

Spread Spectrum Communications and Jamming
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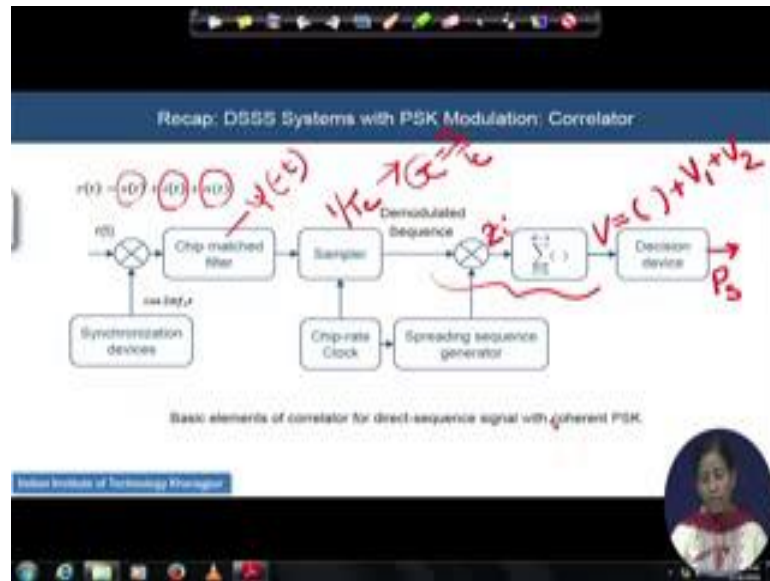
Lecture - 19
Performance Analysis in Presence of Gaussian Interference

Hello students. In continuation of our discussion related to the performance analysis of the direct sequence spread spectrum communications in presence of jamming. In this module we will continue the same with the consideration that now the property distribution of this jamming signal will be considered in the calculation, and we will consider in this module that this jamming signal or the interfering signal is having a Gaussian distribution.

In the last 2 module we have learnt, we have seen, we have derived also the symbol error probability, in presence of different kind of the chips we have seen the effect of the choice of the processing gain, we have also seen over the symbol error probability verses the detected signal I decided signal, signal power or receive signal power after the decision device after the spreading also with respect to the interfering signal be plotted, and we could see actually that when the what was the effect of will be the effect of if the tone jamming is exactly on the centre frequency of our interest, and it is having actually a small it is present on the another tone frequency which is close to the centre frequency of our interest, that we did not consider anything on the distribution function of the signal.

So, now with the understanding of the P_s that we have derived we will slowly proceed towards the considering will proceed and we will revisit all those symbol error probability calculation, in presence of the Gaussian distribution of the interfering signal.

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Refer the same block diagram that we have referred in the last two. So, we are I am not going in detail we understand that the receive signal is modeled as a combination of the transmitted intended signal, the interfering signal, and the noise signal. The match filter here at the front end of the receiver is a transfer function is match to the chip waveform; and after coming down to the baseband and after the output of the match filter is getting sampled at the rate of the chip rate which is $1/T_c$, the sampler and the spreading sequence generator of the receiver they are in sync in this consideration, and their sync is carried out by the clock chip rate clock.

The output of this demodulated sequence with the spreading sequence the multiplied signal of this 2 is we are mentioning it as Z_i and once they are added over the capital G number of the samples, this samples are generated by the sampler; because if it is sampling at $1/T_c$ rate is targets is to give you back, the capital G number of the chips who are present over the duration of symbol; and this combined effect of this multiplication class addition he will give you the despreading operation and we are really very interested to know the output of the adder circuit or the despreading circuit, where this V is having basically 3 section; one section we saw is a signal contribution, another part is the contribution from the jamming signal, and third part was the contribution from the noise section.

And we were kindly interested that we understand that the noise as well as the jamming as well as a noise signal both are of random nature and as they are having the randomness, and they are means basically determining the value of this V the statistical probe they are defining the statistical property of V, I mean the mean and the variance of V is largely dependent upon all of them and hence the decision we had property calculation at the output of the decision device we carried out, where we are whole discussion is ending up. And with this understanding we will proceed again in this module. So, we are talking about a Gaussian interference now.

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Gaussian Interference: DSSS Performance Analysis

- Gaussian interference is interference that approximates a zero-mean, stationary Gaussian process.
- If $s_i(t)$ is modeled as Gaussian interference and carrier frequency $f_c \gg 1/T_c$, where T_c is the chip duration, then

$$s_i(t) = \int_{t_1}^{t_1+T_c} [G(\omega)\phi(\omega - f_c) \cos 2\pi f_c t] d\omega \quad (1.43)$$
- where $\phi(t)$ is the chip waveform. A trigonometric expansion, the dropping of a negligible double integral, and a change of variables give

$$R_s(t) = \frac{1}{2} \int_{t_1}^{t_1+T_c} \int_{t_1}^{t_1+T_c} R_s(t_1 - t_2) \phi(t_1) \phi(t_2) \cos[2\pi f_c (t_1 - t_2)] dt_1 dt_2 \quad (1.44)$$
- where $R_s(t)$ is the autocorrelation of $s(t)$.
- Since $R_s(t)$ does not depend on the index i ,

$$\text{var}(V_i) = \sum_{i=1}^N R_s(0) \quad (1.45)$$
- gives

$$\text{var}(V_i) = cR_s(0) \quad (1.46)$$

Handwritten notes on the slide include: $f_c \gg 1/T_c$, $Z_i = S_i + J_i + N_i$, and $V = C + V_1 + V_2$.

So, Gaussian interference can be defined like this; it is an interference that approximates a 0 mean stationary Gaussian process, and I t will be symbolized for this Gaussian interference in our analysis in this module, and we also considered the same and assumption will continue with the same assumption that we have done in the last 2 module.

The consideration was that transmission frequency of interest f_c is definitely much much larger than a chip rate. So, that actually we can omit all the higher frequency terms, and we understand that this J_i we saw this expression of this interfering signal at the input at the input of this adder. So, J_i is a part like this, we saw that input of the adder in the last block diagram we saw the input of this adder was given by Z_i , and Z_i had 3 parts one is my S_i another is my J_i and the last one was my N_i for the i th chip.

So, this J_i expression we have seen earlier; that J_i can be expressed that is i multiplied by the locally generated ψ_{t-T_c} , cost $2\pi f_c t$ was contributed from the front end of the receiver, which synchronizes it and brought it down to the baseband. So, fundamentally the contribution of the J_i over a one chip interval will be given by this. And our target is what? Our target is to now replace the i replace the computation replace the i by this consideration of the Gaussian interference.

We consider that now this i is a Gaussian interference and if this is ψ_t is definitely the chip waveform for consideration, and then if we are trying to compute now the J_i square, then definitely you have to compute the relative autocorrelation of this Gaussian interference i . If I come try to compute that in the expression would look like this 1.44, if I try to compute the variance of this Z_i square finally, I will boil down here and then inside that this $R_j T_1 - T_2$ is coming because there is an i square t which is basically the autocorrelation of this Gaussian interference, coming into picture in this derivation and this autocorrelation the expression for this autocorrelation we will see in the next slide.

But finally, see this value of this expected value of the J_i square which is a variance is not affecting on the he has no contribution, it is not dependent that all on the index i see in the 1.44 items are there is no presence of small i . So, the variance so will be basically if I now talk about the output of this adder, where the V is residing and where actually V_1 will be the corresponding portion of the jamming section at inside the V .

So, J_i is mapping to this V_1 in the V section, where V is V_1 is actually that this interference this variance of the i th chip, and that is getting added up I mean added up over the g number of the samples, if this is the that is the situation we happening at the output of the add up then as this I is $G_i J_i$ is not dependent on i ; that means, when is you are calculating for each and every I sample they are independence. So, I can add up the variance. So, finally, it we will end up with the G times the variance of these contributed by this expected value of the J_i square. So, finally, 1.45 balls down to 1.46.

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Gaussian Interference: DSSS Performance Analysis

- where $d = \frac{D}{T_s}$ with symbol duration T_s . Assuming that $\psi(t)$ is rectangular, we change variables in (1.44) by using $r = t_1 - t_2$ & $s = t_1 + t_2$.
- The Jacobian of this transformation is 2. Evaluating one of the resulting integrals and substituting the result into (1.46) yields

$$\text{var}(V_0) = \frac{1}{T_s} \int_{-T_c}^{T_c} A_c^2(r) A_c^2\left(\frac{r}{2}\right) \cos^2 \pi f_c r dr \quad (1.47)$$

- $A_c(t)$ represents the triangular pulse. The limits in this equation can be extended to $\pm\infty$ because the integrand is truncated.

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Now, we know that G_v the processing gain is given by T_s by T_c , and we assume again first that the ψ_T is a rectangular chip waveform; we also substitute that $t_1 - t_2$ and is equal to τ and capital S will be $t_1 + t_2$. So, here actually this substitution will be by τ , and capital G we understand that will be given by T_s by T_c and this ψ_t now we will continue with rectangular chip waveform, and another parameter is coming called as small s we will be giving the $t_1 + t_2$ value.

And this transformation the Jacobian of this transformation is equal to 2 and if you try to evaluate the integration of resulting of the resulting integrals of this (Refer Time: 09:51) coming from 1.44, if I try to substitute the value and if I try to do the integration, then this 1.46 so will turn down, and if I do G into this whole integration and if we try to solve it, it will come down to this point. I remember that I told that this is a autocorrelation section of contributed by the interfering signal, and there is a triangular waveform coming into picture associated to it, which will is a function of this $t_1 - t_2$ the difference between the time delay between the 2 pulses involved in this autocorrelation process and T_c the chip duration and remember the limit of this equation minus to $c/2 + T_c$ it can be extended to plus minus infinity also because this integration is all the integrand is there truncated already.

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Gaussian Interference: DSSS Performance Analysis

- Since $A_i(\tau)A_c^2(\tau)$ is an even function, the cosine function may be replaced by a complex exponential.
- Then the convolution theorem and the known Fourier transform of $\Lambda(\tau)$ yield the alternative form

$$\text{var}(V_1) = \frac{1}{4} T_c T_c \int_{-\infty}^{\infty} S_i(f) \sin^2[(f - f_c)T_c] df \quad (1.48)$$

where,

- $S_i(f)$ is the power spectral density of the interference after passage through the initial wideband filter of the receiver.
- Since $i(t)$ is a zero-mean Gaussian process, the $\{j_i\}$ are zero-mean and jointly Gaussian.
- Therefore, if the $\{j_i\}$ are given, then (V_1) is conditionally zero-mean and Gaussian.
- $\text{var}(V_1)$ doesn't depend on the $\{j_i\}$, V_1 without conditioning is a zero-mean Gaussian random variable.

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Now, the function that we have seen here this $R_j \tau$ and dell multiplied with the triangular function this is an even function. If this is a even function given here then the corresponding this $\cos 2 \pi f_c \tau$, this \cos term itself they can be also substituted by the exponential term. If I do that and I understand that the Fourier transform of this triangular function will be giving a sinc function again, we will be boiling down once again another form of this variance we can write down like 1.48, but this $S_j f$ is nothing, but the power spectral density of the interfering signal after passing through the wideband filter of the receiver, and the $i(t)$ which was considered in the earlier slide, which is 0 mean Gaussian process for with which we started hence actually if $i(t)$ is we are starting with a 0 mean Gaussian process.

So, Z_i will be also having a 0 mean and jointly Gaussian. If this P_i are given in the earlier slide whatever we have seen here. In the definition of all these this J_i square will be the summation of this P_i multiplied by Z_i also, if the P_i is given and then the V_i is conditionally 0 mean over and then it is also Gaussian. This variance of the V_1 it does not depend on the P_i because we have seen the actually that variance V_1 is the contribution of J_i , and J_i is actually not having any contribution from the I itself and. So, P_i is not playing approximately not having a lot of roll on it and then. So, V_1 without conditioning it is a 0 mean Gaussian random variable blankly it is following the statistical property of $i(t)$. $i(t)$ is $Z_i J_i$ is was following the property of $i(t)$ and J_i is

influencing the V 1. So, the variance of V 1 is also getting largely dominated by the i t itself fundamentally.

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Gaussian Interference: DSSS Performance Analysis

- The independence of the thermal noise and the interference imply that $V = V_1 + V_2$ is a zero-mean Gaussian random variable.
- Thus, a standard derivation yields the symbol error probability:

$$P_s = Q\left(\sqrt{\frac{E_b}{N_{0,t}}}\right) \quad (1.49)$$

where,

$$N_{0,t} = N_0 + 2\int_{-B/2}^{B/2} S_j(f) \cos^2(\pi f T) df \quad (1.50)$$

- N_0 is the one sided PSD of white noise. If $S_j(f)$ is the interference power spectral density at the input and $H(f)$ is the transfer function of the initial wideband filter, then $S_j(f) = |S_j(f) H(f)|^2$.
- Suppose that the interference has a flat spectrum over a band within the passband of the wideband filter so that

$$S_j(f) = \begin{cases} \frac{I}{2B_j}, & |f - f_0| \leq \frac{B_j}{2} \\ 0, & \text{Otherwise} \end{cases} \quad (1.51)$$

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So, it is actually 0 mean Gaussian random variable finally, we are ending up with; we understand that the thermal noise and the interfering signal they are completely IID process I mean the independent and identically distributed and hence the total noise that we will be considering here V 1 plus V 2 and if I try to see actually the mean value of both of them, they will be actually this capital V will be V 1 plus V 2 and it is a 0 mean Gaussian random variable finally, and the standard derivation yields the symbol error probability will be a Q function.

Because it is a Gaussian random variable finally, ending up with, where it will be given by the symbol energy to the noise power spectral to one sided noise power spectral density, where this noise power spectral density will have the contribution from one sided noise power spectral density, and this noise is the combined power one sided power spectral density of the noise plus the jamming signal, which will have a part of noise one sided noise power spectral density, plus actually the one sided power spectral density contributed by the jamming signal, and this equation is directly brought from the expression here of 1.48.

Now, see the consideration see let us look inside it that if; we consider that this $S_j(f)$ can be given by the interference power spectral density multiplied by the transfer function of

the initial wideband filter, because noise will be always having a will be band limited by the wideband filter itself. So, if this is the situation. So, this interference power spectral density $S_j(f)$ that will be basically we can shift with by means of your S dash to j f into f square and if it is has a flat spectrum suppose over the whole band of their interest within the pass band of this wideband where the wideband filter is operating, so then this $S_j(f)$ can be given by I by $2w$.

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Gaussian Interference: DSSS Performance Analysis

- If $f_c \gg 1/T_c$, the integration over negative frequencies in (1.50) is negligible and

$$N_{int} = N_b \int_{f_c - B/2}^{f_c + B/2} \frac{1}{f_c - \omega_c} \sin^2[(f - f_c)T_c] df \quad (1.52)$$
- This equation shows that $f_i = f_c$ or $f_i = 0$ coupled with a narrow bandwidth increases the impact of the interference power.
- Since the integrand is upper bounded by unity, $N_{int} \leq N_b \cdot BT_c$.
- This upper bound is intuitively reasonable because $BT_c = B - B_c$, where,
 - $B = 1/T_c$ is the bandwidth of narrowband interference after the despreading.
 - B_c is its power spectral density.

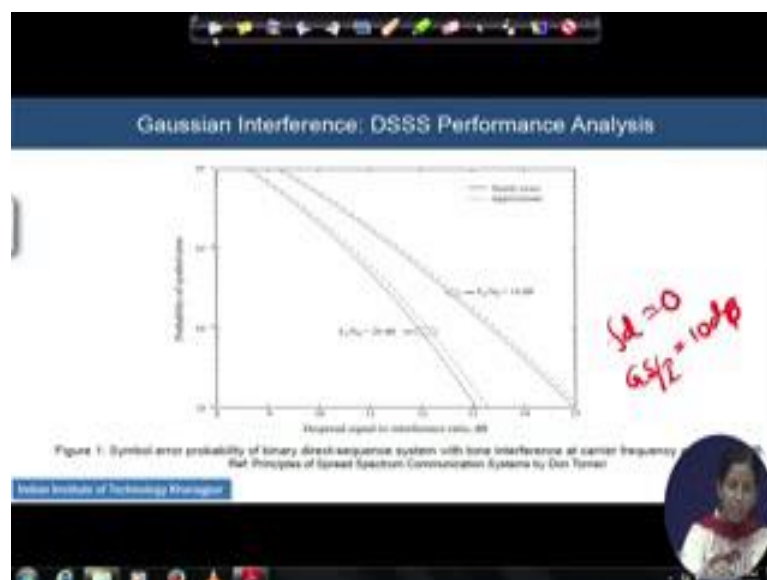
Where the when the mode of this frequency is less than equal to w by 2 and it will give you the 0 otherwise. So, I by w substituting the value of I by w in the expression, and considering the fact that the transmission frequency is much higher than your chip rate, we will be coming down to this expression of 1.52 we are substituting the value into 1.50 using 1.51 we are down to 1.52.

So, now this equation shows you some nice thing actually; if my f_1 is equal to my f_c or your f_d equal to 0 . So, then actually meaning is that that they are now the coupled with some narrow bandwidth coupled with the narrow bandwidth increases narrow bandwidth, and then it will in keep on increasing the impact of the interference power. So, question is actually if we are having a exactly coinciding interference on the transmission intended transmission frequency, that is why your f_d is equal to 0 , the first situation that we have considered. And then even if actually f_1 and otherwise actually f_1 is equal to your f_c and.

So, and then actually you are having a very narrow bandwidth of this interfering signal, then the impact of the over the interference power its keep on increasing; and since the integrand upper boundary is bounded by unity. So, this effect of this one sided power spectral density will be always less than equal to this one sided power spectral density of the noise, plus some contribution coming express like this. This I into T c is nothing, but this I by the total bandwidth which we are taking as 0, and this bandwidth is equal to given by 1 by T c is the bandwidth of the narrow band interfering signal after the dispreading and this is a power spectral density of the power spectral density finally, because it is a with the power of the incoming signal and it is divided by the bandwidth of this interfering signal after dispreading.

So, if I compute this guy. So, I 0 is the contribution from the power spectral density contributed by the jamming signal. So, N o e can be having either less than the both of them or it can be actually the equal to that and this equation is finally, showing and proving you that if you are having a very narrow bandwidth interference, very close to the centre carrier frequency of your interest or close to that or exactly on the centre carrier frequency of your transmission, you are effect on the impact of the interference power how actually it will be varying.

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We have seen this graph in the earlier module, where we discussed that for if you are having a interference close to the centre frequency, and if you are having a very high

processing gain. So, you can control the deviation of the model developed similar probability model developed in the last module with compared to the nearly exact consideration, and at the target bitrate of a data communication of 10 to the power minus 5 that approximated model is proven to be close to the nearly exact model and they are deviating around 0.1 dB. If I consider all the other parameters which we are considered to generate this result for example, that G value was equal to 17 dB, G s by i equal to g s by i; that means, the despreading signal spread signal to the interference ratio we considered to be 10 dB, we consider that f d will be equal to 0. So, for all that consideration if we hold good same way and now we are considering now that the distribution of this interference is equal to Gaussian.

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Gaussian Interference: DSSS Performance Analysis

- The expression,

$$P_b = Q\left(\sqrt{\frac{P_s}{P_n}}\right) \quad (1.53)$$
- yields

$$P_b \leq Q\left(\sqrt{\frac{P_s}{P_n + I_c}}\right) \quad (1.54)$$

$N_o e \leq N_o + I T c$
 $I_o = 1/B$

- This upper bound is tight if $f_d = 0$ and the Gaussian interference is narrowband.
- A plot of (1.54) with the parameter values of Figure 1 (previous slide) indicates that roughly 2 dB more interference power is required for worst-case Gaussian interference to degrade P_b as much as tone interference at the carrier frequency.

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Then we will see that the error probability that you are ending up with here the error probability was given by that square root of twice e_s by $N_o e$ that we have seen earlier and which is basically less than equal to the N_o plus $I T c$ because we have already established the expression that $N_o e$ will be less than equal to always the N_o plus $I T c$ and where my $I T c$ is basically I_o where I_o was given by I by capital B or $T c$ equal to 1 by capital B it is a power spectral density of the interfering signal and hence it will be the symbol error probability will be always less than equal to this Q function, and this upper bound is really very very tight.

If and only this will be really very tight if f_d is closed to 0 and the Gaussian interference is a narrowband interference, and if I plot the same graph with the parameter that I have shown earlier with the parameter that we have considered for the last module case, then there is a very nice observation the re plot of this expression or this 1.54 basically 1.05 expression 1.54 with the parameter that we have considered for the last slide, and the last module which is equal to my gain is equal to 17 dB and your GS by I, I mean received signal to the interference power to be 10 dB and my f_d is equal to 0. Only consideration is that the power is I mean distribution of the interference signal is Gaussian in that case what we find that there is roughly around 2 dB more interference power you will be required for the worst case Gaussian interference to degrade the symbol probability, the symbol error probability as much as a tone interference at the carrier frequency does.

So, situation is such that worst case for worst case Gaussian interference 2 dB more interface power you have to put. If you wish to degrade the symbol error probability as much as the tone interference at the carrier frequency does. You have a gap of around 2 dB, 2 dB value in terms of the interference power if you consider the Gaussian distribution is going on. So, worst possible a Gaussian interference also needs 2 dB more power to degrade this symbol error probability equal to the tone interference exactly happening at the carrier frequency.

So, we will go back and revisit we will go back and revisit; the whole equation and the target what we have try to do in this module. We thought that we will do the analysis for a Gaussian interference; target is that the Gaussian interference was a 0 mean having stationary Gaussian process. So, by means of each now the interfering our system, and we also considered that the transmission frequency waves having a much much higher value compared to our chip rate, and we have re computed the received signal I mean receive insert the received signal what is the contribution of this jamming signal.

We saw that actually with this Gaussian process we can nicely boiled down to some known autocorrelation structure; and that autocorrelation structure will followed as with a triangular kind of web shipping, triangular function involved inside that variance computation. Because of the involvement of this a triangular function we saw that if we are applying the standard convolution property and we are introducing the known Fourier transformation for this triangular function.

So, the variance will be the function of given by a power spectral density involved inside the interference or interfering signal, and followed by the other parts of the analysis, other parts of the element and we considered here few things to be remembered when your interference is having a Gaussian distribution, and if you are considering that the Gaussian distribution or the signal having a Gaussian distribution is having a 0 mean and that we have considered it is considered to be followed when we have entered after the sampler, we are trying to consider the contribution of the sample; contribution of the jamming part inside the sampled signal, and we carry forwarded the 0 mean; and the Gaussian distribution consideration jointly inside that also.

And we have seen nicely that this variance computation of this J_i , which is the interference part acting role playing some role on the incoming or sampled signal it is independent of i . So, that is why actually the various furthermore the variance computed from this Z_i , which is actually the variance of interference or the jamming signal entering into the decision device, he is also having no effect on the I and basically he is also not dependent on the P_i , is P_i is the sequence of values plus 1 or minus 1.

And as the variance is this is a one direction, and in other direction we saw that the variance computation total variance of the V which is contributed by the variance of the noise signal and the variance of the interfering signal, we saw that as the noise sample and the interfering sample they are independent and identically distributed, and there is they are mutually independent process also enhance that is no coupling in between and they are the 0 mean Gaussian, Gaussian on random variable each of them are and finally, leading the distribution of the capital V to be a 0 mean Gaussian random, and that is why we could apply the classical standard derivation for the symbol error probability which is governed by the Q function.

But inside that Q function we saw that there is noise power spectral density, but noise power spectral density here is governed by the one sided power spectral density, and plus of contribution from the interfering signal. Inside that interfering signal contribution we have a power spectrum, interference power spectral density, interference the power spectrum of the interfering signal and that can be further simplified considering the wideband filter bandwidth. And given that actually he is giving the waveform and the interference is having a flat kind of the flat spectrum over the bandwidth of our interest wideband filter into bandwidth interest, then we could find out that this N_o e what is a

one sided power spectral density of a combined effects; we could compare and we could finally, see that this one sided power spectral density.

Now whatever we are getting it is basically less than the power spectral individual power addition power spectral density of this N_0 plus I into T_c and finally, the symbol error probability the expression for this Gaussian distribution we could find that it is always less than equal to the Q function of square root of twice $e S$ by N_0 by $I T_c$ because it is upper bounded by 1; and to get a symbol error probability equivalent to the tone interference that equivalent to an tone interference, the you have to with a Gaussian interference we have to put a 2 dB more interference power to get to degrade the symbol error probability up to the previous situation when the tone is exactly present on the centre frequency of our interest. So, degradation would not be that much with respect to the Gaussian interference, if we consider interfere to be a Gaussian interference that is the solution that is a final conclusion that we have learnt from this module.