

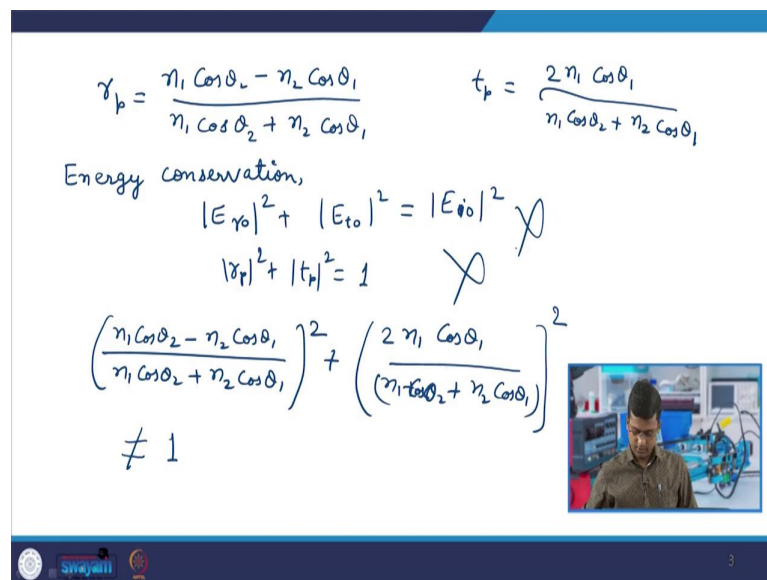
**Optical Sensors**  
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**Lecture – 06**  
**Basic Optics for Optical Sensing – IV**  
**Polarization by reflection – Brewster angle sensor, Total Internal Reflection**

Welcome to the 6th lecture of Optical Sensors course. In the last lecture, we discussed the propagation of an electromagnetic wave at an interface and we solved for the reflection and transmission coefficients for a p-polarized wave; p-polarized means TM polarized wave where, the electric field components are in the plane of incidence.

And, I gave a homework for the waves, which have electric field component perpendicular to the plane of incidence. So, I hope that you have solved for the reflection and transmission coefficients for that. Now, we move ahead and we discuss certain properties associated with this and want to see what happens to it.

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$$r_p = \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1} \quad t_p = \frac{2 n_1 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1}$$

Energy conservation,

$$|E_r|^2 + |E_t|^2 = |E_i|^2$$

$$|r_p|^2 + |t_p|^2 = 1$$

$$\left( \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1} \right)^2 + \left( \frac{2 n_1 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1} \right)^2 \neq 1$$

So, let us see the reflection coefficient, that was  $n_1 \cos \theta_2 - n_2 \cos \theta_1$  divided by  $n_1 \cos \theta_2 + n_2 \cos \theta_1$ , this was the reflection coefficient. And the transmission coefficient  $t_p$  was equal to  $2 n_1 \cos \theta_1$  divided by  $n_1 \cos \theta_2 + n_2 \cos \theta_1$ . So, we had these two.

Now, if we solve the energy conservation - according to energy conservation,  $E_r^2$  plus  $E_t^2$  should be equal to  $E_i^2$ ; which means that  $r^2$  plus  $t^2$  is equal to 1. Let us try to solve it. So, it becomes like  $n_1 \cos \theta_2 - n_2 \cos \theta_1$  divided by  $n_1 \cos \theta_2 + n_2 \cos \theta_1$  squared plus  $2 n_1 \cos \theta_2$  divided by  $n_1 \cos \theta_2 + n_2 \cos \theta_1$  squared plus  $n_2 \cos \theta_1$  squared, this all squared. So, what do you get? You will get - this denominator is the same.

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$$\left[ \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1} \right]^2 + \left[ \frac{2 n_1 \cos \theta_2}{n_1 \cos \theta_2 + n_2 \cos \theta_1} \right]^2$$

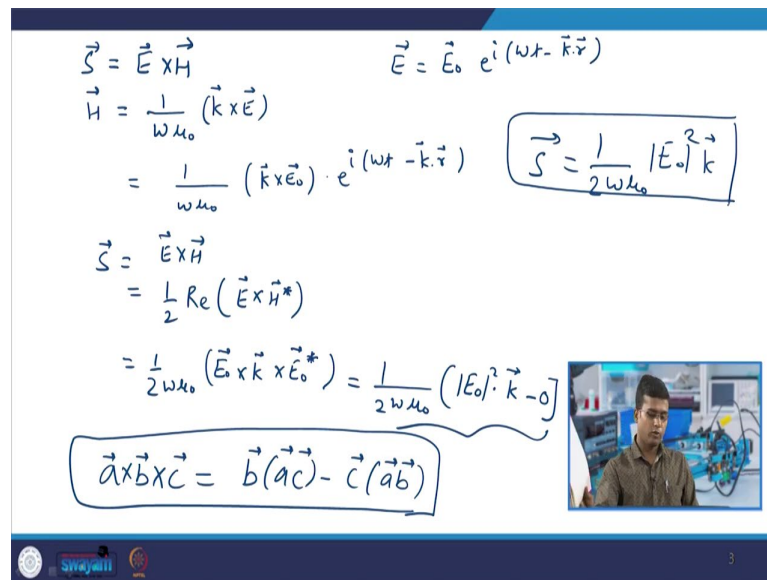
$$\Rightarrow \frac{(n_1 \cos \theta_2)^2 + (n_2 \cos \theta_1)^2 - 2 n_1 n_2 \cos \theta_1 \cos \theta_2 + 4 n_1^2 \cos^2 \theta_2}{(n_1 \cos \theta_2 + n_2 \cos \theta_1)^2}$$

$$\Rightarrow \frac{\text{Numerator}}{\text{Denominator}} \neq 1$$

So, you can have  $n_1 \cos \theta_2 - n_2 \cos \theta_1$  divided by  $n_1 \cos \theta_2 + n_2 \cos \theta_1$  whole square plus  $2 n_1 \cos \theta_2$  divided by  $n_1 \cos \theta_2 + n_2 \cos \theta_1$  square. So, you can see that - in the denominator you have  $n_1 \cos \theta_2 + n_2 \cos \theta_1$  whole square. And here you have  $n_1 \cos \theta_2$  square plus  $n_2 \cos \theta_1$  square minus  $2 n_1 n_2 \cos \theta_1 \cos \theta_2$  plus  $4 n_1^2 \cos^2 \theta_2$ .

So, numerator - you can see that is not equal to  $n_1 \cos \theta_2 + n_2 \cos \theta_1$  square; because you have this - a square term, b square term, but you do not have plus  $2 ab$  term so, this is not equal to this. Hence, numerator divided by denominator is not equal to 1 and you see that this does not come equal to 1. So, where are we wrong? I mean there should be something wrong with it. It does not come 1. So, what is the problem? Why are we not getting this? So, something is wrong here. The energy of an electromagnetic wave is given by the Poynting vector. So, we have to solve for the Poynting vector. So, let us solve for the Poynting vector.

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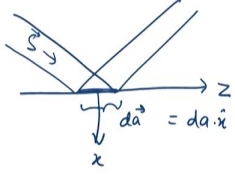
$$\begin{aligned}\vec{S} &= \vec{E} \times \vec{H} & \vec{E} &= \vec{E}_0 e^{i(\omega t - \vec{k} \cdot \vec{r})} \\ \vec{H} &= \frac{1}{\omega \mu_0} (\vec{k} \times \vec{E}) \\ &= \frac{1}{\omega \mu_0} (\vec{k} \times \vec{E}_0) \cdot e^{i(\omega t - \vec{k} \cdot \vec{r})} & \boxed{\vec{S} = \frac{1}{2\omega \mu_0} |\vec{E}_0|^2 \vec{k}} \\ \vec{S} &= \vec{E} \times \vec{H} \\ &= \frac{1}{2} \text{Re}(\vec{E} \times \vec{H}^*) \\ &= \frac{1}{2\omega \mu_0} (\vec{E}_0 \times \vec{k} \times \vec{E}_0^*) = \frac{1}{2\omega \mu_0} (|\vec{E}_0|^2 \vec{k} - 0) \\ \boxed{\vec{a} \times \vec{b} \times \vec{c} = \vec{b}(\vec{a} \cdot \vec{c}) - \vec{c}(\vec{a} \cdot \vec{b})}\end{aligned}$$

So, the Poynting vector  $\vec{S}$ ;  $\vec{S}$  was given by  $\vec{E}$  cross  $\vec{H}$  and  $\vec{H}$  was given by  $1/\omega\mu_0$   $\vec{k}$  cross  $\vec{E}$  and  $\vec{E}$  is equal to  $\vec{E}_0 e^{i(\omega t - \vec{k} \cdot \vec{r})}$ , you know this. So, this can be written as  $1/\omega\mu_0$   $\vec{k}$  cross  $\vec{E}_0$  into  $e^{i(\omega t - \vec{k} \cdot \vec{r})}$ , right. What does it give?

So, if we want to calculate  $\vec{S}$ , that is  $\vec{E}$  cross  $\vec{H}$ , that is equal to half of real of  $\vec{E}$  cross  $\vec{H}^*$  - you can solve it for this and that is  $1/2\omega\mu_0$   $\vec{E}_0$  cross  $\vec{k}$  cross  $\vec{E}_0^*$  that is  $1/2\omega\mu_0$   $|\vec{E}_0|^2$   $\vec{k}$  minus 0. You know this identity, I told you about this identity.  $\vec{a} \times \vec{b} \times \vec{c}$  was equal to  $\vec{b}(\vec{a} \cdot \vec{c}) - \vec{c}(\vec{a} \cdot \vec{b})$ . So, you use this identity, I told you on that day to prove it. So, go back and prove it and try to see what happens. So, we end up with this relation.

So, that is  $\vec{S}$  is equal to  $1/2\omega\mu_0$   $|\vec{E}_0|^2$   $\vec{k}$ .  $\vec{S}$  gives the direction of flow of energy. So, we solve for it and, we go to see what happens.


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Energy entering in the area  $d\vec{a}$  per unit time  
 $\vec{S}_i \cdot d\vec{a}$

" reflected from " " " " "  
 $\vec{S}_r \cdot d\vec{a}$

" transmitted from " " " " "  
 $\vec{S}_t \cdot d\vec{a}$



So, this is our interface. A beam is coming like this, it is getting reflected from here and this is the area. So, it was x direction if you remember, this is z direction this is S now flowing in this direction and this is da, the area where it is falling that is da into x. So, energy entering in the area da per unit time -  $\vec{S}_i \cdot d\vec{a}$ . Similarly, energy reflected from area da per unit time is -  $\vec{S}_r \cdot d\vec{a}$ . Energy transmitted from area da per unit time is  $\vec{S}_t \cdot d\vec{a}$ .

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$$\vec{S}_i \cdot d\vec{a} = \vec{S}_t \cdot d\vec{a} + \vec{S}_r \cdot d\vec{a}$$

$$|E_{i0}|^2 \vec{k}_i \cdot d\vec{a} = |E_{t0}|^2 \vec{k}_t \cdot d\vec{a} + |E_{r0}|^2 \vec{k}_r \cdot d\vec{a}$$

$$\Rightarrow |E_{i0}|^2 \frac{1}{2} n_1 \cos \theta_1 = |E_{t0}|^2 \frac{1}{2} n_2 \cos \theta_2 + |E_{r0}|^2 \frac{1}{2} n_1 \cos \theta_1$$

$$\Rightarrow |E_{i0}|^2 = |E_{t0}|^2 + \frac{n_2 \cos \theta_2}{n_1 \cos \theta_1} |E_{r0}|^2$$

This is the equation which must be satisfied for ENERGY CONSERVATION

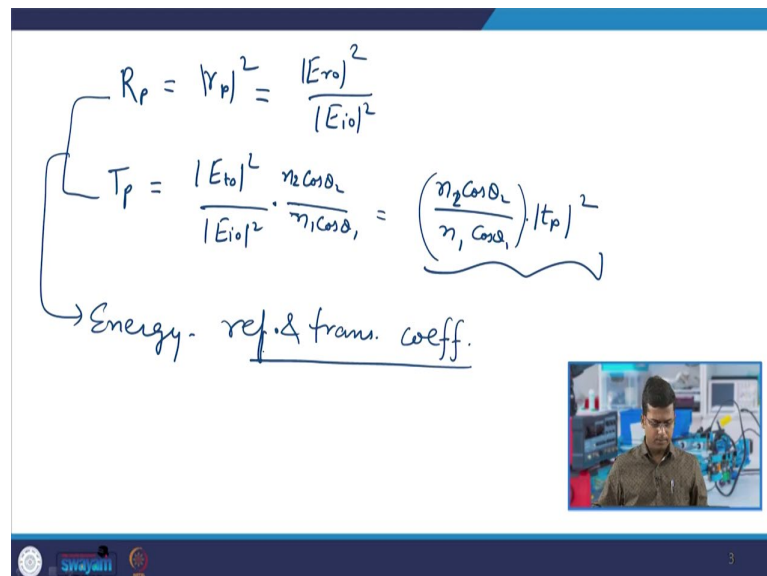


So, in principle,  $S_i \cdot da$  should be equal to  $S_t \cdot da$  plus  $S_r \cdot da$ ; that is  $\text{mod } E_i^2 \cos^2 \theta_1$ ,  $k_1$  is equal to  $\text{mod } E_r^2 \cos^2 \theta_2$ ,  $k_2$  it is also  $k_1$  no, this one is  $k_2 \cdot da \cdot r$  actually plus  $\text{mod } E_r^2 \cos^2 \theta_1 \cdot da$ .  $k$  is small actually sometimes I write it seems like capital, but it is small  $k$ .

So, you have actually  $\text{mod } E_i^2 \cos^2 \theta_1$ ;  $k_1$  is  $\omega$  by  $c$  into  $n_1 \cos \theta_1$ , you take the  $\theta_1$  component is equal to  $\text{mod } E_r^2 \cos^2 \theta_2$   $\omega$  by  $c$ . Again  $n_1 \cos \theta_1$  plus  $\text{mod } E_t^2 \cos^2 \theta_2$   $\omega$  by  $c$  now  $n_2 \cos \theta_2$ ; because it was a vector, that is why you have  $\cos \theta_2$  and I have removed  $da$  now, ok.

So, we arrive to this relation.  $\omega$  by  $c$  cancels out from here. Now, you have  $\text{mod } E_i^2 \cos^2 \theta_1$  is equal to  $\text{mod } E_r^2 \cos^2 \theta_2$  plus  $n_2 \cos \theta_2$  divided by  $n_1 \cos \theta_1$  into  $\text{mod } E_t^2 \cos^2 \theta_2$ . This is the equation, which needs to be satisfied for energy conservation. If you simply want to say that  $\text{mod } r_p^2$  and  $\text{mod } t_p^2$  is equal to 1, that is wrong interpretation. You must have it in terms of the Poynting vector because that is the vector which gives you the energy flow. And from here we arrive to this relation which gives you the actual equation which must be satisfied to prove the energy conservation.

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$$R_p = |r_p|^2 = \frac{|E_{r0}|^2}{|E_{i0}|^2}$$

$$T_p = \frac{|E_{t0}|^2}{|E_{i0}|^2} \cdot \frac{n_2 \cos \theta_2}{n_1 \cos \theta_1} = \left( \frac{n_2 \cos \theta_2}{n_1 \cos \theta_1} |t_p| \right)^2$$

→ Energy ref. & trans. coeff.

So, from here if you want to calculate what are the  $R_p$  - is equal to simply  $\text{mod } r_p^2$  square and that is equal to  $E_r^2$  divided by  $E_i^2$  and  $T_p$  - is equal to which is  $\text{mod } E_t^2$  divided by  $E_i^2$  into  $n_2 \cos \theta_2$  divided by  $n_1 \cos \theta_1$

and this is into  $n_2 \cos \theta_2$  divided by  $n_1 \cos \theta_1$  into mod  $t_p$  square; this is the correction. So, it is not like that mod  $t_p$  square is not equal to  $T_p$ . You have to have this coefficient also.

So, now we have arrived here and we know the energy term. These are called energy reflection and transmission coefficients reflection and transmission coefficients. If you want to have total energy you have to get sum of it, ok. So, now, we know that if an electromagnetic wave is incident at an interface of two media at an oblique angle incidence, then its reflection and transmission is governed by these Fresnel equations and from there you can calculate the amplitude of the reflected and transmitted wave.

And, from all this exercise which we have done, you can arrive to the condition where you can calculate the energy transmission and reflection coefficients. And, let us see what happens at certain special cases when this reflection and transmission goes 0.

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$$r_p = \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1}$$

If numerator = 0  
 $r_p = 0$

$n_1 \cos \theta_2 - n_2 \cos \theta_1 = 0$   
 $\Rightarrow n_1 \cos \theta_2 = n_2 \cos \theta_1$

From Snell's Law,  
 $n_1 \sin \theta_1 = n_2 \sin \theta_2$

The slide also features a diagram of an interface between two media with incident, reflected, and transmitted rays, and a small video inset of a person in a lab setting.

So, we know that  $r_p$  is equal to  $n_1 \cos \theta_2$  minus  $n_2 \cos \theta_1$  divided by  $n_1 \cos \theta_2$  plus  $n_2 \cos \theta_1$ . If numerator is equal to 0, then  $r_p$  is equal to 0. What does it mean? It means that, for p-polarized light: p-polarized light means that the electric field component which is in the plane of the incident light will not be transmitted. So, there would not be any reflection for this electric field.

Let us see what happens. So,  $n_1 \cos \theta_2$  minus  $n_2 \cos \theta_1$  becomes equal to 0 this means  $n_1 \cos \theta_2$  is equal to  $n_2 \cos \theta_1$  - this is one condition. From Snell's law, we know that  $n_1 \sin \theta_1$  equal to  $n_2 \sin \theta_2$ . So, if we divide equation 1 to equation 2, what will happen?

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$$\begin{aligned}
 n_1 \sin \theta_1 &= n_2 \sin \theta_2 \quad \text{--- (1)} \\
 n_1 \cos \theta_2 &= n_2 \cos \theta_1 \quad \text{--- (2)} \\
 n_1 n_2 \sin \theta_1 \cos \theta_2 &= n_1 n_2 \sin \theta_2 \cos \theta_1 \\
 \sin 2\theta_1 &= \sin 2\theta_2 \\
 \Rightarrow 2\theta_1 &= \pi - 2\theta_2 \\
 \Rightarrow (\theta_1 + \theta_2) &= \frac{\pi}{2} \\
 n_1 \sin \theta_1 &= n_2 \sin (\pi/2 - \theta_1) = n_2 \cos \theta_1 \\
 \Rightarrow \frac{\sin \theta_1}{\cos \theta_1} &= \frac{n_2}{n_1} \Rightarrow \tan \theta_1 = \frac{n_2}{n_1}
 \end{aligned}$$

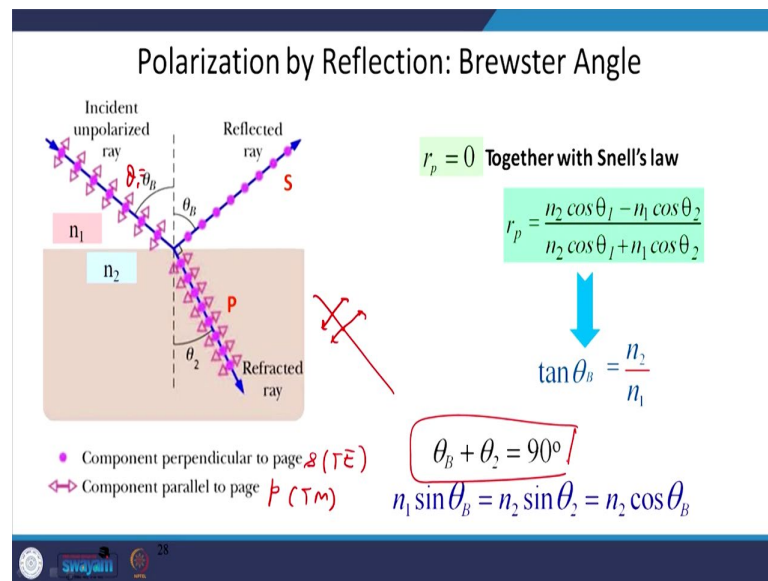
$\theta_1 \equiv \text{Brewster angle}$   
 when  $\theta_1 + \theta_2 = 90^\circ$  &  $r_p = 0$

So, let us see if we divide it then what will you get. Again, I am writing  $n_1 \sin \theta_1$  is equal to  $n_2 \sin \theta_2$  and you have  $n_1 \cos \theta_2$  equal to  $n_2 \cos \theta_1$ . So, you can have it like this is, suppose, equation 1, this is equation 2. You can have  $n_1 n_2 \sin \theta_1 \cos \theta_2$  is equal to  $n_1 n_2 \sin \theta_2 \cos \theta_1$ . So,  $n_1 n_2$  cancels out - you have  $\sin 2\theta_1 \sin 2\theta_2$  is equal to  $\sin 2\theta_2 \sin 2\theta_1$  is equal to  $\sin 2\theta_2$ ; when is it this possible? This implies that,  $2\theta_1$  is equal to  $\pi - 2\theta_2$  to satisfy this. This implies that  $\theta_1 + \theta_2$  is equal to  $\pi/2$ .

What does it mean? It means that, this angle  $\theta_2$  when light was incident -  $\theta_1 + \theta_2$  should be 90 degree. So, if you have this wave which is traveling and if you have  $\theta_1$ , you have  $\theta_2$  then you have all the light like this which is coming here, all the light gets transmitted - no light gets reflected. So, if it is  $\theta_1$ , basically this angle should be 90 degree. So,  $\theta_1 + \theta_2$  is equal to  $\pi/2$ . If you have  $n_1 \sin \theta_1$  is equal to  $n_2 \sin \pi/2 - \theta_1$  then; that means, is equal to  $n_2 \cos \theta_1$ .

So, it becomes like  $\sin \theta_1 \cos \theta_1 = n_2 / n_1$ ; this implies that  $\tan \theta_1$  is equal to  $n_2 / n_1$ . This  $\theta_1$  is called Brewster angle. So, this is called  $\theta_1$  is Brewster angle, when  $\theta_1 + \theta_2$  is equal to 90 degree and  $r_p$  is equal to 0. So, when  $r_p$  is equal to 0 it satisfies this condition - this is Brewster's condition and it is called Brewster's angle.

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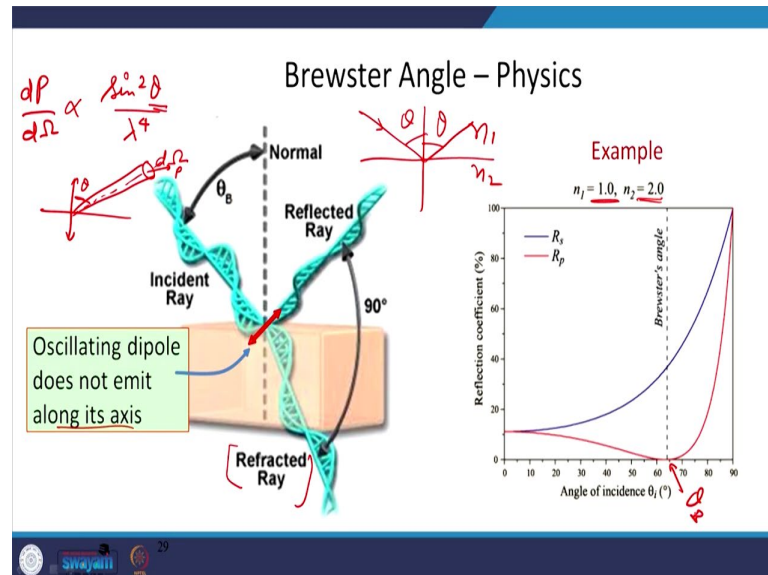
So, what happens? At Brewster angle  $r_p$  goes equal to 0 and you see that we can have this ray like this. You have electric field components in the plane and electric field components out of the plane. So, these ones - components perpendicular to the page and components parallel to the page. So, this one is parallel to the page - this is called p polarization, and this is called s polarization or TE. And this is TM - Transverse Magnetic.

So, you see that when the angle of incidence  $\theta_1$  is equal to  $\theta_B$  - the Brewster angle, all the p polarized light gets transmitted, it does not get reflected. Only s polarization gets reflected. And this was the condition we derived, and it was equal to 90 degree.

So, why it happens so? What is the reason behind this kind of transmission - complete transmission of light at Brewster angle, if you have p polarized light then all the light goes into the transmission medium: does not reflect back into the same medium. And this happens only when, this angle is 90 degree - means  $\theta_B + \theta_2$   $\theta_1 + \theta_2$

2 is equal to 90 degree. If this is 90 degree this is totally 180 degree from here to here. So, this is 90 degree what is the reason? So, the here is the Physics.

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You know that when light is incident on any medium I told you that how it propagates. So, when light gets transmitted through a medium what happens actually, that it excites dipoles. And the dipole oscillations: we discussed that power  $dP$  by  $d\Omega$  was proportional to  $\sin^2 \theta$  by  $\lambda^4$ , where this  $\theta$  was the angle made from the axis of the dipole. So, if this was the axis of the dipole and you want to measure here at an angle  $\theta$  and this was the solid angle if you remember  $d\Omega$  and wanted to see how much power it is here it was making from the axis actually.

So, at  $\theta$  is equal to 0, there is no power radiated and the maximum radiation goes in 90 degree to the dipole oscillations. So, if it is incident in such a way that reflected ray and transmitted refracted ray - these make 90 degree angle; that means, that the dipole is oscillating in such a way that it does not produce any radiation in this direction. So, all the light comes in that direction. That is a basic physics behind this. So, an oscillating dipole does not emit along its axis, all the light is going, that is why, into that ray. So, this is something very important. This is a very basic concept and most of the people forget; I also sometime forgot about this.

So, how does it look like when you have an interface, say, from  $n_1$  to  $n_2$  light is going like this and you increase the angle  $\theta$ , you keep on increasing the angle what will

happen? You want to measure the reflected light. That is how you perform the experiment for Brewster angle. This is also theta 1.

So, what happens actually that, when you start from 0 degree of angle of incidence for this particular condition when you have n 1 is equal to 1 and n 2 is equal to 2, the energy reflection coefficients R s and R p have been plotted here. And you can see that R s goes like - this this blue curve; while R p shows a dip here and this is because of the Brewster angle. So, at the Brewster angle theta B all the light gets transmitted and the reflection is 0.

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Can we do Sensing using Brewster Angle?

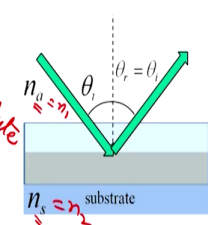
$\theta = f(n_a)$   
 $\frac{d\theta}{dn_a} = S$

$\tan \theta_B = \frac{n_s}{n_a}$

Use:  $\frac{d \tan x}{dx} = \frac{1}{\cos^2 x}$  To get:

$\frac{d \tan \theta_B}{dn_a} \cdot \frac{1}{\cos^2 \theta_B} \cdot \frac{d\theta_B}{dn_a} = -\frac{n_s}{n_a^2} \Rightarrow \frac{d\theta_B}{dn_a} = -\cos^2 \theta_B \frac{n_s}{n_a^2}$

$a = \text{analyte}$

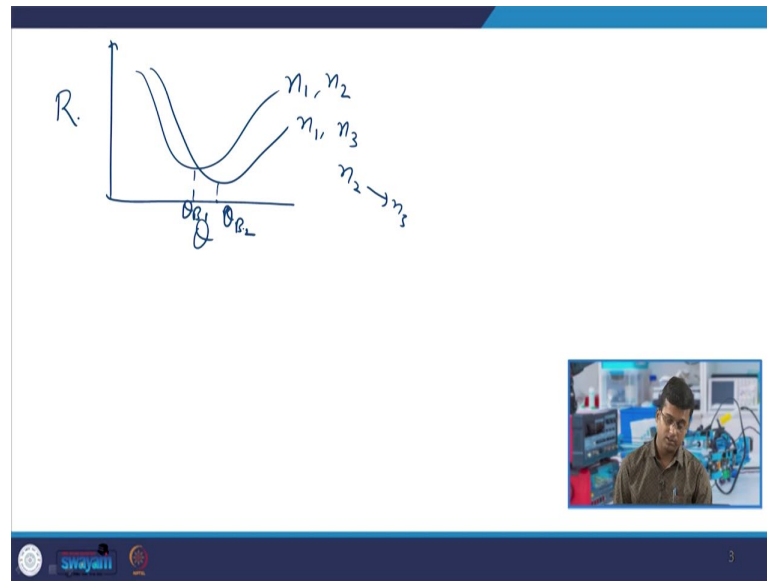


Sensitivity

$S = \frac{d\theta_B}{dn_a} = -\frac{1}{1 + \tan^2 \theta_B} \frac{n_s}{n_a^2} = -\frac{1}{1 + n_s^2/n_a^2} \frac{n_s}{n_a^2} = -\frac{n_s}{n_a^2 + n_s^2}$

So, can we do sensing using Brewster angle. How?

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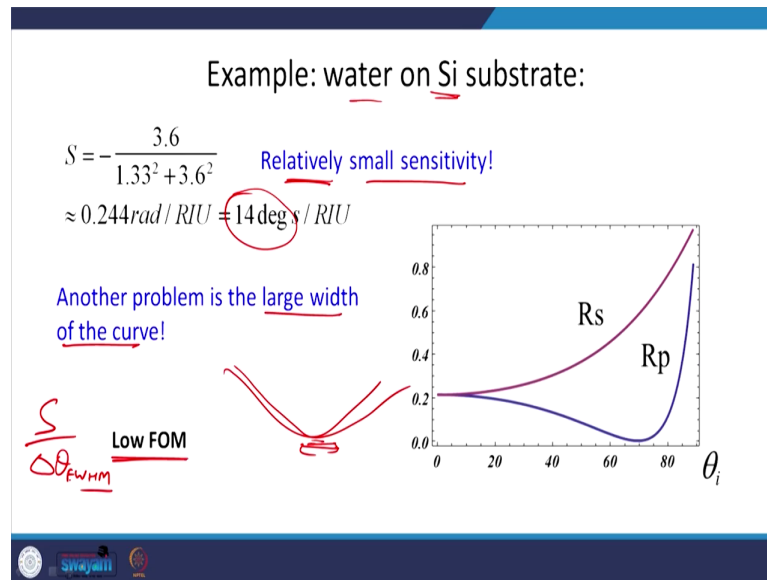
How do I say that - if you remember that when we were discussing sensors, it was shown that it has certain characteristic. Here I have theta and here I have reflected power and I want to see what happens? Say, suppose this is condition for  $n_1, n_2$ . Now, I just changed from  $n_2$  to  $n_3$ . Does it shift? Can I measure the shift?

The basic idea behind that is can we use it for sensing applications? That is the basic question and the answer is yes, we can use it. So,  $\tan \theta_B$  was given by  $n_s$  by  $n_a$ . Now, I have put it  $n_s$  was actually  $n_2$  and this is  $n_1$ . And now why I write a and s is like - s is for substrate and n a is for analyte, that is how I write. Analyte is the medium which we are trying to sense. So, I have already a substrate, suppose I have glass slide; I put a drop of water and I want to see the Brewster angle. If you have this relation, we know that if we are measuring theta as a function of  $n_a$ , then  $d\theta/dn_a$  will be the sensitivity. We want to calculate the sensitivity.

So, we can use it for sensing as I told you here that if we move from  $n_2$  to  $n_3$ , this Brewster angle  $\theta_{B1}$  will be  $\theta_{B2}$ . So, it can be done in a principle. But if it works as a sensor, what will be its sensitivity? That is the question. So, what you do is that, you take the derivative of this and derivative is given by this relation. You know that  $d \tan x / dx$  is equal to  $1 / \cos^2 x$  that is  $\sec^2 x$ . So, you can write  $d \tan \theta_B / dn_a$  into  $1 / \cos^2 \theta_B d\theta_B / dn_a$ .

So, you arrive to this relation. Somehow these have changed, actually, this has to be theta B. And what we see is that we get this relation ultimately that the sensitivity depends only on the refractive indices  $n_s$  and  $n_a$ .

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So, to take an example, we have put water on silicon substrate and you know that the sensitivity is around fourteen degrees per refractive index unit, which is very small. I will show you that the sensors have very high sensitivity. This is very poor sensitivity. Also there is a problem with the large width of the curve. I told you that if there is a very small change, suppose this curve is like this and then you have another curve which is like this, it is very difficult to find what is the change in the curve parameter due to the shift in the refractive index.

So, it has very small figure of merit. I hope that you remember how you define figure of merit - that was sensitivity was divided by delta, here it will be delta theta. So, if the delta theta means FWH, the theta FWHM is broad that means the figure of merit will be poor.

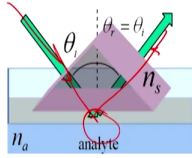
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Can we do Sensing using Brewster Angle? Incidence from the Substrate Side (prism)

$$\tan \theta_B = \frac{n_a}{n_s}$$

Use:  $\frac{d \tan x}{dx} = \frac{1}{\cos^2 x}$  To get:

$$\frac{d \tan \theta_B}{dn_a} \frac{1}{\cos^2 \theta_B} \frac{dn_a}{dn_a} = \frac{1}{n_s} \Rightarrow \frac{d \theta_B}{dn_a} = \cos^2 \theta_B \frac{1}{n_s}$$

$$S = \frac{d \theta_B}{dn_a} = - \frac{1}{1 + \tan^2 \theta_B} \frac{1}{n_s} = \frac{1}{1 + n_a^2 / n_s^2} \frac{1}{n_s} = \frac{n_s}{n_a^2 + n_s^2}$$


The same expression as before!

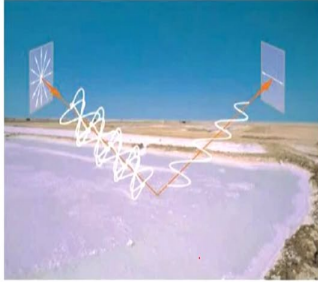

If we want to use it other way around like on a substrate we were putting a drop and we were shining from here. So, here was the analyte, which you do not prefer most of the time. Can we put light from here and see what happens and measure the reflectivity here? That can be attained by using a prism.

So, the analyte is from the other side and you shine from the prism side that goes here gets reflected from here and here is your analyte. So, you arrive to the same equation - only there is a minus sign in the previous one. So, the sensitivity is the same, it does not make any difference.

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### Bio-World and Brewster Angle

Brewster angle for the air/water interface is about 53deg., at which maximum polarization in reflection occurs !



R. Wehner, J. Experimental Biology, 204, 2589, 2001 Landscape by Sabkhat al Muh, south-east of Tadmur, Syria

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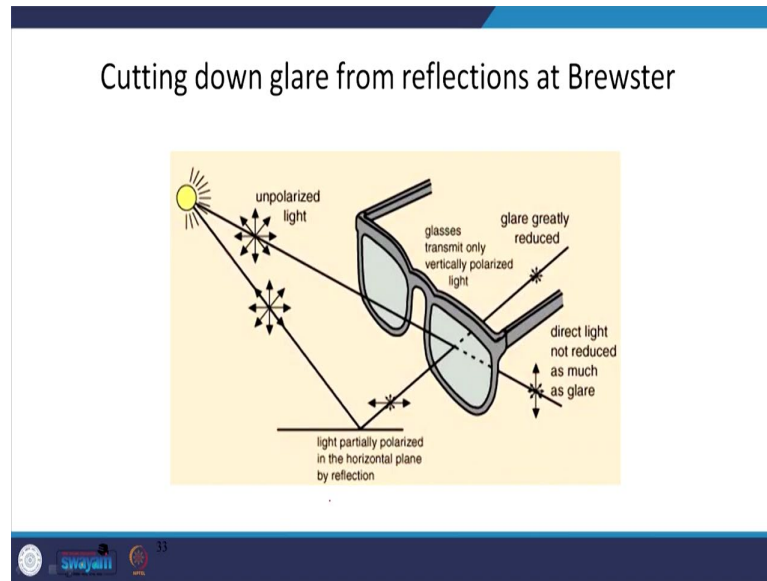
Water beetles, bugs and birds use this fact to detect bodies near the water surface – **depends on the sun's height !**

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Brewster angle for the air water interface is about 53.5 degrees at which maximum polarization by reflection occurs. So, you can see that when the angle is large, say, during the morning or evening times you have maximum polarization in reflection. So, sometimes you do not see, even, reflection only if you are using a p-polarized light.

Similarly, what can be shown here is that when you are looking at a grazing angle, at an angle about 53 degrees or so, you see only small reflections coming from. So, that is used basically in photography, that if you want to avoid speckles, you use these kinds of filters at this particular angle. Water beetles, bugs and birds use this fact to detect bodies near the water surface and, you can cut down the glare from reflections at Brewster angle.

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So, we studied polarization by reflection at Brewster angle and the potential use and limitations of Brewster angle for sensing applications we are presented.

Thank you.