$Q_3 = Q_{g3} - QL_3 = (0 - 45.2) \text{ MVAR} = -45.2 \text{ MVAR}$$

$$\therefore Q_3 = -0.452 \text{ pu MVAR}$$

Slack bus voltage

$$V_1 = (1.05 + j0.0) \text{ pu}$$

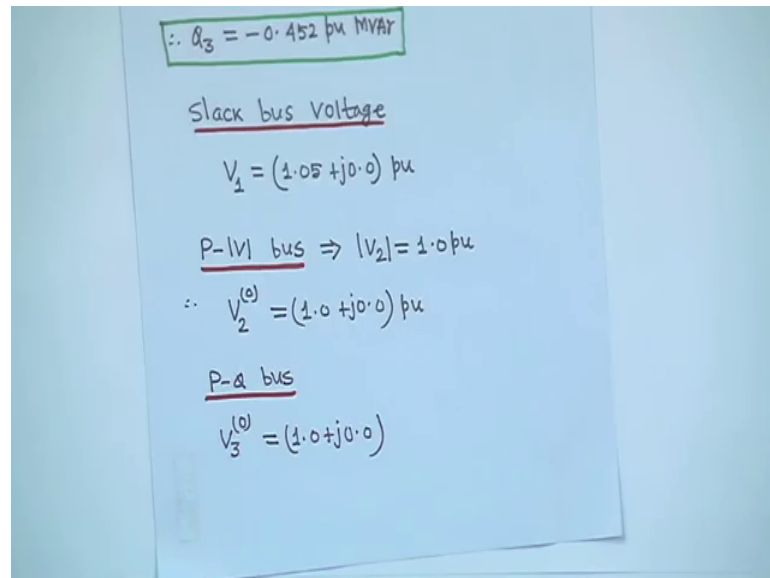
P-V bus $\Rightarrow |V_2| = 1.0$

So, similarly P 3 is equal to Pg 3 minus PL 3. So, that is no genert that is no generator at bus 3 sothis 0 minus 138.6 megawatt that minus 138.6 megawatt. So, it is divided by 100, I am not dividing it 100, but if you divided by 100, it is h100 mb is the base so minus 1.386 power unit megawatt right. Similarly per Q 3 is also Qg 3 minus QL 3 is minus 45.2 megawatt so divided by hundred it will be minus 0.452 power unit megawatt. A slack bus voltage is same 1.05 plus j 05 and 0 right.

Now, Pv bus magnitude of voltage magnitude V 2 is equal to one right; that means, V 2 is 0 actually you can take 1 plus j 0, in this case what we will do that the way we solve

that your I will follow they its distinc this thing different write the different procedure are this iterative method right.

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$$\therefore Q_3 = -0.452 \text{ pu MVAR}$$

Slack bus voltage

$$V_1 = (1.05 + j0.0) \text{ pu}$$

P-V bus $\Rightarrow |V_2| = 1.0 \text{ pu}$

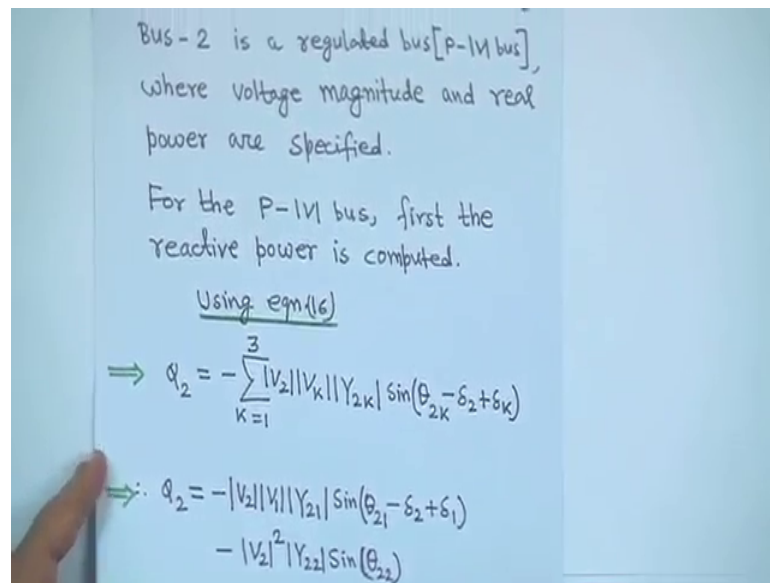
$$\therefore V_2^{(0)} = (1.0 + j0.0) \text{ pu}$$

P-Q bus

$$V_3^{(0)} = (1.0 + j0.0)$$

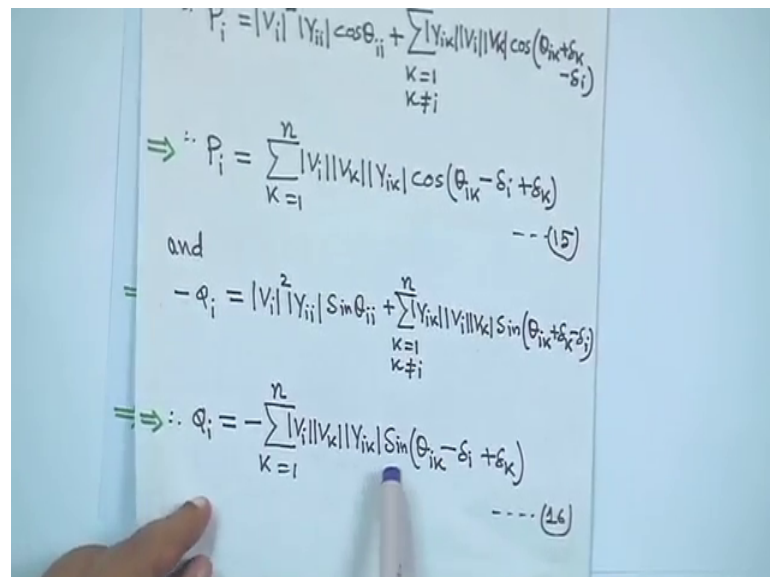
So, what we will do that V 2 is 0 all though this voltage magnitude actually constant right. So, you are soon V 2 0 is equal to 1 plus j 0; that means, it magnitude is 1 the initial angel is 0 right. So, this way we assume, but magnitude will always remain constant magnitude will be untouchable right it is given and for PQ bus V 3 0 1 plus j 0 right so, but this PQ bus V 3 both magnitude and angel will vary at here magnitude has to be Q fix right.

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So, this one your bus 2 is a regulated bus that is Pv bus right where voltage magnitude and real power are specified right, and for the Pv bus first the reactive power is computed using equation 16, just let me find out for is equation 16 right I will tell you. So, here it is right.

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So, this one your equation 16 and n is equal to 3, this is equation 16 then n is equal to 3 because at bus 2 it is your Pv bus. So, in that bus your what you call Q 2 is not known right. So, we have to see that how iteratively you can made it right. So, what you will do

it that from this equation n is equal to 3 you expand for i is equal to 2 right because bus 2 actually is it Pv bus right. So, put i is equal to 2 and k is equal to 1 2 n, because n is equal to 3 because there are 3 bus problem are solving right therefore, if you put i is equal to 2 n minus it is it is minus sign, minus sign is there right.

So, it is k is equal to 1 2 3, then it will magnitude V 2 V k magnitude Y 2 k sin theta 2 k minus delta 2 plus delta k. For k is equal to 1 2 3 you expand this equation right. If you expand this equation right then you will get this Q 2 is equal to this 1 that minus magnitude V 2 magnitude V 1 magnitude Y 2 1 sin theta 2 1 minus delta 2 plus delta 1 then minus magnitude V 2 square magnitude Y 2 2 sin theta 2 2 right minus magnitude V 2 magnitude V 3 magnitude Y 2 3 right sin theta 2 3 minus delta 2 plus delta 3

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$$\Rightarrow Q_2 = - \sum_{k=1}^3 |V_2| |V_k| |Y_{2k}| \sin(\theta_{2k} - \delta_2 + \delta_k)$$

$$\Rightarrow Q_2 = - |V_2| |V_1| |Y_{21}| \sin(\theta_{21} - \delta_2 + \delta_1) - |V_2|^2 |Y_{22}| \sin(\theta_{22}) - |V_2| |V_3| |Y_{23}| \sin(\theta_{23} - \delta_2 + \delta_3)$$

$$\Rightarrow Q_2^{(p+1)} = - |V_2^{(p)}| |V_1^{(p)}| |Y_{21}| \sin(\theta_{21} - \delta_2^{(p)} + \delta_1) - (|V_2^{(p)}|)^2 |Y_{22}| \sin(\theta_{22}) - |V_2^{(p)}| |V_3^{(p)}| |Y_{23}| \sin(\theta_{23} - \delta_2^{(p)} + \delta_3^{(p)})$$

Now, if we want for iterative procedure right then Q 2 P plus 1 right then V 2 P right V 1 is a slack bus. So, no question of put in this one Y 2 1 in a constant sin theta 2 1 minus delta 2 P because bus 2 is a PQ bus delta 2 will also vary that is why it is P plus delta one is the slack bus angle otherwise it is a 0 actually right then minus V 2 P whole square right because it is V 2 square right and when this one this magnitude one these V 2 P square magnitude one actually no need to put P, because this is actually bus 2 is a Pv bus this voltage magnitude will remain constant. So, minus V 2 square rather right no P then magnitude Y 2 2 sin theta 2 2 minus again here also magnitude of V 2 will remain constant no need to put P right.

So, magnitude V_2 because V_p your bus 2 is a P_v bus. So, V_2 is fixed magnitude V_2 is constant. So, no need to put P right then into $V_3 P$ capital $Y_{23} \sin \theta_{23} - \delta_{23} P + \delta_{3p}$, but bus 2 that δ_{2p} you have to put it here and here because it all it is a P_v bus. So, δ is varying, but magnitude V_2 always constant. So, no need to put P right. So, this is your $Q_2 P$ plus; now Y matrix is a same as example one same Y matrix right; so no change.

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$$|Y_{21}| = 22.36, \quad \theta_{21} = 116.5^\circ$$

$$|Y_{22}| = 58.13, \quad \theta_{22} = -63.4^\circ$$

$$|Y_{23}| = 35.77, \quad \theta_{23} = 116.6^\circ$$

Iteration-1:

Set $p=0$

$$Q_2^{(1)} = -|V_2^{(0)}| |V_2^{(0)}| |Y_{21}| \sin \theta_{21}$$

$$- (|V_2^{(0)}|)^2 |Y_{22}| \sin \theta_{22}$$

$$- |V_2^{(0)}| |V_3^{(0)}| |Y_{23}| \sin \theta_{23}$$

$|V_1| = 1.05, \quad \delta_1 = 0$

So, in that case; so these are the Y matrix these magnitude an angle magnitude an angle magnitude an angle all Y_{21}, Y_{22}, Y_{23} . So, now iteration set P is equal to 0 look we are not computing at present any voltage anything only we are computing king power injection at bus 2 right.

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Iteration-1:

Set $p=0$

$$Q_2^{(1)} = -|V_2|^{(0)} |V_1| Y_{21} \sin(\theta_{21} - \delta_2^{(0)} + \delta_1)$$

$$- (|V_2|^{(0)})^2 Y_{22} \sin \theta_{22}$$

$$- |V_2|^{(0)} |V_3|^{(0)} Y_{23} \sin(\theta_{23} - \delta_2^{(0)} + \delta_3^{(0)})$$

$$|V_1| = 1.05, \delta_1 = 0.0^\circ$$

$$|V_2|^{(0)} = 1.0, \delta_2^{(0)} = 0.0^\circ$$

$$|V_3|^{(0)} = 1.0, \delta_3^{(0)} = 0.0^\circ$$

Therefore because after that we will see how will go for iterative process right. So, in this case that Q_2 when P is equal to 0, when P is equal to 0 here you write Q_2 . So, this is be this Q_2 this equation will be right that your magnitude your this one what you call here also magnitude V_2 this P also should not be there because magnitude voltage is this thing is your magnitude is constant.

So, here also this is not require, here also this is not require, here also this is not require actually right this is not require. So, and rest you are the way the they are your given δ_2 , δ_2 , δ_3 all are there. δ_1 anyway it is 0 angle right because it is slack bus and slack bus voltage also low question of iteration because it is fixed right. So, we with that you put Q_2 . So, V_1 is 1.05 angle δ_1 magnitude V_2 actually it cannot be 0, because it will magnitude will all are remain constant right and δ_2 is equal to 0.0 degree and V_3 is equal to 1.0 and δ_3 0.0. All these in substitute here you substitute here you substitute here right.

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$$Q_2^{(1)} = -1.0 \times 1.05 \times 22.36 \sin(116.6^\circ) - (1.0)^2 \times 58.13 \sin(-63.4^\circ) - 1.0 \times 1.0 \times 35.77 \sin(116.6^\circ)$$

$$\therefore Q_2^{(1)} = -1.0067 \text{ pu MVAR}$$

The value of $Q_2^{(1)}$ is taken as net reactive power injected at bus-2, i.e., $Q_2 = -1.0067 \text{ pu MVAR}$

Now compute

$$\Rightarrow V_{c2}^{(p+1)} = \frac{1}{Y_{22}} \left[\frac{P_2 - jQ_2^{(p+1)}}{(V_2^{(p)})^*} - Y_{21}V_1 - Y_{23}V_3^{(p)} \right]$$

If you do so, then what you will get? You will get $Q_2^{(1)}$ values put and simplified right you get compute $Q_2^{(1)}$ is minus 1.0067 power unit megawatt this is the value of $Q_2^{(1)}$ right. Now the value of $Q_2^{(1)}$ is taken as net reactive power injected at bus 2 right that is $Q_2 = Q_2^{(1)} = -1.0067$ will take right. So, first of your doing for Pv bus your trying first after your trying to compute that are Pv bus the reactive power injection right. So, that that for we will take that Q_2 is equal to this much as reactive power injection at bus 2, iteratively you have to obtained iteratively right.

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The value of $Q_2^{(1)}$ is taken as net reactive power injected at bus-2, i.e., $Q_2 = Q_2^{(1)} = -1.0067 \text{ pu MVAR}$

Now compute,

$$\Rightarrow V_{c2}^{(p+1)} = \frac{1}{Y_{22}} \left[\frac{P_2 - jQ_2^{(p+1)}}{(V_2^{(p)})^*} - Y_{21}V_1 - Y_{23}V_3^{(p)} \right]$$

$$\Rightarrow V_{c2}^{(1)} = \frac{1}{Y_{22}} \left[\frac{P_2 - jQ_2^{(1)}}{(V_2^{(0)})^*} - Y_{21}V_1 - Y_{23}V_3^{(0)} \right]$$

So, Q_2 is equal to Q_{21} that is a Q_2 value in the very fast iteration right I hope you are understanding this right, once it is done then instead of writing equation V_{21} will writing $V_{c2} P_{21}$, because this is not the correct value of the your what you call bus 2 because bus 2 is a Pv bus and its voltage values is one, but using this equation it will never be magnitude will never be one right.

So, but same equation variety $1 \text{ upon } Y_{22} P_2 - jQ_2$, instead of Q_2 I writing $Q_2 P_{21}$ plus 1 because that $Q_2 P_{21}$ plus 1 that equation your what you to call that this you have opted iteratively. So, this $Q_2 P_{21}$ plus 1, this is $Q_2 P_{21}$ plus 1 right. So, you have put in minus $jQ_2 P_{21}$ upon V_{21} conjugate minus same as before Y_{22} and V_1 minus $Y_{23} V_3$ P right that mean this is V_{c2} not just making V_{c2} . So, in P is equal to 0 and P is equal to 0 that V_{c2} 1, is equal to 1 upon $Y_{22} P_2 - jQ_2$, Q_2 1 is already computed here Q_2 1 is already computed here right here it is, here it is and P 2 already earlier your made it generate injected power at bus 2 those that are known right minus $Y_{21} V_1$ minus $Y_{23} V_3$ 0 this is the thing.

Now, same as before you compute $P_2 - jQ_2$ multiply this whole thing by $1 \text{ upon } Y_{22}$; so you have to compute $P_2 - jQ_2$ upon Y_{22} minus Y_{21} upon Y_{22} minus Y_{23} upon Y_{22} right. So, if you do so, then P_2 minus P_2 are minus 2.556 and Q_2 are just Q_2 1 was just minus 1.0067 here computed. So, substitute all divided by Y_{22} you will get 0.04725 angle 221.9 degree.

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Now,

$$\frac{P_2 - jQ_2}{Y_{22}} = \frac{-2.556 + j1.0067}{58.43 \angle -63.4^\circ} = 0.04725 \angle 221.9^\circ$$

$$\frac{Y_{21}}{Y_{22}} = -0.3846; \quad \frac{Y_{23}}{Y_{22}} = -0.6153$$

$$\therefore V_{c2}^{(1)} = \left[\frac{0.04725 \angle 221.9^\circ}{(V_2^{(0)})^*} + 0.3846 V_1 + 0.6153 V_3^{(0)} \right]$$

$$\therefore V_{c2}^{(1)} = \frac{0.04725 \angle 221.9^\circ}{1.0} + 0.3846 \times 1.05$$

And next capital Y 2 1 upon capital Y 2 2 earlier we have got it that is minus 0.3846 similarly capital Y 2 3 upon capital Y 2 2 earlier we have got it minus 0.6159 with these this equation $V_{c2}^{(1)}$ that mean this equation that is this equation this equation will become your $0.04725 \angle 221.9^\circ$ divided by $V_2^{(0)}$ conjugate plus $0.3846 V_1$ plus $0.6153 V_3$ right.

So, with this all $V_2^{(0)}$ known V_1 known $V_3^{(0)}$ known everything is known then you substitute all and then it then you simplify you can compute. It is coming $V_{c2}^{(1)}$ 0.98396 minus $j 0.03155$ if you take its magnitude it is never one right, but you have to make it one.

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The image shows a handwritten derivation on a light blue background. It starts with the equation for $V_{c2}^{(1)}$ as a sum of three terms in brackets, divided by the conjugate of $V_2^{(0)}$. The first term is $0.04725 \angle 221.9^\circ$. The second term is $0.3846 V_1$ and the third is $0.6153 V_3^{(0)}$. Below this, the terms are simplified: the denominator is 1.0 , the first term is $0.04725 \angle 221.9^\circ$, the second is 0.3846×1.05 , and the third is 0.6153×1.0 . The final result is $V_{c2}^{(1)} = (0.98396 - j0.03155)$. A note at the bottom states: "Since $|V_2|$ is held constant at 1.0 pu, only the imaginary part of $V_{c2}^{(1)}$ is retained, i.e."

$$\therefore V_{c2}^{(1)} = \left[\frac{0.04725 \angle 221.9^\circ}{(V_2^{(0)})^*} + 0.3846 V_1 + 0.6153 V_3^{(0)} \right]$$

$$\therefore V_{c2}^{(1)} = \frac{0.04725 \angle 221.9^\circ}{1.0} + 0.3846 \times 1.05 + 0.6153 \times 1.0$$

$$\Rightarrow V_{c2}^{(1)} = (0.98396 - j0.03155)$$

Since $|V_2|$ is held constant at 1.0 pu, only the imaginary part of $V_{c2}^{(1)}$ is retained, i.e.,

So, what we will do Pv bus consideration in Gauss-Seidel method. What you will do since V_2 is held constant at 1.0 per unit right only the imaginary part of $V_{c2}^{(1)}$ is retained; that means, what we will do.

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$$f_2^{(1)} = -0.03155 \text{ and its real part is obtained from,}$$
$$e_2^{(1)} = \sqrt{|V_2|^2 - (0.03155)^2}$$
$$\therefore e_2^{(1)} = \sqrt{(1.0)^2 - (0.03155)^2}$$
$$\therefore e_2^{(1)} = 0.9995$$

Thus,

$$\Rightarrow V_2^{(1)} = (0.9995 - j0.03155)$$

That imaginary part whatever you have got it using that Q 2 V your considering that Q 2 injection that imaginary part will retained, but this one will compute this one will find out how will do this.

(Refer Slide Time: 19:35)

$$V_2 = e_2 + jf_2$$
$$\therefore |V_2| = \sqrt{e_2^2 + f_2^2}$$
$$\therefore e_2^2 + f_2^2 = |V_2|^2$$
$$\therefore e_2 = \left(|V_2|^2 - f_2^2 \right)^{1/2}$$

Now; that means, imaginary part we will take f_2 is equal to because your V_2 actually V_2 is equal to your say $e_2 + jf_2$ right this your taking. That means, your magnitude of V_2 is equal to root over e_2 square plus f_2 square; that means, other way you can write e_2 square plus f_2 square is equal to magnitude of V_2 square right; that means, e_2

is equal to your magnitude V_2 square minus your f_2 square to the power half right whatever value comes.

.So, what same thing where doing it here that your f_2 is here we got minus 0.03155. So, this is my f_2 right this is my f_2 . So, and its real part is obtain from these equation e 2 1 just now I wrote now V_2 square minus f_2 square to the power half, same thing that your V_2 square root over V_2 square minus f_2 square here actually in bracket one it although it will be positive one minus sign is there before here it is minus because here it is minus. So, 1 minus is there right.

So that means, your this one, but V_2 will be here constant at one. So, this one we have kept fix right minus your here also minus is missed. So, this is also your minus right.

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Handwritten mathematical derivation on a blue background:

$$\therefore e_2 = \sqrt{(1.0)^2 - (0.03155)^2}$$

$$\therefore e_2^{(1)} = 0.9995$$

Thus,

$$\Rightarrow V_2^{(1)} = (0.9995 - j0.03155)$$

$$\therefore V_2^{(1)} = 1.0 \angle -1.807^\circ$$

Now,

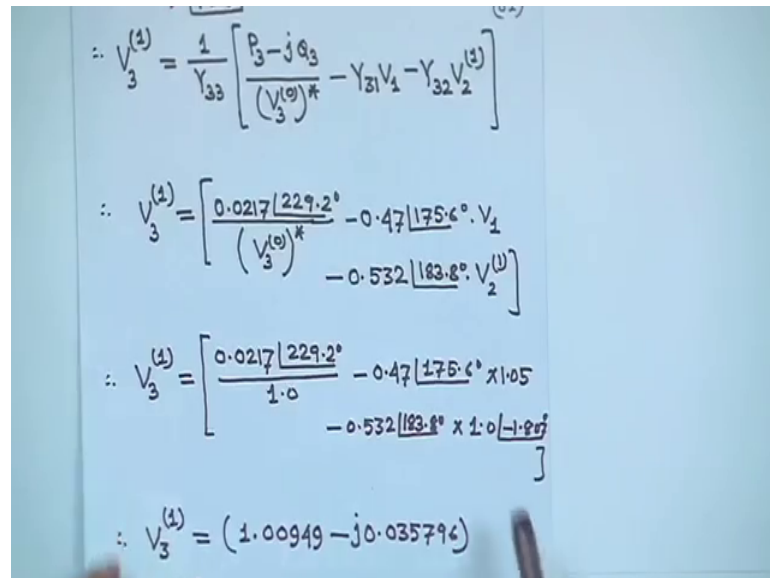
$$V_3^{(k+1)} = \frac{1}{Y_{33}} \left[\frac{P_3 - jQ_3}{(V_3^{(k)})^*} - Y_{31}V_1 - Y_{32}V_2^{(k+1)} \right]$$

So; that means, it will become e 2 1 that is 0.9995, then you will take V_2 1 actually 0.9 triple 95 minus j this 1, this will give you magnitude one because based on that only got this e right and it a angle is be minus 1.807 degree that mean this one this one using Q 2 injection that is we got 0.98396 and minus j 0.0315, but corrected value we corrected right.

By considering this approach considering this approach such that be your this one magnitude if you take it will become one now an angle will be minus 1.807 degree, that mean this V_2 in first iteration magnitude is fixed because Pv bus, but angle you have got

it right. So, similarly your, but the bus 3 is your PQ bus, bus 3 is a PQ bus. So, in that case this same equation same way you can write this equation $V_3^{(1)}$ plus 1 upon Y_{33} capital Y_{33} , P_3 minus jQ_3 upon $V_3^{(0)}$ conjugate minus capital Y_{31} , V_1 minus capital Y_{32} $V_2^{(0)}$ plus 1 because V_2 already computed; so I writing $V_2^{(0)}$ plus 1 not $V_2^{(1)}$ right.

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$$\therefore V_3^{(1)} = \frac{1}{Y_{33}} \left[\frac{P_3 - jQ_3}{(V_3^{(0)})^*} - Y_{31}V_1 - Y_{32}V_2^{(0)} \right]$$

$$\therefore V_3^{(1)} = \left[\frac{0.0217 \angle 229.2^\circ}{(V_3^{(0)})^*} - 0.47 \angle 175.6^\circ \cdot V_1 - 0.532 \angle 183.8^\circ \cdot V_2^{(0)} \right]$$

$$\therefore V_3^{(1)} = \left[\frac{0.0217 \angle 229.2^\circ}{1.0} - 0.47 \angle 175.6^\circ \times 1.05 - 0.532 \angle 183.8^\circ \times 1.0 \angle -1.8^\circ \right]$$

$$\therefore V_3^{(1)} = (1.00949 - j0.035794)$$

So, if these with these with P is equal to 0 the first iteration $V_3^{(1)}$, all these thing are there this is the equation right. So, P there minus jQ_3 upon $V_3^{(0)}$ already you have computed before it is same here right and this one also same this one also same right. So, if that put all these values all these value for being the equation of V_3 all these values. So, you will get $V_3^{(1)}$ is equal to 1.0101 angle minus 2.03 degree V_3 is a PQ bus. So, no question of this thing directly or getting.

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$$\therefore V_3^{(1)} = \left[\frac{-0.47 \angle 175.6^\circ \times 1.05}{1.0} \right]$$

$$\therefore V_3^{(1)} = (1.00949 - j0.035796)$$

$$\therefore V_3^{(4)} = 1.0101 \angle -2.03^\circ$$

After 1st Iteration

$$V_2^{(1)} = 1.0 \angle -1.807^\circ$$

$$V_3^{(4)} = 1.0101 \angle -2.03^\circ$$

So, after first iteration you got V_2 1 is equal to magnitude remain constant because Pv bus right angle minus 1.807 degree and V_3 1 is 1.0101 angle minus 2.03 degree right.

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$$\rightarrow \text{Set } p=1 \tag{62}$$

$$\Rightarrow Q_2^{(2)} = -|V_2||V_1||Y_{21}| \sin(\theta_{21} - \delta_2^{(1)} + \delta_1) - (|V_2|)^2 |Y_{22}| \sin \theta_{22} - |V_2||V_3||Y_{23}| \sin(\theta_{23} - \delta_2^{(1)} + \delta_3^{(1)})$$

$$\rightarrow \delta_1 = 0.0^\circ, \delta_2^{(1)} = -1.807^\circ, \delta_3^{(1)} = -2.03^\circ$$

$$\rightarrow |V_1| = 1.05, |V_2| = 1.0, |V_3| = 1.0101$$

$$\Rightarrow \therefore Q_2^{(2)} = -1 \times 1.05 \times 22.36 \sin(116.58^\circ + 1.807^\circ)$$

This is after first iteration, now at list what you have to do is now again you have to compute Q_2 for the second iteration you have to find out again and you have to go for the correction to the real part of that Pv bus voltage magnitude right real part of the Pv bus voltage. So, if similarly set P is equal to 1 then this Q_2 2 will be the same equation will come right.

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$$\begin{aligned} &\rightarrow \delta_1 = 0.0^\circ, \delta_2^{(1)} = -1.807^\circ, \delta_3^{(1)} = -2.03^\circ \\ &\rightarrow |V_1| = 1.05, |V_2| = 1.0, |V_3^{(1)}| = 1.0101 \\ &\Rightarrow \therefore Q_2^{(2)} = -1 \times 1.05 \times 22.36 \sin(116.56^\circ + 1.807^\circ) \\ &\quad - (1.0)^2 \times 58.13 \sin(-63.4^\circ) \\ &\quad - 1.0 \times 1.0101 \times 35.77 \sin(116.6^\circ + 1.807^\circ - 2.03^\circ) \\ &\Rightarrow \therefore Q_2^{(2)} = -1.0507 \text{ pu} \end{aligned}$$

And all the units all the values are delta 1 is 0, delta 2 1 is computed this much minus 1.807 degree delta 3 1 minus 2.03 degree magnitude V 1 is 1.05, magnitude V 2 all is constant 1 and magnitude V 3 in first iteration 1.0101 per unit right.

So, all these values all these values you substitute here you substitute here right. If you do so, then you will get after calculation Q 2 2 will be minus 1.0507 per unit right

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$$\begin{aligned} &\Rightarrow \therefore V_{c2}^{(2)} = \left[\frac{0.04725 | 221.9^\circ}{(V_2^{(1)})^*} + 0.3846 V_1 \right] + 0.6153 V_3^{(1)} \\ &\therefore V_{c2}^{(2)} = \frac{0.04725 | 221.9^\circ}{1 | -1.807^\circ} + 0.3846 \times 1.05 \\ &\quad + 0.6153 \times 1.0101 | -2.03^\circ \\ &\Rightarrow \therefore V_{c2}^{(2)} = (0.9888 - j0.05244) = e_2^{(2)} + j f_2^{(2)} \\ &\text{Now, } f_2^{(2)} = -0.05244 \\ &\therefore |V_{c2}^{(2)}| = \sqrt{(0.9888)^2 + (-0.05244)^2} = 0.9986 \end{aligned}$$

This Q 2 will get and the once you get these in same way you calculate your that your what you call that Vc took a Vc 2 computation right . So, you will you will get that Vc 2

in the second iteration will be in this form same thing, again you make it this is constant this is constant and you will find with that values of Q this is more or less same right this 0.04725 all most same right.

So, when you all the initial value all the values are known to you. So, you substitute all the values right.

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Handwritten mathematical derivation on a piece of paper:

$$\Rightarrow \therefore V_{c2}^{(2)} = (0.9986 - j0.05244) = e_2^{(2)} + j f_2^{(2)}$$

Now,

$$f_2^{(2)} = -0.05244$$

$$\therefore e_2^{(2)} = \sqrt{1.0^2 - (-0.05244)^2} = 0.9986$$

$$\therefore V_2^{(2)} = (0.9986 - j0.05244)$$

$$\Rightarrow \therefore V_2^{(2)} = 1 \angle -3^\circ$$

So, in that case what will get $V_{c2}^{(2)}$ in the second iteration, 0.9986 minus j 0.05244 this one we can write $e_2^{(2)}$ in the second iteration real part plus j in an real part $f_2^{(2)}$ in the second iteration. Now $f_2^{(2)}$ here written in this is your taking minus 0.05244, but $e_2^{(2)}$ because voltage magnitude and bus 2 has to be will constant. So, it is one. So, $e_2^{(2)}$ is root over 1.0 square minus this minus 0.05244 whole square that is coming 0.9986 right; that means, $V_2^{(2)}$ actually 0.9986 minus this one. All though all though with are key reactive power injection it was coming like this, but it is corrected right and now it is not 0.9986 and minus j 0.05244.

So, $V_2^{(2)}$ actually one angle minus 3 degree magnitude is fixed again, but all the angle is baring right.

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$$(64)$$

$$\Rightarrow V_3^{(2)} = \left[\begin{array}{l} \frac{0.0217 \angle 229.2^\circ}{(V_3^{(2)})^*} - 0.47 \angle 175.6^\circ V_2 \\ -0.532 \angle 183.8^\circ V_2^{(2)} \end{array} \right]$$

$$\Rightarrow V_3^{(2)} = \left[\begin{array}{l} \frac{0.0217 \angle 229.2^\circ}{1.0101 \angle 2.03^\circ} - 0.47 \angle 175.6^\circ \times 1.05 \\ -0.532 \angle 183.8^\circ \times 1 \angle -3^\circ \end{array} \right]$$

$$\Rightarrow \therefore V_3^{(2)} = (1.0093 - j0.04619)$$

$$\Rightarrow \therefore V_3^{(2)} = 1.0103 \angle -2.62^\circ$$

Similar way right similar way that V 3 2 you can compute again you compute all these values this will remain constant, this are also constant we already computed only this values we have to substitute right therefore, V 3 2 you will get in a V 2 3 is second iteration right you put it you will get it is 1.0093 minus j 0.04619.

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$$\Rightarrow \therefore V_3^{(2)} = (1.0093 - j0.04619)$$

$$\Rightarrow \therefore V_3^{(2)} = 1.0103 \angle -2.62^\circ$$

After 2nd Iteration

$$V_2^{(2)} = 1.0 \angle -3^\circ$$

$$V_3^{(2)} = 1.0103 \angle -2.62^\circ$$

So, V 3 2 is 1.0103 angle minus 2.6 degree. So, after second iteration that V 2 and V 3 in the second iteration its 1 V 2 magnitude fixed one angle 0 minus 3 degree and this one

1.0103 angle minus 2.6 this is the result after second iteration actually I have done it up to second iteration right.

So, this is your what you call that Gauss-Seidel method that have one can use Gauss-Seidel method a solving load flow studies right. So, only thing is that in Gauss-Seidel method that number it takes more number of iteration because convergence characteristic actually is a linear right. If time permits at the end if time permits then I can show you the proof that convergence characteristic of Gauss-Seidel linear and Newton-Raphson its a quadratic if time permits there not at the end of this topic, but at the end right if I find one hour extra time there I can show you the proof right.

So, question is that in whatever to examples we have seen it is a 3 bus problem only right and with that also you have seen the huge computations are required right. [I am giving you lecture. So, making all these things, but a when you will calculate it, it will take more time right. So, this is one thing and you have took make all the calculations correctly and all these angles 175, 175 183 or 229 all these angles when you are making it be is check carefully which coordinative are. Accordingly you take the angles sometime calculator you will take something calculator making different angle may be this way.

So, you have to see that which coordinate this thing are an accordingly you take the take the angle the accordingly I have taken right otherwise you make otherwise there is a possibility of you know mistake right. So, be careful about that and all the calculations Y matrix other thing and charging admittance are not considered right, but your what you call this, but you have got they your what you call got some ideas, that how to solve load flows using in Gauss-Seidel method for considering you have in bar a buses are PQ bus or buses and bus another thing is the Pv bus right.

So, but a these are the thing, but different buses are consideration of Pv buses are there in the literature for Gauss-Seidel method, but I have given you this bus an because I found this bus an is quite is easier right with next we will take Newton-Raphson method little break.

Thank you.