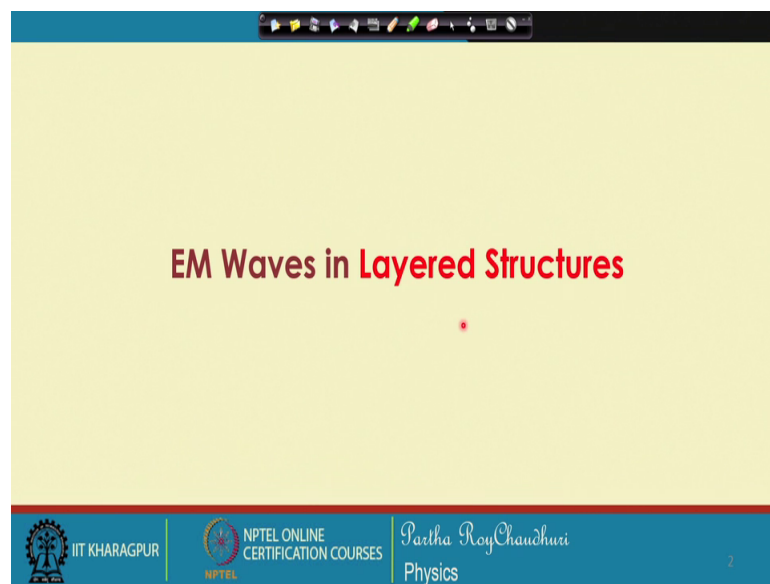


Modern Optics
Prof. Partha Roy Chaudhuri
Department of Physics
Indian Institute of Technology, Kharagpur

Lecture – 14
Wave propagation in layered structures (Contd.)

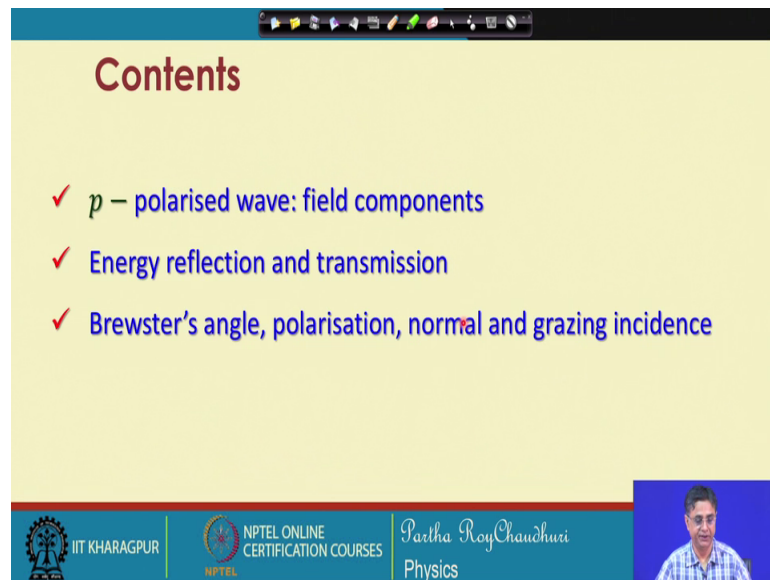
So, we have seen waves the basic configuration of electromagnetic waves at the interface of two dielectric media.

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And, now we will consider you have seen that the reflection amplitude reflection and amplitude transmission coefficients for the p-polarised wave.

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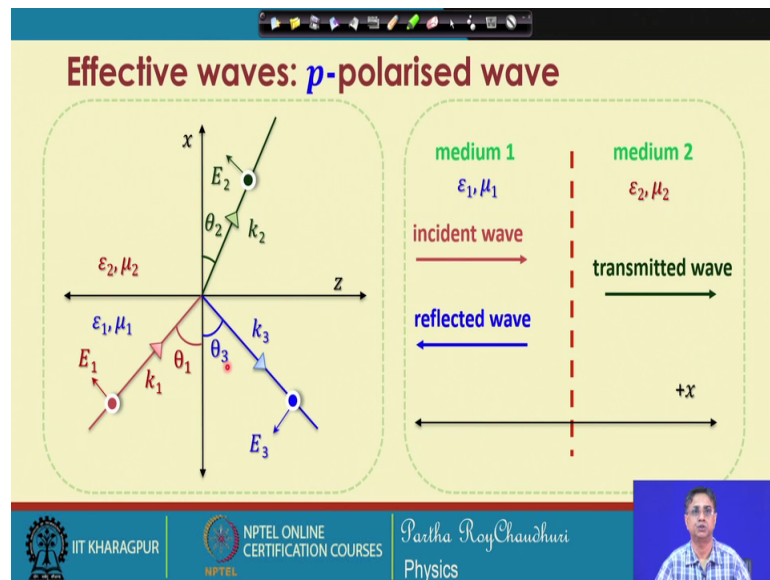
- ✓ p – polarised wave: field components
- ✓ Energy reflection and transmission
- ✓ Brewster's angle, polarisation, normal and grazing incidence

At the bottom of the slide, there is a blue footer bar containing the IIT Kharagpur logo, the NPTEL Online Certification Courses logo, the name "Partha RoyChaudhuri", and the word "Physics". A small video inset in the bottom right corner shows a man in a blue shirt speaking.

We will continue this p-polarised wave in terms of how to evaluate the field expressions, field components at the different regions. And, from the from the known expression of the energy amplitude reflection coefficient and amplitude transmission coefficient how to calculate using the pointing vector along the direction of propagation perpendicular to the direction of propagation and so on.

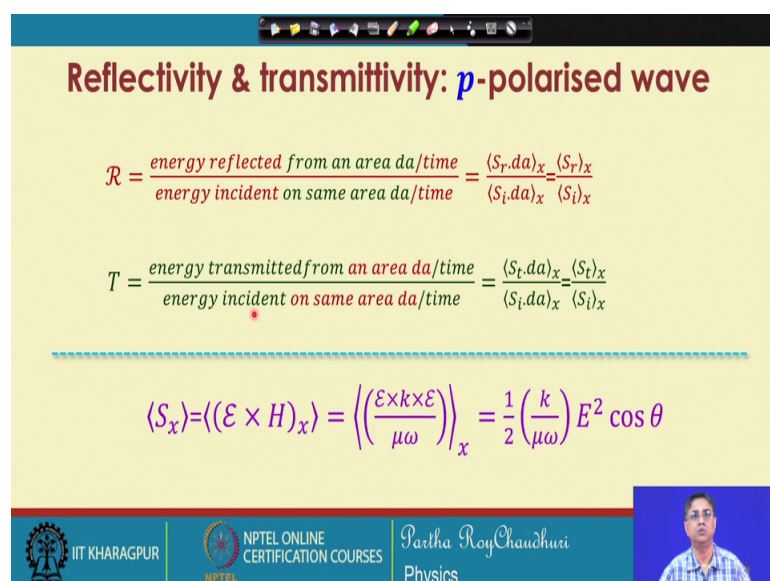
The energy reflection and energy so, the amount of energy that is associated in the process of reflection and transmission, that also we will try to understand. Then we will consider few representative cases in the case of p-polarized wave. For example, normal incidence, grazing incidence then if there is no reflection, then we will consider this individual cases to know more about this p-polarized like when they undergo a reflection transmission at the interface of two dielectric media.

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So, so the effective arrangement for this p-polarized wave I try to show here that you have a medium and this is the interface. So, the interface you have an incident media incident electromagnetic wave and this electromagnetic wave is reflected back and the transmitted wave. So, effective arrangement of this configuration you have the electric field which is lying in the in the x z plane. This is your x axis, this is your z axis and perpendicular the plane of the paper is y axis. So, the magic fields are along the y direction $k_1 \theta_1$ f $E_2 \theta_2$ $k_3 \theta_3$; all these things are by now it is known and we have defined those parameters.

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Now, the reflection and transmission in terms of the energy we want to evaluate. So, the energy reflection coefficient is defined as the energy reflected from an arbitrary area da per unit time divide by the energy incident on the same area da per unit time. So, we have a infinite similar area da on which the energy is incident that amount to be we want to calculate. And how much energy is reflected from that area, this ratio will give me the energy reflection coefficient; in terms of the pointing vectors.

Because, the pointing vector which is associated with the reflected wave is S_r which is E cross H and then for the area da we write this $S_r \cdot da$ and take the time average value of the x component of this. Because, we are interested if you go back we are interested in the energy reflection and transmission only along the x direction. So, this is the effective transfer of energy reflected energy from this wall and transmitted energy through this wall. So, it is only the x component that we are interested.

So, this gives you this S_r of x S_i of x and similarly for the energy transmission coefficient, we want to calculate we define in the same way that is the ratio of energy incident on an infinitesimal small area da per unit time. And, the ratio of this to this energy transmitted from an area da the same area per unit time. Therefore, in the same way we can we can express the energy transmission coefficient as the pointing vector associate with the transmitted wave and the average value of time average value of this.

So, you can represent in this form S_{tx} , x component of the pointing vector averaged the time average value. So, S_x can be written as if we write in terms of E and H fields this should E . So, E cross H x component this will be E cross k cross E , this is all known divided by ν into ω which is equal to because k cross E by ω we know that is equal to k by ω . So, you can write this expression in terms of this $E^2 \cos^2 \theta$.

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$$\langle S_x \rangle = \frac{1}{2} \left(\frac{k}{\omega \mu} \right) E^2 \cos \theta$$

but $\frac{k}{\omega \mu} = \frac{v}{\mu} = \frac{\sqrt{\mu \epsilon}}{\mu} = \sqrt{\frac{\epsilon}{\mu}}$

$$\langle S_x \rangle = \frac{1}{2} \left(\frac{\epsilon}{\mu} \right)^{1/2} |E|^2 \cos \theta$$

So, this S_x half equal to half k μ ω E cross cosine square theta, we will translate this S_x as k by μ ω you know k by μ ω may be written as v by μ is equal to μ ϵ under root by μ . So, effectively this gives you the square root of the permittivity of the ratio of the permittivity to the permeability.

So, this is your k by ω μ and this is also called the reciprocal of the μ by ϵ not under root is the characteristic impedance of the medium, we will see this later. So, now S_x can be written in this form half ϵ by μ square root of that E square cosine square theta. So, we will use this expression for S_x for the reflected and transmitted wave to evaluate how much part of the energy is reflected or transmitted in the process of undergoing reflection and transmission from the interface.

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Reflectivity: p -polarised wave

$$\mathcal{R}_p = \frac{\langle S_r \rangle_x}{\langle S_i \rangle_x}$$
$$\mathcal{R}_p = \frac{\frac{1}{2} \left(\frac{\epsilon_1}{\mu_1} \right)^{1/2} |E_3|^2 \cos \theta_3}{\frac{1}{2} \left(\frac{\epsilon_1}{\mu_1} \right)^{1/2} |E_1|^2 \cos \theta_1} = \left| \frac{E_3}{E_1} \right|^2 = |r_p|^2 \quad \theta_3 = \theta_1$$

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So, reflection energy reflection coefficient given by this can now be written in terms of this epsilon 1 by mu 1 square root of that in the numerator, which is to represent the time averaged value of the pointing vector along the x direction, in this form for the reflected wave. And, this is the same quantity for the incident wave, but interestingly because the incident waves medium and the reflected wave medium there the same. So, we have seen that epsilon 1 mu 1 and epsilon 3 mu 3, they are the same. So, they will cancel and as a result you just get end up with this expression that E 3 square by E 1 square because, theta 1 is also equal to theta 3.

So, this quantity also goes out, this cosine theta 1 cosine theta 1 in the denominator. They will be cancelled, this part will be cancelled. So, we are just left with E 3 by E 1 mod square which is equal to the nothing, but the r p square this also we have seen the amplitude reflection coefficient. So, energy reflection coefficient and the amplitude reflection coefficient they are related directly by just square of the amplitude reflection coefficient. So, this is an interesting finding, but this is not the same case when we will consider the amplitude transmission coefficient a connection for the amplitude energy transmission coefficient.

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Reflectivity: p -polarised wave

$$r_p = \frac{n_1^2 \sin \theta_1 \cos \theta_2 - n_2^2 \sin \theta_2 \cos \theta_1}{n_1^2 \sin \theta_1 \cos \theta_2 + n_2^2 \sin \theta_2 \cos \theta_1}$$

$$\mathcal{R}_p = |r_p|^2 = \left| \frac{n_1^2 \sin \theta_1 \cos \theta_2 - n_2^2 \sin \theta_2 \cos \theta_1}{n_1^2 \sin \theta_1 \cos \theta_2 + n_2^2 \sin \theta_2 \cos \theta_1} \right|^2$$

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But, now r_p we have seen is given by this. So, capital \mathcal{R}_p that is the energy transmission coefficient will be equal to the square of this quantity, square of r_p square.

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Reflectivity: p -polarised wave

$$\mathcal{R}_p = |r_p|^2 = \left| \frac{n_1^2 \sin \theta_1 \cos \theta_2 - n_2^2 \sin \theta_2 \cos \theta_1}{n_1^2 \sin \theta_1 \cos \theta_2 + n_2^2 \sin \theta_2 \cos \theta_1} \right|^2$$

$$= \left| \frac{n_1 n_2 \sin 2\theta_1 - n_1 n_2 \sin 2\theta_2}{n_1 n_2 \sin 2\theta_1 + n_1 n_2 \sin 2\theta_2} \right|^2$$

$$\mathcal{R}_p = \left| \frac{\sin 2\theta_1 - \sin 2\theta_2}{\sin 2\theta_1 + \sin 2\theta_2} \right|^2$$

$n_1 \sin \theta_1 = n_2 \sin \theta_2$

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And therefore, r_p square we can simply we can just simplify this expression in terms of because $n_1 \sin \theta_1$ can be taken as $n_2 \sin \theta_2$. So, you have cosine θ_2 and $\sin \theta_2$ n_1 and n_2 . So, we write in this from $n_1 n_2 \sin 2\theta_1$ $\sin 2\theta_1$ and here $n_2 n_2 \sin n_2 \sin \theta_2$ is equal to $n_1 \sin \theta_1$. So, this will give you n_1

cosine theta 1. So, it should be 1, this should be 2 and similarly for the denominator also, but if you reverse it remains the same.

So, this is how we can we can write this expression, that energy reflection coefficient is equal to sin 2 theta 1 different sin 2 theta 2 divide by some of this sin 2 theta 1. So that means, this is the reduced form that means, that it does not involve any n 1 or n 2. It is only the theta 1 and theta 2, the angle of incidence and angle of refraction. They are going to decide the amount of energy that will be reflected; the amount of energy that will be reflected from the interface.

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Transmittivity: p-polarised wave

$$T_p = \frac{\langle S_t \rangle_x}{\langle S_i \rangle_x} = \frac{\frac{1}{2} \left(\frac{\epsilon_2}{\mu_2}\right)^{1/2} |E_2|^2 \cos \theta_2}{\frac{1}{2} \left(\frac{\epsilon_1}{\mu_1}\right)^{1/2} |E_1|^2 \cos \theta_1} = \left(\frac{\epsilon_2}{\epsilon_1}\right)^{1/2} \frac{|E_2|^2 \cos \theta_2}{|E_1|^2 \cos \theta_1}$$

$$T_p = |t_p|^2 \left(\frac{\epsilon_2}{\epsilon_1}\right)^{1/2} \frac{\cos \theta_2}{\cos \theta_1}$$

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Now, the remaining part that is the energy transmission coefficient we can evaluate in the same way. The pointing vector associated with the transmitted wave and the pointing vector associated with the reflected wave, with the incident wave and you can write this expression because, we have written the general expression for the pointing vector. So, in case of the transmitted wave we will have to write in this form that is cosine theta 2 and E 2 square and for the first medium that is for associated with the incident wave we write this in this form.

But, this time you can see is since mu 1 and mu 2 we have assume that that is there non-magnetic and is equal to mu 0 so, they will cancel. And, it effectively gives you epsilon 2 by epsilon 1 sorry, there is a mistake it should be epsilon 1 epsilon 2 by epsilon 1 under root of that multiplied by this two. And, this time cosine theta 2 and cosine theta 1 theta 1

theta 2 being different they will be retained in the expression for energy transmission coefficient. So, we can write this equation in this form, that energy transmission coefficient is equal to t p square amplitude transmission coefficient square multiplied by the ratio under root of the ratio of the dielectric permittivities. This should be epsilon 1 and the ratio of the angles cosine of the angles.

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Transmittivity: *p*-polarised wave

$$T_p = |t_p|^2 \left(\frac{\epsilon_2}{\epsilon_1} \right)^{1/2} \frac{\cos \theta_2}{\cos \theta_1}$$

$$= \frac{4\epsilon_1\epsilon_2 \sin \theta_1 \cos \theta_1 \sin \theta_2 \cos \theta_2}{(\epsilon_2 \cos \theta_1 \sin \theta_2 + \epsilon_1 \sin \theta_1 \cos \theta_2)^2}$$

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So, this is how we can write this expression T p equal to this, which can be can be written in this form. Because, if we use this expression for t p that the transmission amplitude transmission coefficient, if we use that expression we can write T p equal to this equation.

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Transmittivity: p-polarised wave

$$T_p = \frac{4n_1^2 n_2^2 \sin \theta_1 \cos \theta_1 \sin \theta_2 \cos \theta_2}{(n_2^2 \cos \theta_1 \sin \theta_2 + n_1^2 \sin \theta_1 \cos \theta_2)^2}$$
$$= \frac{4n_1^2 n_2^2 \sin 2\theta_1 \sin 2\theta_2}{(n_1 n_2 \sin 2\theta_2 + n_1 n_2 \sin 2\theta_1)^2}$$
$$T_p = \frac{4 \sin 2\theta_1 \sin 2\theta_2}{(\sin 2\theta_2 + \sin 2\theta_1)^2}$$

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So, the energy transmission reflection of energy transmission coefficient can be again expressed in this form. And, if I use the same principle that is $n_1 \sin \theta_1 = n_2 \sin \theta_2$ which comes directly from the Snell's law. We can write down the expression for the numerator $n_1 \sin \theta_1 \cos \theta_1$ will give you $\sin 2\theta_1$ $n_2 \sin \theta_2 \cos \theta_2$ will give you $\sin 2\theta_2$ multiplied by 4 and multiplied by 4 in the denominator.

So, you can do some algebra, some simple manipulation of the above expression using $n_1 \sin \theta_1 = n_2 \sin \theta_2$, we will end up with this expression. And so, you can write this compact you know expression for the energy transmission coefficient for the p-polarized wave using this. So, we have both the energy reflection coefficient as R_p and the energy transmission coefficient as capital T_p for the p-polarized wave.

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Reflectivity & transmittivity: p -polarised wave

$$R_p = \left(\frac{\sin 2\theta_1 - \sin 2\theta_2}{\sin 2\theta_1 + \sin 2\theta_2} \right)^2$$
$$T_p = \frac{4 \sin 2\theta_1 \sin 2\theta_2}{(\sin 2\theta_1 + \sin 2\theta_2)^2}$$

$R_p + T_p = 1$

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So, these are the reflectivity and transmissivity. So, this two if we put together you get R_p plus T_p equal to 1. So, very evident this square of this difference then, if you add $4 \sin 2\theta_1 \sin 2\theta_2$ denominator it remains the same so, it become say equal to 1. So, that tells you that the total energy which is incident is equal to, if you assume it is equal to 1 unity so, that remains the same. So, that is through this process of reflection and transmission the conservation of energy remains valid.

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Consequences: p -polarised wave

- ✓ Fresnel coefficients p – polarised waves
- ✓ A few observations under certain given conditions

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Now, with this understanding that we have been able to evaluate the reflection amplitude reflection, amplitude transmission coefficients as well as the energy reflection and energy transmission; that is the reflectivity and transmissivity. So, knowing all these parameters we will now, study few representative cases, few special conditions which are under certain conditions; what happens with the reflection or transmission.

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Reflectivity: *p*-polarised wave

case-I: *p* – polarised wave

when $n_1 = n_2$

Snell's law $n_1 \sin \theta_1 = n_2 \sin \theta_2 \Rightarrow \theta_1 = \theta_2$

amplitude reflection coefficient

$$r_p = \frac{n_1^2 \sin \theta_1 \cos \theta_2 - n_2^2 \sin \theta_2 \cos \theta_1}{n_1^2 \sin \theta_1 \cos \theta_2 + n_2^2 \sin \theta_2 \cos \theta_1} \Rightarrow r_p = 0$$

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So, let us take this condition that in the equation for reflectivity or amplitude reflection coefficient and transmission coefficient, if I use this condition the first case that is n_1 equal to n_2 . If you use this condition that both the media are having the same refractive indices; in that case, what will happen $n_1 \sin \theta_1$ equal to $n_2 \sin \theta_2$, this tells you that θ_1 must be equal to θ_2 . If θ_1 is equal to θ_2 , there are two possibilities: one is that these two media are the same exactly the same; that means there is no interface.

So that means, the ray will not undergo any reflection or transmission, it is simply penetrate through the medium we under deviated and undistorted θ_1 remains exactly equal to θ_2 . And, there is a second possibility if I use this n_1 equal to n_2 , you find that r_p equal to 0; because, $n_1 \sin \theta_1 = n_2 \sin \theta_2$. So, all of them will make this right hand side equal to exactly 0. Now, for this case n_1 equal to n_2 we have seen θ_1 equal to θ_2 , amplitude reflection coefficient r_p equal to this.

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Reflectivity: p -polarised wave

case-I: p – polarised wave

when $n_1 = n_2$ $\theta_1 = \theta_2$ $r_p = 0$

- ✓ $r_p = 0$ means no reflected wave
- ✓ If you put a transparent object (glass) inside a liquid of same RI, the object is not visible
- ✓ Both media may be same

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This means that there is no reflected wave, the second possibility that now we are interested. First one is that the two media at the same media, that is it is one medium through which the wave is traveling and therefore, because there is no interface θ_1 remains θ_2 and the wave goes undeviated, undistorted. But it could so, happen that there to different media, but their effective indices are the same. In that case we put r_p equal to 0; that means, there is no reflected wave. It means that, if you put a transparent objective glass inside a liquid of same refractive index this situation, the object will not be visible because there is no reflection.

If there is no reflection from any object we cannot see that object and the first possibility that we have already discussed that is both the media may be the same media. So, this is one special situation when n_1 equal to n_2 and we plug in into the Fresnel's condition, Fresnel equation and we have seen that it could be two way possible.

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Reflectivity: p -polarised wave

case-II: p – polarised wave

when $r_p = 0$ at some angle of incidence

then $n_1^2 \sin \theta_1 \cos \theta_2 = n_2^2 \sin \theta_2 \cos \theta_1$

multiply both sides by $\sin \theta_2$ and use Snell's law

$$n_1^2 \sin \theta_1 \cos \theta_2 \sin \theta_2 = n_2^2 \sin^2 \theta_2 \cos \theta_1$$
$$\sin 2\theta_1 = \sin 2\theta_2$$

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Now, second thing is that if you assume that r_p itself equal to 0, the reflection amplitude reflection coefficient is 0 that is that may happen for some angle of incidence. For some angle of incidence the reflection amplitude is 0 that is there is no reflection. When does it happen? If $n_1^2 \sin \theta_1 \cos \theta_2$ is equal to because, I put r_p equal to 0 from where I can write this equation. Now, if you multiply both sides by $\sin \theta_2$ and use Snell's law, we can simply show that $\sin \theta_2 \cos \theta_1 = \sin^2 \theta_2$.

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Reflectivity: p -polarised wave

case-II: p – polarised wave

$$\sin 2\theta_1 = \sin 2\theta_2$$

✓ thus, either $\theta_1 = \theta_2$ \Rightarrow condition-I

✓ or may be when $\theta_1 = \frac{\pi}{2} - \theta_2$

i.e., when $\theta_1 + \theta_2 = \frac{\pi}{2}$

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This could be true, if theta 1 is equal to theta 2 is a direct condition theta 1 equal to theta 2 or it may so, happen that theta 1 equal to pi by 2 minus theta. That is pi theta 1 plus theta 2 is equal to pi, this is also possible.

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Reflectivity: *p*-polarised wave

case-II: *p* – polarised wave $r_p = 0$

$\theta_1 + \theta_2 = \frac{\pi}{2}$

- ✓ reflected and transmitted waves are at right angles to each other, there is no reflected wave
- ✓ no reflection for parallel component of E i.e., for E lying in the xz – plane

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Now, for this case when there is no reflection and theta 1 plus theta 2 equal to pi, this situation is already known to us this involves the Brewster's condition. In this case the reflected and transmitted waves are at 90 degree. These two waves reflected and transmitted waves are at 90 degree to each other and there is no reflection when there is only that p-polarised to f, this p-polarised to f.

And, there is no s polarised f, there is no parallel component of the electric field only the only this component the electric fields are lie in the exact plane. So now, reflection for parallel component of E and for the situation that is E lying in the exact plane, so, this gives you a situation that the waves are incident and they will be transmitted out. There will be no reflection because for which you get this condition r p equal to 0.

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Reflectivity: p -polarised wave

case-II: p – polarised wave $\theta_1 + \theta_2 = \frac{\pi}{2}$

the corresponding **angle of incidence**:

$$\cos \theta_1 = \sin \theta_2 = \frac{n_1}{n_2} \sin \theta_1 \Rightarrow \tan \theta_2 = \frac{n_1}{n_2}$$

when angle of incidence $\theta_1 = \theta_p = \tan^{-1} \frac{n_1}{n_2}$
and the incident wave is unpolarised
reflected wave contains ONLY E_y field \Rightarrow linearly polarised

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Now, this $\theta_1 + \theta_2 = \frac{\pi}{2}$, for this the corresponding angle of incidence we are interested because, this will happen only for a very special, only for a fixed for a specific angle of incidence which will depend on the two media involved. So, the condition is $\cos \theta_1 = \sin \theta_2$ because, by using this $\theta_1 + \theta_2 = \frac{\pi}{2}$ will give you $\sin \theta_2 = \cos \theta_1$. And, from here by using Snell's law we can write this equation. The consequences very straight forward, $\tan \theta_2 = \frac{n_1}{n_2}$ which is again a very known condition, which is again a very this should be $\tan \theta_1 = \frac{n_2}{n_1}$, sorry there is a mistake this would be θ_1 .

So, when angle of incidence θ_1 is equal to θ_p , that is this p -polarized angle of incidence which is equal to $\tan^{-1} \frac{n_1}{n_2}$, then the incident wave and if you assume that the incident wave is unpolarized and the angle of incidence is this. Then the reflected wave contains only E_y because, the component of the electric field which is lying in the exit plane, for the incident wave will not be reflected. Only the component which is perpendicular to the exit plan, that is along E_y that will be transmitted through. Such a situation is the linearly polarized wave. So, we have an incident wave which has this component E_y and also exit plane component and it gives you a linearly polarized light output.

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Reflectivity: *p*-polarised wave

case-II: *p* – polarised wave

angle of incidence

$$\theta_1 = \theta_p = \tan^{-1} \frac{n_2}{n_1}$$

↓

Brewster's angle

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So, you can see the situation the incident wave has both the polarizations the s polarized wave and p-polarized wave, but the transmitted wave will be partially polarized and the reflected wave we will contain only the perpendicular component, that is the E y component of the electric field. So, this light is purely polarized, but this happens only at a certain angle theta 1 equal to theta p equal to tan inverse of n 2 by n 1 by n 2. So, this specific angle of incidence for which the reflected wave is purely polarised is called the Brewster's angle.

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Reflectivity: *p*-polarised wave

case-III: *p* – polarised wave

normal incidence

use Snell's law: $n_1 \sin \theta_1 = n_2 \sin \theta_2$ in

$$r_p = \frac{n_1^2 \sin \theta_1 \cos \theta_2 - n_2^2 \sin \theta_2 \cos \theta_1}{n_1^2 \sin \theta_1 \cos \theta_2 + n_2^2 \sin \theta_2 \cos \theta_1}$$

• $r_p = \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1}$ ← another form

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Now, we will consider two more cases: that is the normal incidence and the grazing incidence. For the normal incidence we use Snell's law $n_1 \sin \theta_1 = n_2 \sin \theta_2$ in the expression for this r_p . This we have seen that another form of this amplitude reflection coefficient can be written in this way $r_p = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2}$. So, we will use this expression for normal incidence.

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Reflectivity: p -polarised wave

case-III: p – polarised wave

normal incidence: $\theta_1 = \theta_2 = 0$

$$r_p = \frac{n_1 - n_2}{n_1 + n_2}$$

for air-glass interface: $n_1 = 1.0$ and $n_2 = 1.5$

$r_p = -0.2$ and $R_p = 0.04$ ← 4% Fresnel reflection

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Normal by normal incidence what do you mean that, the angle of incidence is 0, angle of reflection, angle of transmission all of them will be eventually 0. So, r_p we can write as $\frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2}$ from this expression, from this expression $\cos \theta_2 = \cos \theta_1 = 1$ and so on. So, you get $r_p = \frac{n_1 - n_2}{n_1 + n_2}$ and this is a very well known expression for Fresnel reflection, for the air glass interface; where $n_1 = 1$ and you assume for glass $n_2 = 1.5$.

And, this gives you $r_p = -0.2$ and this energy reflection is 0.04 that is 4 percent. So, this is usually termed as the 4 percent Fresnel reflection from air glass interface. And, this is the reason that from ordinary glass in the air we can see some reflected light, we can see partially our face if you look at the glass surface.

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Reflectivity: *p*-polarised wave

case-IV: *p* – polarised wave

grazing incidence: $\theta_1 = \frac{\pi}{2}$

$$r_p = \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1} \Rightarrow r_p \approx 1 - \frac{2 \left(\frac{n_2}{n_1}\right)^2 \alpha_1}{\sqrt{\left(\frac{n_2}{n_1}\right)^2 - 1}}$$

$$\alpha_1 = \frac{\pi}{2} - \theta_1$$

Then the possibility that the incidence the angle of incidence is very large that is at grazing angle that is theta 1 we will use theta 1 equal to pi by 2. So, r_p will be equal to $n_1 \cos \theta_2 - n_2 \cos \theta_1$, where we will use theta 1 equal to pi by 2. And, if you do some calculation some algebraic manipulation, you can show that r_p will be approximately equal to $1 - \frac{2 \left(\frac{n_2}{n_1}\right)^2 \alpha_1}{\sqrt{\left(\frac{n_2}{n_1}\right)^2 - 1}}$ where alpha 1 is nothing, but pi by 2 minus theta. We have substituted for pi by 2 minus theta 1 is equal to alpha that is the small angle which is the wave is making with the interface, this angle is alpha.

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Reflectivity: *p*-polarised wave

case-IV: *p* – polarised wave

grazing incidence: $\theta_1 = \frac{\pi}{2}$

when $n_2 > n_1 \Rightarrow |r_p| \rightarrow 1$

reflection is complete

So, you can see this figure a small angle α_1 which they wave mix with the interface and at grazing angle it reflected, it is reflected out. And, from this expression you can see that you can see that, for this situation when n_2 is greater than n_1 this r_p tends to unity. That means, the reflection is almost complete that is entire part of the wave will be reflected and there is no transmitted wave.

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Reflectivity: p -polarised wave

case-IV: p - polarised wave

grazing incidence: $\theta_1 = \frac{\pi}{2}$

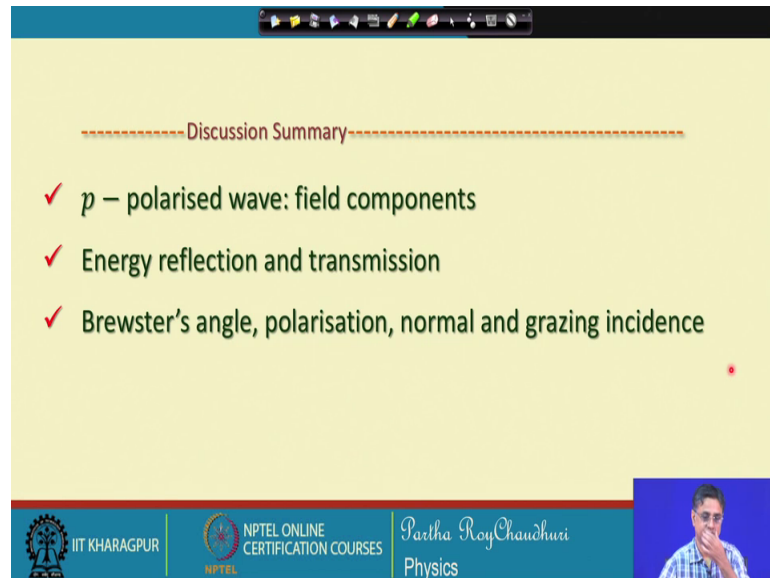
when $n_1 > n_2$ \Rightarrow

total internal reflection

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For the other situation that is, if n_1 is greater than n_2 , this medium having refractive index higher than this one; the rarely faded medium. In that case this angle is more than the critical angle of incidence as a result the wave we will undergo total internal reflection. So, in the case both the case that is when n_2 is greater than n_1 then also the reflection is complete and the other case when n_1 is greater than n_2 , then the wave undergoes a total internal reflection.

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-----Discussion Summary-----

- ✓ p – polarised wave: field components
- ✓ Energy reflection and transmission
- ✓ Brewster's angle, polarisation, normal and grazing incidence

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Thus, we have we have discussed all the possibilities with a p-polarized wave starting from the amplitude reflection, amplitude transmission coefficient, their energy reflection and energy transmission, that is the reflectivity and transmissivity. Then, we have also discussed some representative situations when r_p equal to 0 or n_1 , the media are having the same refractive indices and what is the consequence of all these things.

With this knowledge and background, in the next section we will consider the s polarized wave that is t polarized wave and we will look at the energy reflection and transmission coefficients and other properties. We will also look at the total internal reflection, we will also compare the situation, certain things will be same for both the polarization waves polarized waves that also we will consider.

Thank you.