

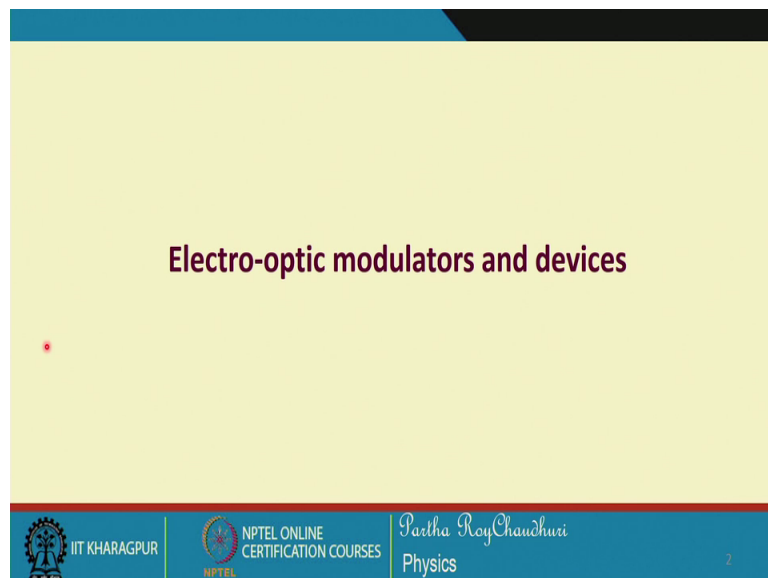
Modern Optics
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Lecture - 40
Electro-optic Modulators and Devices (Contd.)

Good morning. So, far we have studied the principles of electro optic effect. We have studied various electro optic materials in terms of their longitudinal configuration transverse configuration and in terms of the applications. We discussed how the electro optic crystals can be configured for a phase modulation, amplitude modulation.

Both of these are widely used for commercial applications and having known those basic understanding basic properties of the electro optic materials with regard to the applied electric field, we will now discuss the applications in terms of the electro optic devices electro optic modulators. And we will discuss few of them which are very important and commercially available devices

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Contents

- ✓ Electro-optic modulators and devices, applications, properties, transverse and longitudinal modulators
- ✓ Integrated EO modulator, dynamic wave retarder, Mach-Zehnder interferometer intensity modulator, beam deflectors, scanner, spatial light modulators, directional coupler

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So, we have discussed we are going to discuss this today's discussion under the following heading that is electro optic modulators and devices, look at the applications and the properties and particularly their properties required for transverse and longitudinal modulators application. Then we will discuss few of the a very useful electro optic modulators like integrated optic modulator and a very common and versatile use is a dynamic wave retarder which could be incorporated in any photonic circuits any photonic devices.

Then Mach-Zehnder interferometer intensity modulator, this is a very powerful modulator in terms of this is very widely used in sensing applications also apart from switching of the light signals. Then beam deflectors and scanners, spatial light modulators and another very important use is the use of directional coupler for switching a versatile device for many applications.

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Electro-optic modulators

- ✓ Encode analogue or digital signals on an optical wave
- ✓ Transfer optical power to desired frequency windows
- ✓ Used to control power/phase of laser beam
- ✓ Used as fast switching of laser Q-switching
- ✓ Laser scanning microscopy, interferometric metrology
- ✓ Short laser pulse generation, and many more..

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So, for electro optic modulators these are the basic things that that have to be taken care before designing and going for application; this electro optic modulator basically enclode encode analog or digital signals on an optical wave, in the form of phase or amplitude modulator which carries the modulation signal.

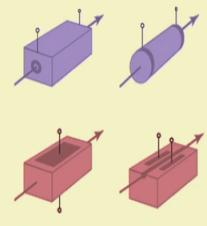
Then this transfer optical power to desired frequency windows. This task is also done there are many more applications, of course, modulators electro optic modulators are used to control power and phase which is nothing but the same like if I can control the retardation, the phase delay then under amplitude modulation, it can be used to control the power then the phase can also be controlled by we have discussed that the one has to launch the light into one of the Eigen polarizations of the crystal.

And have to use it as a phase modulator used as a first switching and these are being used for many years for Q switching of laser beam. Laser scanning microscopy, interferometric metrology then modulators are very widely used in laser pulse generation and there are many more to list.


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Properties desired: EO modulators

- ✓ **Dimensions of the device**
- ✓ **aperture of the EO-crystal**
(limits the beam-size of modulated beam)
- ✓ **Bandwidth of modulation**
(typically beyond GHz for EO modulators)
- ✓ **Maximum phase delay obtainable**
- ✓ **Drive voltage to switch modulator**



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The basic properties that is required are the dimensions of the device. It is important from the design point of view for extracting the best performance of the device. Then aperture of the electro optic crystal that is also very important the designer has to take care of that because it limits the beam size of the modulated beam the spot size of the modulated beam.

The bandwidth of modulation this is typically for electro optic modulation of the order of gigahertz. And one has to look at [the maximum obtainable phase delay with minimum applied voltage that is very high performance device. Then the drive voltage to switch the modulator that is to get a phase delay of π at the drive voltage should be of the order of because we have seen it can vary from kilo volt to volts.



So, looking at the specific application desired application, one has to take this point as one of the important designing factor.

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Electro-optic phase modulators

EO modulator used to control the phase of a laser beam

- ✓ wavelength tuning of single-frequency laser
- ✓ active mode locking of lasers
- ✓ laser frequency stabilization: a few schemes
- ✓ fiber-optic communication: data transmitter
- ✓ Interferometer configuration
- ✓ Spectroscopic measurements

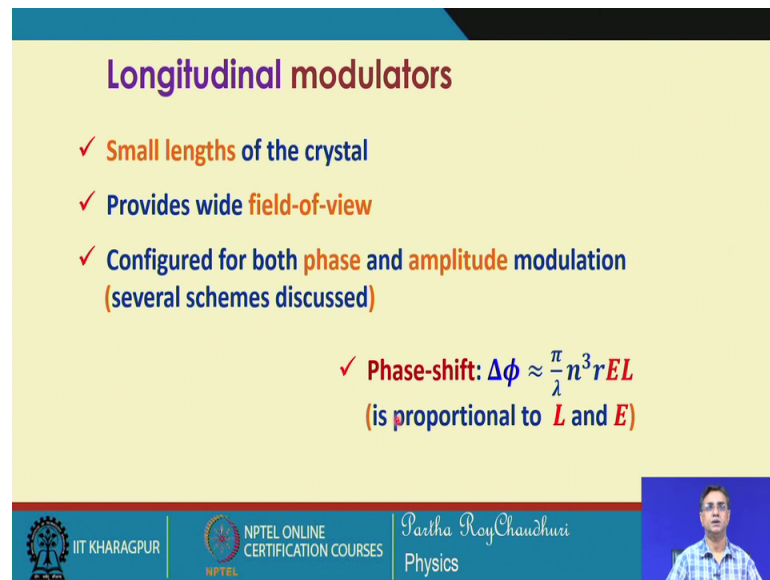


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The electro optic modulators when used as a phase modulator then it controls the phase of the laser beam, phase of the electromagnetic wave. Wavelength tuning of and that has directed in application in wavelength tuning of single frequency lasers, active mode locking of the laser beam, laser frequency stabilization there are number of schemes to do that we will not discuss those things, but the basic task is that by using an electro optic modulator the phase can be modulated.

Then widely used in fiber optic data communication used as a data transmitters because the data the information in the form of electrical signal can be impressed on to the light signal, through an electro optic modulator. It could be in the form of phase modulation, it could be in the form of amplitude modulation. Then interferometric configuration several configurations are already well known in the photonic devices, for sensing application, for signal processing and spectroscopic measurements also.

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Longitudinal modulators

- ✓ Small lengths of the crystal
- ✓ Provides wide field-of-view
- ✓ Configured for both phase and amplitude modulation (several schemes discussed)

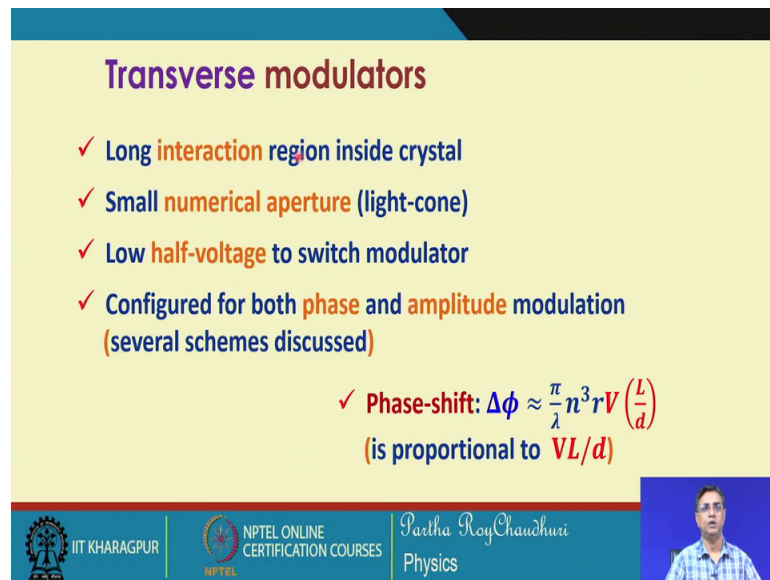
✓ Phase-shift: $\Delta\phi \approx \frac{\pi}{\lambda} n^3 r E L$
(is proportional to L and E)

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In the case of longitudinal modulators when we devise an electro optic crystal to function as a longitudinal modulator, then it should be of small length and it provides a wide field of view. Then this longitudinal modulator can be configured this we have seen with all the theoretical and basics of understanding, that how it could be implemented as a phase modulator or an amplitude modulator. And that is what we have discussed several schemes of you know orienting the crystal the configuring the crystal with respect to the applied voltage.

And in such longitudinal modulator case, the phase shift that is obtainable is proportional to the length of the crystal is the electric field and this we have seen with many examples. And we see that it is proportional to L and E ; applied voltage on the length of the crystal.

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Transverse modulators

- ✓ Long interaction region inside crystal
- ✓ Small numerical aperture (light-cone)
- ✓ Low half-voltage to switch modulator
- ✓ Configured for both phase and amplitude modulation (several schemes discussed)

✓ Phase-shift: $\Delta\phi \approx \frac{\pi}{\lambda} n^3 r V \left(\frac{L}{d}\right)$
(is proportional to VL/d)

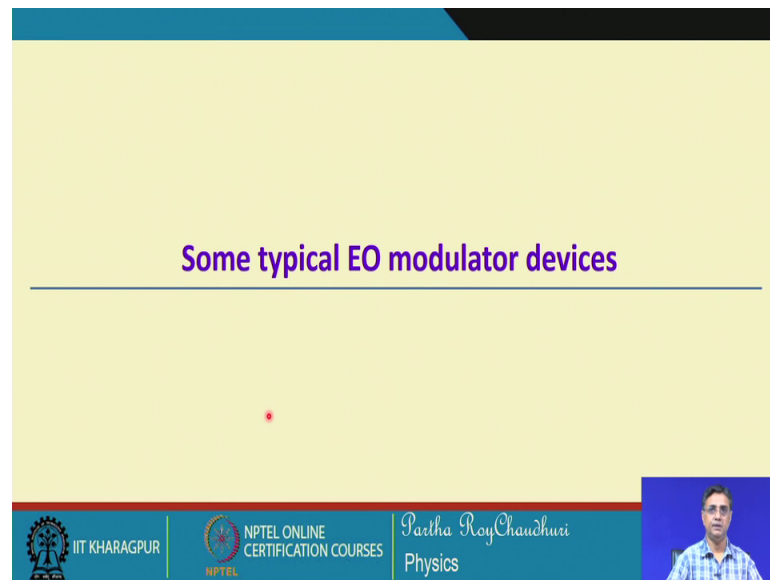
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But for transverse modulators, we usually require a long interaction region inside the crystal interaction of the light wave with the crystal and we require a small numerical aperture that is the light cone the acceptance angle of the light from the input side.

This is useful because we have also studied the beam geometry to optimize to maximize the performance of the modulator in the case of transverse modulation, transverse for configuration. Effectively, as a consequence of this it requires much less half voltage to switch the modulator, we have seen examples and with numerical problems also that it really required a requires voltage of the order of volts.

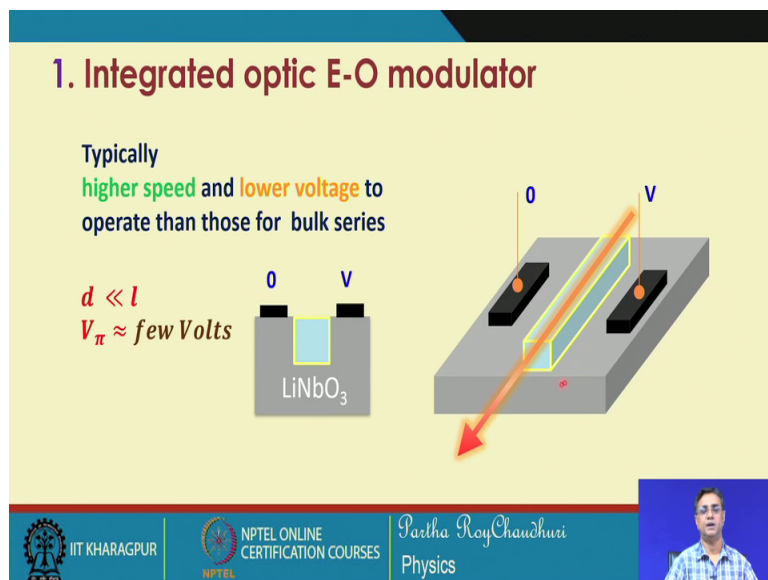
Then again it can be configured this transverse modulations. These examples also you have seen that it could be implemented as a phase modulator, amplitude modulator and but in the case of transverse configuration, the phase shift is proportional to both the voltage and the and inversely proportional to the width of the crystal linearly proportional to the length of the; so, you have a better freedom of 3 parameters, voltage. Voltage of course, is the main control factor to tune the phase delay and length and d and L can be used to optimize the performance of the device.

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Now, we will discuss some typical modulator devices which are very important and we will also try to understand how they operate.

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Integrated optic electro optic modulator, the basics configuration is this. You have a light signal which is passing through the waveguide integrated optic waveguide. This is the high index region that is the core of the waveguide. And these are the electrodes which are connected to the applied voltage.

This is the ground, this is the potential V and this is a cross section of a typical lithium niobate electro optic modulator V pi we have seen we have studied with examples and numbers also that it requires only a few volts.

But basically this is based on the principle of phase delay between the 2 Eigen polarization polarized light.

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2. Dynamic wave retarder

- ✓ An anisotropic medium has two independent polarization modes that travel with different velocities c/n_1 and c/n_2
- ✓ If the medium exhibits Pockels effect, then on applying an E-field the RI's seen by two eigen polarisations modify to:

$$n_{1(E)} \approx n_1 - \frac{n_1^3}{2} r_1 E \quad \text{and} \quad n_{2(E)} \approx n_2 - \frac{n_2^3}{2} r_2 E$$

- ✓ Thus, the birefringence and retardation can be dynamically controlled by varying the properties of the applied E-field

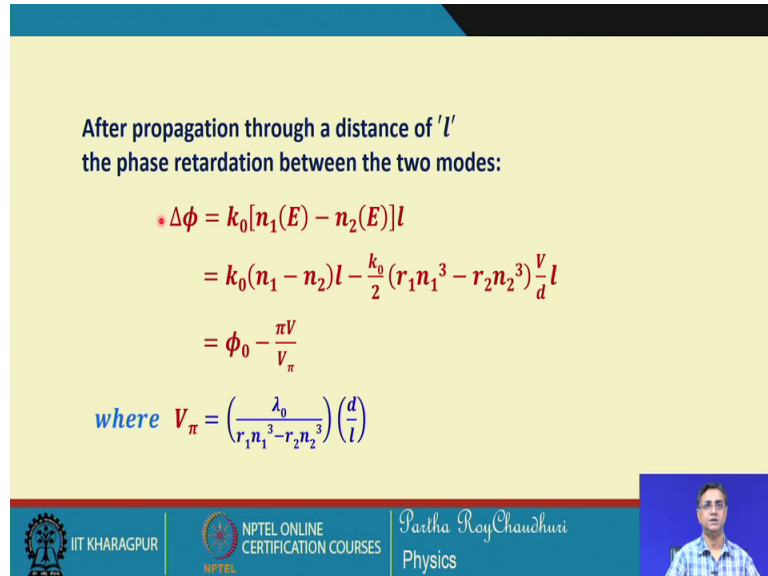
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That is propagating to the crystal and making use of that fact this dynamic wave retarder is very versatile and a tunable retarder device which is very useful for many applications the but the basic philosophy is that this anisotropic medium has 2 independent polarizations, polarization modes and they have 2 different phase velocities in the inside the crystal, but because of the different phase velocities they will develop a phase difference, which will lead to a phase delay. And this phase delay that is the retardation that can be controlled by externally applied electric field.

In the medium, if the medium is a Pockel type of medium Pockel crystal Pockels crystal then on applying an electric field this refractive index seen by the 2 Eigen polarizations will be modified, as long as the electric field is present. We will have n_1 polarization refractive index is this the other one n_2 is this. And therefore, there is a birefringence the induced between these 2 as long as the electric field is present, apart from the fixed birefringence which will come from n_1 and n_2 that is the static birefringence which is independent of the external voltage.

So, this voltage dependent birefringence can be controlled to get a tunable and dynamic to match the requirement of a specific application.

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After propagation through a distance of 'l'
the phase retardation between the two modes:

$$\begin{aligned} \Delta\phi &= k_0[n_1(E) - n_2(E)]l \\ &= k_0(n_1 - n_2)l - \frac{k_0}{2}(r_1n_1^3 - r_2n_2^3)\frac{V}{d}l \\ &= \phi_0 - \frac{\pi V}{V_\pi} \end{aligned}$$

where $V_\pi = \left(\frac{\lambda_0}{r_1n_1^3 - r_2n_2^3}\right)\left(\frac{d}{l}\right)$

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So, this delta phi which is equal to k_0 that is twice pi upon lambda then n_1 and n_2 , but n_1 and n_2 this is the fixed static birefringence in absence of the electric field, but this is the field induced birefringence.

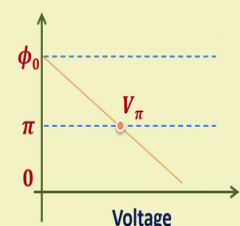
So, with more compact notation this ϕ_0 , the static birefringence is the one which is always sitting there and this is the voltage dependent birefringence and you can express this we have seen that this is πV by V_π ; V_π is the half voltage to switch the modulator to get a phase difference of pi. So, this V is this that also we have seen in the case of transverse modulator because d by l it appears, d is the width of the crystal, l is the length of the crystal and these are the electro optic coefficients ok.

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Retarder response

$$\Delta\phi = \phi_0 - \frac{\pi V}{V_\pi}$$

where $V_\pi = \left(\frac{\lambda_0}{r_1 n_1^3 - r_2 n_2^3} \right) \left(\frac{d}{l} \right)$



The active length of the medium behaves as an electrically controllable dynamic retarder

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So, the response of this because you have a static birefringence sitting here, so, when the applied voltage is 0, applied voltage is 0 you get the phase delay ϕ_0 which is equal to this, but as the voltage increases this will take away from the total phase take away from ϕ_0 to get the net phase effective phase delay. So, it decreases as the voltage increases.

And it becomes π which we will call the switching voltage the V_π that is the half voltage and that is in this case this we have seen before also. So, the active length of the medium behaves as an electrically controlled controllable dynamic retarder. So, just by changing the applied voltage one can actually get the obtain any desired amount of phase between 0 to π by 2. So, that is a very useful device.

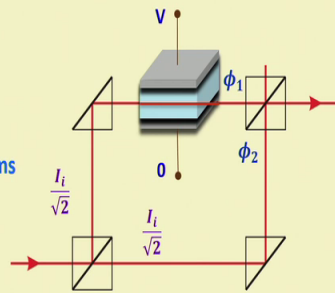
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3. Interferometric intensity modulator

$$I_o = \frac{1}{2}I_i + \frac{1}{2}I_i \cos \phi = I_i \cos^2 \frac{\phi}{2}$$

where $\phi = \phi_1 - \phi_2$
phase difference between two arms

But $\phi_1 = \phi_{10} - \frac{\pi V}{V_\pi}$



The diagram shows a Mach-Zehnder interferometer setup. An input light beam with intensity I_i enters from the left. It passes through a beam splitter, splitting into two arms. Each arm has an intensity of $\frac{I_i}{\sqrt{2}}$. The top arm passes through a phase shifter with phase ϕ_1 , and the bottom arm passes through a phase shifter with phase ϕ_2 . The two arms then recombine at a second beam splitter. An electro-optic modulator (EOM) is placed between the two phase shifters, with an external voltage V applied across it. The output light intensity is I_o .

Now, intensity interferometric intensity modulator; this is actually a Mach-Zehnder scheme where you have an input light which is part of the light is 50 percent in the ideal situation. The part of the light is reflected and again it is reflected then there is another beam splitter from which part of the light is reflected and part of the light 50 percent of the light is transmitted. And in the same way the remaining half of the light which is transmitted through this first beam splitter again gets reflected then again it is a part of the light is reflected and 50 percent of the light is transmitted.

So, if you observe that the path that is travelled by both these waves are the same because you have 1 reflection here, 2 reflection here and if we consider this wave then it is 3 reflection here. In this case, it is transmitted, reflected and again transmitted. So and the other way if you look at the transmitter then you have 2 reflection and you have 2 reflection; one here, one here and one transmission here.

So, it is only the phase that is accumulated due to the propagation. In addition, there is another phase which is added as an induced phase by applying the external voltage, where the light beam has to travel through an electro optic medium. So, this is the basic working principle of this interferometric intensity modulator.

Now, that this when these 2 waves are mixed at one of the outputs this is one output and this is another output, when they are mixed at one of the outputs this depending on the phase if the phase difference between these 2 is pi then there is no light here and if the

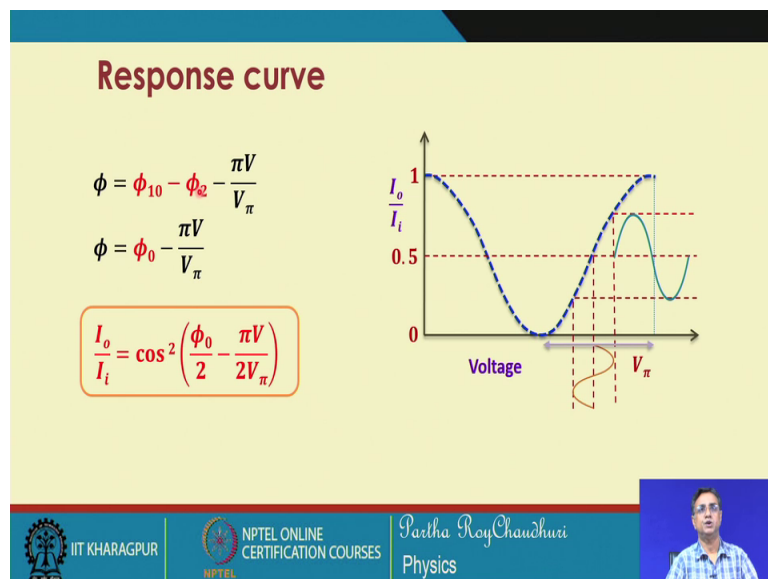
phase difference is 0 or twice pi we will get the maximum intensity. Or depending on the phase it can have any intensity distribution between these 2. So, any one of these outputs can be used as an intensity modulator.

So, this is the basic understanding that you have I input by under root 2 is the no so, this is this will be square root of square root of I. So, this is and then if you take the is this should be E I by root 2 E I by root 2 and this travels through a length of this. So, if I add these 2 vectorially or the phaser addition including this cosine phi 1 and cosine phi 2, then we can get this I intensity is equal to this which is the intensity available.

And then phi is the phase difference between these 2 light beams is phi 1 and phi 2; phi 1 is the phase difference which is due to this path and phi 2 is the phase difference along this path.

Now, phi 1 because you have an additional phase which is incorporated by this impressed external electric field. So, this is apart from the best phase you have an additional variable phase.

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So, this phi 1 0 minus because if I plug in this phi 1 value here in this expression then we it will get that phi equal to phi 0 minus pi V by pi. And then this look at this expression, this is this intensity output intensity as a cosine square function of the input intensity and

you have this response this cosine square function which looks like this. If this is the input intensity you get the output intensity which is modulated in this form.

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Host of multiple devices

$$\frac{I_o}{I_i} = \cos^2\left(\frac{\phi_0}{2} + \frac{\pi V}{2V_\pi}\right)$$

Can be used

- ✓ as an intensity modulator by adjusting (bias) $\phi_0 = \frac{\pi}{2}$
- ✓ in sensing using its linear response around $\frac{I_o}{I_i} = 0.5$
- ✓ as an optical switch by making $\frac{\phi_0}{2} = 0, 2\pi$ such that

$$\begin{cases} \frac{I_o}{I_i}(V=0) = 1 \\ \frac{I_o}{I_i}(V=V_\pi) = 0 \end{cases}$$

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So, this is a very interesting application and one can see that if you put this ϕ_0 by 2 this ϕ_0 equal to π by 2. Then this will be equal to π by 4 and it can be used as an intensity modulator. In that case you can use this Mach-Zehnder, this setup as a as to control the intensity of the light in sensing using the linear response where I_0 by I equal to 0.5, this value is 0.5 at this region you can get a linear.

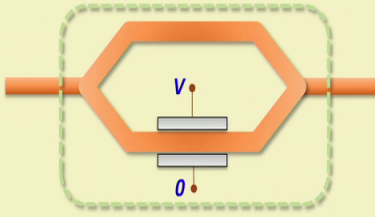
You look at this part of the curve is almost linear and it can be used by making ϕ_0 by 2 equal to 0 or twice π . So, if it is 0 then cosine square of this will be just you can look at this V equal to 0 I_0 by I_0 this is already 0. So, cosine 0 will give you 1 and V equal to V_π will give you 0.

So, you can switch the light in any of the output port just by controlling the voltage. When volt there is no applied voltage then the state is 1, when the applied voltage is V_π the state is 0. And the reverse will happen in the other port that is a complimentary port; we have 2 ports, here 2 out exit ports. So, it can be used as a switch which is very powerful and very much useful.

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4. Mach-Zehnder Interferometer

Very high speed commercially available I/O modulated (25GHz)



The diagram shows a Mach-Zehnder Interferometer (MZI) setup. An input beam enters from the left and is split into two paths by a beam splitter. The upper path is the reference arm, and the lower path is the signal arm. In the signal arm, there is an electro-optic modulator (EOM) consisting of two parallel plates with a bias voltage V applied across them. The output beams from both arms are recombined at a second beam splitter. The resulting output intensity is controlled by the phase delay introduced in the signal arm by the EOM.

- ✓ Uses electro-optic effect to vary RI
- ✓ A variable phase interference with light combined at output
- ✓ Bias voltage controls phase delay between the two outputs
- ✓ The output intensity is controlled

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Then this is also a Mach-Zehnder setup where you have beam where optical path which is split into 2 parts. And then again they are combined into one signal and in the paths in between one of the arm is mounted with this electro optic modulator. And when you apply the external field it works in the same way as discussed in the free space this intensity modulation scheme. It works in exactly in the same way.

And so, by applying this bias you applying this bias one can modulate the refractive index and as a result a variable phase interference pattern; so, interference pattern that is in terms of the intensity of the light only. There is no special pattern in this case and that that is controllable by the externally applied electric field. So, this bias voltage can control the phase delay between these 2 and the output intensity can be controlled.

So, this basic understanding is the same as we discussed in the previous case.

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Mach-Zehnder: LiNbO_3 intensity modulator

$A_{out} = A_1 + A_2$

Here $A_1 = \frac{1}{2}A_0 e^{i\beta n_0 L}$ and $A_2 = \frac{1}{2}A_0 e^{i\beta(n_0 + \Delta n)L}$

$A_{out} = \frac{1}{2}A_0 e^{i\beta n_0 L} (1 + e^{i\beta \Delta n L})$

Hence

$$I_{out} = |A_{out}|^2 = \frac{1}{4} I_0 |(1 + e^{i\beta \Delta n L})|^2$$

$$= I_0 \cos^2(\beta \Delta n L / 2)$$

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So, again moving with this bit of understanding that this amplitude for this field can be written as n_0 which and the length of propagation L , length of propagation L . And in the case of the second part that is the other beam you have an additional phase Δn which is sitting which is active over a length of L and therefore, A_{out} is the sum of these 2, the sum of these 2 amplitudes and then you take the mod of this, to get the intensity which gives you $I_0 \cos^2$.

This β is k_0 by twice π ; this is k_0 that is twice π by λ and then Δn into L by 2. So, this gives you the output intensity. And this is a very useful device and commercially available for many applications in communications in photonics in basic optics also.

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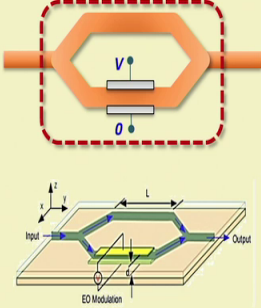
LiNbO₃ intensity modulator


$$I_{out} = I_0 \cos^2 \left(\frac{\pi}{\lambda} \Delta n L \right)$$

But $\Delta n = \frac{1}{2} n_0^3 r_{33} \frac{V}{d}$ (ignoring sign)

$$I_{out} = I_0 \cos^2 \left(\frac{\pi}{\lambda} n_0^3 r_{33} \frac{V}{d} L \right)$$

For Mach-Zehnder: $\frac{\pi}{\lambda} n_0^3 r_{33} \frac{V}{d} L = \frac{\pi}{2}$


$$V_{\pi} = \frac{\lambda d}{n_0^3 r_{33} L}$$




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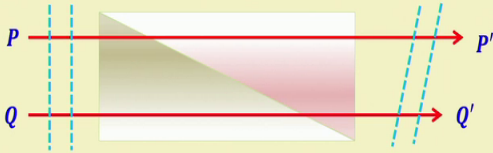
Lithium niobate in the case of this delta n is known we have seen this if you ignore the sign. And under this Mach-Zehnder configuration, then if I have to switch this we put this equal to pi by 2. It gives you that v pi equal to this and this value no having known this value we can use this modulator as a as a switching device.

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5. Beam deflector and scanner

Made from a pair of prisms

an EO crystal cut and oriented such that an applied electric field increases the RI of one prism while decreases that of the other




This produces a differential phase shift between beams traveling through the upper and lower portion of the crystal-combination



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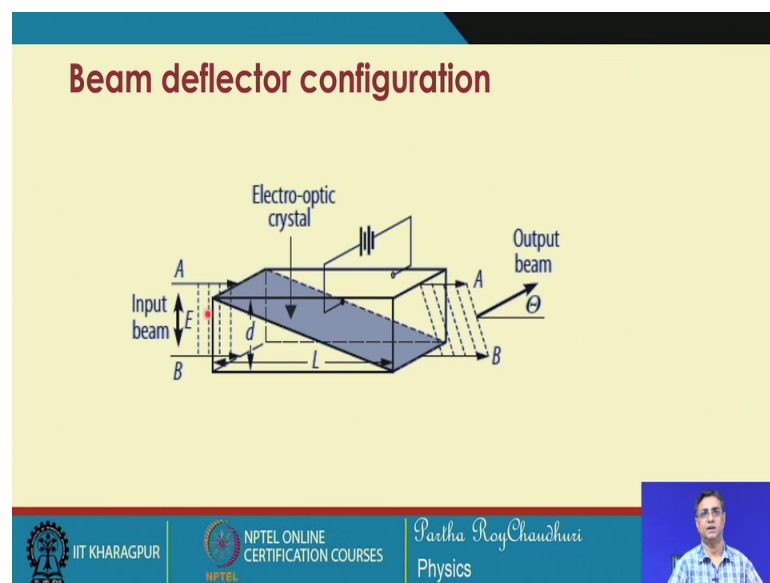


Now a beam scanner this is another very interesting application an electro optic crystal cut and oriented in such a way that the refractive index under the application of external

field the refractive index of the one prism increases, while the other prism decreases. The configuration is such that which is we will see which is very simple and doable.

This produces the differential phase delay because the light which is travelling at the lower part and that one which is travelling at the per part they will see different optical path and there will be a phase delay. And the beam while coming out will be tilted and in order to maintain this the plane wave front of the input then this entire beam will be deflected with a certain divergence angle.

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And let us see this is the configuration you have the electro optic crystal you apply the transverse configure in the transverse mode. So, you have an a applied voltage the beam is this is the input side, where the a beam is launched and this is the deflected beam and it makes an angle theta. Is the same this is how it is configured is very useful to understand.

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Beam deflector

The position of a wavefront at output face : $y' = n(x')L$

The wavefront undergoes a tilt by an angle : $\theta = -dy'/dx' = -L dn/dx'$

Tilt measured from beam divergence angle : $\theta_{beam} = \lambda/\pi w_0$

This results the number of resolvable spots :
(the deflector can produce when $d = 2w_0$)

$$N = \frac{\pi d L}{2\lambda} \frac{dn}{dx'}$$


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Then let us try to understand how it works the position of a wavefront at the output is here equal to you see this refractive index as a function of x' . Because it varies from here to here for the wavefront undergoes a tilt by an angle θ you see there is a there is an tilt by an angle θ which this is from the basic prism optics that this tilt angle is $L dn/dx'$.

This is the differential change in the refractive index over the length L . And that gives you the beam divergence angle θ and for this beam divergence can be calculated as $\theta = \lambda/\pi w_0$ where w_0 is the spot size of the beam the width of the beam.

So, this results in the number of resolvable spots under this confocal configuration this deflection can produce N when it is d equal to twice the spot size that is the $2w_0$. And with this one can have the number resolvable spots given by this expression. We will see how it comes this number of resolvable parts which is very useful in designing a device for beam deflection operation.

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Beam deflector

For KDP beam deflector (z-cut)

RI seen by wave at top: $n_p = n_o - \frac{1}{2} n_o^3 r_{63} E_z$ $\frac{dn}{dx} = \frac{\theta}{L} = n_o^3 r_{63} E_z$

RI seen by wave at bottom: $n_q = n_o + \frac{1}{2} n_o^3 r_{63} E_z$

The deflection angle is: $\theta = \frac{(n_q - n_p)L}{d} = \frac{L}{d} n_o^3 r_{63} E_z$

No. of resolvable spots $N = \frac{\theta}{\theta_{beam}} = \frac{L}{d} \frac{n_o^3 r_{63} E_z}{\lambda} \pi W_0 = \frac{L}{d} \frac{n_o^3 r_{63} E_z \pi d}{\lambda} \frac{1}{2} = \frac{\pi n_o^3 r_{63} E_z L}{2\lambda}$

$$N = \frac{\pi n_o^3 r_{63} E_z L}{2\lambda}$$

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So, for a KDP crystal let us suppose then we take the values the numbers here. So, for the upper part of the beam upper part of the beam which travels in a refractive index effective refractive index n_p equal to this and for the lower part of the beam which travels through an effective refractive index this is induced birefringence between them is just the difference of this and L into $\frac{dn}{dx}$ is the divergence θ equal to L times $\frac{dn}{dx}$. So, that gives you this relation because the difference between these 2 is $n_o^3 r_{63} E_z$.

Now, the deflection angle θ this θ equal to L times $\frac{dn}{dx}$, which can be written as n_q minus n_p by d . And that straight forward it comes out from here difference of this n_p minus n_q L by d that is what is here. So, number of resolvable spots is the divergence and divided by the beam divergence the deflection of the spot total by the beam divergence. So, if you take this if I plug in the values for θ , I use this number and for θ_{beam} I will use this number $\frac{\pi}{\lambda}$ by πW_0 , but W_0 under this optimum condition will be equal to d by 2.

So, it turns out $\frac{2\lambda}{\pi d}$ by $\frac{2\lambda}{\pi d}$. So, $\frac{2\lambda}{\pi d}$ by πd . So, when put together we get this expression which is the number of resolvable spots number of resolvable spots. So, that is what is shown here this, $\frac{dn}{dx}$ if you write in place of that the difference this electro optic coefficient refractive index cube and the external field.

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Beam deflector

Can be looked upon as:


RI seen by wave at top: $n_p = n_0 - \frac{1}{2} n_0^3 r_{63} E_z$ $\frac{dn}{dx'} = \frac{\theta}{L} = n_0^3 r_{63} E_z$


RI seen by wave at bottom: $n_q = n_0 + \frac{1}{2} n_0^3 r_{63} E_z$


Therefore, the number of resolvable spots: $N = \frac{\pi d L}{2\lambda} \frac{dn}{dx'} = \frac{\pi L}{2\lambda} n_0^3 r_{63} E_z$

$N = 1, \frac{1}{2} n_0^3 r_{63} E_z = \frac{\pi}{\lambda}$

Or $\Delta\phi = \pi$ gives $N = 1$








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Now, this would be lambda by now if you set n equal to 1 into this expression n equal to 1 then lambda by pi will be equal to lambda by pi will come to this side will be equal to n 0 r 6 3 E z L divided by 2. So, that is equal to what or the other way round that if we put delta phi or the phase difference equal to pi we will get n equal to 1.

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Beam deflector


For KDP beam deflector (z-cut)


The number of resolvable spots: $N = \frac{\pi L}{2\lambda} n_0^3 r_{63} E_z$

For deflection by one spot $N = 1, \frac{1}{2} n_0^3 r_{63} E_z = \frac{\pi}{\lambda}$ i.e., $\Delta\phi = \pi$

to fully deflect the spot, almost full half-voltage is required








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So, for one resolvable points we require this and. So, the deflection for at least by one spot we require this condition that n equal to 1. It is the other way that if you put del phi equal to pi you will get n equal to 1. To fully deflect the spot almost full half voltage is

required that is very interesting, but usually for electro optic crystal is the voltage requirement is very high. So, in practice in some applications this is used, but more frequently used is the acousto optic beam deflector which we will be discussing in later occasion.

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Scanner

$\theta = (n - 1)\alpha$
 $\Delta\theta = \alpha\Delta n = -\frac{1}{2}\alpha r n^3 E = -\frac{1}{2}\alpha r n^3 \frac{V}{d}$

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Now, the scanner this is another important device, but basically based on the same principle of the beam deflection for individual prism we know that is for thin prism that this refractive index minus 1 which is an alpha is the angle of the prism. So, you have delta theta which is equal to this. And now by applied voltage V you can actually control the you know the angle of emergence from the prism which can be used to scan different objects on the screen.

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Scanner

$\Delta\theta \propto V$

- ✓ Varying the applied voltage can be used to do **scanning**
- ✓ Several prisms can be **cascaded** by alternating the field

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So, by varying this and it can be actually the gain can be multiplied by cascading several prisms in the appropriate you notice a with appropriate design configuration

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6. Spatial light modulator

A device that modulates light intensity at different spatial position by a given factor

$$I_o(x, y) = T(x, y) I_i(x, y)$$

transmittance: $T(x, y) \propto V(x, y)$

- ✓ $T(x, y)$ is an array signal:
an image stored in the medium
- ✓ used as an image storage device
- ✓ incident beam is the read beam

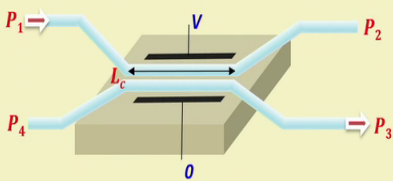
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Then there is another interesting application because by making use of this it can be used as a spatial light modulator where I_0 is a function of this transmission. And this applied voltage the spots you know the different points can be a modulated and it can be used as an image storage incident beam is a read beam. And the same beam can be used for right beam also.

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7. Directional Coupler

Control the coupling between the two parallel waveguide



Light is split into two output ports of two waveguides by coupling of guided modes

Complete transfer of power occurs when the modes interact over a length $L_c = \frac{\pi}{2K}$

K : coupling coefficient is a function of the RI profile of the two waveguides (composite)

K : coupling coefficient for modes of two waveguides, can be controlled electrically

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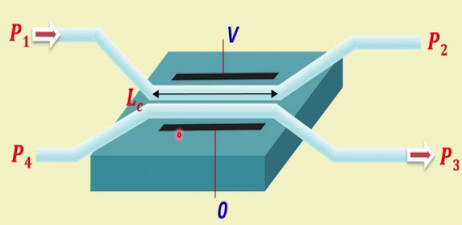
Directional coupler this is another very powerful device which where this electro optic effect is used to control the power output we have seen that if you launch light into one of the ports it can be split into 2 ports. Let us suppose that this is the 50 divider splitter, then by applying this voltage this refractive index of the composite structure can be controlled because this coupling coefficient this is this the length required to switch light from one port to another is the coupling length, which is the function of this kappa, but this kappa the coupling coefficient is a function of the refractive index of the composite structure of the total structure, the way it is done figured if it is just to.

So, but actually it is both the parallel wave guides through which this refractive index is one controlled. So, by controlling the voltage across this the west of the coupler, one can modulate the refractive index which will modulate the phase of the light which is travelling through this. And the splitting ratio can be controlled and this is this is very useful you may like to switch the light from here to here, but for a fixed coupler you cannot do, but using a electro optic modulation scheme, you can switch the light from here to here back and forth depending on the requirement which is which can be used for router applications for modulation applications and many more.

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7. Directional Coupler

Control the coupling between the two parallel waveguide



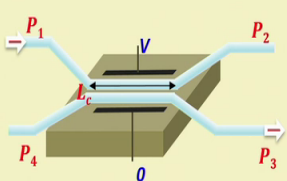
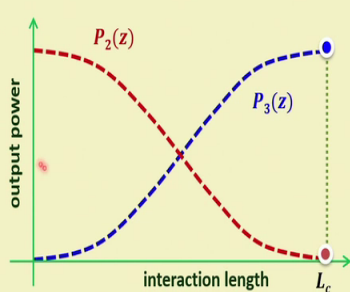
- ✓ Power transfer can be controlled by applied voltage
- ✓ Used as a SWITCH to toggle light between P_2 and P_3

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So, this directional coupler basically the basic physics that I have. So, you can switch this light from P 2 and P 3 by just applying the voltage.

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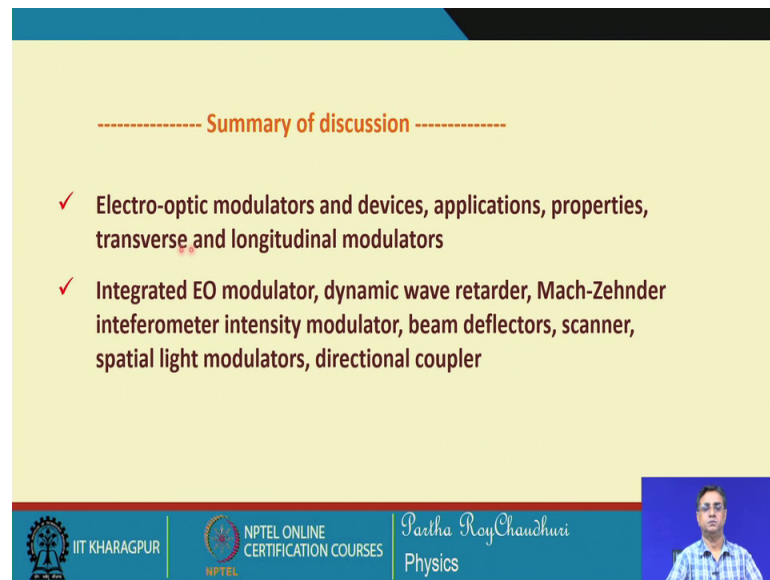
Response curve



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Between these 2, the response curve we have seen that it is a sine square cosine square function. In the case of optical directional coupler, you have seen this and at the switching point where L equal to L_c you have this point. So, the power is here and in the case of this L_c that is coupling port here the power is this. So, the light can be switched back and forth just by applying this external bias voltage, which is a very useful device.

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----- Summary of discussion -----

- ✓ Electro-optic modulators and devices, applications, properties, transverse and longitudinal modulators
- ✓ Integrated EO modulator, dynamic wave retarder, Mach-Zehnder interferometer intensity modulator, beam deflectors, scanner, spatial light modulators, directional coupler

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So, through this discussion we have tried to understand we have actually described few very useful electro optic modulators and devices, there the requirements to configure it as a longitudinal or a transverse modulator in terms of the geometry in terms of the properties. Then we discussed few devices in integrated electro optic modulator dynamically retarder Mach-Zehnder intensity modulator beam deflector scanner and directional coupler spatial light modulator.

Thank you very much.