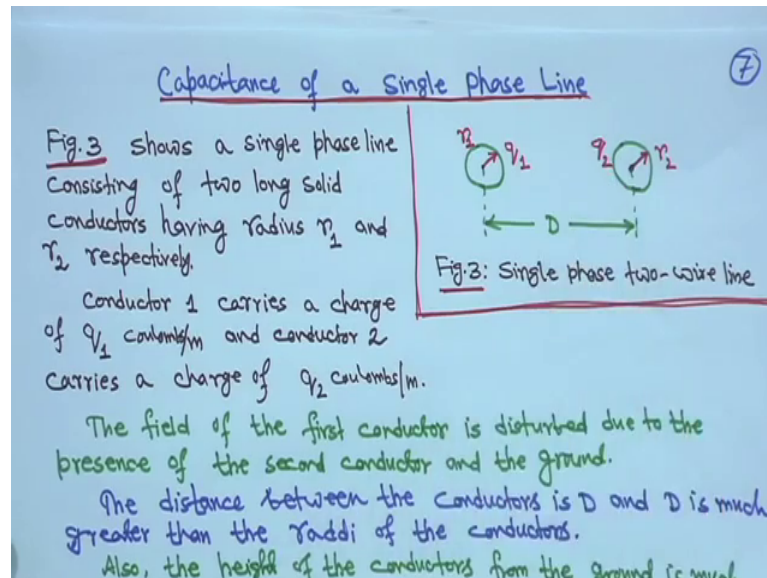


Power System Analysis
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Lecture - 12
Capacitance of Transmission Lines

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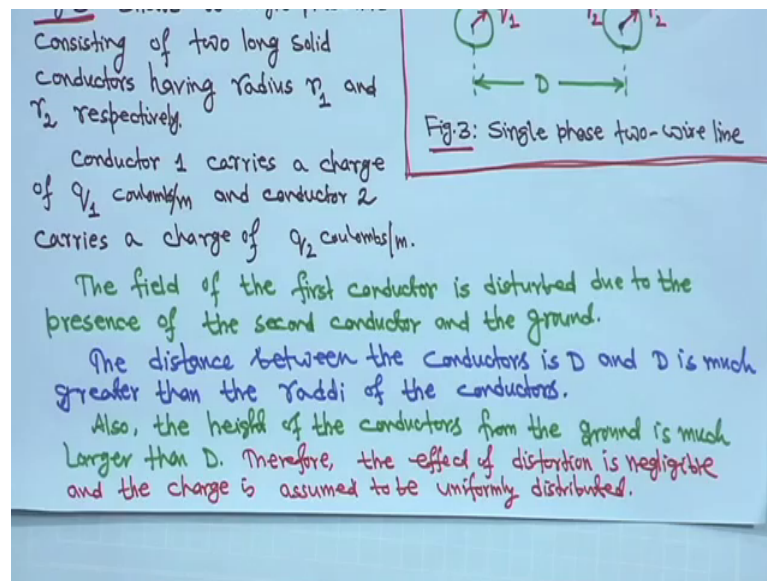
So, next is the capacitance of a single phase line right now look at this figure you have 2 conductors listen one thing for the capacitance case there is no question of r dash right like inductance. So, this should be in your mind. So, now, you consider a single phase line this is there are 2 conductors this is q_1 and q_2 the charge is q_1 q_2 and if q_1 is equal to q is a positive charge then q_2 will be your minus q right. So, later we will see.

Now, the radius of this conductor is r_1 right the radius of this conductor is r_2 we have initially we have taken that what you call radius of 2 conductors are different and center to center distance is D right center to center and of course, D is much much larger than r_1 and r_2 right. So, this is single phase 2 wire line right. So, conductor one carries a charge of q_1 coulomb I told you per meter and conductor 2 carries a charge of q_2 coulomb per meter right the field of the first conductor is disturbed due to presence of the second conductor and the ground right.

So, basically if you take now you are considering single phase dual line naturally field of this one will be disturbed by this one as well as by the ground; we will see later right. So,

the distance between the conductor is D and D is much much greater than the radius of the 2 conductors r_1 and r_2 right also the height of the conductor from the ground is much larger than D because conductors are always above the ground right. So, that height h is much much greater than D , but when you will consider h that we will see later.

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So, therefore, the effect of distortion is negligible and charge is assumed to be uniformly distributed. So, we are assuming that the effect of distortion is negligible and the charge is assumed to be uniformly distributed right.

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The potential difference V_{12} can be obtained in terms of q_1 and q_2 by using eqn. (5). Thus,

$$V_{12} = \frac{1}{2\pi\epsilon_0} \sum_{m=1}^2 q_m \ln\left(\frac{D_{2m}}{D_{1m}}\right) \text{ volt}$$

$$\therefore V_{12} = \frac{1}{2\pi\epsilon_0} \left[q_1 \ln\left(\frac{D_{21}}{D_{11}}\right) + q_2 \ln\left(\frac{D_{22}}{D_{12}}\right) \right] \text{ volt}$$

Since, $q_2 = -q_1$, $D_{21} = D_{12} = D$, $D_{11} = r_1$ and $D_{22} = r_2$

$$\therefore V_{12} = \frac{1}{2\pi\epsilon_0} \left[q_1 \ln\left(\frac{D}{r_1}\right) - q_1 \ln\left(\frac{r_2}{D}\right) \right] \text{ volt}$$

$$\therefore V_{12} = \frac{2q_1}{2\pi\epsilon_0} \cdot \ln\left(\frac{D}{\sqrt{r_1 r_2}}\right) \text{ volt}$$

The potential difference V_{12} can be obtained in terms of q_1 and q_2 using equation 5 that general equation we have given m is equal to 1 to n . So, the same equation for 1 to 2 you are using 1 upon $2\pi\epsilon_0$ 2 conductors are there m is equal to 1 to 2 this is $q_m \ln \frac{D_{2m}}{D_{1m}}$ right volt right.

So, this expression this expression just now we given no this expression $\frac{D_{21}}{D_{11}}$ upon $\frac{D_{22}}{D_{12}}$ right. So, D_{21} is equal to D and your D_{11} is equal to r_1 right. So, therefore, the m is equal to 1 to 2. Now V_{12} is equal to $\frac{1}{2\pi\epsilon_0}$ then $q_1 \ln \frac{D_{21}}{D_{11}}$ plus $q_2 \ln \frac{D_{22}}{D_{12}}$ volt now since q_2 is equal to minus q_1 and D_{21} equal to D_{12} actually 2 conductors are there conductor 1 and conductor 2. So, that is why D_{21} and D_{12} ; that means, this is here to here 1 to 2 1 basically this distance is D , but this is a generalized formula after that we are replacing this right and D_{11} I told you that if k is equal to m or k is equal to m then D_{mm} is equal to r .

So, when D_{11} is equal to r_1 and D_{22} is equal to r_2 right therefore, V_{12} is equal to $\frac{1}{2\pi\epsilon_0} q_1 \ln \frac{D}{r_1}$ minus $q_1 \ln \frac{r_2}{D}$ upon D because q_2 is equal to minus q_1 that is why minus $q_1 \ln \frac{r_2}{D}$ upon D volt right. Therefore, V_{12} is equal to $2q_1$ upon $2\pi\epsilon_0$ $\ln \frac{D}{\sqrt{r_1 r_2}}$ because if you if this is k if you take q_1 common and it will be basically plus $\ln \frac{D}{r_2}$ because it is minus $\ln \frac{r_2}{D}$ upon D it will be D upon r_2 . So, that your after that you simplify this it will be $\frac{D}{\sqrt{r_1 r_2}}$

upon $2\pi\epsilon_0 \ln \frac{D}{r_1 r_2}$ upon $\sqrt{r_1 r_2}$ I mean these things are simple just for your clarification just writing one line.

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$$\begin{aligned}
 V_{12} &= \frac{1}{2\pi\epsilon_0} \left[q_1 \ln\left(\frac{D}{r_1}\right) - q_1 \ln\left(\frac{D}{r_2}\right) \right] \\
 &= \frac{q_1}{2\pi\epsilon_0} \left[\ln\left(\frac{D}{r_1}\right) + \ln\left(\frac{r_2}{D}\right) \right] \\
 &= \frac{q_1}{2\pi\epsilon_0} \ln\left(\frac{D^2}{r_1 r_2}\right) \\
 &= \frac{q_1}{2\pi\epsilon_0} \ln\left\{ \frac{D}{\sqrt{r_1 r_2}} \right\}^2 \\
 &= \frac{2q_1}{2\pi\epsilon_0} \ln\left(\frac{D}{\sqrt{r_1 r_2}}\right)
 \end{aligned}$$

So, V_{12} is equal to $\frac{1}{2\pi\epsilon_0} \ln \frac{D}{r_1 r_2}$ upon $\sqrt{r_1 r_2}$ right minus it is written $q_1 \ln \frac{D}{r_2}$ upon D right therefore, this is equal to $\frac{1}{2\pi\epsilon_0}$ you sorry you take q_1 common right this is $\ln \frac{D}{r_1} + \ln \frac{r_2}{D}$ that is equal to $\frac{q_1}{2\pi\epsilon_0} \ln \frac{D^2}{r_1 r_2}$ right this one. You can write $\frac{q_1}{2\pi\epsilon_0} \ln \frac{D^2}{r_1 r_2}$ then you can write D root over $r_1 r_2$ right this square this is square is equal to $2q_1$ it is q_1 actually it is no you are putting your this thing it is q_1 . So, it is q_1 then $2q_1$ upon $2\pi\epsilon_0 \ln \frac{D}{\sqrt{r_1 r_2}}$ right. So, that is the simplification.

So, that is why we were writing here this one is your what you call $\frac{2q_1}{2\pi\epsilon_0 \ln \frac{D}{\sqrt{r_1 r_2}}}$ volt right; that means, therefore, our objective is that you have to find out capacitance between the 2 lines C_{12} .

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$$\therefore C_{12} = \frac{q_1}{V_{12}} = \frac{\pi \epsilon_0}{\ln\left(\frac{D}{\sqrt{r_1 r_2}}\right)} \text{ F/m} \quad \dots(7)$$

If $r_1 = r_2 = r$

$$\therefore C_{12} = \frac{\pi \epsilon_0}{\ln\left(\frac{D}{r}\right)} \text{ F/m} \quad \dots(8)$$
$$\therefore C_{12} = \frac{0.0121}{\log\left(\frac{D}{r}\right)} \mu\text{F/km} \quad \dots(9)$$

Eqn. (9) gives the line-to-line capacitance between the conductors. For the purpose of transmission line modeling, it is convenient to define capacitance between each conductor and a neutral as shown in Fig. 4.

Therefore this C_{12} is equal to it is q_1 upon you know q is equal to $C V$ in general therefore, C is equal to q by V therefore, C_{12} is equal to q_1 upon V_{12} is equal to $\pi \epsilon_0$ upon \ln because this; this $2/2$ will be cancelled right $2/2$ will be cancelled I did not make it here, but this 2 will be cancel right. So, therefore, C_{12} is equal to q_1 upon V_{12} is equal to $\pi \epsilon_0$ upon $\ln D$ under root $r_1 r_2$ farad per meter this is equation seven right therefore, if both the conductors' radius same then r_1 is equal to r_2 is equal to r therefore, C_{12} is equal to $\pi \epsilon_0$ \ln divided by $\ln D$ farad per meter this is equation eight right.

So, ϵ_0 you know 8.854×10^{-12} farad per meter this is known right and this is this is your natural log, but you convert you convert it to this log right. So, this conversion is up to you right. So, this simple thing you can do it. So, generally for all the numerical this that we will use log of this thing right not the natural log right because many things easy to remember therefore, C_{12} is equal to if you simplify it will be 0.0121 divided by $\log D$ upon r microfarad per kilometer right. So, this is equation 9 right. So, this is the capacitance. So, this equation 9 actually it gives the line to line capacitance between the conductors right, but for the purpose of transmission line modeling it is convenient define the capacitance between each conductor and the neutral as shown in figure 4.

So, this is line to line your line to line capacitance, but in between line 1 and 2 if you have a neutral then you have to find out that capacitance from each conductor to neutral that is C_{1n} and C_{2n} .

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Since the potential difference to neutral is half of V_{12} , therefore,

$$C_{1n} = C_{2n} = 2C_{12}$$

or

$$C_{1n} = C_{2n} = \frac{0.0242}{\log\left(\frac{D}{r}\right)} \mu\text{F/km} \quad \text{--- (10)}$$

The associated line charging current is:

$$I_c = j\omega C_{12} V_{12} \text{ Amp/km} \quad \text{--- (11)}$$

Fig.4: (a) line-to-line capacitance
(b) Line-to-neutral capacitance

So; that means, if you come to this come to this part when 1 to 2 this is C_{12} that is whatever you got whatever you have got C_{12} is this one right equation 9; now if you have a neutral in between this is a neutral n right. So, this side 1 to n this is the C_{1n} and this is C_{2n} right and these 2 are in series right this is conductor 1 this is conductor 2 right. Therefore, C_{1n} is equal to C_{2n} is equal to $2C_{12}$ because they are in series. So, C_{1n} is equal to C_{2n} is equal to $2C_{12}$; that means, C_{1n} is equal to C_{2n} is equal to this will be multiplied by 2 right; that means, it will be 0.0242 divided by $\log D$ by r microfarad per kilometer this is equation 10 right.

Now, the associate line charging current will be I_c is equal to $j\omega C_{12} V_{12}$ ampere per kilometer right. So, it will be if you think like this something like this that if you try to find out the reactance say I put X_{12} say X_{12} your what you this thing your generally you know that X is equal to 1 upon ωC right.

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$$X_{12} = \frac{1}{j\omega C_{12}}$$
$$X_{12} = \frac{j}{\omega C_{12}}$$
$$I_c = \frac{V_{12}}{X_{12}} = j\omega C_{12} V_{12}$$

Therefore if I make it X_{12} is ω by C_{12} right. So, this is that reactance therefore, when you try to find out the charging current say I_c say I_c right is equal to in general I am putting. So, voltage is V_{12} divided by your X_{12} is equal to your ωC_{12} into V_{12} , but as it is a as it is a capacitance right. So, this; what you call then you instead of magnitude here you put j here you put j therefore, it will be j therefore, right. So, that is why that is why this line charging current will be I_c will be equal to $j\omega C_{12}$ into your V_{12} ampere per kilometer, but you take the magnitude then j should not be there if the magnitude is taken right.

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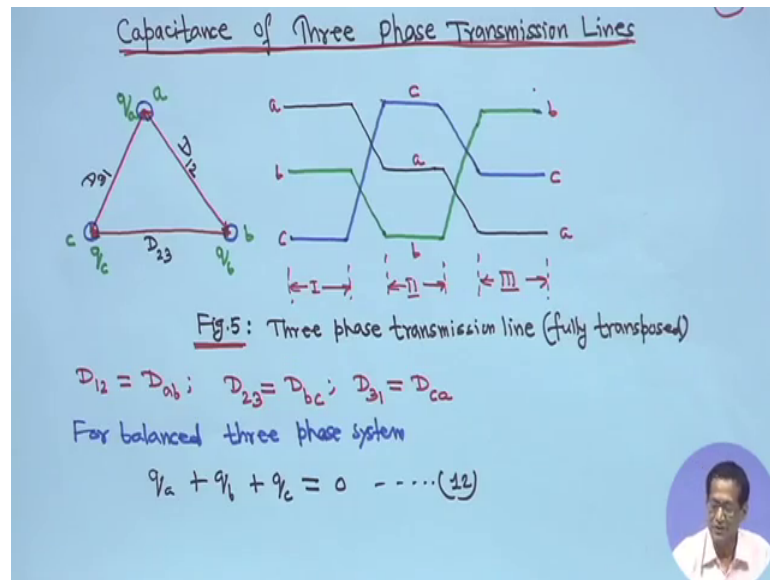
$$X_{12} = \frac{j}{\omega C_{12}}$$
$$I_c = \frac{V_{12}}{X_{12}} = j\omega C_{12} V_{12}$$
$$I_c = \omega C_{12} V_{12} \text{ (900 Amp/km)}$$

charging current is:

$$I_c = j\omega C_{12} V_{12} \text{ Amp/km} \text{ ---(11)}$$

So, it is a leading current it is a leading current right so; that means, this one, this one; one more line I am writing for you; that means, this one will be I charging current will be $\omega C \cdot 12 \cdot V \cdot 12 \text{ angle your ninety degrees because } j \text{ is there. So, this ampere per kilometer right therefore, this is this is your general thing.}$

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Next is capacitance of a 3 phase transmission line right. So, for transposition no need to explain here now because already for inductance case we have explained that transposition of transmission line right. So, you assume your 3 phase transmission line right and this capacitance of 3 phase transmission line and lines are transposed. So, this is phase a phase sorry phase a phase b and phase C right distance between a to your a to your C actually D 3 1; that means, D a c actually D 3 1 I have not written it, but I am telling from my mouth. So, you too know it right.

Similarly, D a b actually is equal to D 12 right and similarly D b c actually D 23 capital right not making it here, but at the time of derivation we will see if. So, you want you can make it, but D a b is literally D 12 D a c is equal to a b b c c a. So, D b c will be D 23 and D c a will be D 31 right. So, this is the line transpose. So, first section; section 1, it is a b c, next section it will be c a b that is section 2 and third section it will be b c a in the third section. So, this already we have seen for the inductor right. So, 3 phase transmission line this is figure 5 fully transposed, but here I have written here D 12 D a V D 23 D b c and D c a is equal to D 31 now for balance 3 phase system $q_a + q_b + q_c = 0$

C is equal to 0 this is equation 12 right like your current I a plus I b plus I c is equal to 0 right assuming no neutral right. So, next is we will apply the same formula right.

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Potential difference between phase a and b for the first transposition cycle can be obtained by applying eqn (5), $V_{ab}(I)$ is: (12)

$$V_{ab}(I) = \frac{1}{2\pi\epsilon_0} \left[q_a \ln\left(\frac{D_{12}}{r}\right) + q_b \ln\left(\frac{r}{D_{12}}\right) + q_c \ln\left(\frac{D_{23}}{D_{31}}\right) \right] \dots (13)$$

Similarly, for the 2nd transposition cycle

$$V_{ab}(II) = \frac{1}{2\pi\epsilon_0} \left[q_a \ln\left(\frac{D_{23}}{r}\right) + q_b \ln\left(\frac{r}{D_{23}}\right) + q_c \ln\left(\frac{D_{31}}{D_{12}}\right) \right] \dots (14)$$

For the third transposition cycle,

$$V_{ab}(III) = \frac{1}{2\pi\epsilon_0} \left[q_a \ln\left(\frac{D_{31}}{r}\right) + q_b \ln\left(\frac{r}{D_{31}}\right) + q_c \ln\left(\frac{D_{12}}{D_{23}}\right) \right] \dots (15)$$

So, potential difference between phase a and b for the first transposition cycle I mean for the first one for the first transposition that is section 1 section 2 section 3. First we will see the first one here right so; that means, can we obtain by applying equation 5 the same equation again we will use the generalized equation therefore, V_{ab} in bracket I means it is not current it is section 1 right V_{ab} bracket; that means, for the this section 1 this section 1 right is equal to $\frac{1}{2\pi\epsilon_0} [q_a \ln\left(\frac{D_{12}}{r}\right) + q_b \ln\left(\frac{r}{D_{12}}\right) + q_c \ln\left(\frac{D_{23}}{D_{31}}\right)]$ this is equation thirteen, but same equation 5; the generalized equation we are applying for for inductance also we for cross linkage we applied 1 generalized equation for capacitance for voltages also the same equation we are putting in this form right.

That means $q_a \ln\left(\frac{D_{12}}{r}\right) + q_b \ln\left(\frac{r}{D_{12}}\right) + q_c \ln\left(\frac{D_{23}}{D_{31}}\right)$; that means, $q_c \ln\left(\frac{D_{23}}{D_{31}}\right)$; that means, $q_c \ln\left(\frac{D_{23}}{D_{31}}\right)$ that is $q_c \ln\left(\frac{D_{23}}{D_{31}}\right)$ right because V_{ab} your a b right due to further section 1. So, this is that configuration of section 1 this triangular configuration for this one and this one you can draw right for inductance case we have shown it. So, no need right therefore, your this one will be $\frac{1}{2\pi\epsilon_0} [q_a \ln\left(\frac{D_{12}}{r}\right) + q_b \ln\left(\frac{r}{D_{12}}\right) + q_c \ln\left(\frac{D_{23}}{D_{31}}\right)]$ is nothing, but D_{ab} upon r right then q_b this $q_b \ln\left(\frac{r}{D_{12}}\right)$ right plus q_c this is the $q_c \ln\left(\frac{D_{23}}{D_{31}}\right)$ right b that because you want to find out

the potential that is your V_a to b right if you recall voltage 1 to 2 D_2 upon D_1 that very first diagram that C_{12} calculation V_{12} calculation. So, if you think that way; that means, it is your from here to here it is D_{23} and then D_{31} right I hope you are understanding this right.

So, similarly for the second transposition cycle I mean this one this one you make this configuration and this configuration of your own because inductance we have seen it right therefore, for the second transposition cycle it will be V_a to b this is for this 2 means this is for second transposition cycle this is the first transposition cycle section 1 is equal to 1 upon $2\pi\epsilon_0$ right then $q_a \ln D_{23}$ upon r plus $q_b \ln r$ upon D_{23} plus $q_c \ln D_{31}$ upon D_{12} this is equation 14 right.

Then for the third transposition cycle that is V_a to b this is third transposition cycle 3 is equal to 1 upon $2\pi\epsilon_0$ $q_a \ln D_{31}$ upon r plus $q_b \ln r$ upon D_{31} plus $q_c \ln D_{12}$ upon D_{23} this is equation 15 from your imagination also you can write this equation without looking into that diagram also if you understood then no need to look into the diagram from your intuition you can write it right.

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The average value of V_{ab} is:

$$V_{ab} = \frac{1}{3} [V_{ab(I)} + V_{ab(II)} + V_{ab(III)}]$$

$$\therefore V_{ab} = \frac{1}{2\pi\epsilon_0} \left[q_a \ln \left\{ \frac{(D_{12} D_{23} D_{31})^{1/3}}{r} \right\} + q_b \ln \left\{ \frac{r}{(D_{12} D_{23} D_{31})^{1/3}} \right\} \right]$$

$$\therefore V_{ab} = \frac{1}{2\pi\epsilon_0} \left[q_a \ln \left(\frac{D_{eq}}{r} \right) + q_b \ln \left(\frac{r}{D_{eq}} \right) \right] \dots (16)$$

where $D_{eq} = (D_{12} D_{23} D_{31})^{1/3} = (D_{ab} D_{bc} D_{ca})^{1/3} \dots (17)$

Therefore 3 3 different transposition cycles we got V_a to b for section 1 V_a to b for section 2 and V_a to b for section 3 now you take the average value of V_a to b right.

So, the average value of V_{ab} will be equal to $\frac{1}{3} V_{ab}$ for first transposition cycle plus V_{ab} the second transposition plus V_{cb} or V_{ab} for the third transposition cycle right you substitute all and then simplify you will get the step you please do it I have made this one final one that $\frac{1}{2\pi\epsilon_0} q_a \ln \frac{D_{eq}}{r}$ it will be D_{12}, D_{23}, D_{31} to the what you call to the power one third divided by r plus $q_b \ln \frac{r}{D_{eq}}$ to the power your 1 by 3 right cube root. Therefore, V_{ab} is equal to $\frac{1}{2\pi\epsilon_0} q_a \ln \frac{D_{eq}}{r}$ upon r plus $q_b \ln \frac{r}{D_{eq}}$ where D_{eq} is equal to $D_{12} D_{23} D_{31}$ to the power one third cube root is equal to I am writing here capital D_{abc} into D_{cba} ; one third this is equation seventeen right. So, this is average value of V_{ab} right similarly this is an exercise for you because I have done for you V_{ab} right.

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Similarly, average value of V_{ac} is:

$$V_{ac} = \frac{1}{2\pi\epsilon_0} \left[q_b \ln \left(\frac{D_{eq}}{r} \right) + q_c \ln \left(\frac{r}{D_{eq}} \right) \right] \dots (18)$$

Adding eqn.(16) & (18), we get,

$$V_{ab} + V_{ac} = \frac{1}{2\pi\epsilon_0} \left[2q_a \ln \left(\frac{D_{eq}}{r} \right) + (q_b + q_c) \ln \left(\frac{r}{D_{eq}} \right) \right] \dots (19)$$

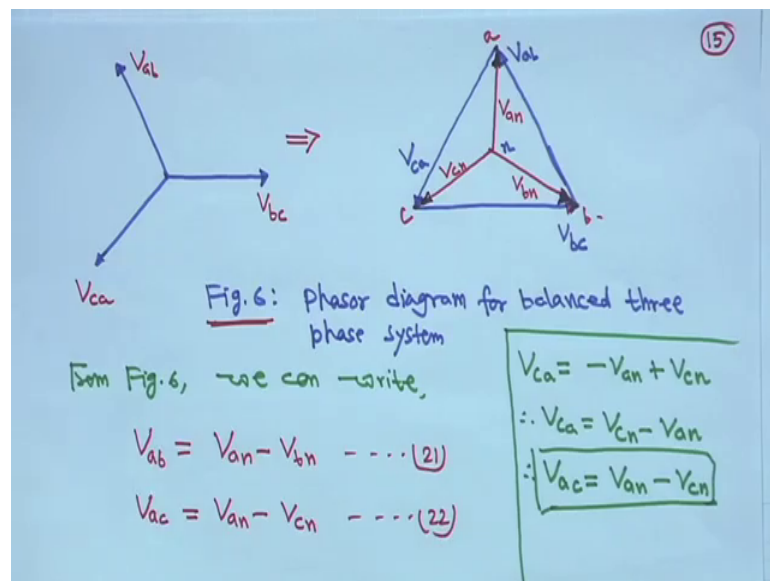
From eqn.(12), substituting $q_b + q_c = -q_a$ in eqn.(19), we have,

$$V_{ab} + V_{ac} = \frac{3q_a}{2\pi\epsilon_0} \ln \left(\frac{D_{eq}}{r} \right) \dots (20)$$

Similarly, average value of V_{ac} from the inspection you can write V_{ac} will be $\frac{1}{2\pi\epsilon_0} q_a \ln \frac{D_{eq}}{r}$ look here it is V_{ab} q_a and q_b right. So, q_c will be eliminated automatically when you will substitute no q_c will automatically be eliminated and V_{ab} will be in terms of q_a and q_b . So, here also from your intuition you can write V_{ac} will be $\frac{1}{2\pi\epsilon_0} q_a \ln \frac{D_{eq}}{r}$ it will be $q_a \ln \frac{D_{eq}}{r}$ upon r plus $q_c \ln \frac{r}{D_{eq}}$ this is eighteen. So, straightforward you can write after this you add equation sixteen and eighteen; that means, V_{ab} plus V_{ac} these 2 add if you add it will be $\frac{1}{2\pi\epsilon_0}$ please add of this thing it will be $2q_a \ln \frac{D_{eq}}{r}$ upon r plus q_b plus q_c into $\ln \frac{r}{D_{eq}}$ which is equation nineteen, but we know that $q_a + q_b + q_c$ is equal to 0.

Therefore this from your equation 12 therefore, $q_b + q_c$ is equal to minus q_a equation 12 it was $q_a + q_b + q_c$ equal to 0 therefore, $q_b + q_c$ is equal to minus q_a substitute here in the equation nineteen substitute here if you do simplify just put it directly you can write them it will become $V_{ab} + V_{ac}$ is equal to $3q_a$ upon $2\pi\epsilon_0 l n$ in bracket $D e q$ upon r this is equation twenty that is $V_{ab} + V_{ac}$ is equal to your $3q_a$ upon $2\pi\epsilon_0 l n D e q$ upon r this is equation 20 I hope you have understood no things are simple right.

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Therefore after that you have to make it some mathematical you know Phasor representation because you have to calculate the capacitance right. So, make it this is V_{bc} reference this is V_{ca} V_{bc} V_{ab} and V_{ca} right.

Now, this one you make it like this if you make it like this; this is your V_{bc} , this phase is your V_{bc} right and this is V_{ab} . So, from here I am drawing the triangle that this is V_{ab} right and this is V_{ca} . So, drawing the triangle arrow is downwards V_{ca} ; that means, this Phasor you cannot triangle this is balanced system not unbalanced balanced system right neutral will be here right. So, if it is a neutral. So, this tip actually this is V_{ab} this tip will be a and this is V_{bc} . So, this tip will be b and this is V_{ca} . So, this tip will be c; that means, for your understanding this will be actually a right and this is V_{bc} . So, this is b and this is V_{ca} ; this is C right therefore, and this is the neutral.

So, this voltage keep it here this voltage is V_{an} this voltage is V_{bn} this voltage is V_{cn} and this angle actually thirty degree this angle thirty degree and this angle 120 degree right, but not writing here then figure will become clumsy, but this is understandable right. So, what I am doing that what we are doing is this V_{bc} is this reference. So, this is V_{ab} . So, this is V_{ab} . So, this is V_{ab} and this is V_{ca} . So, make this V_{ca} the arrow direction will be same as it is just triangular format and this is neutral side right therefore, Phasor diagram for balance 3 phase system now from figure six; that means, from figure six you can write V_{ab} is equal to V_{an} minus.

Now, you do vector the Phasor also V_{ab} is equal to V_{an} minus V_{bn} that is your this V_{bb} this look this V_{ab} now you do the vector Phasor V_{ab} is equal to V_{ab} is equal to this tip is here opposite. So, minus V_{bn} plus V_{n} I am writing this one first and then this one, but if you take for your understanding I am telling this V_{ab} equal to V_{n} minus V_{bn} because arrow tip is here opposite. So, minus V_{bn} this tip is here plus V_{an} . So, writing V_{an} first minus V_{bn} this is equation 21 I hope you have understood similarly we want a b C c a first you see that V_{ac} right. So, in this case V_{ab} plus V_{ac} . So, V_{ac} will be equal to V_{an} minus V_{cn} first see the V_{ca} ; V_{ca} is equal to it will be minus V_{an} because V_{ca} is equal to the way you do the vector Phasor also same thing that Phasor is a rotating vector right this is the difference between Phasor and the vector right.

So, your V_{ca} is equal to minus V_{an} writing fast plus V_{cn} right therefore, V_{ca} is equal to V_{cn} minus V_{an} , but if we write V_{ac} it will be just opposite V_{ac} will be then you just interchange that c and a it will be V_{an} minus V_{cn} right therefore, V_{ac} is equal to V_{an} minus V_{cn} this is the equation 22 I hope this simple thing, but sometimes, but sometimes confusion arises. So, hope there should not be any confusion I hope you have understood right.

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Also, (6)

$$V_{bn} = V_{an} \angle -120^\circ \quad \dots (23)$$

$$V_{cn} = V_{an} \angle -240^\circ \quad \dots (24)$$

Adding eqm. (21) and (22) and substituting $V_{bn} = V_{an} \angle -120^\circ$ and $V_{cn} = V_{an} \angle -240^\circ$, we have,

$$V_{ab} + V_{ac} = 3V_{an} \quad \dots (25)$$

From eqm. (20) & (25), we have,

$$\frac{3V_a}{2\pi\epsilon_0} \ln\left(\frac{D_2}{D_1}\right) = 3V_{an}$$

Therefore then from this Phasor diagram your V_b your what you call from this Phasor dia here also V_{bn} is equal to V_{an} minus angle 120 degree right. So, this is your V_{an} this is your V_{an} . So, V_{bn} actually lagging from lagging by 120 degree because this angle is 120 degree therefore, V_{bn} is equal to V_{an} angle minus 120 degree we are writing twenty 3 understandable.

Then V_{cn} V_{cn} is equal to V_{an} from here to here from here to here it is 240 degree, but lagging. So, V_{cn} is equal to V_{an} angle minus 240 degree this is equation 24 hope this is no no confusion right straight forward this; this V_{bn} is reference then V_{bn} is equal to V_{an} angle minus 120 degree and V_{cn} move this way V_{an} angle minus 240 degree this is equation 24 right.

Therefore adding equation 21 and 22 and these 2 equation you add V_{ab} plus V_{bc} these 2 equation you add right and substituting V_{bn} is equal to V_{an} angle minus 120 degree and V_{cn} is equal to V_{an} angle minus 240 degree you substitute and you add substitute and simplify this is your job right. All these things we have discussed and explained right there should not be any confusion anywhere right therefore, if you do. So, V_{ab} plus V_{ac} actually is equal to $3V_{an}$ this is equation 25 this relationship you have to establish that V_{ab} plus V_{ac} is equal to $3V_{an}$ this is 25.

Now, from equation 20 and 25; that means, this is 25 this is equation 20 this is V_{ab} that is V_{ab} plus V_{ac} this is actually equal to $3V_{an}$ therefore, $3q_a$ upon $2\pi\epsilon_0$ l_n

$D e q$ upon r is equal to $3 V a n$. So, $3 3$ will be cancelled both sides right cancel both sides. So, you can write q a upon $2 \pi \epsilon_0 l n$ right.

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(17)

$$\therefore \frac{q_a}{2\pi\epsilon_0} \ln\left(\frac{D_{eq}}{r}\right) = V_{an} \dots (26)$$

The capacitance per phase to neutral of the transposed transmission line is then given by

$$C_{an} = \frac{q_a}{V_{an}} = \frac{2\pi\epsilon_0}{\ln\left(\frac{D_{eq}}{r}\right)} \text{ F/m} \dots (27)$$

or

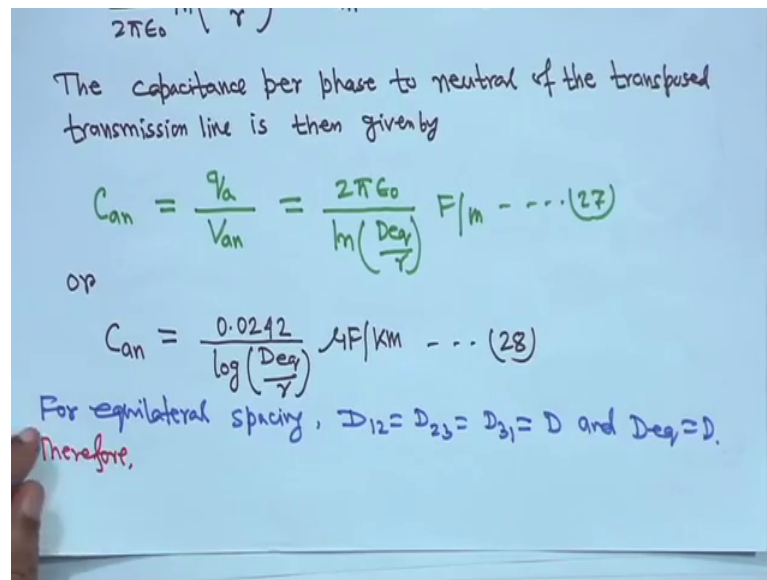
$$C_{an} = \frac{0.0242}{\log\left(\frac{D_{eq}}{r}\right)} \mu\text{F/km} \dots (28)$$

For equilateral spacing, $D_{12} = D_{23} = D_{31} = D$ and D
Therefore,

$D q$ upon r is equal to $V a n$ this is equation twenty six right therefore, capacitance now directly you can use that the capacitance per phase to neutral of the transposed transmission line is then given by $C a n$ is equal to q a upon $V n$ plus q equal to $C V$ you know in general. So, $C a n$ is equal to q a upon $V a n$ is equal to $2 \pi \epsilon_0 l n D e q$ upon r farad; farad per meter. So, natural log you convert to this log right or you can get it $C a n$ is equal to $0.0242 \log D e q$ upon r micro farad per kilometer this is equation 28 right.

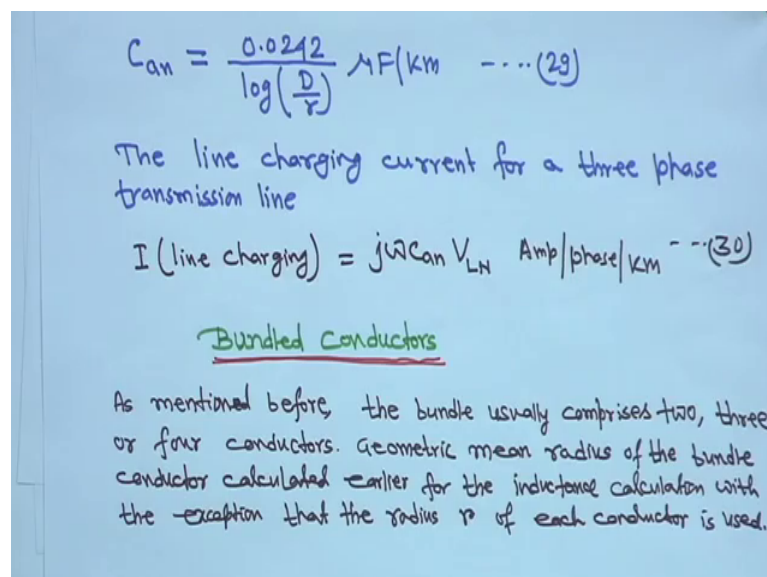
So, up to this things are explained right therefore, for equilateral spacing that if we assume that equilateral spacing that $D 12$ is equal to $D 23$ is equal to $D 31$ is equal to D .

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Therefore D_{eq} will also be equal to D because D into D into D to the power one third is equal to D therefore, therefore, C_{an} is equal to 0.0242 by $\log D$ upon r microfarad per kilometer this is equation 29 right.

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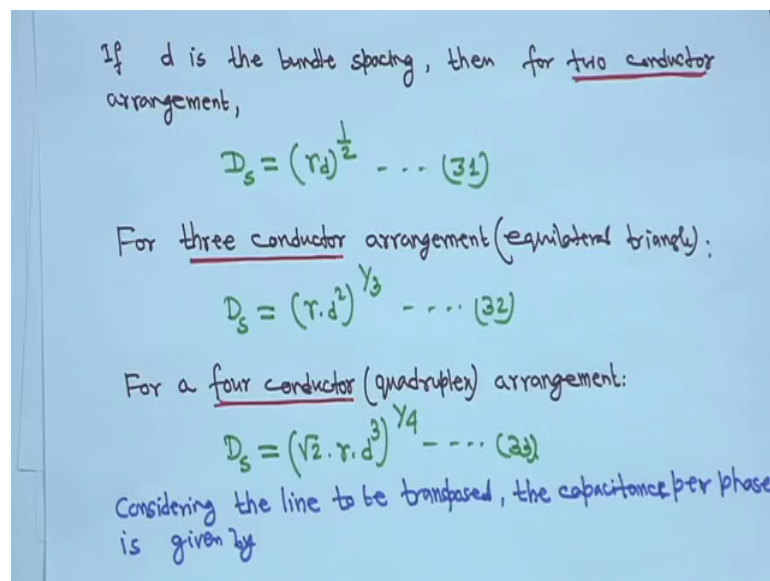


Therefore the line charging current sorry the line charging current for a 3 phase transmission line I in bracket I am writing line charging same as before $j\omega C_{an} V_{LN}$ means line to neutral voltage that is if you have a phase a b c; that means, it is either V_{an} or V_{bn} or V_{cn} in this case we are using C_{an} . So, in this case I will be

equal to V_{ln} line to neutral, but not writing right because your C_{an} ; C_{bn} ; C_{cn} for balance thing all are same, but anyway this is ampere per phase per kilometer this is equation thirty right.

Next one is bundled conductor. So, up to this charging current is required later you will see right particularly for the for your characteristic of transmission line then your this at that time we will see all the details right, but this is this is necessary now bundled conductor bundled conductors we have seen for 2 conductors 3 conductors and four conductors right. So, it is 3 2 already we have seen for induction cases. So, here I am not giving you the diagram the same diagram. So, the geometric mean radius of the bundled conductor can be you have calculated earlier for the inductance calculation with the exception that the radius r with conductor is used right. So, in that case for bundled conductor case for inductance we have used r dash right that is for calculation of internal inductance here no internal your capacitance. So, nothing is there no internal capacitance is there. So, that is why we use r only, but not r dash right.

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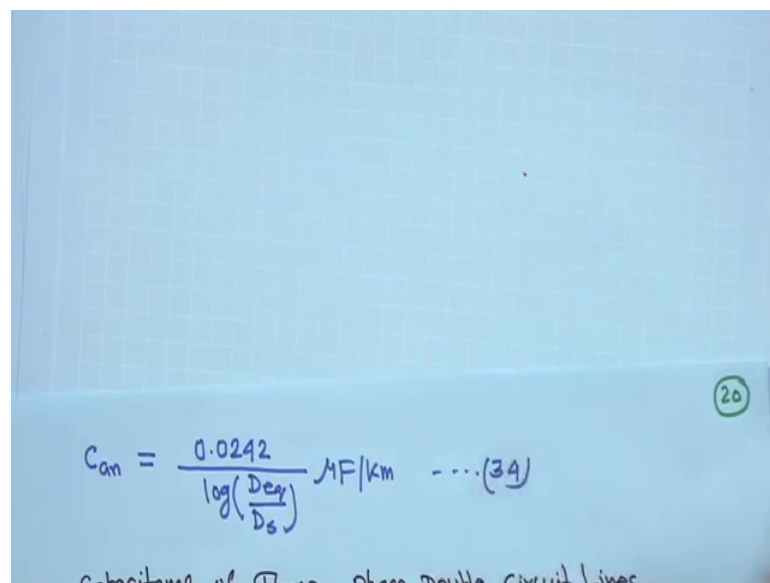


Therefore if D is the bundle spacing then for 2 conductors arrangement just imagine 2 conductors 3 conductors four conductors we have taken no. So, D_s is equal to r D to the power half right the geometric mean radius for 2 conductor case in the case of inductance it was actually r dash, but in the case of capacitance it is r go back to the diagram.

Similarly, for the 3 conductor arrangement that is equilateral triangle this diagram also shown for inductance cases, but in this case D_s will be $r D^2$ to the power one third. So, here no question of r dash again only r this is your thirty 2 and for a four conductor that is quadruplex arrangement D_s will be $\sqrt{2} r$ into $D e q$, but in the case of inductance it was r dash. So, here it is no r dash to the power $1/4$ this is equation thirty 3 right. So, considering the line to be transposed the capacitance per phase is given by if we assume the line is a transposed line right.

So, these are the conductor arrangement is given if you have this kind of arrangement instead of a b C right if you have this; this equation basically this equation that \log of D upon r instead of this equation we can write if we assume that considering the line to be transposed the capacitance per phase is given by in general right.

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$$C_m = \frac{0.0242}{\log\left(\frac{D_e q}{D_s}\right)} \mu\text{F/km} \dots (34)$$

This one that C_m is equal to $0.0242 \log D e q$ upon D_s micro farad per kilometer this is equation 34 we are writing we are writing D upon r that is for equilateral spacing, but if we have that kind of configuration. So, generally we write $\log D e q$ upon D_s microfarad per kilometer this is equation 34.

Thank you.