

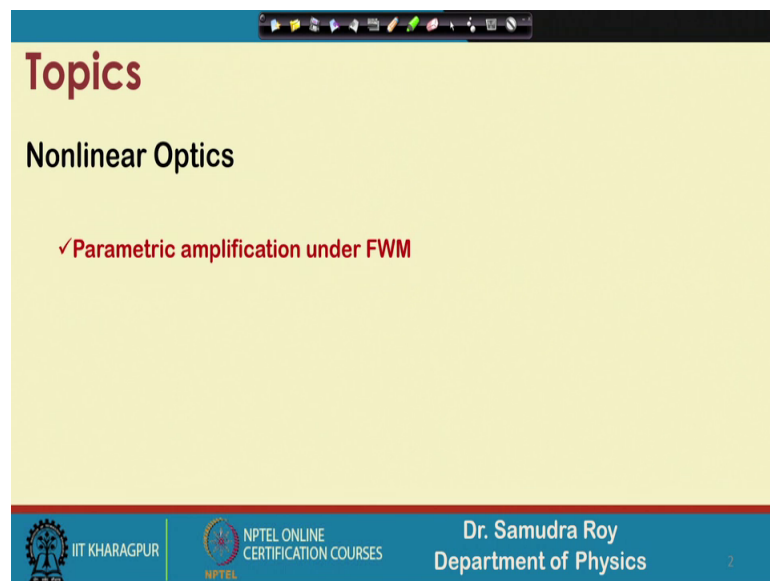
Introduction to Non-Linear Optics and Its Applications
Prof. Samudra Roy
Department of Physics
Indian Institute of Technology, Kharagpur

Lecture – 51
Parametric Amplification Under FWM

So welcome student to the new class of introduction of Non-Linear Optics and Its Application. So, today we have lecture number 51. So, in the previous lecture, we discussed about four wave mixing and generation of cross phase cross talk frequencies, how the crosstalk frequencies can be generated with making some phase matching condition which is Δk is equal to 0.

So, today we will learn more about the four wave mixing because this is a fascinating process and how this process is used to amplify a signal that we will going to learn today. So, today our topic will be Parametric Amplification under Four Wave Mixing.

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Topics

Nonlinear Optics

✓ **Parametric amplification under FWM**

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So, parametric amplification means we launched the parametric amplification process we have already learned in the second order effect where we launch a light and another signal is there and we call this light is a pump light. And because of these non-linear interaction what happened? The there is the increment of this signal also another wave is generating which is called the idler wave and this was entirely a K^2 effect; that means, the second order effect.

So, only two waves are mixed there to generate the third one or amplify one of them. Today we will going to learn a similar kind of process, but instead of having two wave; we have interaction instead of having the second order interaction, we have the third order interaction. So, the interaction will be now not restricted with the two wave we will have three wave; however, this three wave not necessarily be distinct to each other. If two waves are launched, then there will be mixing of these two wave in such a way that one wave can come twice and we will generate a four wave mixing kind of stuff.

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FWM: Sum Frequency

ω_3
 ω_2
 ω_1

$\chi^{(3)} \neq 0 \rightarrow \omega_4 = \omega_1 + \omega_2 + \omega_3$

Virtual State
 $\hbar\omega_3$
 $\hbar\omega_2$
 $\hbar\omega_1$
Ground State

$\omega_4 = \pm\omega_1 \pm \omega_2 \pm \omega_3$

Momentum conservation

$\vec{k}_1, \vec{k}_2, \vec{k}_3, \vec{k}_4$

$$\nabla^2 E^{(\omega_4)} - \mu_0 \epsilon(\omega_4) \frac{\partial^2 E^{(\omega_4)}}{\partial t^2} = \mu_0 \frac{\partial^2 P_{NL}^{(4)}}{\partial t^2}$$

$$2ik_4 \frac{dE_4}{dz} e^{i(k_4 z - \omega_4 t)} = -\frac{6}{4} \mu_0 \epsilon_0 \omega_4^2 \chi^{(3)} E_1 E_2 E_3 e^{i(k_1 + k_2 + k_3)z - i\omega_4 t}$$

$$\Delta k = k_4 - (k_1 + k_2 + k_3)$$

$$\frac{dE_4}{dz} = i \frac{3\omega_4 \chi^{(3)}}{4 n_4 c} E_1 E_2 E_3 e^{-i\Delta k z}$$

$$\frac{dE_3}{dz} = i \frac{3\omega_3 \chi^{(3)}}{4 n_3 c} E_4 E_1^* E_2^* e^{i\Delta k z}$$

$$\frac{dE_2}{dz} = i \frac{3\omega_2 \chi^{(3)}}{4 n_2 c} E_4 E_1^* E_3^* e^{i\Delta k z}$$

$$\frac{dE_1}{dz} = i \frac{3\omega_1 \chi^{(3)}}{4 n_1 c} E_4 E_3^* E_2^* e^{i\Delta k z}$$

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So, let us try to find out what we try to say here. In Four Wave Mixing, there are different kind of categories because the generation of the frequencies are large. So, this is a typical example of some frequency generation. So, what is happening here, I am launching 3 fields with frequency omega 1, omega 2 and omega 3 as shown in here. K 2 is not equal to 0; that means, we should have a non-linear interaction between these frequencies, this non-linear interaction will be of the order 3.

So, E cube term is will be associated with that. So, when cube term is associated with that so we will have the combination of frequency. So, this is a very specific combination the sum, simply the sum of all frequencies whatever the frequencies we launch. We should have a 4 frequency omega 4 which is sum of omega 1, omega 2 and omega 3. You should always remember that omega 4 in general can be generated in this many waves plus minus of omega 1, plus minus of omega 2, plus minus of omega 3. So, these are the

numbers there are huge numbers I think this is a 8 different combination. You can consider and omega 4 can be generated with 8 different configuration, if we consider omega 1, omega 2, omega 3 are distinct.

So, among this eight configuration or frequencies, we choose a particular frequencies which is just omega 1 plus omega 2 plus omega 3 which is this one. If I want to generate a frequency omega 4 which is sum of all the frequencies under this Four Wave Mixing process, then the corresponding energy diagram will be simple like this.

So, omega 1, omega 2, omega 3 these are the 3 frequencies that will merge each other and generate a omega 4 frequencies the energy conservation is $h \times \omega_1 + h \times \omega_2 + h \times \omega_3$ with a plus sign. So, $h \times \omega_1 + h \times \omega_2 + h \times \omega_3$ is simply cross to $h \times \omega_4$, which is this equation; this is the energy conservation.

But at the same time if I consider the momentum conservation, then I can write that k_1 , k_2 and k_3 are the propagation constant or the wave vectors of the photon with frequency omega 1, omega 2 and omega 3. And they will sum up and generate another photon with a frequency omega 4 whose wave vector is moving in k_4 direction.

So, this momentum conservation figure suggests that the phase matching may not be collinear. So this is a non collinear kind of phase matching that is possible or normally this is the case. As far as the equations are concerned, so we already solved this equation in the previous class.

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FWM: Sum Frequency

ω_3
 ω_2
 ω_1 → $\chi^{(3)} \neq 0$ → $\omega_4 = \omega_1 + \omega_2 + \omega_3$

Virtual State
 $\hbar\omega_3$
 $\hbar\omega_2$
 $\hbar\omega_1$
Ground State

Momentum conservation
 \vec{k}_1
 \vec{k}_2
 \vec{k}_3
 \vec{k}_4

$$\nabla^2 E^{(\omega_4)} - \mu_0 \epsilon(\omega_4) \frac{\partial^2 E^{(\omega_4)}}{\partial t^2} = \mu_0 \frac{\partial^2 P_{NL}^{(4)}}{\partial t^2}$$

$$2ik_4 \frac{dE_4}{dz} e^{i(k_4 z - \omega_4 t)} = -\frac{6}{4} \mu_0 \epsilon_0 \omega_4^2 \chi^{(3)} E_1 E_2 E_3 e^{i(k_1 + k_2 + k_3)z - i\omega_4 t}$$

$$\Delta k = k_4 - (k_1 + k_2 + k_3)$$

$$\frac{dE_4}{dz} = i \frac{3\omega_4 \chi^{(3)}}{4n_4 c} E_1 E_2 E_3 e^{-i\Delta k z}$$

$$\frac{dE_3}{dz} = i \frac{3\omega_3 \chi^{(3)}}{4n_3 c} E_4 E_1^* E_2^* e^{i\Delta k z}$$

$$\frac{dE_2}{dz} = i \frac{3\omega_2 \chi^{(3)}}{4n_2 c} E_4 E_1^* E_3^* e^{i\Delta k z}$$

$$\frac{dE_1}{dz} = i \frac{3\omega_1 \chi^{(3)}}{4n_1 c} E_4 E_2^* E_3^* e^{i\Delta k z}$$

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This is the starting equation; that means the non-linear Maxwell's equation. So, this non-linear Maxwell equation, we have a source term the procedure is exactly identical that we have been using. From that we now put E and when I put E omega and P NL omega, I will have evolution equations of this. So, P non-linear omega will contain omega 4 frequencies. So, that is why E 1, E 2, E 3 will be here.

And eventually we will be having differential equation for 4 fields E 1, E 2, E 3 and E 4. E 4 is more important and in E 4, I find that it is associated with E1, E 2, E 3. So these are the source terms. So, these are the coupled equation. So, if I want to solve this coupled equation we need to check that how this equation can be solved. It will be not that easy, but in principle we can solve this coupled equation numerically and find out how this field will be evolving.

(Refer Slide Time: 06:45)

FWM: Parametric Amplification

$\omega_1 + \omega_2 = \omega_3 + \omega_4$ ✓

$\chi^{(3)} \neq 0$

Virtual State

Ground State

Momentum conservation

$\vec{k}_1 + \vec{k}_2 = \vec{k}_4 + \vec{k}_3$ ✓

$$E^{(\omega_1)} = \frac{1}{2} (E_1 e^{i(k_1 z - \omega_1 t)} + c.c)$$

$$E^{(\omega_2)} = \frac{1}{2} (E_2 e^{i(k_2 z - \omega_2 t)} + c.c)$$

$$E^{(\omega_3)} = \frac{1}{2} (E_3 e^{i(k_3 z - \omega_3 t)} + c.c)$$

$$E^{(\omega_4)} = \frac{1}{2} (E_4 e^{i(k_4 z - \omega_4 t)} + c.c)$$

$$E_T = (E^{(\omega_1)} + E^{(\omega_2)} + E^{(\omega_3)} + E^{(\omega_4)})$$

$$P_{NL} = \epsilon_0 \chi^{(3)} E_T^3$$

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Now, we will go to the next thing which is Parametric Amplification. So, some frequency generation is one kind of Four Wave Mixing, but parametric amplification is quite interesting, where omega 1 and omega 2 are launched and we are getting omega 4 and omega 3 at the output. So we are launching two frequencies omega 1 and omega 2 and we are getting omega 3 and omega 4.

So, here the energy relation is or the energy diagram is something like this omega 1 and omega 2 are merge to generate omega 3 and omega 4. So, this is the energy conservation equation. Similarly in the momentum conservation equation is also like something. So momentum conservation equation suggests $k_1 + k_2$ has to be equal to $k_4 + k_3$. So, this is the figure of momentum conservation.

Now, I want to find out in parametric amplification how this omega 4 and omega 3 will going to evolve and the concept is if I now launch something here, small signal omega 3 this omega 3 will be amplified because omega 3 will be generated inside this four wave this under Four Wave Mixing this parametric process. Also omega 4 can be evolved. So, I can amplify certain signal having frequency omega 3 and omega 4.

(Refer Slide Time: 08:03)

FWM: Parametric Amplification

$\omega_1 + \omega_2 = \omega_3 + \omega_4$

$\chi^{(3)} \neq 0$

Virtual State

Ground State

Momentum conservation

$$E^{(\omega_1)} = \frac{1}{2} (E_1 e^{i(k_1 z - \omega_1 t)} + c.c)$$

$$E^{(\omega_2)} = \frac{1}{2} (E_2 e^{i(k_2 z - \omega_2 t)} + c.c)$$

$$E^{(\omega_3)} = \frac{1}{2} (E_3 e^{i(k_3 z - \omega_3 t)} + c.c)$$

$$E^{(\omega_4)} = \frac{1}{2} (E_4 e^{i(k_4 z - \omega_4 t)} + c.c)$$

$$E_T = (E^{(\omega_1)} + E^{(\omega_2)} + E^{(\omega_3)} + E^{(\omega_4)})$$

$$P_{NL} = \epsilon_0 \chi^{(3)} E_T^3$$

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So, let us try to find out how the field equations one can generate which is again the similar process. The starting point is to define our electric field of E 1, E 2, E 3 and E 4 where E 1, E 2, E 3, E 4 are the corresponding frequencies the field of the corresponding frequencies omega 1, omega 2, omega 3 and omega 4.

(Refer Slide Time: 08:40)

FWM: Parametric Amplification

$\omega_1 + \omega_2 = \omega_3 + \omega_4$

$\chi^{(3)} \neq 0$

Virtual State

Ground State

Momentum conservation

$\omega_3 = \omega_1 + \omega_2$

$\omega_4 = \omega_1 + \omega_2 - \omega_3$

$$E^{(\omega_1)} = \frac{1}{2} (E_1 e^{i(k_1 z - \omega_1 t)} + c.c)$$

$$E^{(\omega_2)} = \frac{1}{2} (E_2 e^{i(k_2 z - \omega_2 t)} + c.c)$$

$$E^{(\omega_3)} = \frac{1}{2} (E_3 e^{i(k_3 z - \omega_3 t)} + c.c)$$

$$E^{(\omega_4)} = \frac{1}{2} (E_4 e^{i(k_4 z - \omega_4 t)} + c.c)$$

$$E_T = (E^{(\omega_1)} + E^{(\omega_2)} + E^{(\omega_3)} + E^{(\omega_4)})$$

$$P_{NL} = \epsilon_0 \chi^{(3)} E_T^3$$

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So, these 4 fields are now combined together to generate the total electric field ET. So, total electric field ET is now P Non-Linear related to P Non-Linear and this P Non-Linear is epsilon 0 chi 3 and total electric field cube. So, when I make the total electric

field cube, so omega 1, omega 2, omega 3 and omega 4 will combine because I am making a Q of that and as a result we will go to generate different kind of frequencies. But our aim here is to find out the frequencies omega 3 and omega 4.

So, if I do, then quite easily I can say; omega 3 is omega 1 plus omega 2 minus omega 4 and omega 4 is omega 1 plus omega 2 minus of omega 3. The structure is again some sort of this crosstalk frequencies, that omega 1 plus omega 2 minus omega 3 or omega i plus omega j minus omega k where i, j, k are not same.

(Refer Slide Time: 10:00)

$$P_{NL} = \epsilon_0 \chi^{(3)} E_T^3$$

$$P_{NL} = \epsilon_0 \chi^{(3)} (E^{(\omega_1)} + E^{(\omega_2)} + E^{(\omega_3)} + E^{(\omega_4)})^3$$

$$P_{NL}^{(\omega_1)} = \frac{6}{8} \epsilon_0 \chi^{(3)} E_3 E_4 E_2^* e^{i[(k_1+k_3-k_2)z - \omega_1 t]}$$

$$\nabla^2 E^{(\omega_1)} - \mu_0 \epsilon(\omega_1) \frac{\partial^2 E^{(\omega_1)}}{\partial t^2} = \mu_0 \frac{\partial^2 P_{NL}^{(\omega_1)}}{\partial t^2}$$

$$\Delta k = k_1 + k_3 - k_1 - k_2$$

$$\omega_1 + \omega_2 = \omega_3 + \omega_4$$

$$2ik_1 \frac{dE_1}{dz} = -\frac{6}{4} \mu_0 \epsilon_0 \omega_1^2 \chi^{(3)} E_3 E_4 E_2^* e^{i\Delta k z}$$

$$\frac{dE_1}{dz} = i \frac{3\omega_1 \chi^{(3)}}{4 n_1 c} E_3 E_4 E_2^* e^{i\Delta k z}$$

$$\frac{dE_2}{dz} = i \frac{3\omega_2 \chi^{(3)}}{4 n_2 c} E_3 E_4 E_1^* e^{i\Delta k z}$$

$$\frac{dE_3}{dz} = i \frac{3\omega_3 \chi^{(3)}}{4 n_3 c} E_1 E_2 E_4^* e^{-i\Delta k z}$$

$$\frac{dE_4}{dz} = i \frac{3\omega_4 \chi^{(3)}}{4 n_4 c} E_1 E_2 E_3^* e^{-i\Delta k z}$$

Handwritten notes in red:

- $k_1 = k_3 + k_4 - k_2$
- $\omega_1 = \omega_3 + \omega_4 - \omega_2$
- $6 E_3 E_4 E_2$

So, next let us see how these things. So, P Non-Linear will be epsilon 0 chi 3 ET whole cube. ET is the total electric field, as I mentioned, it is e omega 1, omega 2, omega 3, omega 4 whole cube and now I try to find out only the corresponding frequency omega 1. So, omega 1; if I want to find out how this omega 1 can be there, so, omega 1 is omega 3 plus omega 4 minus omega 2.

So; that means, in P non-linear term, this frequency component omega 3, omega 4 are plus; that means, I should have electric field E 3, E 4 multiplied and omega 2 minus; that means, I will have E 2 star. So, this should be the structure of the electric field in P non-linear term and here this is the thing.

Since these 3 fields are distinct, so, we will have a 6 term as a degeneracy factor. So, this 6 is sitting here we are making cube of this whole field. So, according to our definition it

was a half of that. So, 1 by 8 term will come, because I am making a cube of that thing exponential term should be there also. So, exponential term since I am talking about omega 1, it is omega 3, omega 4 minus omega 2. So, k 1 should be k 3 plus k 4 minus k 2.

So, here it is written which is a k component; the phase term and omega 1 will be 3 because I am generating the frequency omega 1 here. So, my P non-linear term is ready. Once my P non-linear terms is ready and total electric field the expression of the total electric field is ready, I can use again my non-linear Maxwell's equation.

(Refer Slide Time: 12:11)

$$P_{NL} = \epsilon_0 \chi^{(3)} E_T^3$$

$$P_{NL} = \epsilon_0 \chi^{(3)} (E^{(\omega_1)} + E^{(\omega_2)} + E^{(\omega_3)} + E^{(\omega_4)})^3$$

$$P_{NL}^{(\omega_1)} = \frac{6}{8} \epsilon_0 \chi^{(3)} E_3 E_4 E_2^* e^{i[(k_1+k_3-k_2)z - \omega_1 t]}$$

$$\nabla^2 E^{(\omega_1)} - \mu_0 \epsilon(\omega_1) \frac{\partial^2 E^{(\omega_1)}}{\partial t^2} = \mu_0 \frac{\partial^2 P_{NL}^{(\omega_1)}}{\partial t^2}$$

$$\Delta k = k_1 + k_3 - k_1 - k_2$$

$$\omega_1 + \omega_2 = \omega_3 + \omega_4$$

$$2ik_1 \frac{dE_1}{dz} = -\frac{6}{4} \mu_0 \epsilon_0 \omega_1^2 \chi^{(3)} E_3 E_4 E_2^* e^{i\Delta k z}$$

$$\frac{dE_1}{dz} = i \frac{3 \omega_1 \chi^{(3)}}{4 n_1 c} E_3 E_4 E_2^* e^{i\Delta k z}$$

$$\frac{dE_2}{dz} = i \frac{3 \omega_2 \chi^{(3)}}{4 n_2 c} E_3 E_4 E_1^* e^{i\Delta k z}$$

$$\frac{dE_3}{dz} = i \frac{3 \omega_3 \chi^{(3)}}{4 n_3 c} E_1 E_2 E_4^* e^{-i\Delta k z}$$

$$\frac{dE_4}{dz} = i \frac{3 \omega_4 \chi^{(3)}}{4 n_4 c} E_1 E_2 E_3^* e^{-i\Delta k z}$$

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When I use the non-linear Maxwell's equation, I readily find out what is the field equation and the field equation is simply $2ikE \frac{d}{dz} = -\frac{6}{4} \mu_0 \epsilon_0 \omega_1^2 \chi^{(3)} E_3 E_4 E_2^* e^{i\Delta k z}$ the entire term where delta k is the corresponding difference of the corresponding k 1 plus k 3 minus k 1 minus k 2. This is the difference between the propagation constants.

So, if I simplify, it should be like this. I believe now, so many times we are deriving the electric fields of different frequencies. So, you are now quite familiar with the procedure. So, you can apply the same procedure for other 3 fields and you can generate the evolution of all the fields. So, these are the evolution equation or the governing equation of all the fields under four wave mixing. Only thing is that here it is E 3, E 4, E 2 star; for 2 it should be E 3, E 4, E 1 star. You just remember that all the cases, you need to find

out the correct frequencies. So, here the frequencies is frequency component is omega 2. So, how you get the omega 2, we will get omega 2 as omega 3 plus omega 4 minus omega 1. So, that is why it is a star. In the similar logic, you will get omega 3 the field of omega 3 and the field associated with omega 4.

(Refer Slide Time: 14:05)

Manley-Rowe relation $I_1 = \frac{1}{2} \epsilon_0 n_1 c |E_1|^2$

$$\frac{dI_1}{dz} = \frac{1}{2} \epsilon_0 n_1 c \left[E_1 \frac{dE_1^*}{dz} + E_1^* \frac{dE_1}{dz} \right]$$

$$\frac{dI_1}{dz} = i \frac{1}{2} \epsilon_0 n_1 c \frac{3 \omega_1 \chi^{(3)}}{4 n_1 c} \left[-E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} + E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

$$\frac{1}{\omega_1} \frac{dI_1}{dz} = i \frac{3}{8} \epsilon_0 \chi^{(3)} \left[-E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} + E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

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Once you have this four equation in our hand, then the next thing that to from this four equation, we can derive the Manley Rowe relation. So, this Manley Rowe relation is nothing, but some sort of energy conservation. So, all the four equations are coupled to each other, if you look carefully. They are coupled to each other; that means the energy E 1 E 2 E 3 E 4, they are evolving. They are evolving in such a way that there is a interrelationship between these things.

So, this is the source term; in the source term, they are coupled. So, some sort of energy exchange is always there in between and that is the case because if you look that omega 1 and omega 2 is generating omega 3 and omega 4. That means, obviously, some kind of energy distribution is there energy exchange is there. Now the question is the total energy for this case will remain conserved or what kind of things we have.

So, in order to do these things we need to calculate the total electric intensity. So this total electric intensity is something like half epsilon 0 n 1 c E 1 mod of E 1 square which is the total intensity of electric field E 1. So, now, d I 1 d z is equal to half of these things

whatever we have as a constant and the correspond derivative. So, the derivative with respect to z gives you this quantity.

(Refer Slide Time: 15:55)

$$P_{NL} = \epsilon_0 \chi^{(3)} E_T^3$$

$$P_{NL} = \epsilon_0 \chi^{(3)} (E^{(\omega_1)} + E^{(\omega_2)} + E^{(\omega_3)} + E^{(\omega_4)})^3$$

$$P_{NL}^{(\omega_1)} = \frac{6}{8} \epsilon_0 \chi^{(3)} E_3 E_4 E_2^* e^{i[(k_1+k_3-k_2)z - \omega_1 t]}$$

$$\nabla^2 E^{(\omega_1)} - \mu_0 \epsilon(\omega_1) \frac{\partial^2 E^{(\omega_1)}}{\partial t^2} = \mu_0 \frac{\partial^2 P_{NL}^{(\omega_1)}}{\partial t^2}$$

$$\Delta k = k_1 + k_3 - k_1 - k_2$$

$$\omega_1 + \omega_2 = \omega_3 + \omega_4$$

$$2ik_1 \frac{dE_1}{dz} = -\frac{6}{4} \mu_0 \epsilon_0 \omega_1^2 \chi^{(3)} E_3 E_4 E_2^* e^{i\Delta k z}$$

$$\frac{dE_1}{dz} = i \frac{3 \omega_1 \chi^{(3)}}{4 n_1 c} E_3 E_4 E_2^* e^{i\Delta k z}$$

$$\frac{dE_2}{dz} = i \frac{3 \omega_2 \chi^{(3)}}{4 n_2 c} E_3 E_4 E_1^* e^{i\Delta k z}$$

$$\frac{dE_3}{dz} = i \frac{3 \omega_3 \chi^{(3)}}{4 n_3 c} E_1 E_2 E_4^* e^{-i\Delta k z}$$

$$\frac{dE_4}{dz} = i \frac{3 \omega_4 \chi^{(3)}}{4 n_4 c} E_1 E_2 E_3^* e^{-i\Delta k z}$$

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Now dE_1/dz is known. From the previous slide if you look, so dE_1/dz is here; it is here. So, this I will use in the next slide and if I multiply this dE_1/dz with E_1 . So, I will have $E_1 E_3 E_4$ with a star E_2 and the corresponding because this is the star of that. So we have a complex conjugate, once we have a complex conjugate I should have i as minus i ; so that is why this minus term is there and i take common outside. For the next term, I will have a similar kind of things, but it is again a complex conjugate of the first term. So, I should have $E_1^* E_4 E_3 E_2 e^{i\Delta k z}$.

(Refer Slide Time: 16:45)

Manley-Rowe relation $I_1 = \frac{1}{2} \epsilon_0 n_1 c |E_1|^2$

$$\frac{dI_1}{dz} = \frac{1}{2} \epsilon_0 n_1 c \left[E_1 \frac{dE_1^*}{dz} + E_1^* \frac{dE_1}{dz} \right]$$

$$\frac{dI_1}{dz} = i \frac{1}{2} \epsilon_0 n_1 c \frac{3 \omega_1 \chi^{(3)}}{4 n_1 c} \left[-E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} + E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

$$\frac{1}{\omega_1} \frac{dI_1}{dz} = i \frac{3}{8} \epsilon_0 \chi^{(3)} \left[-E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} + E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

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From here also we can see few things that $n_1 c$ and $n_1 c$ will cancel out and eventually we have half epsilon 0 which is a constant $\chi^{(3)}$ is a constant and ω_1 is again a constant. But I want to write this ω_1 here in the left hand side like $\frac{1}{\omega_1} \frac{dI_1}{dz}$ is this term. Now here you can see this term is really a constant; even it is not depending on ω_1 , ω_2 , ω_3 or $n_1 n_2 n_3$. This should be same for all the terms. Inside the bracket we have something here.

(Refer Slide Time: 17:33)

$$\frac{1}{\omega_1} \frac{dI_1}{dz} = i \frac{3}{8} \epsilon_0 \chi^{(3)} \left[-E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} + E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

$$\frac{1}{\omega_2} \frac{dI_2}{dz} = i \frac{3}{8} \epsilon_0 \chi^{(3)} \left[-E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} + E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

$$\frac{1}{\omega_3} \frac{dI_3}{dz} = i \frac{3}{8} \epsilon_0 \chi^{(3)} \left[E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} - E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

$$\frac{1}{\omega_4} \frac{dI_4}{dz} = i \frac{3}{8} \epsilon_0 \chi^{(3)} \left[E_1 E_3^* E_4^* E_2 e^{-i\Delta k z} - E_1^* E_3 E_4 E_2^* e^{i\Delta k z} \right]$$

$$\frac{1}{\omega_1} \frac{dI_1}{dz} = \frac{1}{\omega_2} \frac{dI_2}{dz} = -\frac{1}{\omega_3} \frac{dI_3}{dz} = -\frac{1}{\omega_4} \frac{dI_4}{dz}$$

$$\Delta N_1 = \Delta N_2 = -\Delta N_3 = -\Delta N_4$$

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Now, we will do the same thing for E_2 , E_3 , and E_4 . If we do these things for E_3 , E_4 , E_2 and E_4 , you will going to get a similar kind of expression here for I_2 so; that means, these two are identical expression. But once we have I_3 and I_4 , you will again have a similar expression, but with the negative sign.

So, this term will become positive and this term will become negative again dI/dz id ω_4 we will have the same thing, but only thing is this term will be positive and this term will be negative. So, from this four expression, we can write a general thing, and which is $1/\omega_1 dI/dz$ is equal to $1/\omega_2 d^2/dz$ is equal to $1/\omega_3 dI/dz$ with a negative term and $1/\omega_4 dI/dz$.

So, this is basically this relation is the Manley Rowe relation. This relation we have already figure out in our second order effects, when we generate some frequency generation or difference frequency generation or other parametric generation. This is always valid. In terms of photon number I can say, the ΔN_1 is the photon number the change of photon for ω_1 frequency, then the change of number of photon for ω_2 frequency it is same, because ω_1 and ω_2 are combining to generate ω_3 and ω_4 . So, that is why the change of ω_1 photon is equal to the negative change so; that means, if I write a minus sign here. So, ω_1 and ω_2 photon are collapsing to generate the equal number of ω_3 and ω_4 photon.

So, this basically the physical significance of the Manley Rowe relation; and we will readily get this expression starting from our old Maxwell's equation or a non-linear Maxwell's equation. Just evolve the field equation and from this field equation, we can find this expression.

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Parametric amplification under FWM in optical fiber

$$\hbar\omega_p + \hbar\omega_p = \hbar\omega_s + \hbar\omega_i$$

$$E^{(\omega_p)} = \frac{1}{2} (E_p e^{i(k_p z - \omega_p t)} + c.c)$$

$$E^{(\omega_s)} = \frac{1}{2} (E_s e^{i(k_s z - \omega_s t)} + c.c)$$

$$E^{(\omega_i)} = \frac{1}{2} (E_i e^{i(k_i z - \omega_i t)} + c.c)$$

$$P_{NL} = \epsilon_0 \chi^{(3)} (E^{(\omega_p)} + E^{(\omega_s)} + E^{(\omega_i)})^3$$

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Well, next we will go further we will try to study the parametric amplification under Four Wave Mixing in optical fibers. So, what in optical fibers we do? So, so far we have a knowledge that how four wave mixing can generating different frequencies. It is not generating different frequencies, it is also generating some frequencies and which can be amplified so this can be use as a amplifier. So, using this concept, now we try to apply this in fiber optics where we launch this is the schematic diagram of what is going on here. So, we launch a very strong pump here ω_p and very weak signal and in the output we are going to generate ω_i which is the idler and ω_s which is there because I am launching a very strong signal; a very strong pump.

And here the signal is amplified. So, we have an amplification of this signal that is important. So, I launch a very small amount of signal in the output with that we launch a very strong pump. The strong pump will be there, ω_i will generate as idler frequencies and ω_s will generate and it will rather amplify because I have some amount of ω_s at the input z equal to 0 point.

Now, if I write the energy equation in the previous case which was a degenerate kind of amplification. So, non degenerate rather non degenerate amplification, the previous slide if I go. So, we were generating the frequencies ω_1 ω_2 and an generating ω_3 ω_4 . Now if ω_1 ω_2 was same which is the case, we called it this ω_1 ω_2 same thing as ω_p . So, this energy diagram we slightly

change ω_p and ω_s to ω_p photon will combine and as a result it will go to generate ω_i and ω_s two different frequencies.

(Refer Slide Time: 22:17)

Parametric amplification under FWM in optical fiber

Diagram: A fiber with input frequencies ω_s (red arrow) and ω_p (blue arrow) and output frequencies ω_i (green arrow) and ω_s (red arrow). The fiber is labeled $\chi^{(3)} \neq 0$. Energy level diagram shows $\hbar\omega_p$ and $\hbar\omega_s$ as input levels and $\hbar\omega_i$ as an output level. The equation $\omega_p + \omega_p = \omega_s + \omega_i$ is shown.

Equations:

$$\hbar\omega_p + \hbar\omega_p = \hbar\omega_s + \hbar\omega_i$$

$$E^{(\omega_p)} = \frac{1}{2} (E_p e^{i(k_p z - \omega_p t)} + c.c)$$

$$E^{(\omega_s)} = \frac{1}{2} (E_s e^{i(k_s z - \omega_s t)} + c.c)$$

$$E^{(\omega_i)} = \frac{1}{2} (E_i e^{i(k_i z - \omega_i t)} + c.c)$$

$$P_{NL} = \epsilon_0 \chi^{(3)} (E^{(\omega_p)} + E^{(\omega_s)} + E^{(\omega_i)})^3$$

Handwritten notes in red: $\omega_1 = \omega_2 = \omega_p$, $\omega_3 = \omega_s$, $\omega_4 = \omega_i$, $\omega_1 + \omega_2 = \omega_3 + \omega_4$.

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So, in the previous notation it was something like $\omega_1 + \omega_2 = \omega_3 + \omega_4$. Now I just modify this I say, change the name ω_1 is ω_2 which is ω_p , ω_3 is suppose ω_s and ω_4 is idler frequency ω_i . If I replace these things, so, I will have an expression like this is energy expression; So, energy conservation expression.

(Refer Slide Time: 22:55)

Parametric amplification under FWM in optical fiber

Diagram: A fiber with input frequencies ω_s (red arrow) and ω_p (blue arrow) and output frequencies ω_i (green arrow) and ω_s (red arrow). The fiber is labeled $\chi^{(3)} \neq 0$. Energy level diagram shows $\hbar\omega_p$ and $\hbar\omega_s$ as input levels and $\hbar\omega_i$ as an output level. The equation $\omega_p + \omega_p = \omega_s + \omega_i$ is shown.

Equations:

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$$E^{(\omega_i)} = \frac{1}{2} (E_i e^{i(k_i z - \omega_i t)} + c.c)$$

$$P_{NL} = \epsilon_0 \chi^{(3)} (E^{(\omega_p)} + E^{(\omega_s)} + E^{(\omega_i)})^3$$

Handwritten notes in red: $\omega_s = (2\omega_p - \omega_i)$.

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So, now we have 3 fields; omega i omega s and omega p. Omega p is half E p e to the power i k p z minus omega p t plus complex conjugate omega s is half E i e to the power i k i z m inus omega z and similarly for omega i. Again p non-linear should be the combination of these 3 field because inside we have these 3 fields cube of that epsilon 0 chi 3 and E cube where E is the total fields I make a cube of that so; that means, there will be combination of omega p omega s and omega i will be there.

But which frequency I will consider I will consider omega s. So, if I consider omega s, then omega s should be 2 omega p minus omega. This is the component, this is a frequency component we will concern about.

(Refer Slide Time: 24:07)

The slide contains the following content:

- Energy Level Diagram:** Shows a three-level system with ground state 0 , intermediate state $\hbar\omega_p$, and excited state $\hbar\omega_p + \hbar\omega_s$. Transitions are labeled with $\hbar\omega_p$ and $\hbar\omega_s$. A red arrow indicates the transition from 0 to $\hbar\omega_p + \hbar\omega_s$. The equation $\omega_p + \omega_p = \omega_s + \omega_i$ is shown. Handwritten red notes include $\omega_s = 2\omega_p - \omega_i$ and $E_p^2 E_i$.
- Nonlinear Power Equations:**

$$P_{NL}^{(\omega_p)} = \frac{1}{8}\epsilon_0\chi^{(3)} [3|E_p|^2 E_p e^{i(k_p z - \omega_p t)} + c.c.]$$

(Only SPM)

$$P_{NL}^{(\omega_s)} = \frac{1}{8}\epsilon_0\chi^{(3)} [6|E_p|^2 E_s e^{i(k_s z - \omega_s t)} + 3E_p^2 E_i^* e^{i(2k_p - k_i)z - i\omega_s t} + c.c.]$$

(XPM) (FWM)

$$P_{NL}^{(\omega_i)} = \frac{1}{8}\epsilon_0\chi^{(3)} [6|E_p|^2 E_i e^{i(k_i z - \omega_i t)} + 3E_p^2 E_s^* e^{i(2k_p - k_s)z - i\omega_i t} + c.c.]$$
- Footer:** IIT KHARAGPUR, NPTEL ONLINE CERTIFICATION COURSES, Dr. Samudra Roy, Department of Physics.

So, this is the structure energy diagrams are there. The next thing is to find out what is my P non-linear. So, p non-linear will combination of all these frequencies in optical fiber what happened I need to find out my P non-linear this is important and we should be careful enough to find out how these p non-linear terms are there.

So, p non-linear omega p; that means, how the electric field of E p will experience the thing; if I write, I just write this way. It is 3 E p square E p e to the power k p z minus omega. So, there will be many terms. So, omega p term can be generating in other way also, but I only take the self phase modulation term because pump is very strong. So

since pump is very strong, we can consider pump as a constant. So, since it is a constant, I will not going to take any other source term as p non-linear and I just consider only the self phase modulation term.

Once I express the self phase modulation term in this way, for other two cases which is a small signal omega s and generated idler, I will have 1 by 8 epsilon 0 chi 3 as usual. And inside that we have two term: one is the cross phase modulation and another is the Four Wave Mixing. This Four Wave Mixing term we have discussed earlier several time. So, I will not going to discuss this again. So, you know that if I want to generate omega s, it will be 2 of omega P minus omega i. So, the my corresponding electric field will be E p square with generate 2 omega multiplied by E i star exactly, If you look here so, E p star E p square E i star is there. The corresponding electric the corresponding exponential term with the field propagation constant is also written here. And the degeneracy factor three is coming because two distinct there are not three distinct field rather two fields are distinct. But E p and E p are same because I am multiplying twice. So, that is why the degeneracy factor should be 3. But another term should also be considered here which also give rise to omega s frequency and that is the E p E p star. So, we will have a combination.

(Refer Slide Time: 27:13)

The slide contains an energy level diagram and three equations for nonlinear power. The diagram shows a ground state and two excited states at $\hbar\omega_p$. Transitions are labeled with $\hbar\omega_i$ and $\hbar\omega_s$. The equation $\omega_p + \omega_p = \omega_s + \omega_i$ is shown. Handwritten red annotations include $E_p^* E_p E_s$, $E_i E_i E_s$, and $E_s E_s E_s$. The equations are:

$$P_{NL}^{(\omega_p)} = \frac{1}{8} \epsilon_0 \chi^{(3)} [3|E_p|^2 E_p e^{i(k_p z - \omega_p t)} + c.c.]$$

(Only SPM)

$$P_{NL}^{(\omega_s)} = \frac{1}{8} \epsilon_0 \chi^{(3)} [6|E_p|^2 E_s e^{i(k_s z - \omega_s t)} + 3E_p^2 E_i^* e^{i(2k_p - k_i)z - i\omega_s t} + c.c.]$$

(XPM) (FWM)

$$P_{NL}^{(\omega_i)} = \frac{1}{8} \epsilon_0 \chi^{(3)} [6|E_p|^2 E_i e^{i(k_i z - \omega_i t)} + 3E_p^2 E_s^* e^{i(2k_p - k_s)z - i\omega_i t} + c.c.]$$

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E p E p star and E s; E p E p star basically, this is omega p. This is minus omega p and this is omega s. So, I will have this term also. And another term the self phase

modulation and cross phase modulation for other two is also possible, if I write very carefully so; that means, $E_i E_i^* E_s$ also give rise to a frequency ω_s and another term $E_s E_s^* E_s$ also give rise to a same frequency. So, this is a cross phase modulation with E_i , this is a self phase modulation with E_s , this is a cross phase modulation with E_p .

So, E_p will be more important because pump is very high. So, that is why only I took this term here and the corresponding four wave mixing k system which is this. So, these are the two terms you should be very careful. There will be many terms, but which term I am taking here, I am taking only the cross phase modulation term with respect to E_p because E_p a strong field. So, this effect will be much stronger than the cross phase modulation of E_i which is a weak field or the self phase modulation of E_s which is also very small. We can neglect that and the corresponding Four Wave Mixing where E_p is associated with that because E_p is strong.

So, all the strong field related to E_p will be considered in p non-linear which is a source term. In the similar way p non-linear ω_i this is also a source term and we can also generate or write this expression for p non-linear ω_a . So, here I should stop my class because so far we are deriving the equation for deriving the equation for the signal amplification. So, for signal amplification, we derived the source term. There will be three different source term one is for ω_p another for ω_s and another for ω_l . Eventually we will going to use the source term for ω_s , but how these source terms are generated is important to note and this that is why I in detail I try to make you understand; how this different field combination should be there in the source term. So, with this note let me conclude here and see you in the next class.

Thank you for your attention.