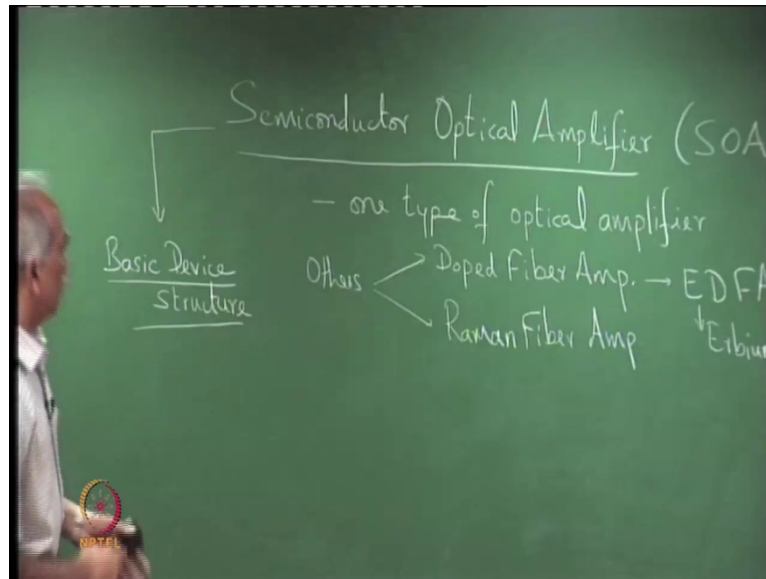


Semiconductor Optoelectronics
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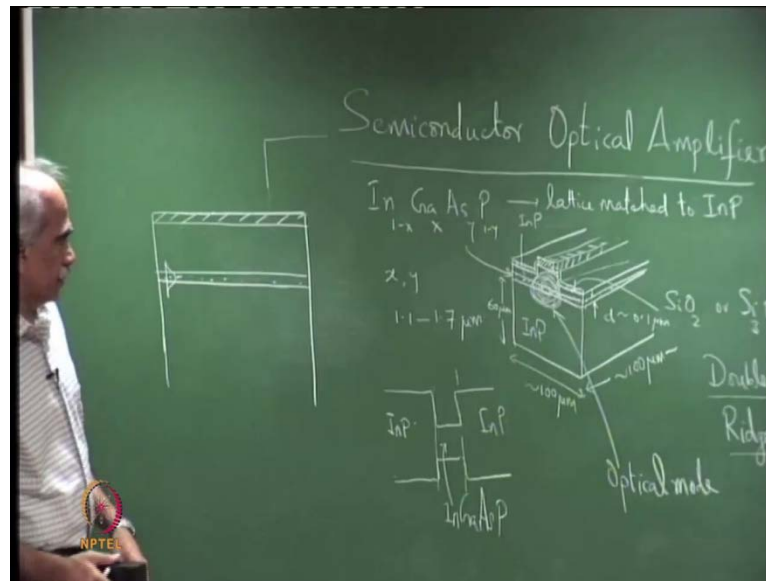
Lecture - 26
Semiconductor Optical Amplifier (SOA)

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Welcome to this lecture on semiconductor optical amplifier. So, today in this class, we will see at another device, which is the semiconductor optical amplifier, or widely used abbreviation as SOA, semiconductor optical amplifier. This is one type of amplifier, one type one of the types of optical amplifier, so a type of optical amplifier. Other commonly employed optical amplifiers include doped fiber amplifiers; so, doped fiber amplifiers and Raman fiber amplifiers. Raman fiber amplifier makes use of the Raman effect, which is a non-linear optical effect, and widely used doped fiber amplifier in optical communication is the EDFA; that is erbium doped fiber amplifier; Erbium doped fiber amplifier, is a widely used amplifier, in optical communication. Let us first start with the basic structure of this device. So, the basic device structure, the basic device structure of this amplifier, is almost similar to the last device that we have discussed; that is the wave guide configuration of electro absorption modulate. The electro absorption modulated in the wave guide configuration, is similar to this in structure, but of course, the operations are different. So, let me show the device structure.

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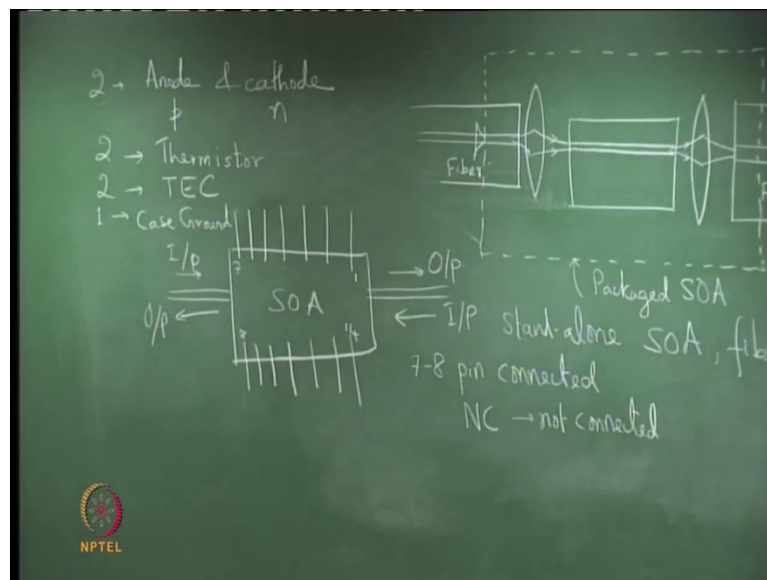
This is the substrate, the active layer, which has the cladding layer, this is a ridge wave guide structure as before, and then we have an insulating layer, and then the metal for contact. So, this region is the metal for contact, and this is the active region, and this is the substrate indium phosphide, widely used material in optical communication window, is the indium one minus x gallium x, that quaternary compound arsenide phosphide p 1 minus y. So, this is because depending on the composition of x and y. One can cover the entire range approximately from 1.1 to 1.7 micrometer, for amplification as well as for laser action. So this the quaternary compound, which is lattice match to indium phosphide, so this is lattice matched to indium phosphide over certain range of x and y values. So, this is the cross section, so the device in three d view will look like this. This layer is also an indium phosphide. So, indium phosphide, indium phosphide, metal for contact on top, this is the metal contact, and this is the layer of dielectric insulating layer, gaping layer. So, usually this insulating layer is SIO 2, or some time silicon nitrite.

Typical dimension would be of the order of 100 to 200 micrometer here, length is again may be several hundred micrometer, the length, and height is so also approximately, so this could be 300 to 1000 micrometer, and this height is approximately 60 micrometer. And this thickness here of the active layer, the thickness of the active layer here, this thickness d is of the order of 0.1 micrometer. So, it is a double hetero structure, so it is a double hetero structure d h, double hetero structure ridge wave, so ridge wave guide configuration, as in the case of electro absorption modulated. So, we can see that indium

phosphide has a larger band gap. So, if you have to plot the band gap of the hetero structured, so this is indium phosphide on both the sides, indium phosphide, and this intermediate layer is the active region, which is indium gallium arsenide phosphide. So, the basic structure is double hetero structure ridge wave guide configuration. The ridge is used for lateral confinement, the refractive index here, so if you see longitudinal cross section of this device, then it would look like this.

If you see the longitudinal cross section, then this the metal contact, and this is the active layer, and of course, this is the substrate. And the optical mode travels here, because refractive index of this region which has a lower band gap, is higher compared to the refractive index of indium phosphide. And therefore, this acts like an optical wave guide, but if we did not have the ridge, there would have been no confinement, no transverse confinement, and light would have been confined of course, in the vertical direction to this plane, but there was no confinement in the transverse direction, and therefore, we use this ridge which confines the optical field to this region, so the optical field. So, what I have schematically illustrated, is the optical mode, the optical mode is confined, otherwise that would have been no confinement, that is why we used the ridge wave guide structure.

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So, the complete device, package would be something like this, so we have wave guide here, the SOA amplifier, again a schematic, and there is a lens, and we use optical fiber

buck couple to this. An optical fiber, which is sometimes it can be buck couple directly, there is no need of this less. So, the optical fiber pig tailing, and pig tailed optical fiber which focus the light beam into the active region. And the package device will look like this, optical fiber, optical fiber, and this whole device. So, let me erase these structure here, the basic structure, and the whole arrangement is encapsulated, it is permatically sealed, so that the device. So, this is the package SOA, which is fiber pig tailed SOA. So, this is a typical arrangement of a standalone SOA optical fiber amplifier, which is fiber pig tailed.

Let me show you the device, a practical device, a fiber pig tailed stand alone SOA, which will contain, the consist for the device, the semiconductor or device, and an arrangement to couple, buck couple or to couple from optical fibers, so that the device can be used as standalone amplifier. So, let me show you the device. So, the typical device would look like this, here is the chip, the SOA chip with fiber pig tailing on both sides, because the amplifier we need. The amplifier is a device which has an input and output, so here is a block diagram of an amplifier. So, you have an amplifier which has an input and an output. So, this is the block diagram of an amplifier here. So, exactly like that, the input is though an optical fiber, which is pig tailed to the chip, the semiconductor chip, and these are micro lenses, micro lenses which help in focusing that is minimizing the insertion loss of the device.

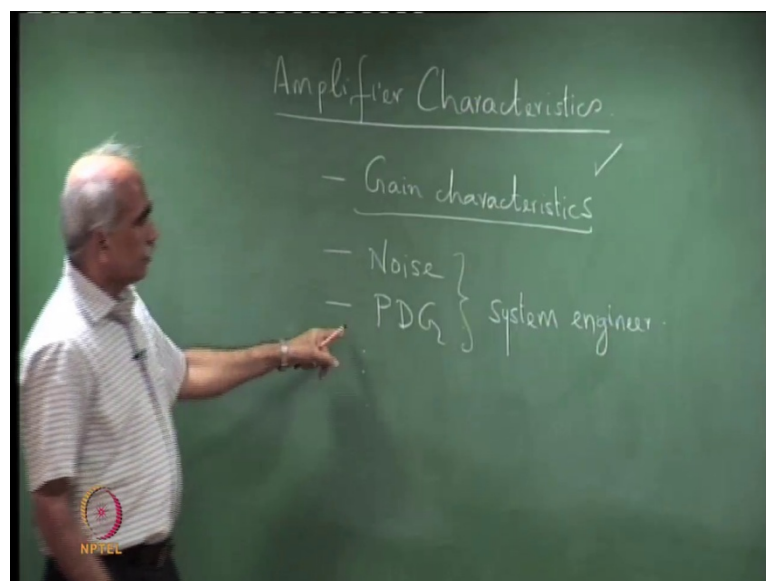
So, there are two fiber at the other end, and the entire thing is packaged in this, so it would a typical amplifier would look like this. So, here is the chip, and this is fiber pig tailing. The whole thing is mounted on a driver here. If there is a, the device is a fourteen pin butterfly device. So, as we can see it is a fourteen pin butterfly device, which means we have. So, this dotted line is this block here, and it is a fourteen pin butterfly device. So, we have 3 4 5 6 and 7, 8 14, and this is the fiber pig tail, so input and output, so this is the SOA chip. Usually there is a marking which shows the terminal number one, and then it is counted in this direction, so this is 1 2 3 4 5 6 7, and terminal number 8 is here 9 10 up to 14. So, this the pin configuration it is a fourteen pin device as you can clearly see.

Not all the pins are useful, usually many of several pins are not connected, and SOA typically has about 7 to 8 pins connected, and the rest of pins are not connected NC; the typical abbreviation use NC not connected. The pins which are usually connected, or the

connection that are repaired or for the anode and cathode; that is connected to p and n side of the device, so two terminal for this two terminals would be there for thermister, because the device is semiconductor chip, is temperature sensitive, so one has to maintain temperature. So, the temperature change is sensed using thermister, and two terminal are used for TEC cooler; that this thermo electric cooler. So, two terminal, and one terminal is generally used for case ground. Most of the terminal are rest of terminal, are usually not connected.

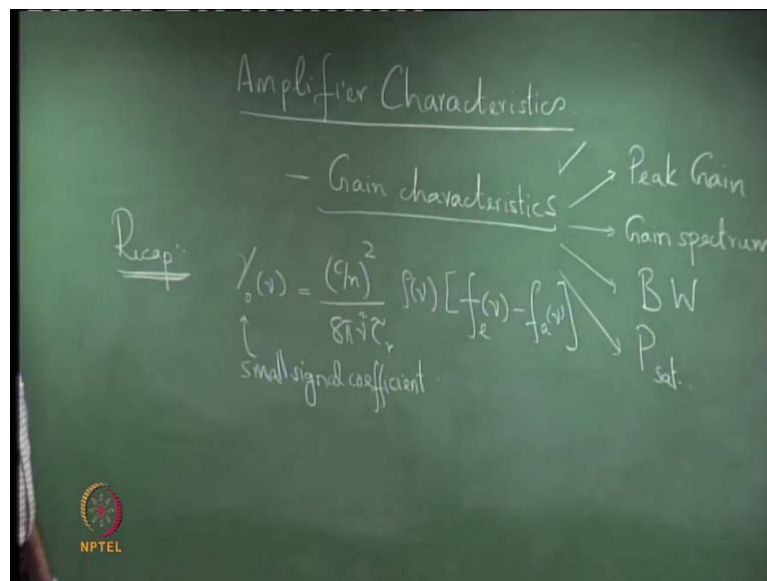
So, this is a device as you can see clearly, the fiber, the input, the fiber is ended with a connector, this is a typical FCPC connector, here FCPC connector, and there are two connectors at the two ends. Either this could be input or that could be input, the SOA is an amplifier as you can see, we could input the weak signal from here, and get an amplified signal from here, or we could also input from this side, it is possible, it's an amplifier, that you could also use this as the input and this side as the output. So, the amplifier is a device, where you can put input and output, and this is a typical amplifier device. A cable normally goes from the mount, which is connected to a driver. A separate driver unit is normally provided where you can set the temperature, the current limits and, so on. So, let us now see little bit about the amplifier characteristics, and what are the characteristics that are of interest to us.

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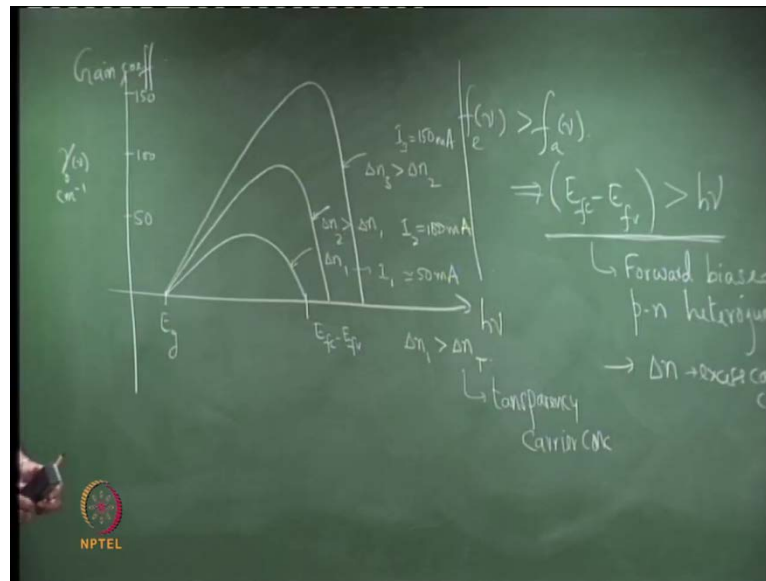
So, let see the amplifier characteristics, primarily these are gain characteristics, and noise. Also there are other parameters which are used; for example, polarization dependent gain PDG and so on. There are several characteristics, which one can study with respect to this amplifier. We are primarily with focusing on the gain characteristics, noise and PDG are more important for system engineers, or a design engineer, but let us first look at the gain characteristics, and this will be discussed in at another course; the noise and PDG characteristics, and therefore, our focus will primarily on gain characteristics.

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So, the gain characteristics include peak gain, gain spectrum, there is the range of wavelength or frequency, over which gain is present, the bandwidth, gain bandwidth. And an important parameter, which is p saturated; that is saturated output power, saturated output power, optical power output. So, let us see one by one these characteristics; recall recap that we have in an earlier class, we have obtained an expression for the gain coefficient γ_0 of μ , the small signal gain coefficient, as c by n square divided by $8\pi^2$ m square by τ into ρ μ , the optical joint density of states, τ is the relaxation time, c is the velocity of light, n is the refractive index of the medium into f_e of μ , probability of emission minus of a of μ . The small signal gain coefficient with, call this as the small signal gain coefficient, because we had assumed that this is independent of the intensity of radiation, signal coefficient, which is not really true at higher power, small signal gain coefficient.

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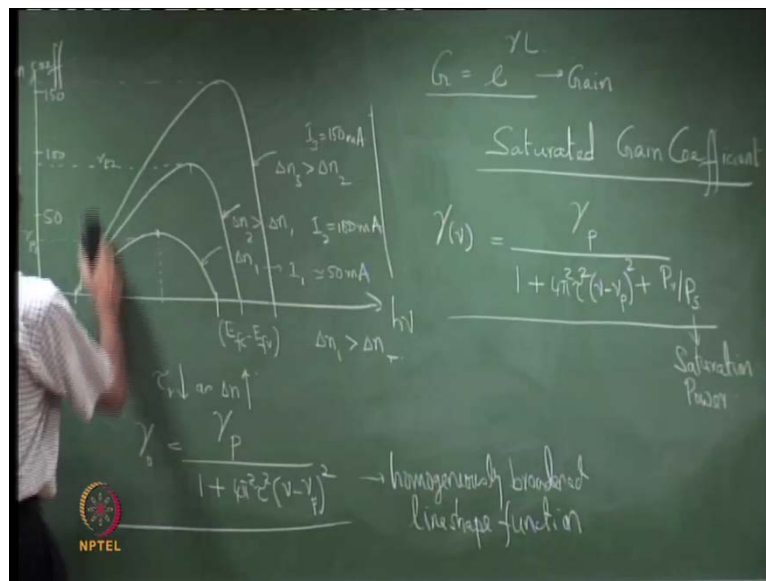


All the parameter in this are positive, all are positive, only this is the parameter which can be negative or positive, depending on whether the probability of emission is greater than the probability of absorption or not. So, to have f_e of μ greater than of f_a of μ , we have seen that the necessary condition is $E_{fc} - E_{fv}$, the separation between the quasi Fermi levels should be greater than $h\nu$. And the one of the methods used in achieving this, is by the use of a forward biased p n junction, forward biased p n hetero junction. We have discussed this already forward biased p n hetero junction. And the separation between them, is a function of forward bias current, because the current the forward bias, induces a Δn excess carrier concentration, which results in separation, increasing the separation between E_{fc} and E_{fv} . And at certain values of Δn , one can have gain coefficient positive; that is f_e of μ greater than f_a of μ . So, if we plot this gain characteristics which we have seen, so $h\nu$ hear, for a certain value of Δn , then this is let's say some value of Δn_1 , which is greater than the transparency carrier concentration.

So, Δn_1 is greater than Δn_T , this is the transparency carrier concentration. Then we gave gain, this is gain co-efficient, gain coefficient γ_0 of μ in centimeter inverse. Let me also give some typical numbers. So, this point is e g, so this is energy axis $h\nu$, and this point is $E_{fc} - E_{fv}$. For this injection current an injection current, which give carrier concentration Δn_1 . If we increase the carrier concentration, then this curve would move like this, and $E_{fc} - E_{fv}$ gets pushed

forward. The separation between them increases, and therefore, the gain coefficient increases, at even a larger value. So, this is for Δn_2 , which is greater than Δn_1 , and this is Δn_3 , which is greater than Δn_2 , may correspond to three different currents, so I_1 . So, Δn_1 corresponds to a forward bias, forward current I_1 ; say 50 milliamphere. I_2 is equal to 100 milliamphere, and I_3 is equal to 150 milliamphere. These are the typical currents used in SOA to achieve gain, gain in and SOA.

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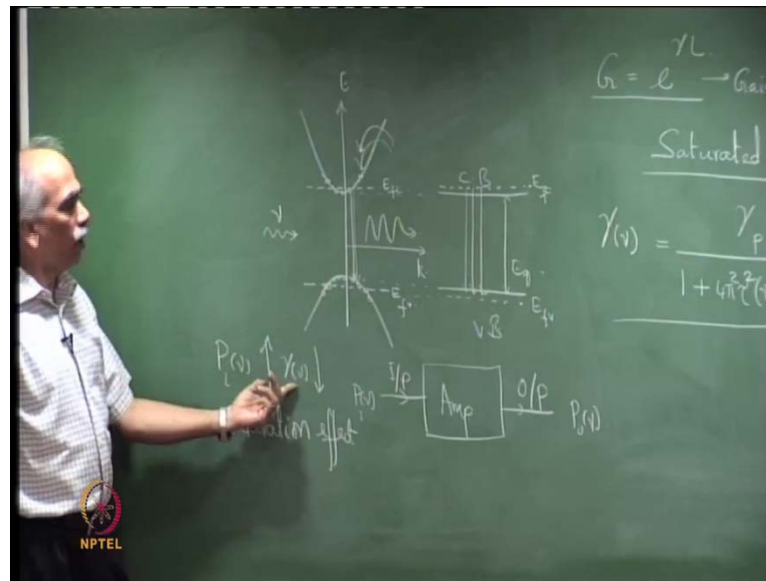
So, the point here is or we can see is as you increase the forward current, through the SOA. Please recall that it is a device, which is a p n device, it is p n junction device, as you increase the gain coefficient as you increase the current through the device, the gain coefficient moves up, and $E_c - E_v$ separation between E_c and E_v moves forward, which means the bandwidth, the frequency range over which the amplification can take place increases. So, this is what we see; that the frequency range increases, and the peak gain also increases. The frequency range increases, because the separation between E_c minus E_v get increases, and the peak gain increases primarily, because τ_r , which is in the denominator of that expression, decreases as Δn increases. The access carrier recombination time decreases as Δn increases, and therefore gain coefficient increases. The peak gain coefficient refers to peak value, so this is the peak gain coefficient. Here this is γ_1 γ_2 γ_3 . So, this is the peak gain coefficient. So, now we know, what we refer to as peak as gain coefficient

please recall that the gain coefficient of a given device, gain is e to the power γ into I , and the peak gain correspond to the e to the power γ_p into I .

So, this gain, and γ is a gain coefficient; this is gain. So, both the gain and the bandwidth increases with increasing forward current. So, the second thing which we have to discuss, is saturated gain coefficient. The gain coefficient obtained in the earlier expression, as the earlier expression was independent of the intensity, intensity of light inside the laser cavity; that is inside the active region, but an actual analysis will give that the gain coefficient γ of μ , depends as γ_p divided by $1 + \dots$. The small signal gain coefficient γ_p , the small signal gain coefficient γ_0 , can be expressed as γ_p divided by the peak gain coefficient divided by $1 + 1 + 4 \pi^2 \tau^2 \dots$, into $\mu - \mu_p$ the whole square. If we assume that the medium is characterized by a homogeneously broadened line shape function. We will not be going into the detail of this, because this is the part of a laser course, homogeneously broadened line shaped function.

There we can show that, the gain coefficient depends in the form a Lorentzian, the gain coefficient is given in terms of a Lorentzian, approximated. This is not exactly a Lorentzian, but this can be, if we assume that the gain is, the medium is characterized by a homogeneously broadened line shape function, than one can represent the gain coefficient as $\gamma_0 = \gamma_p / (1 + 4 \pi^2 \tau^2 (\mu - \mu_p)^2)$, where μ_p is the frequency corresponding to the peak gain coefficient, τ is the relaxation time or carrier recombination time, and γ_p is the peak gain coefficient. However, as the intensity of or power inside the semiconductor increases, then the expression changes to the form $1 + 4 \pi^2 \tau^2 (\mu - \mu_p)^2 + P/P_s$, where P_s is called a saturated power, saturation power. So, this is the expression, if we consider that the gain coefficient also depends on the intensity of radiation. Let me just discuss this a little bit more, why this saturation came into effect. We will not be able to go into derivation in this course, but conceptually we can see why this saturation occurs.

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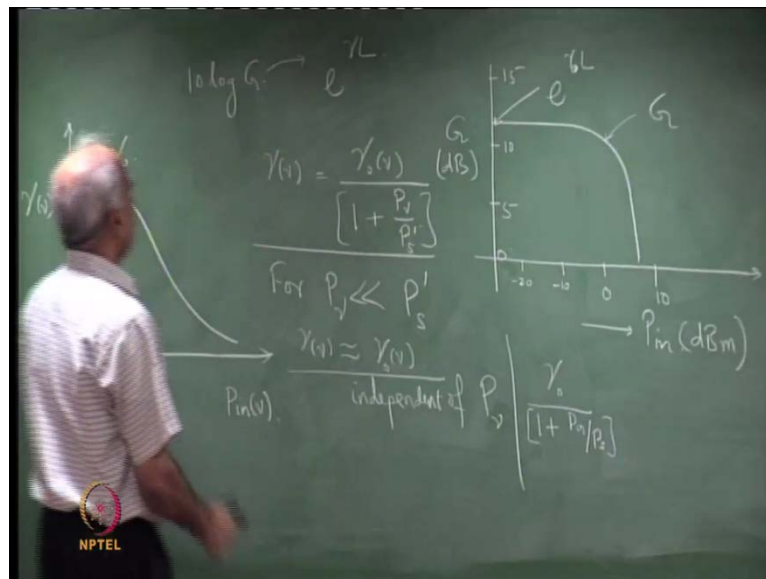
If we recall the $e-k$ diagram, if we have a pumping mechanism, through which we pump large number of electrons to the conduction band. So, here is the equivalent conduction band. This is the $c-b$ conduction band, and this is valence band, this is the $e-k$ diagram picture, and we have large number of holes here, this represent the active region, where you have simultaneously large number of electron, and large number of holes, and the Fermi levels. So, this is E_{fc} and E_{fv} ; the quasi Fermi levels, E_{fc} and E_{fv} , this is $e-g$; the quasi Fermi levels E_{fc} and E_{fv} . A radiation which is passing through the medium, will induce stimulated emission, and stimulated emission will dominate when $E_{fc} - E_{fv}$ is greater than $h\nu$ and you get amplified radiation coming out.

as the density of radiation, as the input here, the density of input radiation increases, it will bring down more and more electron downwards in the process of amplification, and therefore the carrier concentration in these bands drop down, as the intensity here or the input power increases, as the input power to the device, so this is the amplifier, and here is the input and output. As the input power, so this is p_{in} , which is the input p_{in} of μ and p_{out} p_{out} of μ . As the input power signal power increases, it will bring down more and more electrons, it will lead to higher levels of recombination's here, in the process of amplification, and in the process the carrier concentration drops down. When the carrier concentration drops down, E_{fc} will start coming down, E_{fv} will start coming down, in other words the gain coefficient drops. So, as the input power p_{in} increases the gain

coefficient at that value drops down, and this effect is called saturation effect, for low power signal.

For low powers signals this is not an issue, because if the pumping is strong enough, then for low powers the amount of carriers which are recombining, will always be immediately made up of by the pumping. However, when the input power increases, than the carrier concentration in the bands decreases, leading to a lowering of $E_f c$ and $E_f v$ here, resulting in a smaller separation, and hence a smaller value of gamma. This is expressed in this expression here, saturated gain coefficient. We are not going in to the derivation of the expression, but as you can clearly see, that if this is nothing, but the small signal gain coefficient. So, I can write this as γ_0 divided by $1 + p_\mu$ divided by p_s into. So, I take this, this term outside, this whole tern outside, then p_s into one plus $4 \pi \tau$ square into $\mu - \mu_0$ the whole square. The quantity p_s into this, if I call this as p_s dash, then I can write the saturated gain coefficient.

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I can express the saturated gain coefficient as γ of μ , is equal to γ_0 of μ , which is the small signal gain coefficient, which is encircled here, γ_0 of μ divided by $1 + p_\mu$ divided by p_s dash. So, we can represent this in the same expression, I am representing it in this form. So, what it indicate is, for small values of p_μ ; that is for p_μ much less than p_s dash p_s dash, γ of μ is equal to γ_0 , which is independent, this is independent of the input signal power p_s . For p

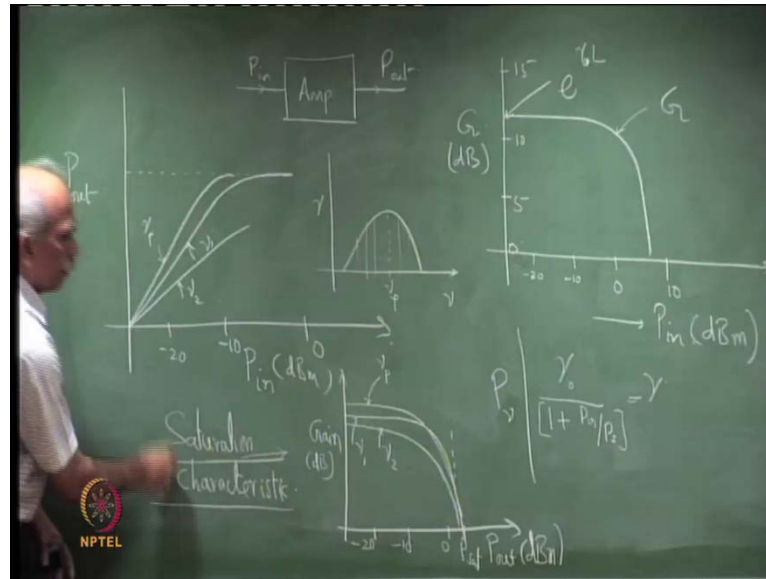
μ much less than independent of the signal power, input power p_{μ} , and this is the small signal gain coefficient. However, when p_{μ} is sufficiently large, or when it is comparable then this term cannot be neglected, and as you can see that p_{μ} is equal to $p_{s \text{ dash}}$, the gain γ_0 will drop down to half of its value.

At p_{new} is equal to $p_{s \text{ dash}}$ this is 1, so $1 + 1/2$. Therefore, the gain coefficient drops down to half of its value. This means that if I plot a curve, if I plot a variation of p_{input} as a function of γ here. This is $\gamma_{\text{of new}}$, than it will for small values of p_{μ} , this is p_{input} at a frequency μ , at a particular frequency μ . For small powers p_{μ} , when p_{μ} is much less than $p_{s \text{ dash}}$, the gain coefficient when p_{μ} is much less than $p_{s \text{ dash}}$, the gain coefficient $\gamma_{\text{of } \mu}$ is constant, is equal to γ_0 of μ . We can see here that this part does not depend on signal power, only this is the signal power, p_{μ} is the input signal power at the frequency μ input signal power.

So, for small power input signal powers the gain remains constant, the gain coefficient here remains constant, but as the signal increases this will start dropping down. So, this if I can show, that this will drop as $1/x$, so it will drop in this way. So, as this increases this drops is, this value here is γ_0 , γ_0 of μ , and this starts dropping down as the signal power increases. Normally we show this in terms of gain g , gain in dB, if we take a typical data sheet, or if you make a measurement, then it would be in this form. So, gain g here in dB; that is $10 \log g$, and g is simply e to the power of γ into l . So, this is in dB, and typical numbers would be 5 10 15 versus p_{in} , a typical SOA characteristics, the gain remains constant for small values of signal power, but then it drops down to, this is 0. Gain equal to 0 means, this going down to 0 dB; that means there is no gain.

This is dropping down with signal power, typical signal power showing here. So, this is $\text{minus } 20 \text{ minus } 10 \text{ minus } p_{\text{in}} \text{ in dB m minus } 10 \text{ plus } 10$, so typical, this is the gain curve g . So, this represent gain saturation, as you increase the signal power the gain coefficient drops down as γ_0 . So, this value here is actually e to the power γ_0 into l , small signal gain coefficient γ_0 into l , where l is the length of the semiconductor chip. So, γ_0 divided by $1 + p_{\text{input}}$ at the frequency μ divided by some saturated power p_s . So, this is a gain characteristics; but usually one tends to plot gain coefficient versus the output power, because it gives an indication, of what is the maximum output power that is possible.

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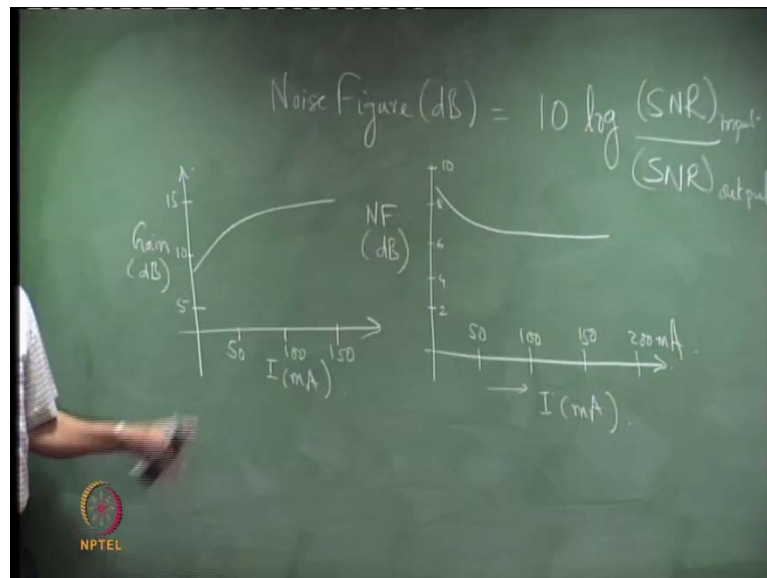
Now to understand this, we can plot input versus output. How would input versus output look like. So, this is P_{in} , let me put the same number minus 20 minus 10 dBm and 0 dBm minus 20 minus 10 input power, input power to the amplifier. So, we are looking at the amplifier here. So, amplifier, this is the P_{in} and P_{out} , so P_{out} . Initially the gain is constant as we can see here, that the gain is constant, which means the input versus output will be a linear straight line here. So, as the signal power increases, the output power increases. However, when the signal power increases, saturation takes place; that is the gain coefficient starts dropping down. As the input power increases the gain coefficient γ drops down, and therefore, $e^{-\gamma}$ to the power γ drops down, so the output power, which starts here. The output starts saturating, because as this comes down to 0, 0 means the ratio is $P_{out} / P_{in} = 1$; that means, it will finally lead to saturation here. So, this is the saturated output power. So, whichever be the frequency you take, so, this is for particular frequency.

The gain is a function of frequency, if you recall here in the box. So, new versus gain, μ or μ versus gain, then we know that the gain is the function of frequency, corresponding to this frequency here μ_p we have maximum gain. At another frequency which is on the side, we may have a different gain coefficient, which means in this graph if I were to show, that it could. This is another frequency if I call this as μ_1 , at another frequency this may be μ_2 , and for γ_p of course, the slope will be maximum, so this is γ_p ; that is the centre corresponding to the centre, but all of these lead to a

saturated output power. So, it is customary to plot the gain characteristics, saturated saturation characteristics as this p out in dB m, here versus gain. So, you will have the same characteristics as with p in, but all of them saturating to the. So, any frequency you may take, you may have this gain, but all of them will saturate to the same value. So, this is for some frequency μ .

So, what I have plotted is gain in dB m in dB versus output power. So, this power where all of them is called the p saturated. So, typical numbers could be again, so minus 20 or minus 20 minus 10 0. This is little smaller value, but generally the saturated power could be about 10 to 15 dB m. So, this is at new p , corresponding to the peak, this is another frequency of μ 1 within the gain bandwidth of course μ 2 and so on. So, this is called the saturation characteristics of an amplifier of an SOA. So, we have discussed about the gain spectrum, the bandwidth, and gain saturation, the saturation characteristics of an amplifier. Let me briefly touch upon, so I have already discussed about the gain, peak gain, the saturated gain power, and gain bandwidth, and their dependence on the pump power, and the input signal power. Let me briefly touch upon noise.

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So, the noise figure will not go into many of the details, noise figure is defined in dB is defined as $10 \log f$, which is signal to noise ratio SNR, optical signal to noise ratio, at the input divided by optical signal to noise ratio o SNR at the output. And typical gain noise characteristics of an amplifier, so this is signal to noise ratio. We will not go into the

details of noise figure in this course here, because this will be covered in communication course. And what we have is, as a function of the power, the pump power p out. The current, the pump current i , so this is the pump current i into mA, because depending on the pump current we have gain characteristics. The gain will be larger for larger current through the device, and noise figure here NF in dB typically varies.

So, typical numbers for an SOA 50 mA 100 milliamphere 150 milliamphere, may be 200 milliamphere, and the typical numbers here are; 2 4 6 8 10 noise figure in dB. As initially if you see the gain as the function of i . So, i here versus gain, then typically it looks like gain here, 5 gain dB ten 15 for current, and using the same consistency 50 100 150 milli ampere. So, the gain initially increases with current; that is why the noise figure drops down, because noise figure depends on the gain, and after some time gain is slowly saturating, and therefore the noise figure is also saturating. So, they are consistent gain and noise figure, typical characteristics for semiconductor optical amplifier. How does the performance of SOA compare with a fiber amplifier.

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Typical Characteristics		EDFA
Gain: 20-30 dB	→	30-50 dB
BW: 50-100 nm	→	30-40 nm
P_{sat} : ~10 dBm	→	> 20 dBm
NF: ~6 dB	→	~3-4 dB
Application	→	All optical switching, wavelength converters, logic gates

So, let me, if I give you typical characteristics, I have shown the characteristics typical curves, but typical numbers, all are there in the graph that I have shown. So, gain generally about 20 dB, or may be maximum 20 to 30 dB maximum gain. Bandwidth typically 50 to 100 nanometer gain, bandwidth, p saturated, saturated power, typically 10 dB m of the order of 10 dB m, approximately the order of 10 dB m, and noise figure.

There are several other characteristics, but we are not going in detail in to those characteristics, or primary emphasizes is on the device rather than the characteristics of the device, is of the order of 6 dB. How would this compare with a typical fiber amplifier EDFA. EDFA one can have gain anywhere from 30 to 50 dB, bandwidth of course little less 30 to 40 nanometer, saturation power is greater than, easily one can get greater than 20 dB m, and noise figure, almost 3 dB, almost to the limit, you can get noise figures, almost greater than or equal to, almost at that level 3 to 4 dB, let me write 3 to 3.5 dB.

So, what we see, with these characteristics is that EDFA scores, except for bandwidth, the EDFA scores in every way over an SOA. However, therefore, the application of SOA is not for long haul communication. It is not used for long distance communication, high speed communication, because the noise performance, gain performance, everything is much better in then the case of EDFA. However, the range, the domain of application of EDFA's, he has to do with all optical signal process, all optical switching; for example, all optical logic gates, and very widely used in wavelength converters and so on. So, the range of application of SOA is usually different from those of optical amplification for communication. So, we will not be in a position to go into the details of this, but I would recommend that you see some books; reference books on SOA, to look at the range of application. So, this is being developed for signal processing, and in metro networks, flexibility of wavelengths routing, and application are also being developed for all optical logic gates for signal processing. So, we will stop at this point here.