

**Introduction to Non-Linear Optics and Its Applications**  
**Prof. Samudra Roy**  
**Department of Physics**  
**Indian Institute of Technology, Kharagpur**

**Lecture - 36**  
**Sum Frequency Generation Under OPA**

So, welcome student to the next class of Introduction to Non-linear Optics and its Application. Today we have lecture number 36. In the previous few classes we have studied this parametric amplification process which is generated due to the presence of non-linearity of the medium that we have learnt.

So, today we will going to extend that thing. So, for we have learned how if I launch a field with frequency say  $\omega_p$  which is called the pump, it can split into two different frequencies  $\omega_s$  and  $\omega_i$  which is namely signal and idler and oh when they are propagating together there is a process so that they can amplified. So, this amplification process is generally called parametric amplification process.

So, today we will going to see what happened if two frequency are adding up and then generate a new frequency, which is a summation of that two frequency and how this things we going to amplify and what are the consequences of that. So, in the previous case and this case also, the process is essentially the parametric process. So, let us start with today's topic and today we have a one important topic sum frequency generation under OPA.

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**Topics**

**Nonlinear Optics**

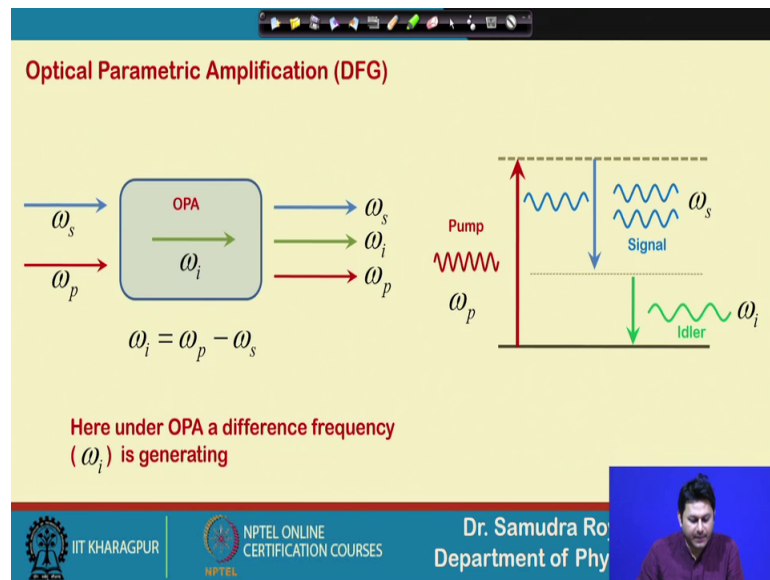
✓ Sum frequency generation under OPA

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So, sum frequency generation we have already started studied in the previous classes. So, the basic concept is known, that if two frequency is a lunch together. So, there is a possibility that we will get a frequency which is sum over that, and this is entirely a non-linear process the non-linear frequency mixing is there, but the field that we will going to generate this sum frequency is going to evolve.

And this evolution process is important and as I mentioned there is a parametric process and it will related to some kind of application. So, it is important to study. Because in many cases we required a frequency and frequency mixing can generate a such kind of frequency, and we can from this frequency we can make some sort of laser with that particular wavelength.

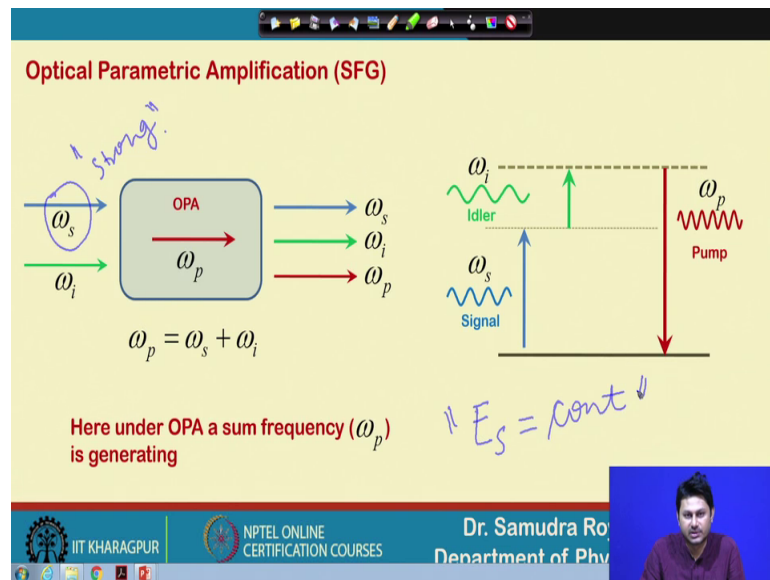
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So, let us see what we have. So, optical parametric amplification for different frequency generation here in the slide DFG suggesting that it is difference frequency generation. The process is understood  $\omega_s$  and  $\omega_p$  are 2 input frequencies that we have launch to the system. And because of the optical parametric amplification 3 different frequencies can evolve with the output  $\omega_s$   $\omega_i$  and  $\omega_p$ . Where  $\omega_i$  is a difference frequency namely it is called the idler frequency. And the process the energy diagram or the energy process is also shown in the right hand side that if a pump is launched into the system, then two different frequencies can generate one is  $\omega_s$  and  $\omega_i$ , but the energy conservation are there and the signal can be amplified because of this process.

And this is this amplification process is basically due to this optical parametric amplification and also the idler will going to generate. So, in difference frequency the evolution of the idler is important, because we need to find out what is this difference what is that frequency that is the difference between  $\omega_p$  and  $\omega_s$  that is launch in the input.

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Well, the scenario is slightly different for sum frequency generation as shown in this figure. In the left hand side the figure is almost same this is a schematic figure of how sum frequencies are generated, that if I launch omega s and omega i the frequencies of 2 fields containing omega s and omega i. Then due to this optical parametric amplification process one new frequencies, one can expect to generate and that new frequency is omega p which is summation over these two frequencies.

So, now the question is how this new frequency is going to evolve, and also the idler is there in the system. So, how the idler wave is there that we need to find out. One thing you should note here that here since I am generating the sum frequency, the launched wave frequency omega s which we called the signal is strong. When you say the pump is strong, then that essentially means that there is no change over distance the amplitude of this wave will not going to change over distance. Here, we say the signal is strong and the word strong means there is no change of amplitude throughout the distance, does not the field associated with omega s if I write this field is  $E_s$  we will consider this as a constant.

So, we have seen before that whenever we make one parameter or one variable constant in the coupled equation then it is easier for us to solve that particular equation. So, here also we will consider that the efficiency of conversion of this pump to signal is relatively low, when the efficiency small, then what happened that a small amount of energy can

pass from this signal to pump and you can consider the signal to be constant. So, it basically help us to solve the differential equation quite easily, otherwise it will be a combustion job to tackle with all the three differential equation, which are couple to each other. So, all these 3 differential equation by the way is already derived and these equations are something like this.

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$$\begin{cases} \frac{dE_p}{dz} = i\kappa_p E_s E_i & \left( \kappa_p = \frac{d\omega_p}{n_p c} \right) \\ \frac{dE_i}{dz} = i\kappa_i E_p E_s^* & \left( \kappa_i = \frac{d\omega_i}{n_i c} \right) \end{cases}$$

$$\frac{d^2 E_p}{dz^2} = i\kappa_p E_s (i\kappa_i E_p E_s^*) = -\kappa_p \kappa_i |E_s|^2 E_p$$

$$E_p(z) = A \sin(\delta z) + B \cos(\delta z)$$

Handwritten notes:  $\delta k z \ (\Delta k = 0)$   
 $\delta^2 = \kappa_p \kappa_i |E_s|^2$

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So, I am talking about the coupled differential equations. So, these are the equations I am talking about, but here we are using only 2 equations; since pump is constant. So, I am not going to since signal is constant here. That means  $E_s$  is constant.

So, I am not going to take the differential equation related to  $E_s$ . So, the first equation is the evolution of the pump and second equation is evolution of the idler. We know that this equation should contain another term which is  $e$  to the power of  $i \delta k Z$ , where  $\delta k$  is a phase mismatch, but for this particular treatment we just consider that there is absolute phase matching. That means,  $\delta k$  is equal to 0. That is the condition for which I can write this kind of equation by just eliminating the exponential term. So, we are using this equation for last few classes. So, the process is exactly same. So, what we need to do to solve this equation when  $E_s$  is constant. That we just replace  $E_i$  from this equation and in order to replace  $E_i$  from this equation or what we need to do? We need to make a derivative of this quantity.

So, if we make the derivative of the first equation once again, then we have a second order derivative  $d^2 E_p / dz^2$ , this quantity  $i \kappa E_s$  is constant because  $E_s$  is constant in our case. So, this term will be here, and we have a derivative of this quantity which is  $d E_i / dz$ . Now  $d E_i / dz$  this term is in our hand this, and we just to replace this things here in place of  $d E_i / dz$ . So, when we replace this term we will have a term like  $\kappa p \kappa i$  with the negative sign because this  $i$  and this  $i$  will give a negative sign, and also we have  $E_s \text{ mod square}$  which is also a constant and  $E_p$ .

Now if I consider this term as  $\Delta^2$  because all these things are positive. So,  $\Delta$  has to be a positive quantity, then we will have an expression like this. So, this is the well-known expression. So, one thing we should mention here that when we are dealing with the difference frequency, then there was a plus sign and the nature of the solution was different. So, in the previous class we try to find out how the difference frequencies evolving under optical parametric amplification and that time we notice that this equation this sign was plus.

So, we have a sine hyperbolic and cos hyperbolic kind of solution, the combination of these two as a solution we get. But here what we are getting is a sign solution because of this negative sign. So that means, somehow the  $E_p$ ; that means, the pump will going to evolve, but this evolution is seems to be periodic in nature. Whatever the boundary condition if I put then we find either it should be a sin cos or combination of both, but there should be some kind of sinusoidal variation.

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$E_p(z=0) = [A \sin(\delta z) + B \cos(\delta z)]_{z=0} = B = 0$   
 $E_p(z) = A \sin(\delta z)$   
 $\left[ \frac{dE_p}{dz} \right]_{z=0} = i \kappa_p E_s E_i|_{z=0} = i \kappa_p E_s E_{i0}$   
 $\left[ \frac{dE_p}{dz} \right]_{z=0} = A \delta \cos(\delta z)|_{z=0} = A \delta$   
 $E_p(z=0) = 0$

Handwritten notes:  $E_i(z=0) \neq 0$ ,  $E_i(z=0) = E_{i0}$ ,  $\omega_p = \omega_s + \omega_i$

So, once we have this expression, the next thing is to evaluate A and B as we have done in our previous class. So, first we try to find out what is my  $E_p$ . So,  $E_p$  at  $z$  equal to 0, that we need to consider to find out the boundary condition and the structure is something like this if you remember. That I launch a signal with  $\omega_s$  I launch a idler with  $\omega_i$  and  $\omega_p$  is generating with the condition that  $\omega_p$  is equal to  $\omega_s$  plus  $\omega_i$  that was the condition. If this is the condition then we can see that this is  $z$  equal to 0 point and this is say  $z$  equal to some L point.

So, the boundary conditions such as that at  $z$  equal to 0, there is no field containing the frequency  $\omega_p$ . That means  $E_p$  at  $Z$  equal to 0 is 0 that is the mathematical description of the boundary condition that we have mentioned. Here if I put this boundary condition because  $E_p$  at any  $Z$  point or the solution of the  $E_p$  is known to us.

So, now if I put  $Z$  equal to 0 in this equation, then we find that this term will not be there and only we have B and this B is 0. That means, one part is readily eliminated when I put the boundary condition and the boundary conditions suggest that there is no pump field or the sum frequency field at  $Z$  equal to 0. So, our equation or the solution simply becomes  $E_p Z$  is equal to  $A \sin \delta z$  that is the solution we have. But still we need to find out what should be our a. So, again in order to find the A the next boundary condition that we are going to use and this is the same procedure that we have been using for last few classes. That therefore, one condition we just put what is the value of the

field at  $z$  equal to 0. And in other case we try to find out the derivative because the derivatives is proportional to the field of other frequencies and we know what is the value of the field of other frequency at  $z$  equal to 0 point. So,  $dE_p/dz$  at  $z$  equal to 0, which is essentially  $i\kappa_p E_s E_i$ . So, this value at  $z$  equal to 0 is simply  $i\kappa_p E_s E_i$ .

So, the condition here that we have taken is the field idler field at  $z$  equal to 0 is not equal to 0 as I mentioned, because we need to launch some idler at the input to generate the frequency at  $\omega_p$ , which is a sum over to frequencies. So, this value we have taken as since this is nonzero value. So, we have taken  $E_i$  at  $z$  equal to 0 is simply  $E_i$  this is the case where we use this things. Now there e you know what is the value of  $E_p$  at  $Z$  point. So, we make a derivative of that. So, when we make a derivative of that you will get  $A\delta$  and once we get  $A\delta$  that should be equal to that quantity; that means,  $A\delta$  has to be equal to this.

So, we will finally, get what should be the value of  $A$ .

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$$A = \frac{i\kappa_p E_s E_{i0}}{\delta} = \frac{i\kappa_p E_s E_{i0}}{\sqrt{\kappa_p \kappa_i} E_s} = i \sqrt{\frac{\kappa_p}{\kappa_i}} E_{i0}$$

$$E_p(z) = i \sqrt{\frac{\kappa_p}{\kappa_i}} E_{i0} \sin(\delta z)$$

$$E_i(z) = \frac{1}{i\kappa_p E_s} \frac{dE_p}{dz}$$

$$\frac{dE_p}{dz} = i \sqrt{\frac{\kappa_p}{\kappa_i}} E_{i0} \delta \cos(\delta z)$$

*Handwritten notes:*  
Left:  $\frac{dE_p}{dz} = i\kappa_p E_s E_i$   
Right:  $\delta^2 = \kappa_p \kappa_i |E_s|^2$

So,  $A$  finally, we find  $A$  should be something like this  $i\kappa_p E_s E_i$  divided by  $\delta$ ; now next I put the value of  $\delta$  because if you remember  $\delta^2$  was  $\kappa_p \kappa_i$  mod of  $E_s$  square. So, root over of  $\delta$  is root over of  $\kappa_p \kappa_i$  and  $E_s$  mod of  $E_s$  square can be considered as a completely real quantity. So, that is why when I take a root over of that. So, I can say this is simply  $E_s$ . So that means, you are not



considered any kind of phase at the input or the if even if there is a phase we can call this phase as 0, and respect to that phase when measuring other phases.

So,  $E_s$  whatever the field we have at the input is having some kind of phase, which we considered the reference. So, we consider these as a 0. So, then this becomes simply a real quantity. So, when we do that then this  $E_s E_s$  will cancel out, by the way this assumption or whatever we are doing here is we can say without any loss of generality. So, there is no harm to take this kind of consideration. So, we all we can always do that. So, A finally, after doing this A become  $i \sqrt{\kappa_p \kappa_p} E_i$ .

So,  $E_p$  finally, I find that  $E_p$  is something like this,  $\sqrt{\kappa_p \kappa_p} E_i \sin \Delta z$ . So that means, it is evolving and it is evolving as a sin function and at  $z$  equal to 0 point this quantity is 0 all the boundary condition is valid. But at the same point we need to find out how the idler is evolving because pump is constants. So, pump is not going to change, but this signal is constant here, to signal is not going to change. So, signal is feeding these two fields pump and idler.

So, once pump and idler are feeded by this signal field. So, both this things will going to evolve. So, we need to find out how  $E_i$  is also evolving. So, in order to find out the evolution of  $E_i$  will not going to solve again everything, rather we just use the relationship between  $E_i$  and  $E_p$  because we know that  $d E_p / dz$  this is again our fundamental equation or the mother equation is  $i \kappa_p$  then  $E_s$  and  $E_i$ , that was our expression.

So,  $E_i$  from here I can write it is one by  $i \kappa_p E_s$  which is this quantity and  $d E_p / dz$  now  $d E_p / dz$  is one can figure out because  $E_p$  the functional form an  $E_p$  is known. And if we do that  $d E_p / dz$  can I find  $d E_p$  it is a simply  $i \sqrt{\kappa_p \kappa_p} E_i \cos \Delta z$ , thus derivative of this quantity with respect to  $z$ .

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$$\frac{dE_p}{dz} = i \sqrt{\frac{\kappa_p}{\kappa_i}} E_{i0} (\sqrt{\kappa_p \kappa_i} E_s) \cos(\delta z) = i \kappa_p E_s E_{i0} \cos(\delta z)$$

$$E_i(z) = \frac{1}{i \kappa_p E_s} \times i \kappa_p E_s E_{i0} \cos(\delta z) = E_{i0} \cos(\delta z)$$

$$E_p(z) = i \sqrt{\frac{\kappa_p}{\kappa_i}} E_{i0} \sin(\delta z)$$

$$E_i(z) = E_{i0} \cos(\delta z)$$

Once we have these quantity  $dE_p/dz$ , then we can just put this things and we can figure out what should be the value of  $p$ . So,  $dE_p/dz$  is this quantity. So,  $i \kappa_p \kappa_i E_{i0}$  and I put this quantity, which is nothing, but  $\delta z$ . So, when I put this  $\delta z$ . So, this  $\delta z$  this quantity  $\kappa_p \kappa_i$  will cancel out, and  $\kappa_p \kappa_i$  become  $i \kappa_p$  and  $E_s$  will be there  $E_s E_{i0}$  will be there and  $\cos$  of  $\delta z$  is there. So, from here we can find out what is my  $E_i$ , because  $E_i$  is this quantity multiplied by whatever we have this thing, this thing I now replace with  $i \kappa_p E_{i0}$ .

So, finally, we come with this solution which is  $E_{i0} \cos$  of  $\delta z$  there. You can see that again the boundary condition is satisfying because we know that  $p$  at  $z$  equal to 0 it  $E_i$  0 and if you put this  $z$  equal to 0 then  $\cos$  of 0 become 1. So, we have  $E_i$  at  $z$  equal to 0 is simply  $E_{i0}$ . So, these two expression we have in our hand which is  $E_p$  and  $E_i$ . So,  $E_p$  evolve in this way  $E_i$  will evolve in this fashion. So, now, after having this expression in our hand; so we now calculate. So, these are the 2 expressions we have these are the 2 expressions we have, we know calculate; what is the value of the corresponding powers because we always present the thing in terms of powers.

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The slide displays the following equations and notes:

$$P_p(z) = I_p(z)A = \frac{1}{2} \epsilon_0 c n_p |E_p(z)|^2 A$$

$$P_p(z) = \frac{1}{2} \epsilon_0 c n_p A \frac{\kappa_p}{\kappa_i} |E_{i0}|^2 \sin^2(\delta z)$$

$$P_i(0) = I_i(0)A = \frac{1}{2} \epsilon_0 c n_i |E_i(0)|^2 A$$

$$\frac{P_p(z)}{P_i(0)} = \left( \frac{n_p \kappa_p}{n_i \kappa_i} \right) \sin^2(\delta z)$$

Handwritten notes on the right side of the slide:

$$E_p(z) = i \sqrt{\frac{\kappa_p}{\kappa_i}} E_{i0} \sin(\delta z)$$

$$E_i(z) = E_{i0} \cos(\delta z)$$

$$P_i(z) = I_i(0)A = \frac{1}{2} \epsilon_0 c n_i E_{i0}^2 \cos^2 \delta z$$

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So, the power associated with the electric field  $E_p$  can be simply written as this  $P_p$  is equal to  $I_p$  multiplied by  $A$ ,  $I_p$  is the intensity and  $A$  is an area. So, intensity multiplied by area is the corresponding power. So, intensity again can be represented in terms of mode of field square. So, which is this expression we are using this expression several times. So, by the time you are familiar with this. So, whenever we have intensity we can replace the intensity in terms of field or whenever we have field we can transform this field to intensity, because intensity is a measurable quantity so as the pump. So, we always try to find out in terms of intensity or power.

So, this quantity  $E_p$  mode of  $z$  square we know because these are the 2 solutions that we have generated through this coupled equation and when we put this thing in this expression, this becomes half  $\epsilon_0$  in  $n_p c$  this quantity is as usual because this is already there, and mode of  $E_p$  square means square of this quantity or this multiplied by the complex conjugate. When we make the complex conjugate this  $i$  term will not be there. So, we have  $\kappa_p \kappa_i$  mode of  $E_{i0}$  and  $\sin^2 \delta z$ .

In the similar way I can also find out what is my  $P_i$ ; that means, the power of idler at  $z$  equal to 0 point. I am just taking what is the value of  $z$  equal to 0 point because when I do this because I know that this is the value at  $z$  equal to 0 point. So, just to replace these things from this equation, I just want to find out what is the ratio of pump power at any point  $z$  to the idler power at  $z$  equal to 0 what is the ratio between these two.

So, we need do, we find that this is simply this now this is cos theta. So, if I want to find out what is my  $P_i(z)$  we can find it out. So, it is  $I_0 A$  which is half of  $\epsilon_0 c n_i$  and then  $E_i$  mode square. So, this term will be simply become  $E_i^2 \cos^2 \delta z$  it will evolve the power will evolve like  $\cos^2 \delta z$ . So, the ratio between these two is having this, when you make a ratio these divided by these. So, half  $\epsilon_0$  in this term will cancel out,  $n_p \kappa_p$  will be there in the denominator we have  $n_i \kappa_i$  which is also there I will also be cancel out, this term this term are canceling out each other. So, we will have  $\sin^2 \delta z$  here. So, this is the ratio of these two things why I am taking the ratio I will show in the next slide.

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The slide displays the following content:

$$\frac{P_p(z)}{P_i(0)} = \left(\frac{\omega_p}{\omega_i}\right) \sin^2(\delta z) \quad \left(\kappa_p = \frac{d\omega_p}{n_p c}; \quad \kappa_i = \frac{d\omega_i}{n_i c}\right)$$

Maximum power transfer,

$$P_p(z)|_{max} = \left(\frac{\omega_p}{\omega_i}\right) P_i(0)$$

Handwritten notes on the slide include:

- A circled equation:  $\frac{P_p(z)}{P_i(0)} = \left(\frac{\omega_p}{\omega_i}\right) \sin^2(\delta z)$
- A circled equation:  $\frac{P_p(z)}{P_i(0)} = \left(\frac{\kappa_p}{\kappa_i}\right) \sin^2(\delta z)$

Two boxed equations at the bottom represent photon fluxes:

- No of idler photon per unit time per unit area:  $N_i = \frac{P_i(0)}{\hbar\omega_i}$
- No of pump photon per unit time per unit area:  $N_p = \frac{P_p(z)}{\hbar\omega_p}$

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So, once we have the ratio of  $P_p(z)$  and  $P_i(0)$ , then this ratio can further be modified because  $\kappa_p$  whatever. So, let me. So, let us right what we had. So, in the previous slide  $P_p$  divided by  $P_i(0)$  this was  $\kappa_p n_p$  divided by  $\kappa_i n_i$ .

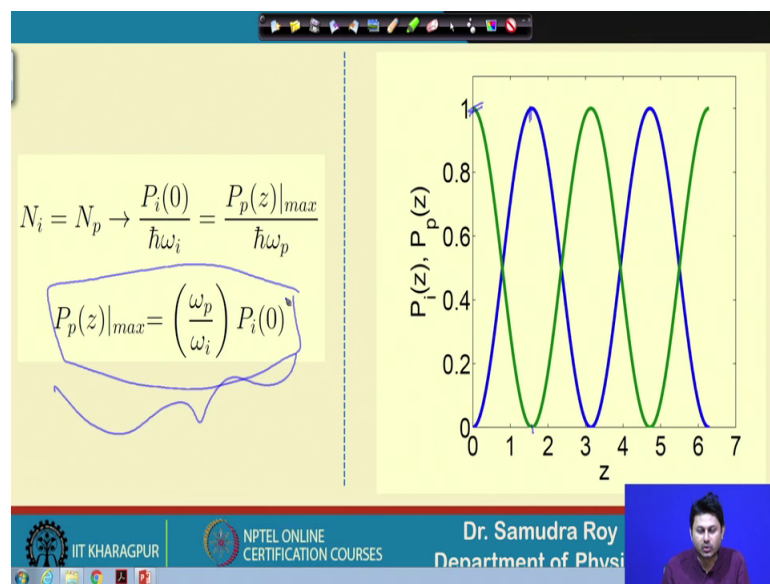
And then there was  $\sin^2 \delta z$ . So, this quantity if I replace with these then we find that  $\kappa_p n_p$  is  $d\omega_p$  divided by  $c$  and  $\kappa_i n_i$  is  $d\omega_i$  divided by  $c$ . So, their ratio simply we can  $\omega_p$  divided by  $\omega_i$   $\sin^2 \delta z$  term will be there as usual. So, the next thing is if I want to find out because these quantities now varying with  $\sin^2 \delta z$ ; that means, the ratio of this quantity is varying sinusoidally now if I consider; what is the maximum power transfer. So, what is the maximum value of this quantity. So, readily we can see that the maximum of this value will be when this

quantity is 1. So,  $\sin^2 \Delta z$  is 1. So, when  $\sin^2 \Delta z$  is one. So, we can say this value is maximum.

So; that means, the maximum power at pump, and this quantity in terms of the idler power at  $z$  equal to 0 is this. This multiplied by sum parameter  $\omega_p$  and  $\omega_i$  this is a frequency of pump and idler. Now the number of idler photon per unit time per unit area that is moving can be represented in terms of power and energy we know that. So, power at 0 point divided by  $z$  equal to 0 of idler power divided by the total energy can give you the total number of idler photon, also we can find out what is the pump photon number of pump photon.

So, now, idler photon and pump photon are related to this expression, and now if we look carefully if I now make a ratio of these two things can we find interesting things.

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That if I say the number of idler photon that is generated, if this is equal to the number of pump photon. Then this condition is same as whatever the condition we figure out regarding the power transfer. So, that suggests that if I now plot these two things together, then we can find that the idler power and pump power can exchange the energy and when total amount of idler power. So, this is the idler input idler power and now it is reducing and reducing to 0 value and the pump idler power the pump power is now increasing to the maxima.

So, now, there is a power exchange between the idler and pump and if this ratio is this; that means, the total amount of idler photon is now totally converted to the total number of pump photon. So, that means, there is a power conversion, and this power conversion is periodic in nature.

So, today we will like to conclude here. So, we have learnt important thing today that sum frequency generation under optical parametric amplification is possible, but in sum frequency generation process we find that like a difference frequency generation, the signal is evolving as well as the idler is evolving over  $z$  monotonically. But here we find that this monotonous evolution is not possible for pump.

So, pump means the sum of these two frequencies. So, that will going to evolve periodically and there is energy exchange between idler photon 2 idler wave 2 in the pump wave, and we can suitably have the value of  $z$  for where for which you we can get the maximum pump power; that means, the sum frequency power.

So, with this note let me conclude here. So, thank you for your attention and see you in the next class where we going to study more about the optical parametric amplification and optical parametric oscillation. So, see you in the next class.

Thanks.