## Introduction to Astrophysical Fluids Prof. Supratik Banerjee Department of Physics Indian Institute of Technology, Kanpur

## Lecture – 18 Derivation of real fluid equations

Hello. So, we continue our discussion of the Derivation of real fluid equations; starting from distribution function which has a small first order perturbation with respect to the zeroth order local Maxwellian distribution.

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\* BGK equation gives, (taking f ≈ f.)  $g \approx -\tau \left[ \frac{\partial}{\partial t} + \vec{u} \cdot \vec{\nabla} + \vec{a} \cdot \vec{\nabla}_{\vec{u}} \right] f_{o}$ \* So now we have to calculate, (a.  $\vec{\nabla_a}$ ) fo [direct]  $\frac{\partial f_0}{\partial t} = \frac{\partial f_0}{\partial n} \frac{\partial n}{\partial t} + \frac{\partial f_0}{\partial T} \frac{\partial T}{\partial t} + \frac{\partial \vec{V}}{\partial t} \cdot \frac{\partial f_0}{\partial v}$ and  $\frac{\partial f_0}{\partial x_i} = \frac{\partial f_0}{\partial n} \frac{\partial n}{\partial x_i} + \frac{\partial f_0}{\partial \tau} \frac{\partial T}{\partial x_i} + \frac{\partial \vec{v}}{\partial x_i} \cdot \frac{\partial f_0}{\partial \vec{v}}$ \* We know  $f_0 = n(\vec{r},t) \left(\frac{m}{2\pi \kappa_B T(\vec{r},t)}\right)^{3/2} - \frac{m(\vec{u}-\vec{v}(\vec{r},t))^2}{2\kappa_B T}$ 

So, we just stated last time that BGK equation considerably simplifies the total formalism just by saying that only one of the term,

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\* Under this distribution function, the collision integral  
can be written as,  

$$C \cdot I \cdot = \int d^3 u_1 \int d\Omega | \vec{u} - \vec{u}_1 | \sigma (\Omega \int f_0' g_1' + f_0' g_1' - f_0 g_1 - f_0 g_1' -$$

that is the last term of the four terms of  $f'_0g'_1 + f'_{01}g' - f_0g_1 - f_{01}g$  is sufficient to adequately recover all the transport phenomena in a usual fluid.

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\* The analytical treatment of transport phenomena using BGIK equations was first done by Liepmann, Nara Simha & Chahine (1962) \* Before attacking this problem, let us realise an interesting thing! let us assume that the main reason for departure from Maxwellian is & brong gradients in the system. In that case,  $\| [\vec{u} \cdot \vec{v})_{f_{o}} \| \sim \frac{|g|}{2}$   $\Rightarrow \| \vec{u} \|_{f_{o}} \sim \|g\| \rightarrow \|g\| \sim \lambda \rightarrow \infty$ 

Now, this was done by three scientists Liepmann, Narasimha and Chahine. So, we said that finally, a very reasonable approximation gives  $g \approx -\tau \left(\frac{\partial}{\partial t} + \boldsymbol{u} \cdot \nabla + \boldsymbol{a} \cdot \nabla_{\boldsymbol{u}}\right) f_0$ . So,  $f_0$  we know. What is  $f_0$ ?  $f_0$  is nothing but the local Maxwellian distribution.

So, now we have to calculate the three term. Now, we know that  $f_0$  is the local Maxwellian distribution. So, calculating  $(\mathbf{a} \cdot \nabla_{\mathbf{u}}) f_0$  is reasonably direct because in  $f_0$ , if you see the

form of  $f_0$  the dependence on u is explicit dependence and that is why this is direct to calculate. So, please calculate at home.

Once again in this course it will be not possible to do all the steps of intermediate algebra, but you are supposed to check all the steps of algebra at home; if in case you are blocked you can ask me or you can just refer to one of the books which I suggested in your course handout.

Then we have to calculate also  $\frac{\partial f_0}{\partial t}$  and  $\frac{\partial f_0}{\partial x_i}$ , which corresponds to first two terms in the expression of g. Now, for that we have to realize the fact that in  $f_0$ , which is the local Maxwellian, the explicit space and time dependent comes through three variables n, T and v.

So, when we will try to calculate  $\frac{\partial f_0}{\partial t}$  the total expression will be simply

$$\frac{\partial f_0}{\partial t} = \frac{\partial f_0}{\partial n} \frac{\partial n}{\partial t} + \frac{\partial f_0}{\partial T} \frac{\partial T}{\partial t} + \frac{\partial f_0}{\partial \nu} \frac{\partial \nu}{\partial t}.$$

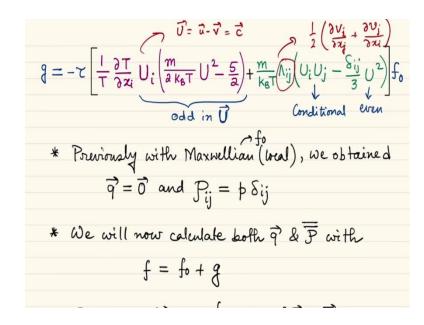
Where,  $\frac{\partial f_0}{\partial v} = \nabla_v f_0$ , so in the similar way you can also write  $\frac{\partial f_0}{\partial x_i}$  as a summation of three terms through their implicit dependence of *n*, *T* and *v* (see below).

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$$g \approx -\tau \left[ \frac{\partial}{\partial t} + \vec{u} \cdot \vec{\nabla} + \vec{a} \cdot \vec{\nabla}_{\vec{u}} \right] f_{\delta}$$
\* So now we have to calculate,  $(\vec{a} \cdot \vec{\nabla}_{\vec{u}}) f_{\delta}$  [direct],  

$$\frac{\partial f_{\delta}}{\partial t} = \frac{\partial f_{\delta}}{\partial n} \frac{\partial n}{\partial t} + \frac{\partial f_{\delta}}{\partial T} \frac{\partial T}{\partial t} + \frac{\partial \vec{V}}{\partial t} \cdot \frac{\partial f_{\delta}}{\partial \vec{V}} ,$$
and  $\frac{\partial f_{\delta}}{\partial z_{i}} = \frac{\partial f_{\delta}}{\partial n} \frac{\partial n}{\partial z_{i}} + \frac{\partial f_{\delta}}{\partial T} \frac{\partial T}{\partial z_{i}} + \frac{\partial \vec{V}}{\partial z_{i}} \cdot \frac{\partial f_{\delta}}{\partial \vec{V}} ,$ 
\* We know  $f_{\delta} = n(\vec{r}, t) \left(\frac{m}{2\pi k_{B}T(\vec{r}, t)}\right)^{3/2} - \frac{m(\vec{u} \cdot \vec{V}(\vec{r}, t))^{2}}{2 k_{B}T}$ 
\* Now a few steps of Straight forward but careful Algebro (Please Check) finally give

So, now you have to do step by step some straight forward but careful algebra. If you make some mistake over here then you will be lost. So, do slowly even at home when you will practice, do slowly but step by step do not do any step jump.



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And this will finally give you g to be equal to the whole thing (see above). So, it may look like a bit I mean lengthy or a bulky, but believe me if you try to understand segment wise this is quite interesting.

So, inside the bracket there are several things. So,  $\left(\frac{\partial}{\partial t} + \boldsymbol{u} \cdot \nabla + \boldsymbol{a} \cdot \nabla_{\boldsymbol{u}}\right) f_0$  all these things give us finally, a factor times  $f_0$ . So, finally, again this whole thing is proportional to  $f_0$  as well this is also proportional to  $\tau$ .

That is very very interesting that it directly says that when your system is strongly collisional,  $\tau$  is very small-your g is small; when  $\tau$  is big and your systems collisionality is very weak then you have basically a considerable g.

So, *g* is consisting of globally two type of contributions one comes from  $\frac{1}{T}\frac{\partial T}{\partial x_i}U_i(\frac{m}{2\kappa_BT}U^2-\frac{5}{2})$  and this one is proportional to  $\frac{\partial T}{\partial x_i}$ , another one proportional to  $\Lambda_{ij}$ ; if you remember what  $\Lambda_{ij}$  was! So  $\Lambda_{ij}$  was just the velocity gradient tensor like  $\frac{1}{2}(\frac{\partial v_i}{\partial x_j}+\frac{\partial v_j}{\partial x_i})$ , this is a symmetric tensor.

So, one term should be proportional to the temperature gradient and you can see that term has an odd dependence on the components of U because there is always one  $U_i$  which is unpaired, which makes component wise the thing odd.

Now, another part which is depending on the velocity gradient has two parts – one is of course, clearly even, the another is conditionally even or odd. So, let us say if you multiplied with  $U_iU_j - \frac{\delta_{ij}}{3}U^2$ , something where both  $U_i$  and  $U_j$  can pair, like if you just multiply  $U_i$  and  $U_j$ , with all the thing, then this part will become behave as a even combination.

On the other hand, if you just multiply with a single  $U_i$ , then  $U_i$  will pair, but  $U_j$  will remain unpaired or uncoupled. So, that will give you an odd contribution. So, this is the conditional part,  $\delta_{ij}U^2$  is even always because it is  $U^2$ .

So, you see after all these simplifications finally, we have a form of g which looks like a bit frightening, but believe me finally this is a very handy form. So, you can decouple the total contribution as a sum of a contribution which is proportional to the linear temperature gradient another is a linear velocity gradient.

So, if you remember now, that from your basic knowledge or previous knowledge of fluid dynamics or something, it is somehow expected that the heat transfer should be related to temperature gradient term and momentum transfer or the viscosity basically you know that viscosity is nothing but a transfer of momentum or transport of momentum should be related to  $\Lambda_{ij}$ , and one of the very simplest models we know is the Newtonian fluid model that I will come later.

But, roughly speaking you can easily understand that maybe the temperature gradient part is related to the thermal conduction or thermal transport part and  $\Lambda_{ij}$  it is related to the momentum transport part. And, we will see that there is no exception to that, what we have guessed is actually correct.

So, previously with Maxwellian distribution we had simply,  $\boldsymbol{q}$  is equal to 0, and the pressure tensor was trivially diagonal with a single value which says that all the diagonal elements were equal. So, it was simply a scalar. So, we will now calculate again  $\boldsymbol{q}$  and  $\overline{P}$ 

with this new distribution function and as we can expect that,  $\boldsymbol{q}$  will no longer be 0,  $P_{ij}$  will no longer be purely diagonal right.

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edd in 
$$\overrightarrow{U}$$
 Conditional even  
\* Previously with Maxwellian (brad), we obtained  
 $\overrightarrow{q} = \overrightarrow{0}$  and  $\overrightarrow{P}_{ij} = \overrightarrow{p} \delta_{ij}$   
\* We will now calculate both  $\overrightarrow{q} & \overrightarrow{P}$  with  
 $f = f_0 + g$   
\* Evidently,  $\overrightarrow{q} = \frac{m}{a} \int (f_0 + g) U^2 \overrightarrow{U} d^3 \overrightarrow{U}$   
 $= \frac{m}{a} \int g U^2 \overrightarrow{U} d^3 \overrightarrow{U}$ 

So, for  $\boldsymbol{q}$  we will have by definition  $\frac{m}{2} \int (f_0 + g) U^2 \boldsymbol{U} d^3 \boldsymbol{U}$ . So,  $\frac{m}{2} \int f_0 U^2 \boldsymbol{U} d^3 \boldsymbol{U} = \boldsymbol{0}$ . So, finally, the term which remains is  $\frac{m}{2} \int g U^2 \boldsymbol{U} d^3 \boldsymbol{U}$ . So, non-zero  $\boldsymbol{q}$  basically is an outcome of non-zero  $\boldsymbol{g}$ .

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\* A caneful observation clearly indicates that the  
part proportional to 
$$\frac{\partial T}{\partial x_i}$$
 will contribute to the  
non-vanishing expression for  $\vec{q}$ .  
\* Again some steps of Atgebra give,  
 $\vec{q} = -K\vec{\nabla}T$  where  
 $K = \frac{Tm}{6T}\int d^3U U^4 \left[\frac{m}{2K_BT}U^2 - \frac{5}{2}\right]f_0$   
 $= \frac{5}{2}T \frac{mk_B^2T}{m} \rightarrow K$  is thermal conductivity

So, a careful observation now here clearly indicates that the part of g which is proportional to  $\frac{\partial T}{\partial x_i}$  will contribute to the non-vanishing expression of q, why is that? That is something very interesting and we have to learn how to check that.

So, here you can see component wise  $\frac{m}{2} \int g U^2 U d^3 U$ , there is an odd functionality, because if you just write it in components you will have  $(U_x + U_y + U_z)U^2$  and from this one if you just do the multiplication, then some of the component of  $\Lambda_{ij}(U_iU_j - \frac{\delta_{ij}}{3}U^2)$  will pair with  $U_iU_j$  part, some component may or may not pair, but finally, the other component will be remained uncoupled.

So, if in case some of them will pair with  $U_i$ , then one will remain uncoupled; if none of them pair with that then simply both of them will be uncoupled. So, in any case this will vanish. Same thing for  $U^2$ , this is an even. So, even times odd gives you something odd with respect to each component of the velocity.

Now, here you have an odd contribution component wise for the velocity. Once again when I say U just remember U is nothing but the fluctuation velocity which sometimes we call c ok. So, just for recapitulation U = u - v = c.

Now, only the part with  $\frac{\partial T}{\partial x_i}$  has an even contribution and that is why you can easily see that the only possibility that the q has a nonzero contribution may only come from temperature

Now, again here you have some few steps of cumbersome algebra I agree, but systematic algebra, so for this type of thing rather than doing this algebra it is rather interesting to understand the physics. So, some steps of algebra can give you  $q = -K\nabla T$ .

So, we already showed that this thing will be so, the part of g which is proportional to  $\frac{\partial T}{\partial x_i}$  will contribute only. So, q should be expected to be proportional to gradient of temperature and if you say that I now suppose that q is equal to some constant, of course, I am writing minus for the conventional purpose, but minus K times gradient of temperature then one can simply calculate just by comparing and by replacing g

$$K = \frac{\tau m}{6T} \int d^3 \boldsymbol{U} U^4 \left[ \frac{m}{2k_B T} U^2 - \frac{5}{2} \right] f_0.$$

So, you see that finally, again this integration is all over all the components of the U. So, it is integrated over U.

So, if you do again the integration from minus infinity to plus infinity that is the I mean domain of integration for classical cases you can show that  $K = \frac{5}{2} \tau \frac{nk_B^2 T}{m}$ .

So, if you can do that finally, try to understand what this is. So, this is some quantity which is the proportionality constant of q, it may or may not be constant. But at least if you just see the expression, it should not depend on U. So, of course, there is T and n.

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non-vanishing expression for 
$$\vec{q}$$
.  
\* Again some steps of Atgebra give,  
 $\vec{q} = -K\vec{\nabla}T$  where  
 $K = \frac{\gamma m}{6T}\int d^{3}UU^{4}\left[\frac{m}{2\kappa_{B}T}U^{2}-\frac{5}{2}\right]f_{0}$   
 $\vec{z} = \frac{5}{2}\frac{\gamma}{m}\frac{k_{B}^{2}T}{m} \rightarrow K$  is thermal conductivity  
\* Note that  $K\uparrow as \gamma\uparrow$ ,  $n\uparrow$  and  $T\uparrow$   
(Think why it is the case Physically!)

So, it will be a function of in general r and t. So, this is not an absolute constant, but this is not a function of kinetic velocity. So, this is another macroscopic quantity if you want. This K, when you match your previous results of real fluids you can see that this is nothing but the thermal wave conductivity.

Now, the physics comes here, you have to note that *K* is proportional to  $\tau$ , *K* is proportional to *n*, *K* is proportional to *T*. Of course, when I am saying proportional to  $\tau$ , that means, *n* and *T* are kept constant. So, by the rule of joint variation you can say that *K* is proportional to  $\tau nT$  the product, when all of them vary and individually saying that *K* actually increases.

Let us say that n is constant, T is constant, then K increases with  $\tau$ . So, if in a system for example, we just do not change the temperature and we do not change the density, but we

just simply say that the collisionality is now becoming weaker and weaker then strangely the thermal conductivity increases. So, that the system is a fluid. So, that is the problem. So, what is the the problem here? because n is constant I understand, but then when  $\tau$  is larger, that simply says that the mean collision time is larger, how can that correspond to a greater K? That is simply because in order that the system still behaves like a fluid it should have a greater transportability.

So, this is the this is the story of the thermal transport. So, *K* is the responsible for the thermal transport. So, at least the duty of *K* is to do the thermal transport efficiently when  $\tau$  increases; that means, the collision basically decreases, so, mean collision time increases.

So, if this is the case then you can see that the systems conductivity should be strong enough, so that the system can efficiently transport energy from one part to the other otherwise the system is no longer fluid. But here we have supposed that already we are representing this as a macroscopic thing.

So, being a macroscopic entity where the collective effects are important the necessity that  $\tau$  is higher is that *K* must be higher. The same thing if your *n* is higher, then *K* is also higher; if your temperature is higher, temperature gradient can also be expected to be higher and then the energy transport should be efficient as well. So, *K* should be higher. So, these things are in consistency with each other.

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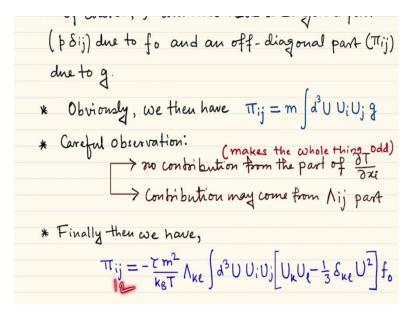
\* What Rappens to the pressure tensor? \* Of course, P will now have a diagonal part ( \$ Sij) due to fo and an off-diagonal part (Tij) due to g. \* Obviously, we then have  $\pi_{ij} = m \int d^3 U U_i U_j g$ \* Careful observation: > no contribution from the part of  $\frac{\partial T}{\partial x_i}$ > Contribution may come from  $\Lambda_{ij}$  part

Now, the question is that was the story of the heat flux tensor. Now, what is the destiny of the pressure tensor, what happens to it? Of course,  $\overline{P}$  will now have a diagonal part  $p\delta_{ij}$  due to  $f_0$  plus an off-diagonal part  $\pi_{ij}$  due to the perturbation g. So, obviously, we now can write that  $\pi_{ij} = m \int d^3 U U_i U_j g$ .

Now, again careful observation simply says, if you just take the part which is proportional to  $\frac{\partial T}{\partial x_i}$ , it will remain odd component wise and making this 0. So, there is no chance of having a contribution from temperature gradient part.

Contribution now may come from  $\Lambda_{ij}$  term. Now, of course in  $\Lambda_{ij}$  when you have this *i* is equal to *j* and this part can also contribute when *i* not equal to *j*, but *ij* is exactly equal to this *ij*. So, that  $U_iU_j$  is now paired with  $U_iU_j$  gives you  $U_i^2 U_j^2$  square.

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So, even multiplied with conditional even makes it globally even. So, if you finally, write the expression explicitly you will see this is nothing but

$$\pi_{ij} = -\frac{\tau m^2}{k_B T} \Lambda_{kl} \int d^3 \boldsymbol{U} U_i U_j \left[ U_k U_l - \frac{1}{3} \delta_{kl} U^2 \right] f_0$$

So, that is the most general way you have to write. So, of course, here you see this i and j they are the free index over there. And kl's are dummy indices; that means, there is a sum over these indices.

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$$( \downarrow \delta_{ij}) \text{ due to } f_{0} \text{ and } an \text{ of } f_{-} \text{ diagonal part } (\Pi_{ij})$$

$$due \text{ to } g.$$

$$* \quad Obviously, we then have \quad \Pi_{ij} = m \int d^{3} \cup \bigcup_{i} \bigcup_{j} g$$

$$* \quad Careful \quad Observation: \qquad (makes the whole thing odd)$$

$$\implies no \ contribution from the part of \quad \underbrace{\partial_{\nabla i}}_{\partial X_{i}}$$

$$\implies Contribution may \ come \ from \ \Lambda_{ij} \ part$$

$$* \ Finally then \ we \ have,$$

$$\Pi_{ij} = -\underbrace{\nabla m^{2}}_{k_{B}T} \Lambda_{ke} \int d^{3} \cup \bigcup_{i} \bigcup_{j} \bigcup_{k} \bigcup_{\ell} -\frac{1}{3} \delta_{ke} \bigcup^{2} f_{0}$$

$$\blacksquare$$

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$$( \downarrow \delta_{ij}) \text{ due to } fo \text{ and } an \text{ off-diagonal part } (\pi_{ij})$$

$$due \text{ to } g.$$

$$* \quad Obviously, we then have \quad \pi_{ij} = m \int d^{3} \cup \bigcup_{i} \bigcup_{j} g$$

$$* \quad Careful \text{ observation:} \qquad (makes the whole thing odd)$$

$$\Rightarrow no \text{ contribution from the part of } \frac{\partial}{\partial x_{i}}$$

$$\Rightarrow \text{ contribution may come from } \Lambda_{ij} \text{ part}$$

$$* \text{ Finally-then we have,}$$

$$\pi_{ij} = -\frac{\tau m^{2}}{k_{B}T} \Lambda_{ke} \int d^{3} \cup \bigcup_{i} \bigcup_{j} \bigcup_{k} \bigcup_{\ell} -\frac{1}{3} \delta_{k\ell} \bigcup_{\ell}^{2} f_{0}$$

For example, and then when you have fixed ij as 1 and 2 respectively for example, then you make a sum over all the values of kl, because repetitive or dummy indices they are basically designating sums. (Refer Slide Time: 24:59)

\* An interesting exercise ! Show that the above form of Tij represents a traceless tensor. (Easy!) \* Again, one can notice that  $\pi_{ij} \propto \Lambda_{ij}$ . Hence, it is tempting to write  $\Pi_{ij} = -2\mu \Lambda_{ij}$ . But we have to maintain the property of tracelessness. Then, the tensor Tij can be expressed as  $\bigotimes \leftarrow \Pi_{ij} = -\lambda \mu \left( \Lambda_{ij} - \frac{1}{3} \underbrace{\delta_{ij}(\vec{v}.\vec{v})}_{\text{This is because}} \right)$ 

The above form of  $\pi_{ij}$  represents a traceless tensor. Why? what is the meaning of traceless tensor?

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$$\left(\begin{array}{c} p \ \delta i j \right) dne \ to \ fo \ and \ an \ of f - diagonal part (\pi i j) \\ dne \ to \ g. \\ * \quad Obviously, we then have \quad \pi_{ij} = m \int d^{3} U \ U_{i} U_{j} \ g \\ * \quad Careful \ observation: \qquad (makes the whole thing odd, \ ) > no \ condoi bution from the part of \ \partial \pi_{i} \\ > no \ condoi bution from the part of \ \partial \pi_{i} \\ > \ Contribution \ may \ come \ from \ \Lambda_{ij} \ part \\ * \ Finally then \ we have, \\ \pi_{ij} = -\frac{\tau \ m^{2}}{k_{gT}} \ \Lambda_{ke} \int d^{3} U \ U_{i} U_{j} \left[ U_{k} U_{\ell} - \frac{1}{3} \delta_{ke} U^{2} \right] f_{e} \\ U^{2} - U^{2} \qquad \pi_{ii} = \sum \pi_{ii} = \pi_{h} + \pi_{22} + \pi_{33} = O$$

That means,  $\pi_{ii} = \sum_i \pi_{ii} = \pi_{11} + \pi_{22} + \pi_{33} = 0.$ 

And, how is that possible? Let say we just take  $\pi_{11}$  so, i = 1, j = 1. So, every time you have  $U^2 - \frac{1}{3}U^2$ . So, after when you sum all these three things you will have finally  $U^2 - U^2$  because  $\frac{1}{3}U^2$  will then contribute thrice to make it a  $U^2$ .

And it will give you something a traceless tensor. So, this is the necessary condition for a traceless tensor basically.

So, again you can notice here that  $\pi_{ij}$  when we just defined that from its basic definition it is proportional to  $\Lambda_{ij}$ . So, if it is proportional to  $\Lambda_{ij}$ , that is also our consideration that this part will now contribute for  $\pi_{ij}$ .

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\* Again, one can notice that  $\pi_{ij} \propto \Lambda_{ij}$ . Hence, it is tempting to write  $\pi_{ij} = -2\mu \Lambda_{ij}$ . But we have to maintain the property of tracelessness. Then, the tensor Tij can be expressed as \* Can we obtain an expression for \$1?

So, we can simply say if this is proportional to  $\Lambda_{ij}$  then of course, it is tempting to write that this  $\pi_{ij}$  is equal to some constant times  $\Lambda_{ij}$ , but we have to remember always that the property of tracelessness should be satisfied. And, for that the correct way of writing mathematically  $\pi_{ij}$  is not simply  $-2\mu\Lambda_{ij}$ , but  $\pi_{ij} = -2\mu(\Lambda_{ij} - \frac{1}{3}\delta_{ij}\nabla \cdot \boldsymbol{\nu})$ .

And, we subtracted the divergence part because we know that the trace of  $\Lambda_{ij}$  is divergence of  $\boldsymbol{v}$ . So, again starting from this expression this is another small exercise for you to check that  $\sum_i \pi_{ii} = 0$ . Now we have introduced  $\mu$  as a proportionality constant but can we obtain an expression for  $\mu$ ?

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\* For that, of course we should calculate 
$$\pi_{ij}$$
 when  
 $i \neq j$ , say,  $\pi_{i2} \Rightarrow$   
 $\pi_{i2} = \frac{Tm^2}{k_BT} \Lambda_{ke} \int d^3 U U_1 U_2 \left[ U_k U_{\ell} - \frac{1}{3} \delta_{ke} U^2 \right] f_0$   
 $= \frac{Tm^2}{K_BT} \Lambda_{ke} \int d^3 U U_1^2 U_2^2 f_0 \left[ \begin{array}{c} non zero \\ Contribution \\ comes from \\ the conditiond \\ part of g]$   
-\* Finally comparing this with the expression  $(A)$ ,

For that of course, we should calculate  $\pi_{ij}$  when *i* is not equal to *j*. Why?

So, it is a very small brain twister can you immediately tell me from the expressions of  $\pi_{ij}$ , why we have to calculate  $\pi_{ij}$  with *i* not equal to *j* to calculate  $\mu$ ? Think about it!

And, this expression finally comes out to be

$$\pi_{12} = \frac{\tau m^2}{k_B T} \Lambda_{kl} \int d^3 U U_1 U_2 \left[ U_k U_l - \frac{1}{3} \delta_{kl} U^2 \right] f_0,$$

because the nonzero contribution only comes from the conditional part of g. Finally, we compare this with the full expression for  $\pi_{ij}$ .

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And, if you do that you will finally, see that

$$\mu = \frac{\tau m^2}{k_B T} \int d^3 U U_1^2 U_2^2 f_0$$

that is equal to, if you correctly do the integration, finally you will see this is nothing but  $\tau nk_BT$ .

Of course, you can calculate mu just by taking let us say *i* is equal to 2, *j* is equal to 3 or *i* is equal to 2, *j* is equal to 1 or *i* is equal to 1, *j* is equal to 3 anything, but *i* is not equal to *j*. You should find the same result to our utter surprise that just like *K*,  $\mu$  is also proportional to  $\tau$ ,  $\mu$  is also proportional to *n* and *T*. So,  $\mu$  increases when *T* increases,  $\tau$  increases or *n* increases. Why?

Now, I discussed about these dependencies for *K*, now for  $\mu$  you have to think. This  $\mu$  from our previous knowledge of fluid equations, the fluid dynamists can match and call that as coefficient of viscosity rather dynamic viscosity coefficient of dynamic viscosity. When this is divided by the  $\rho$ , by the density mass density, it is called the coefficient of kinematic viscosity, but in general this is called roughly coefficient of viscosity.

So, one thing is true that when temperature increases coefficient of viscosity should increase. Now, tell me one thing, it is true, I know for gas, when you increase the temperature  $\mu$  increases, but what happens for oil? When you heat oil in a frying pan and

you increase the temperature of it, you will see the oil is moving around much more easily on the pan. So, can you reconcile that?

So, this is a question not exactly related to the course, but this is a general physics question. So, what happens? So, why the viscosity of a gas and the viscosity of a liquid have different type of temperature dependencies? So, just think.

Here we are talking about mostly about fluid which is gas because here we are just trying to make a macroscopic theory from that of kinetic theory and kinetic theory is only valid for classical gases.

For classical liquid, you cannot make kinetic theory because of the simple fact that in a liquid you have complicated interactions, long range interactions, other than the instantaneous interactions due to binary elastic collisions.

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So, finally our objective was to search whether we can still build up a dynamical theory for macroscopic variables for real fluids or not. Now, for that let us calculate the following terms of first order moment equation the  $\frac{\partial P_{ji}}{\partial x_i}$ . So, for diagonal *P* we had only  $\frac{\partial p}{\partial x_j}$ , for local Maxwellian, now we have the additional term like  $-\mu \left[ \nabla^2 v_j + \frac{1}{3} \frac{\partial}{\partial x_j} (\nabla \cdot \boldsymbol{v}) \right]$  where  $\mu$  is assumed to be constant in space and which is very reasonable for most of the fluids.

So, there is a case, when we will talk about the physics of accretion disc, the  $\mu$  is not constant in space and that actually adds a separate physical flavor to the problem, but here most of the cases we have this.

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So, then you we can write this the double contraction term of *P* tensor and the  $\Lambda$  tensor in the energy equation which was previously just  $p(\nabla \cdot \boldsymbol{v})$ , now we will have an additional term like  $-2\mu \left[\Lambda_{ij}\Lambda_{ij} - \frac{1}{3}(\nabla \cdot \boldsymbol{v})^2\right]$ . So, these terms with  $\mu$  are due to g, g means the perturbation over the local Maxwellian.

Now, experiments show that the viscous term in (ii) (see above) is usually negligible and actually most of the cases the viscous term  $\frac{1}{3}\frac{\partial}{\partial x_j}(\nabla \cdot \boldsymbol{v})$  in (i) is also negligible, but the term in (ii) is much more negligible and this is much more popular actually. Sometimes even in some cases we can keep  $\frac{1}{3}\frac{\partial}{\partial x_j}(\nabla \cdot \boldsymbol{v})$ , but the term in (ii) is mostly neglected.

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So, finally, we get the equations for continuity as  $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \boldsymbol{v}) = 0$ .

equation the momentum as  $\frac{\partial \boldsymbol{\nu}}{\partial t} + (\boldsymbol{\nu} \cdot \nabla)\boldsymbol{\nu} = -\frac{\nabla p}{\rho} + \boldsymbol{g} + \frac{\mu}{\rho} \Big[ \nabla^2 \boldsymbol{\nu} + \frac{1}{3} \nabla (\nabla \cdot \boldsymbol{\nu}) \Big].$ 

g is the body force, not to be confused with the perturbation of the distribution function. This is just the gravitational acceleration plus the new viscous term.

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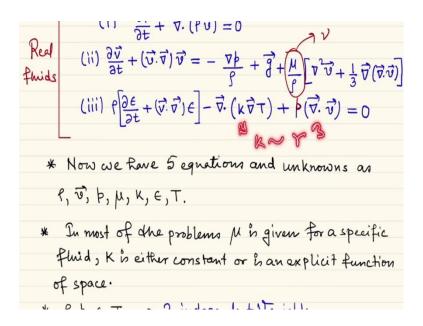
Now, this  $\frac{\mu}{\rho}$  which I was calling the coefficient of kinematic viscosity is in general denoted by  $\nu$ . And finally, the energy equation becomes

$$\rho\left[\frac{\partial\epsilon}{\partial t} + (\boldsymbol{\nu}\cdot\nabla)\epsilon\right] - \nabla\cdot(K\nabla T) + p(\nabla\cdot\boldsymbol{\nu}) = 0.$$

Of course, here we have not yet considered K to be independent of space and that is actually not a very good approximation because most of the cases K has a very explicit dependence on space.

Now, we have again five equations and how many unknowns?  $\rho$ ,  $\nu$ , p,  $\mu$ . g is known,  $\epsilon$ , K and T. Now  $\mu$ , in the most of the problem is given for a specific fluid. So, it is a constant of course, other than this accretion disc problem, but even in accretion disc it is handle able. We will talk about that.

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*K* is either a constant or is an explicit function of space. So, you can always write that *K* is like let us say proportional to  $r^{\alpha}$ .

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Real  
(ii) 
$$\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{v}) \vec{v} = -\frac{\nabla p}{r} + \vec{g} + (\vec{\mu} \cdot \vec{v}) \vec{v} + \frac{1}{3} \vec{v} (\vec{v} \cdot \vec{v})$$
  
(iii)  $\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{v}) \vec{v} = -\frac{\nabla p}{r} + \vec{g} + (\vec{\mu} \cdot \vec{v}) \vec{v} + \frac{1}{3} \vec{v} (\vec{v} \cdot \vec{v})$   
(iiii)  $\frac{\partial \vec{e}}{\partial t} + (\vec{v} \cdot \vec{v}) \vec{e} - \vec{v} \cdot (k \vec{v} \tau) + \vec{p} (\vec{v} \cdot \vec{v}) = 0$   
\* Now we have 5 equations and unknowns as  
 $r, \vec{v}, \vec{v}, \vec{\mu}, \vec{k}, \vec{e}, \tau$ .  
\* In most of the problems  $\mu$  is given for a specific  
Fluid,  $\vec{k}$  is either constant or is an explicit function  
of space.

So, then what happens, if you are just doing some integration, this does not add to the complicacy of the unknown variables and so K in most of the cases, is a known explicit function of space or is a constant; because there are some experiments by which you can actually find the functional form and the functional dependence of K. So, it does not really complicate the scenario.

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And finally,  $\rho$ , p,  $\epsilon$  and T we know that they are all related by two independent variables and most popularly the 2 variables are n and T. So, finally, 2 independent variables from them and 3 components of v, so 5 equations, 5 unknowns. So, finally we succeeded to constitute a dynamical theory for the real fluids. So, that is exactly where I should stop for this lecture. So, in the next discussion we will talk about a very interesting application of these equations and we will talk about the hydrostatic condition, the hydrostatic equilibrium of such a fluid where the viscous effect is negligible, but not the conductive conductivity effect.

So, that we will do, but till now what we have seen something very interesting that, starting from a very simplistic assumption that the distribution function is perturbed only by a very small amount with respect to the Maxwell-Boltzmann equation; finally we retrieved all the, under of course certain approximations, all the transport phenomena in a real fluid.

So, now these set of equation is known as the equations of the real fluids.

Thank you very much.