

# MARINE ENGINEERING

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Lecture11

## Heat flow through pipes and walls

conduction through cylindrical pipe your life heat conduction through cylindrical pipe your life is easy when you have flat plate and heat is getting conducted from one surface to another surface okay but if you have cylindrical pipe circular pipe like this okay then how this heat transfer will be going on what  $x$  value or thickness value will be taking okay because  $r_1$   $r_2$  okay  $r_1$   $r_2$  if you see this area is changing okay when area is changing when  $i$  you you can't use directly the formula whatever you have used for  $k \Delta T$  by  $\Delta x$  right so here formula will change. Here, formula is this,  $q$  equals  $\frac{-kA \Delta T}{dr}$ . You have to take differential form because your area is changing, equals  $\frac{-kA}{dr} \Delta T$ ,  $k$  means area. Which area?

This surface area. So,  $2\pi r$ ,  $2\pi$  means your parameter into  $L$ . surface area because from inside temperature  $T_1$  and outside temperature  $T_2$ , like it is a common circular pipe. In circular pipe, inside temperature may be higher, outside temperature may be lower. So, heat is transferring from inside to outside.

So, area will be the whole cylindrical surface area. That is why  $2\pi RL$  and  $DT$  by  $DR$ . So,  $L$  equals length of the tube pipe or tube whatever you say. So, you have to integrate to get this  $dT$   $dr$  and  $q$  all this. So,  $T$  equals  $T_2$   $T$  equals  $T_1$   $dr$  equals  $r_1$   $r_2$   $q$  by  $2\pi rL$   $2\pi r$  has gone.

So,  $dr$   $\pi r$ ,  $r$ ,  $r$ , they have put here because this is a constant term. So,  $T_2$  minus  $T_1$ ,  $T_2$ , this is  $dt$ , this will be  $dt$ . So,  $T_2$  minus  $T_1$  equals  $q$  by  $2\pi r$ ,  $2\pi kl$  logarithm of  $dr$  by  $r$  log will come, so  $r_2$  by  $r_1$ .

Therefore,  $q$  equals  $2\pi kl$   $2\pi kl$   $T_2$  minus  $T_1$  divided by logarithm of natural log  $r_2$  by  $r_1$ . Now  $Q$  equals  $2\pi L$   $R_2$  minus  $R_1$   $k$   $T_2$  minus  $T_1$   $R_2$  minus  $R_1$   $R_2$  minus  $R_1$  up and down both multiplied  $2\pi$  denominator and numerator both  $2\pi R_2 L$   $2\pi R_1 L$  this is

logarithmic So, this will give  $k A_2 \ln \frac{r_2}{r_1} (T_2 - T_1)$  divided by  $R_2 - R_1$  logarithm of  $A_2$  by  $A_1$ . Now,  $A_1, A_2$  are the inside and outside surface. So,  $Q$

Now,  $A_2$  by minus  $A_1$  by logarithm of  $A_2$  by  $A_1$  inside outside surface area,  $A_1 m$ , they have taken this notation and  $x_w$  equals  $R_2 - R_1$ . This will give  $Q$  equals  $\frac{k A_1 m (T_2 - T_1)}{r_2 - r_1}$  or minus  $k a_1 m (T_2 - T_1)$  by  $r_w$  and here  $r$  equals  $r$  equals  $x_m$  by  $k_1 a_1 m$  now  $r$  equals  $r_1$  plus  $r_2$  so if you have two pipes i'll be giving different shading so that there will be no confusion confusion okay so  $t_1, t_2, t_3$  and so  $r$  equals  $r_1$  plus  $r_2$  equals  $x_w$   $1/k_1 a_1 m$  plus  $x_w$   $2/k_2 a_2 m$

HT through cylindrical pipe

$q = -kA \frac{dT}{dr}$   
 $= -kA (2\pi r L) \frac{dT}{dr}$   
 $\int_{t_2}^{t_1} dt = \int_{r_1}^{r_2} \left( \frac{q}{-2\pi r L} \right) \frac{dr}{r}$   
 $\therefore t_2 - t_1 = \frac{q}{2\pi k L} \ln \left( \frac{r_2}{r_1} \right)$   
 $\therefore Q = \frac{2\pi k L (t_1 - t_2)}{\ln \left( \frac{r_2}{r_1} \right)}$

$R = \frac{r_2 - r_1}{k A_m}$   
 $A_m = \frac{A_1 + A_2}{2}$   
 $A_1 = 2\pi r_1 L$   
 $A_2 = 2\pi r_2 L$   
 $A_m = \frac{2\pi (r_1 + r_2) L}{2} = \pi (r_1 + r_2) L$   
 $R = \frac{r_2 - r_1}{k \pi (r_1 + r_2) L}$

Heat flow through pipes and walls

okay  $x_w$  equals  $r_2 - r_1$  equals then  $x_w$  equals  $r_3 - r_2$  so  $a_1 m$  equals  $a_2 m$  minus  $a_1$  logarithm of  $a_2$  minus  $a_1$  not minus it will divide equals  $2\pi r_2 - r_1$  by logarithm of  $R_2$  by  $R_1$ .  $A_1 m$   $2\pi R_3 - R_2 L$  divided by logarithm of  $R_3$  by  $R_2$ . The rate of heat transfer will be and  $Q$  rate of heat transfer is  $Q$  equals  $T_1 - T_3$  divided by  $R$  equals  $T_1 - T_2$  by  $R_1$  equals  $T_3 - T_2$  by  $R_2$  from which the interface temperature  $T_2$  can be evaluated.

$R = R_1 + R_2$   
 $= \frac{x_w}{k_1 A_1} + \frac{x_w}{k_2 A_2}$

$r_{m1} = \frac{r_2 - r_1}{2}$   
 $x_w = r_2 - r_1$   
 $A_{m1} = \frac{A_1 + A_2}{2} = \frac{2\pi (r_1 + r_2) L}{2} = \pi (r_1 + r_2) L$   
 $A_{m2} = \frac{2\pi (r_2 - r_1) L}{2} = \pi (r_2 - r_1) L$   
 $Q = \frac{T_1 - T_3}{R} = \frac{T_1 - T_2}{R_1} = \frac{T_3 - T_2}{R_2}$

Heat flow through pipes and walls

So, heat conduction through a wall, you have a wall. Now, what will happen? There will be one boundary layer, both side. And through boundary layer also, there is some gradient will be created.  $T_1$ ,  $T_2$ .

And this flow rate will be, heat flow rate is  $Q$ . So,  $R$  equals  $R_1$  resistance left side plus resistance of the metal plus resistance of the other side because of boundary layer. So, the formula will be like  $\frac{1}{h_1 A} + \frac{x}{KA} + \frac{1}{h_2 A}$ . The same area you are using  $Q$  equals  $U A (T_1 - T_2)$ . So, this will be like  $U A (T_1 - T_2) = \frac{T_1 - T_2}{\frac{1}{h_1 A} + \frac{x}{KA} + \frac{1}{h_2 A}}$ .

So,  $U$  is called overall heat transfer coefficient.  $U$  is called overall HT coefficient. So,  $\frac{1}{U A}$ , therefore,  $\frac{1}{U A} = \frac{1}{h_1} + \frac{x}{K} + \frac{1}{h_2}$ . So, hot fluid through a pipe.

Heat transfer through a wall

$$R = R_1 + R_2 + R_3 = \frac{1}{h_1 A} + \frac{x}{KA} + \frac{1}{h_2 A}$$

$$Q = \frac{t_1 - t_2}{R} = UA(t_1 - t_2)$$

$$\therefore \frac{1}{UA} = \frac{1}{h_1} + \frac{x}{k} + \frac{1}{h_2}$$

U = overall H.T. Coeff

Heat flow through pipes and walls

Now, I have one pipe. Again, here inner one boundary layer created and outside also one boundary layer created. okay and this is my pipe i'm shedding the pipe so that it will be clear this is okay now small  $r$  maybe  $r_1$   $r_2$  i can make so  $q$  equals  $t_h$  minus  $t_c$   $r_1$  plus  $r_2$  plus  $r_3$  equals  $t_h$  minus  $t_c$  divided by  $\frac{1}{h_1} + \frac{x}{k} + \frac{1}{h_2}$  okay so  $o$  means outside  $h_i$  or inside okay i can put so  $q$  equals  $u a$  this is hot fluid inside cylinder hot fluid inside cylinder so outside temperature is lower inside temperature is higher  $t_h$  minus  $t_c$  so  $\frac{1}{u a} = \frac{1}{h_1} + \frac{x}{k} + \frac{1}{h_2}$

$\frac{1}{k w a} + \frac{1}{h_o a} + \frac{1}{h_i a}$  or  $h_i$  i can write so if  $x$   $w$  small so  $a$   $o$   $a$   $1$   $m$   $a$   $i$  all equal So,  $\frac{1}{u o} = \frac{1}{h_i} + \frac{x}{k w} + \frac{1}{h_o}$ . So, this is taken from Picanhag book. So, if anything goes wrong, please go through the book.

NPTEL

Heat flow through pipes and walls

Non-dimensional numbers. So, I already discussed non-dimensional numbers like Reynolds number, Prandtl number, Nusselt number. There will be some other numbers like Grashof number, Grashof number and many other numbers are there. So, basically for our convective heat transfer coefficient, we will be using this Reynolds number, Prandtl number, Nusselt number. okay this number is very common actually for any fluid flow we are using so the formula is  $u d \rho$  by  $\mu$  so  $\nu$  is kinetic viscosity uh it for this formula is  $\mu$  by  $\rho$  and unit also you should remember meter square per second okay uh Reynolds number less than 2000

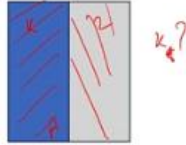
This is called laminar and more than 2000, about then it will be a turbulent. Why laminar and turbulent will be required? When turbulent is there, so we will have more heat transfer coefficient because of forced convection. Nusselt number, already I have given formula,  $h d$  by  $k$  Prandtl number.  $\mu C_p$  by  $K$  and  $H$  equals function of diameter viscosity is  $\rho \mu$   $K C_p$  okay and Nusselt number and Prandtl number many formula may be there but one formula is this like a Nusselt number

equals  $0.023$  Reynolds number power  $0.8$  Prandtl number power  $n$ . So,  $n$  equals  $0.4$  for heated fluid and equals  $0.3$  when fluid is cooled. Now, you see the simpler problem two plates of equal thickness here one plate Another plate is here, cross section area and cross section area from a composite heated medium. Thermal conductivity  $k$  is  $2k$ , area you can assume  $A$ . The effective thermal conductivity of the composite is, so you can see the formula. The steady state heat transfer total  $R_1$  plus  $R_2$ .

So,  $R T$  by  $k A$  area and thickness equal. are total  $2 T k$  effective. So,  $R_1 T$  by  $k$ ,  $R_2 T$  by  $2k$ . So, therefore,  $T$  by  $k$  plus  $T$  by  $2k$  equals  $3 T$  by  $2k$ . So,  $2 T$  by  $k$  effective. So, therefore,  $k$  effective is  $4$  by  $3$ . If you see add all this and it will become a  $4$  by  $3k$ . Another problem is that circular tube transporting hot fluid given data is given circular tube

**Problem-4**

- Two plates of equal thickness (t) and cross-sectional area form a composite heat transfer medium. Thermal conductivities of the plates are K and 2K. The effective thermal conductivity of the composite is \_\_\_ times of K.



Sol:  
For steady state heat transfer  
 $R_{total} = R_1 + R_2$   
 $R = t/K_e$   
Area; & thickness equal.  
 $R_{total} = 2t/K_{eff}$   
 $R_1 = t/K$   
 $R_2 = t/2K$   
Therefore,  $t/K + t/(2K) = 3t/(2K) = 2t/K_{eff}$   
Therefore,  $K_{eff} = 4/3K$



**Heat flow through pipes and walls**



hot fluid is it is transporting so outer diameter 0.5 meter inner temperature T inner temperature 80 outer temperature 25 degree and radius 0.4 this is 0.5 and per meter length of the tube heat transfer. So, Q value already you have to use the formula  $2 \pi L T_i \ln \frac{R_o}{R_i}$ . So, if you put directly the formula the values from the formula then you can get directly 15487 watt per meter.

**Problem-5**

- A circular tube transports hot fluid.  
Given data:  
 $r_o = 0.5 \text{ m}$   
 $T_i = 80^\circ\text{C}$   
 $r_i = 0.4 \text{ m}$   
 $T_o = 25^\circ\text{C}$   
 $K = 10 \text{ W/m-K}$

Q per meter length of the tube = ?



Sol:  
 $q = K \frac{2\pi L(T_i - T_o)}{\ln(\frac{r_o}{r_i})}$   
 $= 10 \times (2 \pi \times 1) (80 - 25) / \ln(0.5/0.4)$   
 $= 15487 \text{ W/m}$



**Heat flow through pipes and walls**

