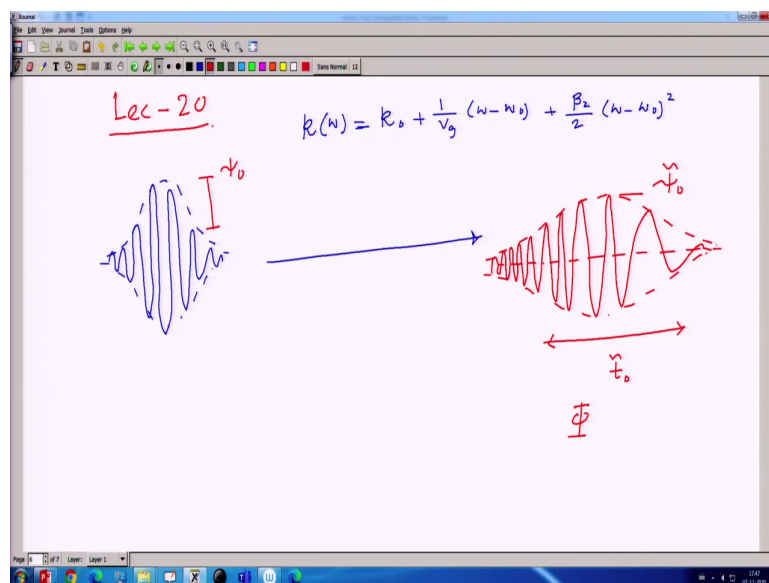


Physics of Linear and Non-Linear Optical Waveguides
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Module - 03
Modes
Lecture - 20
Concept of Modes

Hello student to the new class of Physics of Linear and Non-Linear Optical Waveguide. Today we will going to have lecture number 20 where we are going to understand Concept of Mode. And in the concept of mode is very important in understanding how the field will going to distribute in a given waveguide structure.

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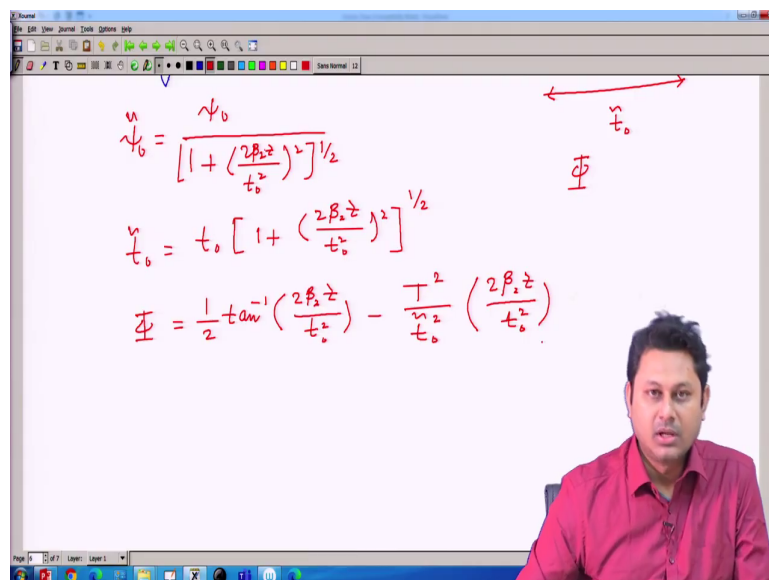


Today we have lecture 20, where we will going to learn modes, but before that let me remind once again what we have done, one concept is still we need to understand. So, in the last class, let me remind quickly if I have a dispersion with k with this form.

As a consequence of this k as a function of ω in this form I have a broadening of pulse. If this is my input pulse, it is moving through the dispersive medium defined by this k and in the output I have a pulse say something like this.

A broadened envelope not only that I may have some kind of chirping here chirping mean there is a phase associated with that. So, amplitude will going to decay this is ψ_0 and now I have according to our notation ψ_0 tilde with we will going to increase t_0 tilde. And also there will be a distribution because I have a ϕ extra ϕ , if you remember I have a phase and rate of change of phase is chirping, the frequency and rate of change of frequency is chirping. So, I may have some kind of chirping there will be a distribution of the frequency inside this pulse as well.

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The whiteboard contains the following handwritten equations:

$$\tilde{\psi}_0 = \frac{\psi_0}{\left[1 + \left(\frac{2\beta_2 z}{t_0^2}\right)^2\right]^{1/2}}$$

$$\tilde{t}_0 = t_0 \left[1 + \left(\frac{2\beta_2 z}{t_0^2}\right)^2\right]^{1/2}$$

$$\Phi = \frac{1}{2} \tan^{-1} \left(\frac{2\beta_2 z}{t_0^2} \right) - \frac{T^2}{\tilde{t}_0^2} \left(\frac{2\beta_2 z}{t_0^2} \right)$$

There is also a diagram of a pulse with a double-headed arrow labeled \tilde{t}_0 and the symbol Φ below it.

If I write down this value once again then things will be clear. So, my ψ_0 was ψ_0 divided by $1 + 2\beta_2 z$ divided by t_0^2 whole square and whole to the power half my \tilde{t}_0 is t_0 $1 + 2\beta_2 z$ divided by t_0^2 whole square and half. And another term Φ which was half of \tan^{-1} of $2\beta_2 z$ divided by t_0^2 minus T^2 square divided by \tilde{t}_0^2 of $2\beta_2 z$ divided by t_0^2 .

These were the 3 values that we evaluated in the last class. The important thing that you need to note that when β_2 equal to 0 then there will be no change of the pulse have at all.

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Handwritten equations on the whiteboard:

$$t_b = t_0 \left[1 + \left(\frac{t_0}{t_b} \right)^2 \right]$$

$$\Phi = \frac{1}{2} \tan^{-1} \left(\frac{2\beta_2 t}{t_0^2} \right) - \frac{T^2}{t_0} \left(\frac{2\beta_2 t}{t_0^2} \right)$$

Conditions listed:

1. $\beta_2 = 0$
2. $\beta_2 > 0 \rightarrow \text{Normal dispersion}$
3. $\beta_2 < 0 \rightarrow \text{Anomalous dispersion}$

But you may remember there are three conditions of beta 1 is beta 2 is equal to 0 another is beta 2 is greater than 0. And another condition one can have is beta 2 is less than 0, this we know what we call is normal dispersion.

When beta 2 is less than 0, we know this situation is anomalous dispersion these two conditions one can have. If you look very carefully to this equation here we have a square term in amplitude. So, if beta is positive and if beta is negative in both the cases it will not go to change. So, that means, amplitude will go to decay even for beta positive and negative. In this term also I have a square here.

So, t_0 which basically the width of the optical pulse envelope, it will also go to increase irrespective of the sign of the beta it may be positive it may be negative depending on the situation, but in both the cases there will be an increment of pulse width. However, you

can see here there is a β_2 is sitting in such a way that it depends very much on the sign. So, that means, the distribution I just talked about that inside the pulse there should be some frequency distribution and this frequency distribution can be very much depends on the value of β_2 .

If it is anomalous dispersion then I have a negative sign and this negative sign makes this ϕ negative, if I have a positive sign then ϕ can have a different values. So, it is a combination of plus minus anyway. So, but the point is if β_2 is positive or β_2 is negative depending on that ϕ will going to modify. So, there will be a change of the frequency distribution here that you should know because this is very important in understanding something called optical soliton we will like to cover this part as well in this course.

Where these things can be compensated under non-linearity, how these things will going to be compensated under non-linearity? Then this concept you need to remember that under the dispersion there is a situation where the phase will going to modify depending on the sign of β_2 . Well after that we need to understand about the condition first condition β_2 equal to 0 this is called the 0 dispersion this is a very very important concept in the pulse propagation problem.

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3. $\beta_2 < 0 \rightarrow$ Anomalous dispersion

- Concept of zero-dispersion

When $\beta_2 = D_m = 0 \rightarrow$ zero GVD.

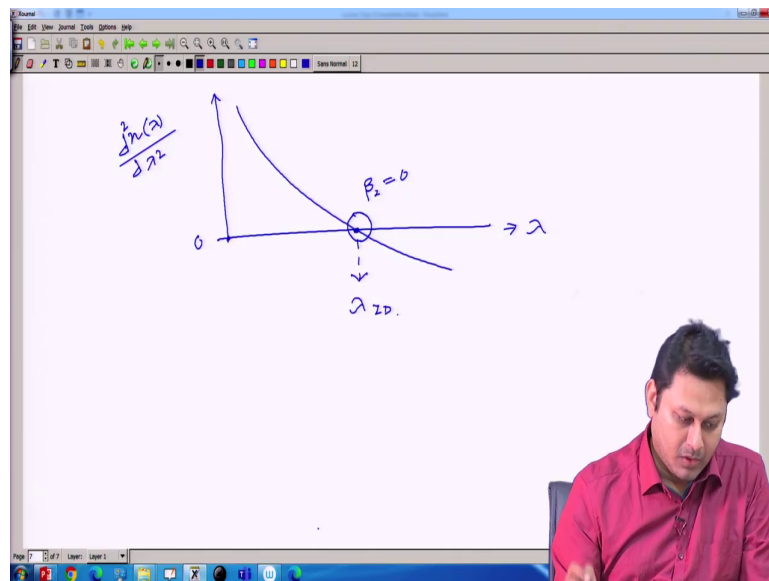
$\beta_2 \rightarrow D_m \rightarrow \left[\frac{d^2 n}{d\lambda^2} \right]$

zero GVD. $\left\{ \begin{array}{l} \beta_2 = 0 \\ D_m = 0 \end{array} \right. \rightarrow \frac{d^2 n}{d\lambda^2} = 0$

So, it is called let me write it as concept of zero dispersion nothing special. We already know that when beta 2 or material dispersion D_m is 0, we can say that it is called the zero group velocity dispersion. If you remember that beta 2 the expression of the beta 2 and in expression of the D_m in both cases we have a common term that $\frac{d^2 n}{d\lambda^2}$ that was the common term in both the cases. So, when I am saying that beta 2 equal to 0 or D_m equal to 0 for zero group velocity dispersion condition.

That essentially means that my $\frac{d^2 n}{d\lambda^2}$ this term is 0 that is the very very important condition here. Whenever I have a wavelength for which this double derivative is 0 then this is called the 0 dispersion wavelength.

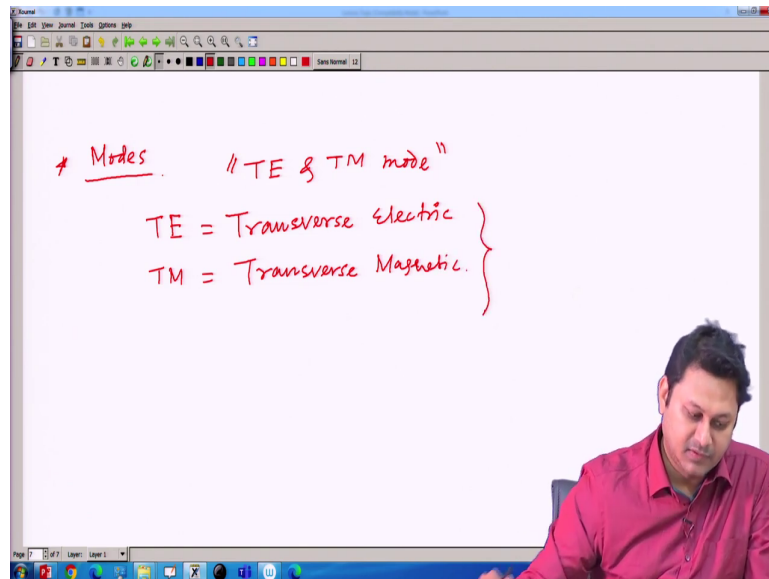
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So, if I now plot my say $\frac{d^2n}{d\lambda^2}$ which is a function of λ and λ^2 . So, at certain wavelength there is a possibility that it cut the 0 point, so this is 0. So, when it cut the 0 point this suppose this is my λ when it cut the 0 point this λ we call the 0 dispersion wavelength. That means, at that particular wavelength or at that particular λ I have my β_2 the consequence is β_2 is 0 and there will be no such pulse dispersion and that particular wavelength that is interesting thing.

So, if I launch a pulse at exactly at that particular point where $\frac{d^2n}{d\lambda^2}$ and λ^2 is 0. Then what happened there should not be any kind of pulse broadening. So, we need to achieve such an certain condition, so that I can reduce the pulse. So, if I make this β_2 low enough or small enough then I can restrict these things. So, the dispersion can be restricted [vocalized- noise].

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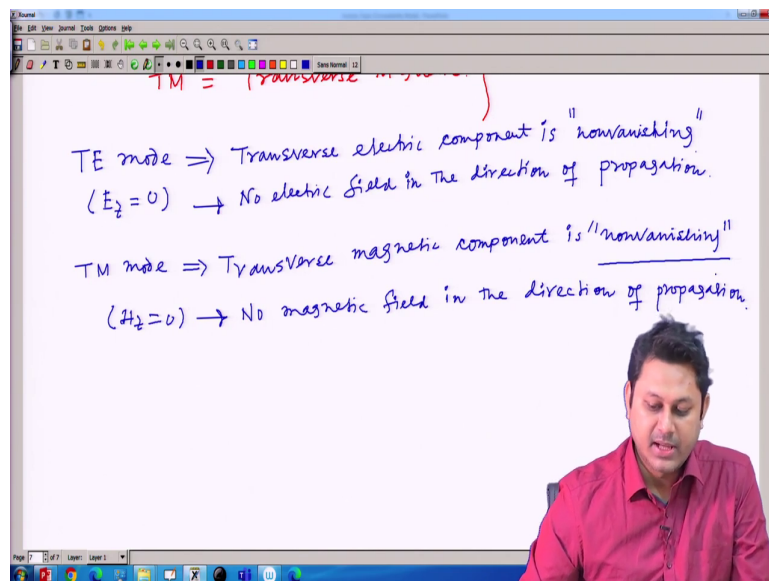
So, that is the thing we [vocalized- noise] at this point we need to know. Next we will going to start today's main topic that I mentioned, that the concept of modes which is very very important. So, let me start with modes. So, before so let me write two term terminology TE and TM modes. I will explain this in detail TE and TM modes. In optical wave guide we will find that when I launch an optical electromagnetic field, then because of the geometry of this optical wave guide certain distribution is there in the field.

So, this certain distribution is in general called the modes of this waveguides. So, we learn this in detail for different geometries for planar waveguide, how the mode will look like and for the cylindrical geometry which we find in optical fiber how the mode will look like. And also we should have something called mode equations.

So, how the mode equation can be evaluated from the fundamental principle like Maxwell's equation that we also going to learn in this course. At this moment we should only mention that if a geometry is given, which we called the waveguide geometry and if I excite an electromagnetic field inside this geometry.

Then this geometry guide a certain amount certain field distribution, the certain field distribution is in general called the mode we term two kind of modes we term here TE and TM mode. So, let us understand what is the meaning of this TE and TM mode. So, TE is coming the term T is for term transverse E stands for electric, TM stands for transverse magnetic.

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So, transverse electric and transverse magnetic. So, what is the meaning of transverse electric mode and transverse magnetic mode? So, TE mode ok, let me change my ink color. So,

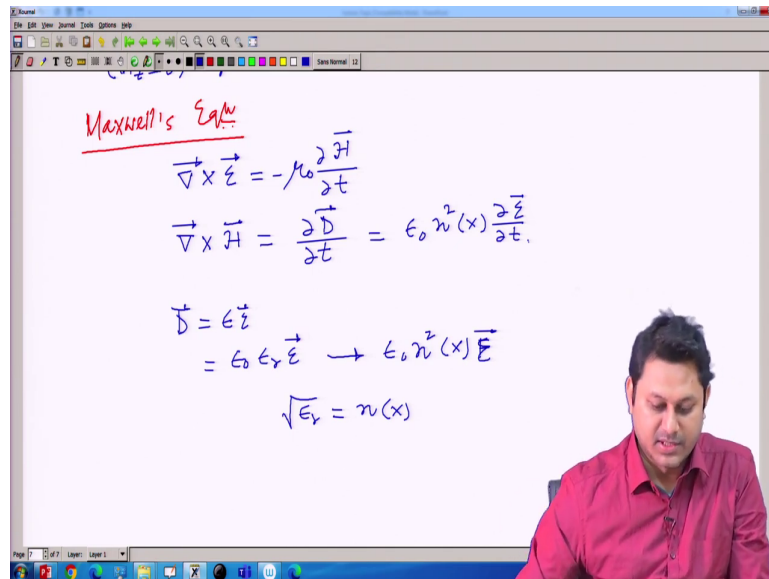
transverse electric mode its means that the transverse electric component is non-vanishing is non-vanishing.

That means if the transverse component is non vanishing and at the same point, if z is a propagation distance the propagation direction then this will be 0. So, no electric field in the direction of propagation no electric field in the direction of propagation.

So, if z is a direction of propagation. So, we should not have E_z component if I have a mode with this structure that E_z is not there, then we can say that this mode is TE mode. In the similar way I can have something called TM mode.

So, TM mode means transverse magnetic component is non-vanishing. So, it is non-vanishing and the transverse magnetic field is non-vanishing. So; that means, here also we have the H_z component is equal to 0. So, no that means, no magnetic field in the direction of propagation ; no magnetic field in the direction of propagation. Well, now we understand roughly what is the meaning of TE and TM modes. Modes I already mentioned that it is a distribution and the field distribution inside a given magnetic in given wave guide. So, we will going to understand in detail.

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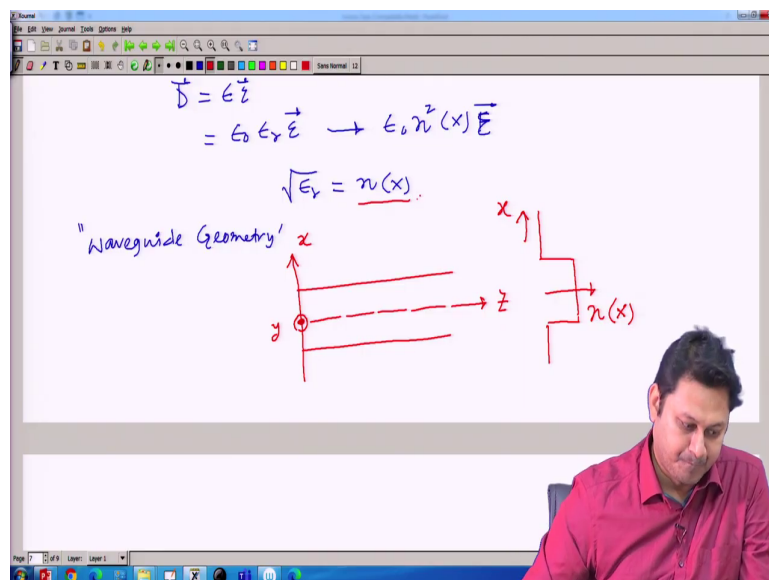
Maxwell's Eqn.

$$\vec{\nabla} \times \vec{E} = -\mu_0 \frac{\partial \vec{H}}{\partial t}$$
$$\vec{\nabla} \times \vec{H} = \frac{\partial \vec{D}}{\partial t} = \epsilon_0 n^2(x) \frac{\partial \vec{E}}{\partial t}$$
$$\vec{D} = \epsilon \vec{E}$$
$$= \epsilon_0 \epsilon_r \vec{E} \rightarrow \epsilon_0 n^2(x) \vec{E}$$
$$\sqrt{\epsilon_r} = n(x)$$

So, let us start with Maxwell's equation. So, Maxwell's equation tells me that the first equation I will going to use these two equation, curl of curly E is equal to minus of mu 0 then del curly H del t this is a one equation. And curl of curly H this one is the Faradays first one is a Faradays law I just write in terms of curly E and curly H. What is the meaning of curly E and curly H? We will going to learn we will going to see it is d of d delta of D d t.

Now, D is epsilon then E, which is epsilon 0 epsilon r E. So, from here I can write it is epsilon 0 n square x E, why it is n square x? I will explain. Where my root over of epsilon r is refractive index considering refractive is a function of x only in one direction. So, why it is that? We will going to explain. So, this equation I can write it as simply epsilon 0 then n square x dt. So, these two equation I start with and then try to understand more. So, as I mentioned that the value n is a function of x.

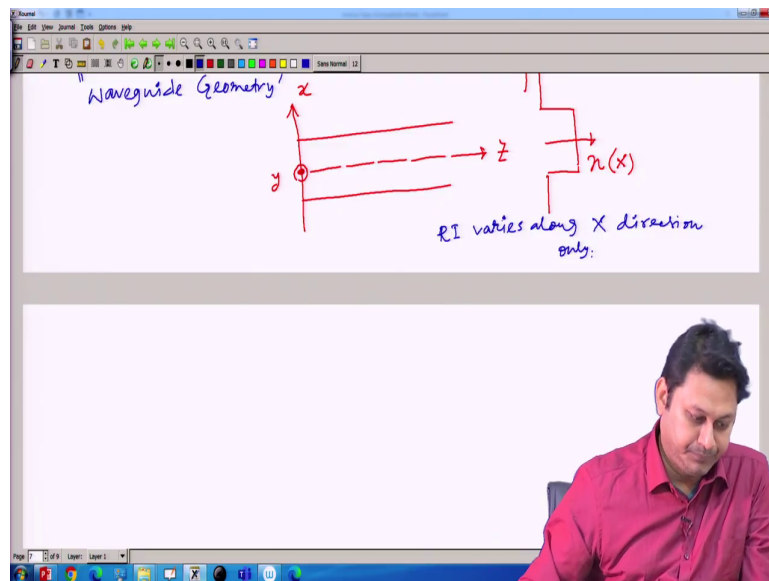
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So, the waveguide geometry I need to define for which this condition is valid. So, my waveguide geometry is something like this. So, I have a block like this, this is a known waveguide geometry rather along this axis I say this is my x y axis is perpendicular to the plane and along this direction I have my z the propagation direction. So, the refractive index profile is like a step index profile. So, along this direction I have x . So, it is changing along x direction.

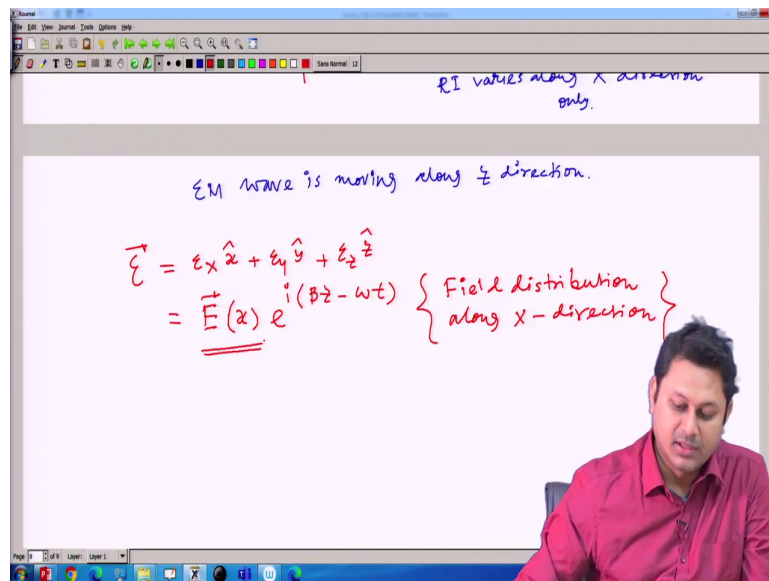
So, refractive index whatever the refractive index I have is only a function of x along z direction or along y direction there is no change. That is why I wrote here that n is a function of x only.

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So, refractive index RI varies along x direction only well.

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An EM wave is moving along z direction. So, now, I will write my electric field the curly E as this way, E_x x unit vector plus E_y y unit vector plus E_z z unit vector.

And I can also write these as E vector which is a function of x e to the power of i beta z minus omega t. So, I write an electric field in this form. So, field distribution, so this is field distribution along X direction. So, this is a field distribution along X direction. So, this is a special geometry for which I considered my electric field is varying along X direction and I will going to show that in which condition it is correct, under which condition I can write that.

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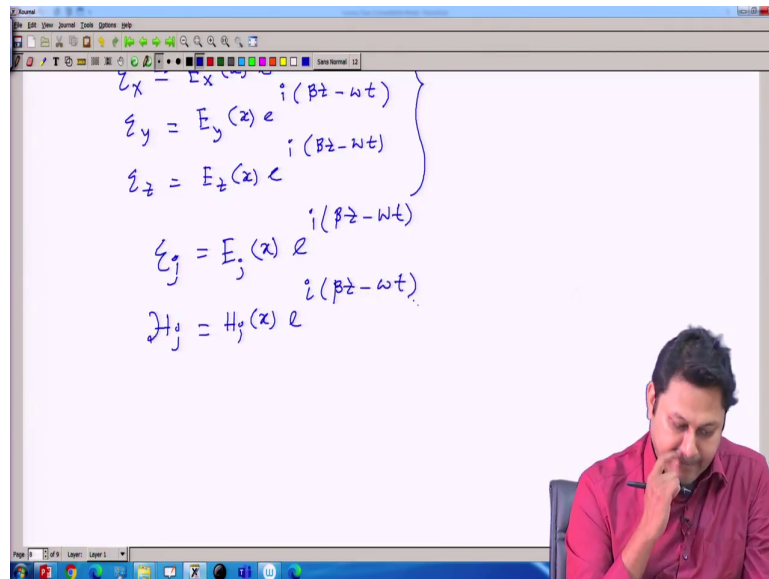
$$= \underline{\underline{\vec{E}(x)}} e^{i(\beta z - \omega t)} \quad \left\{ \begin{array}{l} \text{Field distribution} \\ \text{along } x\text{-direction} \end{array} \right\}$$

$$\left. \begin{array}{l} E_x = E_x(x) e^{i(\beta z - \omega t)} \\ E_y = E_y(x) e^{i(\beta z - \omega t)} \\ E_z = E_z(x) e^{i(\beta z - \omega t)} \end{array} \right\}$$

So, my let me write it component wise. So, how the component will look like E x component will be E x component will be E of x as a function of x e to the power of I because it is a scalar quantity. So, it will be like omega t.

In the similar way E of y is E of y x e to the power of i beta z minus omega t. In the similar way E z curly E z is E of z that is also a function of x e to the power i beta z minus omega t. So, this is the way one can define the E x, E y, E z component.

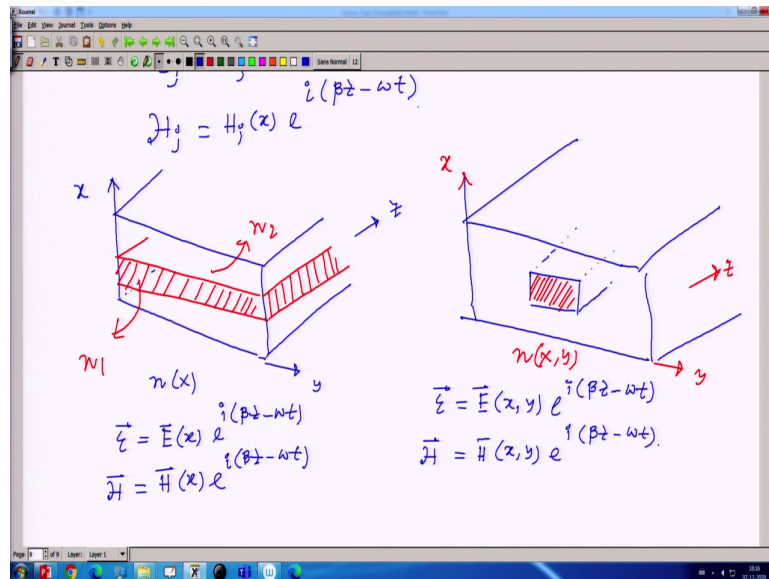
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$$\begin{aligned} E_x &= E_x(z) e^{i(\beta z - \omega t)} \\ E_y &= E_y(z) e^{i(\beta z - \omega t)} \\ E_z &= E_z(z) e^{i(\beta z - \omega t)} \\ H_x &= H_x(z) e^{i(\beta z - \omega t)} \\ H_y &= H_y(z) e^{i(\beta z - \omega t)} \\ H_z &= H_z(z) e^{i(\beta z - \omega t)} \end{aligned}$$

So, in general if I write the i th component is the i th component rather j th component because there is already one i sitting as exponential e to the power i . So, e to [vocalized- noise] e to the power $i\beta z - \omega t$ and H_j component H_j is H of j x e to the power of $i\beta z - \omega t$.

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So, the geometry I was mentioning. So, let me quickly define the geometry and then I will going to conclude the class. So, if I have a geometry like this, along this axis I have x, along this axis I have y and this is my z direction and I have a. So, here the refractive index is different. So, in this regime I have refractive index say n 1 and other part it is n 2.

So, this at this regime there is a change of refractive index like this. So, here I have say refractive index n 1 and in this region I have refractive index n 2 for this kind of structure when it is extended infinitely along y direction, if that is the case.

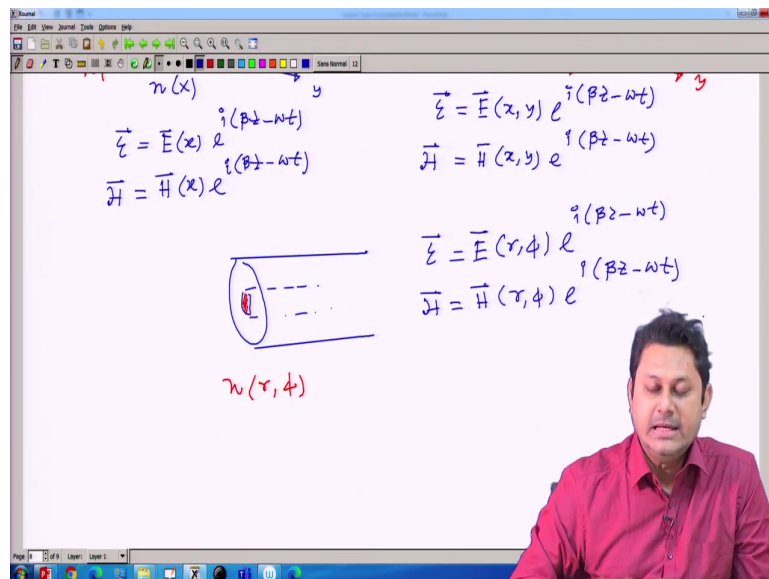
I can write, so n is a function of x; obviously, because it is changing along x direction. So, my electric field can be written in terms of E as a function of x because the distribution in on this direction, this direction there will be no distribution and this direction the pulse is

propagating. So, I can write the distribution in this way or my H will be $H \times e^{i(\beta z - \omega t)}$.

On the other hand if I have a structure like this similar structure, but here I have a block that is inside the system. And the refractive index is now function of x . So, along this direction I have x , along this direction I have y , along this direction I have z and this is the place where the refractive index is varying. So, refractive index is no more a function of x it is a function of x and y both.

So, there is a restriction over y as well. In this case if I now write my E it should be E because the field now we are going to distribute in x and y both direction, it will be distributed in x and y . So, there will be a variation of electric field in both x and y direction. So, it should be a function of x and y .

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The whiteboard contains the following handwritten content:

- Top left: $n(x)$ with an arrow pointing to the y axis.
- Left side equations:

$$\vec{E} = \vec{E}(x) e^{i(\beta z - \omega t)}$$

$$\vec{H} = \vec{H}(x) e^{i(\beta z - \omega t)}$$
- Right side equations:

$$\vec{E} = \vec{E}(x, y) e^{i(\beta z - \omega t)}$$

$$\vec{H} = \vec{H}(x, y) e^{i(\beta z - \omega t)}$$
- Bottom right equations:

$$\vec{E} = \vec{E}(x, y) e^{i(\beta z - \omega t)}$$

$$\vec{H} = \vec{H}(x, y) e^{i(\beta z - \omega t)}$$
- Diagram: A cylinder with a red rectangular block inside. Below the cylinder is the label $n(x, y)$ in red.

Also it is not restricted with this geometry another kind of geometry is possible which is very important, which is the optical fiber. So, in optical fiber we know that my geometry is something like this. So, the refractive index is changing here. So, my refractive index is a function of r and ϕ . So, here I can write my electric field in this structure as E as a function of r ϕ $e^{i(\beta z - \omega t)}$ and my H as $H(r, \phi) e^{i(\beta z - \omega t)}$.

So, today we do not have much time to go forward. So, I will going to conclude my class here. So, in the next class we will study in detail about the mode distribution and calculate the mode for a very simple planar waveguide. And till then I will thank you for your attention and hope we will again have in the next class all this mode distribution and all these things.

Thank you.