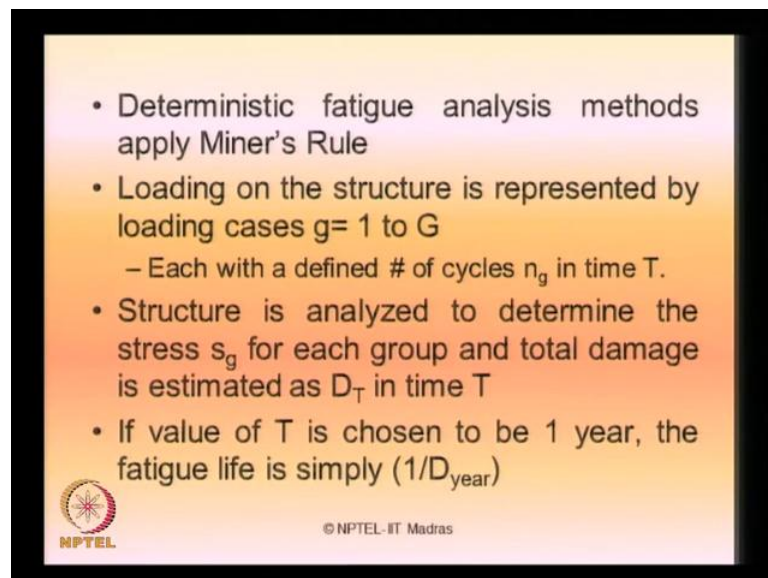


Advanced Marine Structures
Prof. Dr. Srinivasan Chandrasekaran
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Lecture - 4
Deterministic fatigue analysis

In the last lecture, we discussed about the time history. Once I have the stress range time history available to me, based on which you can use what we call as the rain flow counting technique, to find out the fatigue damage of each stress group and successfully the cumulative fatigue damage, okay? In this lecture we will talk about deterministic fatigue damage, using some spectral approach.

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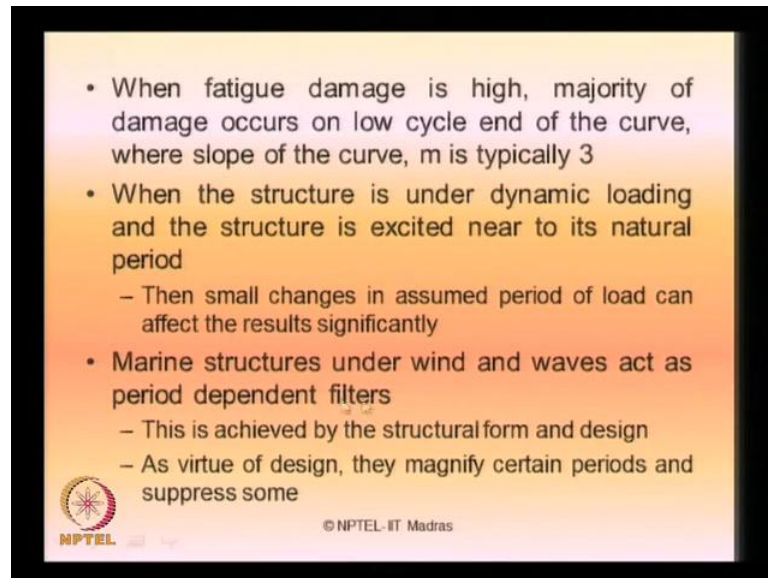


- Deterministic fatigue analysis methods apply Miner's Rule
- Loading on the structure is represented by loading cases $g= 1$ to G
 - Each with a defined # of cycles n_g in time T .
- Structure is analyzed to determine the stress s_g for each group and total damage is estimated as D_T in time T
- If value of T is chosen to be 1 year, the fatigue life is simply $(1/D_{\text{year}})$

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Deterministic fatigue analysis methods actually apply the minus rule, loading on the structure is represented by the loading cases varying from 1 to G , as we saw in the last example. Each cycle will be defined with n_g which is called number of cycles in time T the structure is analyzed to determine the stress group which is g of each group and the total damage is estimated in a given time T . If the value of time t chosen to be 1 year, then the fatigue life is simply 1 by the damage per year.

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- When fatigue damage is high, majority of damage occurs on low cycle end of the curve, where slope of the curve, m is typically 3
- When the structure is under dynamic loading and the structure is excited near to its natural period
 - Then small changes in assumed period of load can affect the results significantly
- Marine structures under wind and waves act as period dependent filters
 - This is achieved by the structural form and design
 - As virtue of design, they magnify certain periods and suppress some

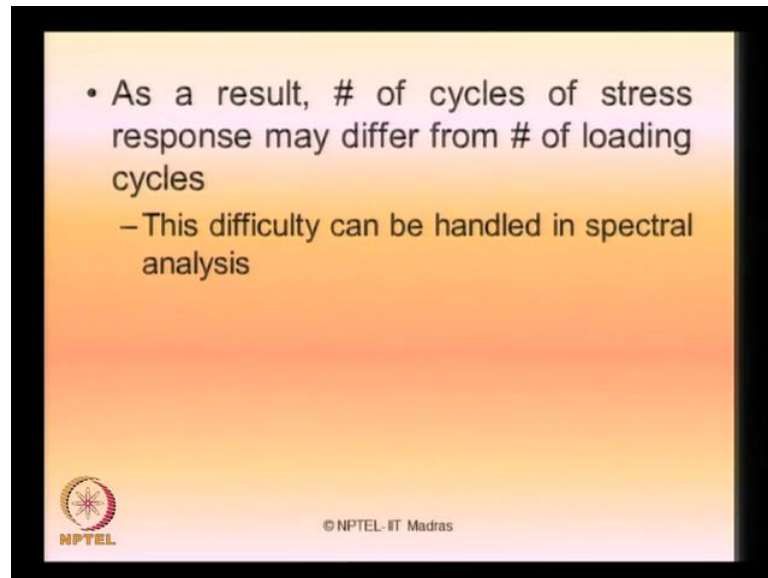
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When the fatigue damage is high, majority of the damage occurs on low cycle end of the curve, where the slope of the curve is typically 3 on marine structure materials. When the structure is under dynamic loading, the structure is then excited near to its natural frequency, in that case the small changes, in assumed period of the load can affect the result significantly, because it will start resonating. So, all your examples all your case studies what you did, when the structure is subjected to dynamic loading and the frequency matches with the natural frequency of the system, then your method of estimating the fatigue damage based on stress cycle count, will be wrong.

So, marine structures under wind and waves act as a period dependent filters, that is a very important property because this property actually comes from the virtual design of a marine system, because we design a floating structure, we design a deep water duct platforms. So, they filter certain frequencies, they allow only certain frequencies. As a virtue of the design they magnify certain periods and suppress some of them, okay? So, this is essentially assumed by the structural form and design what you follow in marine structures.

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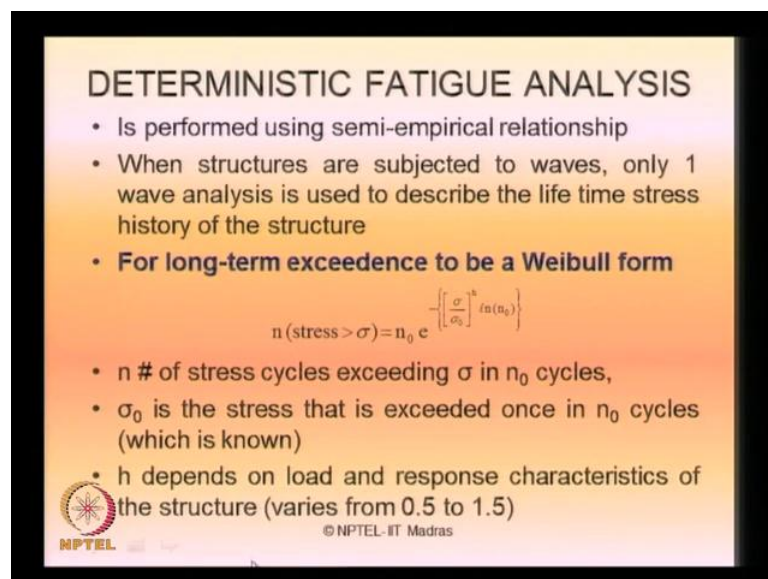


- As a result, # of cycles of stress response may differ from # of loading cycles
 - This difficulty can be handled in spectral analysis

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As a result, the number of cycles of stress response may differ from that of number of loading cycles. That is very important because you are suppressing the loading system on certain frequency domains or certain period domains. So, this difficulty can be handled in what we call, spectral analysis, because once you started playing with the selection of time domain where your structure is operating and at that range you want to locate the fatigue damage, then obviously you cannot do it with the time series of stress cycle ranges, you should look for the spectral analysis.

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DETERMINISTIC FATIGUE ANALYSIS

- Is performed using semi-empirical relationship
- When structures are subjected to waves, only 1 wave analysis is used to describe the life time stress history of the structure
- **For long-term exceedence to be a Weibull form**
$$n(\text{stress} > \sigma) = n_0 e^{-\left\{ \left[\frac{\sigma}{\sigma_0} \right]^h \ln(n_0) \right\}}$$
- n # of stress cycles exceeding σ in n_0 cycles,
- σ_0 is the stress that is exceeded once in n_0 cycles (which is known)
- h depends on load and response characteristics of the structure (varies from 0.5 to 1.5)

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So, let us talk about deterministic fatigue analysis. It is performed using semi empirical relationship, when the structures are subjected to waves, only one wave analysis used to describe the life time stress history of the structure, that is assumed. For long term exceedence to be a Weibull form... If you understand that the long term exceedence is of a Weibull distribution, then the stress which exceeds the range sigma, the number of that will be given by this expression, as you see in the screen now. Where n is the number of stress cycles, exceeding sigma in n naught cycles.

Sigma naught, what you see here, in this equation is the stress that is exceeded once in n naught cycles which is known to you for a given problem. And H, what you see here depends on the load and response characteristics of the structure. Essentially it differs or the value lies between 0.5 to 1.5, so this is an empirical relationship, which is used when the long term exceedence of your stress range is our Weibull distribution.

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• **For long-term exceedence to be a log-linear**

$$n(\text{wave height} > H) = n_0 e^{-\left\{\left[\frac{H}{H_0}\right]^k \ln(n_0)\right\}}$$

- H_0 is wave height exceeded once in a n_0 cycles (which is a known parameter)
- H is the wave height exceeded n times in n_0 cycles
- The long-term exceedence can be combined with the single slope of the S-N curve to estimate the fatigue damage in n_L cycles

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If it is of a different form, let us say it is of a log log linear distribution. These are the two common types of distribution, which is considered for long term exceedence, in marine structures. In that case the equation what you see here, is related to not this stress, but related to the wave height, directly. The H naught what you see here, is the wave height, which is exceeded once in n_0 cycles, which is again a known parameter. And of course, H what you see here, see here is the wave height, which exceeded n times in n_0 cycles. That n is here, which you are finding out and n_0 is already known.

The long term exceedence can be combined, with the single slope of SN curve to estimate the fatigue damage in n L cycles. If your SN curve is having a single slope, m is a unique number.

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Fatigue damage for single slope of SN curve

- **For Weibull distribution**

$$D_L = \frac{n_L \sigma_0^m}{A} \frac{\Gamma\left[1 + \frac{m}{h}\right]}{[\ln(n_0)]^{\frac{m}{h}}}$$
- **For log-linear wave height exceedence**

$$D_L = \frac{n_L [aH_0^b]^m}{A} \frac{\Gamma[1 + bm]}{[\ln(n_0)]^{bm}}$$
- Where gamma function is defined by

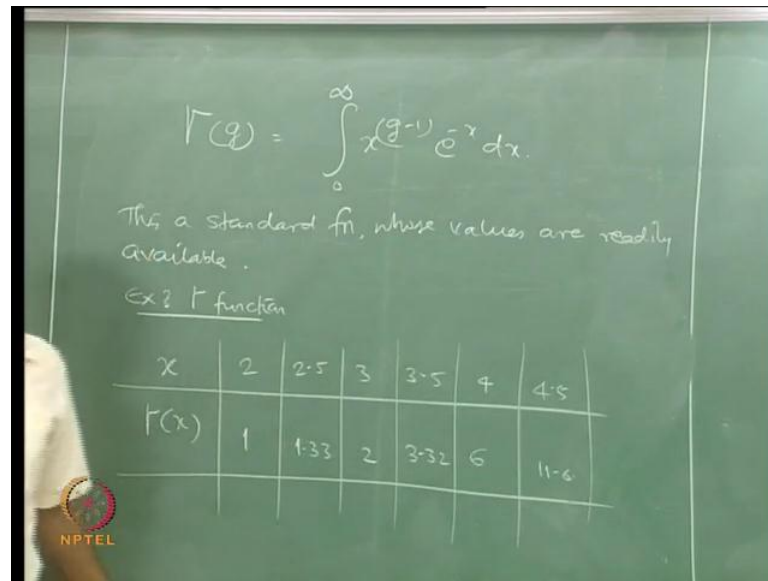
$$\Gamma(g) = \int_0^{\infty} x^{(g-1)} e^{-x} dx$$
- This is a standard function and the values of Gamma function are available in the standard statistical tables

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So, if you want to estimate the fatigue damage for single slope of SN curve, where m is fixed, where m is fixed then if it is a Weibull distribution, I can use this equation DL is given by n L sigma naught to the power m and this is a gamma function. The gamma function is evaluated using this equation. And this is a natural logarithm of n naught m by H, where H is defined already, if it is a log linear wave by it exceedence, then use this equation for fatigue damage.

If the slope of the SN curve is a single value, there also you got the gamma function, in this case use the stress rangewhereas, here use the H value, it is the wave height. The gamma function in both these expressions, is given by a simple equation like this. This is a standard function and the values of gamma function available in the standard statistical tables. For our understanding, let us try to plot or let us try to list some of the gamma function values, which are available in all standard statistics books.

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Let us see how this can be evaluated. Gamma function, which is actually given by an expression $\int_0^{\infty} x^{g-1} e^{-x} dx$. For various values of x , I should say it is a standard function, whose values are readily available in the table, but still let us try to write down this value. So, I should say an example of the gamma function, so let us say for different values of x , I am looking for gamma $x=2, 2.5, 3, 3.5, 4$, and 4.5 , the gamma functions, the value of these functions for different expressions available here or $1, 1.33, 2, 3.32$, these are all the values of the gamma function respective values of the argument, $6, 11.6$.

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Spectral fatigue analysis

- It is applicable to structures that are executed in dynamic loading which has stationary properties for a large # of stress cycles
 - For example, wind turbulence, wave loads etc
- Spectral method uses the shape of the stress spectrum to determine the # of stress cycles of various sizes
- Stress spectrum can be narrow or broad-banded

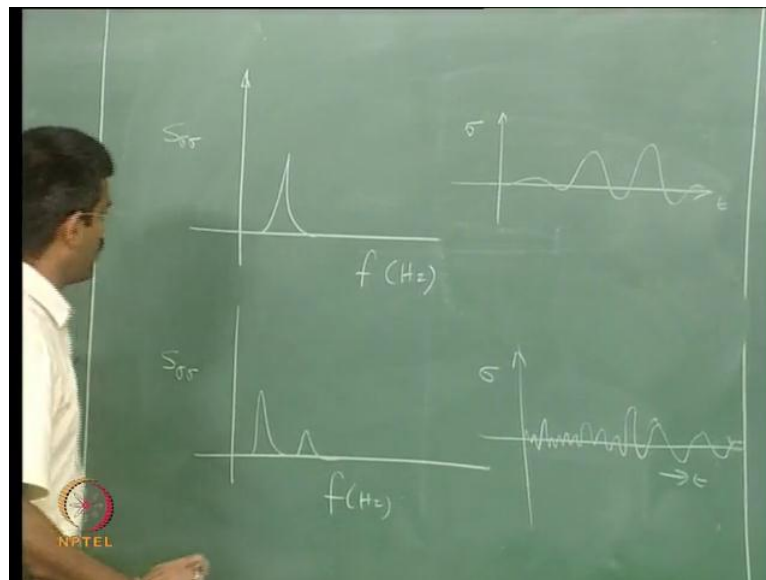
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Now, let us look at the spectral fatigue analysis, it is applicable to structures that has executed the dynamic loading, which has stationary properties for larger number of stress cycles. For example, if you are looking for wind turbulence, wave load effects etcetera, which are executed in dynamic loading format, then I must use what we call spectral fatigue analysis. The spectral method uses the shape of the stress spectrum, to determine the number of stress cycles of various sizes because the last example in the rain flow counting method, the shape of the space spectrum was not counted.

We only look at the peaks and valleys of the stress cycle and counted the cycles, number of cycles in the stress range and found out the fatigue damage estimates. This is not applicable, when the structure is excited in a dynamic loading condition and unfortunately, the frequency content of the loading matches with that of the natural frequency of the system. So, I must use the spectral method, which should impact use the shape of the stress spectrum itself, to determine the number of stress cycles of various sizes, sizes means stress ranges. Now, the stress spectrum can be narrow banded or broad banded. Now, how a narrow band stress spectrum will look like, and how a broad band will look like?

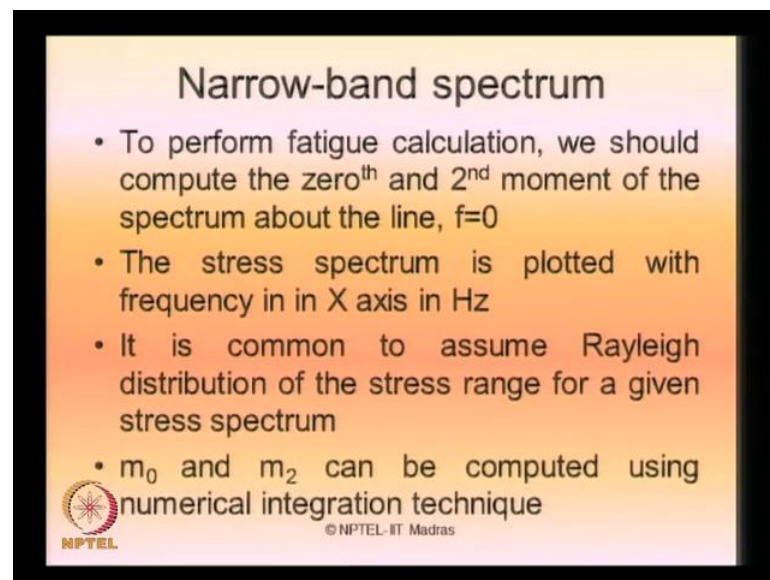
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Let us say, this becomes the narrow band spectrum, where this is my frequency in hertz and this becomes my S_{σ} , and this is my narrow band spectrum and the corresponding time is t can look like this and so on. For a broad band, f in hertz S_{σ} , it have


multiple peaks, in that case look at the time history, this will vary very randomly. In fact, so obviously you cannot easily use a peak and valley counting for this, right? Because a variation is very highly random, so this is what I call a narrow band spectrum and time history, this is broad band spectrum and time history.

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Narrow-band spectrum

- To perform fatigue calculation, we should compute the zeroth and 2nd moment of the spectrum about the line, $f=0$
- The stress spectrum is plotted with frequency in X axis in Hz
- It is common to assume Rayleigh distribution of the stress range for a given stress spectrum
- m_0 and m_2 can be computed using numerical integration technique

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Now, let us say my stress cycle range, it is a narrow band spectrum as you see here. If it is a narrow band spectrum to perform fatigue calculation, we must now compute zeroth and second momentum of the spectrum, about the line where f is equal to 0. I must compute the zeroth and second moment of the spectrum, which I call as m_0 and m_2 , I will come to that. The space, the stress spectrum is now plotted, with the frequency in x axis in hertz. As you see here it is common to assume a Rayleigh distribution of the stress range for a given spectrum. m_0 and m_2 can be computed using numerical integration technique.

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- M_0 is area under the stress spectrum, which corresponds to variance of the signal
- Mean zero crossing period is given by

$$n = \frac{T}{T_z}$$

$$p(\sigma_r) = \frac{\sigma_r}{4m_0} e^{-\frac{\sigma_r^2}{8m_0}}$$

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m naught is area under stress spectrum, which corresponds to variance of the signal.

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Mean zero crossing period, $T_z = \sqrt{\frac{m_0}{m_2}}$

of stress cycles (N) in time T sec

$$n = \frac{T}{T_z}$$

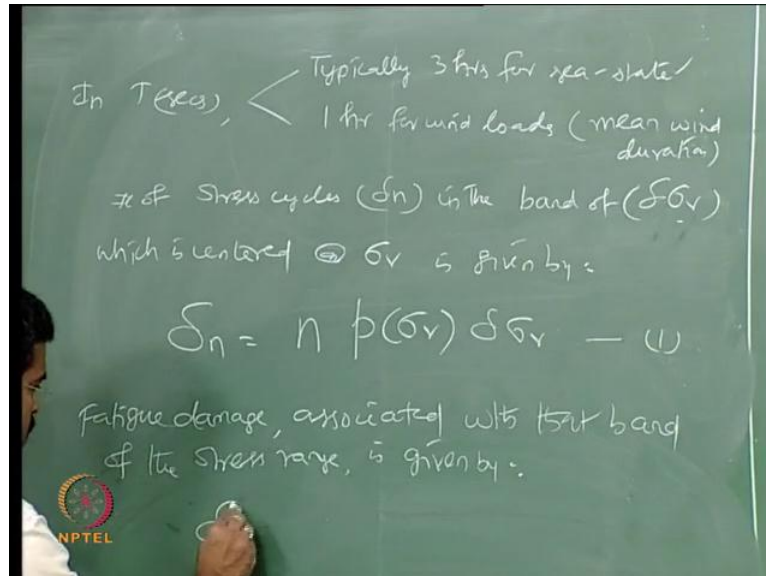
for Rayleigh distribution, pdf of the stress range (σ_r) is given by:

$$p(\sigma_r) = \frac{\sigma_r}{4m_0} e^{-\left(\frac{\sigma_r^2}{8m_0}\right)}$$

The mean zero crossing period is given by the mean 0 crossing period, which I call as T_z will simply given by square root of m_0 by m_2 . And the number of stress cycles, which I call as n in time T seconds is given by simply T by T_z . T_z is already known to me, then the probability density function for Rayleigh distribution, of the stress range, the probability density function of the stress

range, is given by σ_r , which is σ_r by 4 m naught e to the power of minus σ_r square by 8 m naught.

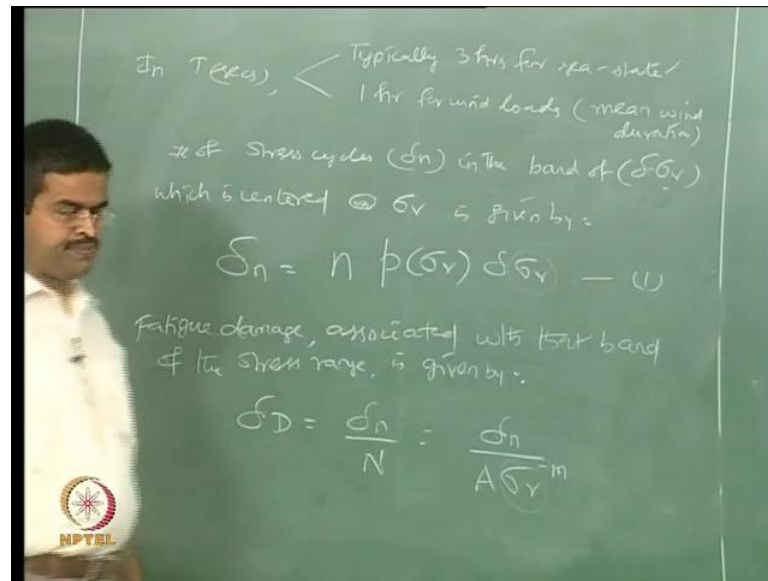
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Therefore, in T seconds, this T seconds can be typically 3 hours, for a sea state. In marine structures can be 1 hour for wind loads. This is for sea state in terms of waves can be 3 hours, it can be 1 hour for mean wind duration. Therefore, in T seconds the number of cycles or the number of stress cycles, which I called as Δn in the band of $\Delta \sigma_r$, which is centered at σ_r is given by $\Delta n = n$. The probability density function, what you already had in the previous case, $\Delta \sigma_r$ now, this is equation number one.

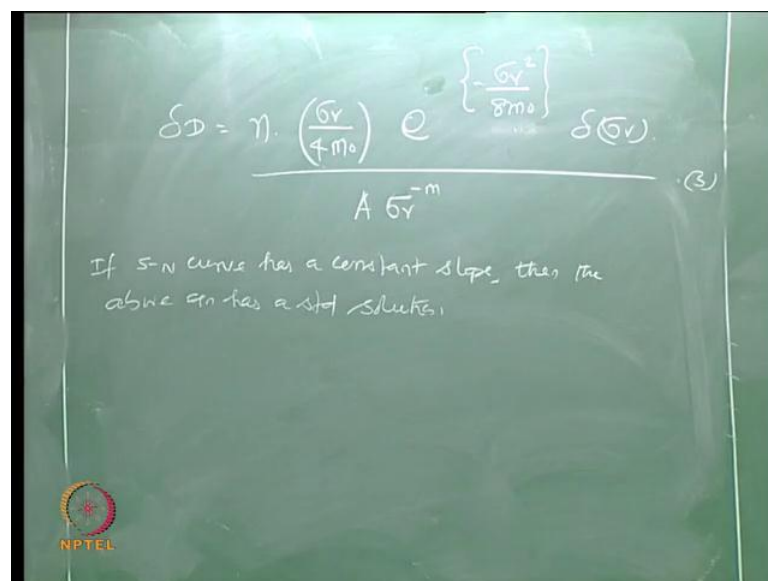
Now, the fatigue damage associated with that band of stress cycle because even in the rain flow counting also, we tried to find out the damage for each range. So, here instead of saying range, we are saying it is band. That is nothing but $\Delta \sigma_r$ is the stress range, that is a small band of stress range, if it is narrow band we are discussing this. So, fatigue damage associated with that band of the stress range is given by ΔD , I am using Δ for the small band, so which is nothing but Δn by n . Δ already you know, we can substitute here.

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Now, we already know n also, Δn by... n is the standard equation for the SN curve which is nothing but $A \sigma_r^{-m}$. I am using this range, which is the range of this band, equation two. Now, I have already know the expression for Δn , which is a function of probability density function of σ_r . Let us substitute back all of them and see that, ΔD can be now simply n of probability density function is σ_r by $A \sigma_r^{-m}$ naught e to the power of minus σ_r square by $8 m$ naught of $\Delta \sigma_r$ by $A \sigma_r^{-m}$, called it is equation number three.

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Now, if the SN curve has a constant slope, then the above equation has a standard solution, for a constant slope. Let us write down that equation here.

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For a constant slope of S-N curve,

$$\int_0^{\infty} x^a \exp(-bx^c) dx$$

$$= \frac{\Gamma\left(\frac{a+1}{c}\right)}{c b^{\frac{a+1}{c}}} \quad (3)$$

where $\Gamma(g) = \int_0^{\infty} x^{g-1} e^{-x} dx$.

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For a constant slope of SN curve, the solution turns out to be a standard gamma function, which is written here, 0 to infinity exponential minus b x to the power of c d x, which can be simply gamma function of a plus 1 by c divided by c b a plus 1 by c. I call this equation number three, where we already know where gamma function of any value g is given by 0 to infinity x of g minus 1 e minus x d x. This is standard equation, where we are evaluating the gamma function. Now, let us compare this equation with our standard form and see what happens?

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The chalkboard contains the following content:

$$\delta D = \frac{n \left(\frac{\sigma_r}{4m_0} \right) \cdot \exp \left\{ -\frac{\sigma_r^2}{8m_0} \right\} S(\sigma_r)}{A \sigma_r^{-m}}$$

fatigue damage for all n cycles, is given by
Integrating the above eqn.

$$D = \int_0^{\infty} \frac{n \left(\frac{\sigma_r}{4m_0} \right) \cdot e^{-\left(\frac{\sigma_r^2}{8m_0} \right)} S(\sigma_r)}{A \sigma_r^{-m}}$$

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Let us say delta D already I know is $n \sigma_r$ by $4 m$ naught exponential minus σ_r square by $8 m$ naught delta σ_r by $A \sigma_r$ minus m . This is the damage for a small narrow band of σ_r . I am looking for the cumulative damage, is it not? That is what we are also doing the last example. So, the fatigue damage for all cycles is given by integrating the above equation. Let us integrate this, so I must get D , which should be integral of 0 to infinity, the same equation simply I write here. $n \sigma_r$ by $4 m$ naught to the power of minus σ_r square by $8 m$ naught delta σ_r by $A \sigma_r$ minus m . Now, the r given to σ_r , let us try to simplify this equation.

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Simplifying, we get

$$D = \frac{N}{4A m_0} \int_0^{\infty} \sigma r^{(m+1)} \exp\left(-\frac{\sigma r^2}{8 m_0}\right) \delta \sigma r$$

Comparing with

$$\int_0^{\infty} x^a \exp(-b x^c) dx$$

Simplifying, we get, I am rewriting this D can be said as n by 4 m naught, n by 4 m naught. I take it out integral of 0 to infinity. So, I have sigma r here, I have sigma r of minus m here, I can say sigma r of m plus 1. Then exponential minus sigma r square by 8 m naught delta sigma r. Now, let us compare this with the standard equation comparing with sorry not A m naught, can be written as 4 m naught, 4A m naught, is that okay? Sigma m plus 1 exponential sigma r square by 8 m naught.

Now, I compare this with the expression x power a exponential minus b x c d x. The argument is, if it is x power a it is d x, if it is sigma r it has delta sigma r, the argument is similar. I can compare these two, when I compare because this also integration from a limit, integration from a limit.

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The chalkboard shows the following derivation:

$$\begin{aligned}
 a &= m+1 \\
 b &= \frac{1}{8m_0} \\
 c &= 2
 \end{aligned}
 \quad \Bigg| \quad \text{hence} \equiv \frac{\Gamma\left(\frac{a+1}{c}\right)}{c \cdot b^{\left(\frac{a+1}{c}\right)}}$$

$$\equiv \frac{\Gamma\left(\frac{m+1+1}{2}\right)}{2 \left(\frac{1}{8m_0}\right)^{\left(\frac{m+2}{2}\right)}} = \frac{\Gamma\left(\frac{m+2}{2}\right)}{2 \left(\frac{1}{8m_0}\right)^{\left(\frac{m+2}{2}\right)}}$$

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I can straight away say a is m plus 1, is it not? a is m plus 1 and b which is 1 by 8 m naught because there is a minus minus, sigma r c x, c can be different but b is 1 by 8 m naught, 1 by 8 m naught and c is 2. So, I can now evaluate this expression, it is a standard gamma function, that gamma functions has given to you. That was gamma of a plus 1 by c by c b raised to the power of a plus 1 by c, is that okay? Is that okay?

Now, I can write this value as, gamma function of a is 1 plus 1, m plus 1 by c is 2 by c is 2 b is 1 by 8 m naught raised to the power of m plus 2 by 2, is it okay? I get this as m plus 2 by 2, which can be gamma of m plus 2 by 2 by... This can be evaluated like this, hence the total fatigue damage for n number of cycles.

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$$D = \frac{n}{4 A m_0} \left\{ \frac{\Gamma\left(\frac{m+2}{2}\right)}{2 \left(\frac{1}{8 m_0}\right)^{\left(\frac{m+2}{2}\right)}} \right\}$$

$$D = \frac{n}{A} 8 m_0^{\left(\frac{m}{2}\right)} \Gamma\left(\frac{m+2}{2}\right) \quad \text{--- (5)}$$

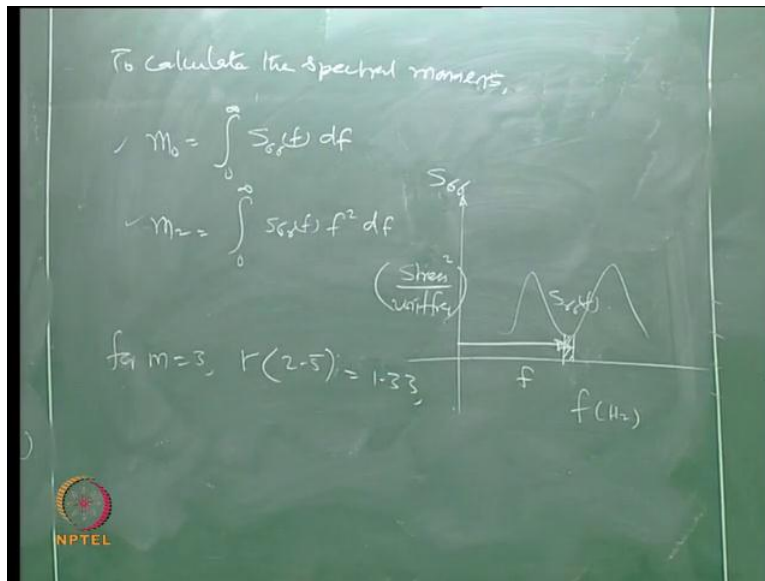
we know that $n = T/T_z$ and $T_z = \sqrt{\frac{m_0}{m_z}}$

$$D = T \sqrt{\frac{m_z}{m_0}} \frac{8 m_0^{\left(\frac{m}{2}\right)}}{A} \Gamma\left(\frac{m+2}{2}\right) \quad \text{--- (6)}$$

D can be now said as, n by 4 A m naught gamma of m plus 2 by 2 divided by 2 of 1 by 8 m naught of m plus 2 by 2, simplifying because I have got m naught here, m naught here, 2, 8, 4 etcetera. Simplifying them, I have got a power also, simplifying them can say by A because this 4 and this 4 goes away. I will get 8 m naught m by 2 of gamma function m plus 2 by 2, that is my total damage, is equation number five. Now, I already know, we already know that n, what is n? Turn back and tell me what is n? n is number of cycle, which we can said T by T z, is it not? And what is T z? Square root of m naught by m z, good. So, I have T z here, substitute here, I have n, I have n here substitute here, I get D as T m 2 by m naught because this T is it a denominator, 8 m 0 raised to the power of m by 2 by A gamma function of m plus 2 by 2, is that okay?

This becomes equation number six. For a given slope, standard slope, these all for constant slope. For a constant slope of m may be 3, you already know it is going to be 2.5, look at the table. For gamma 2.5, we already know the value of this function. So, if you know the spectral moments of m naught m 2 etcetera, m is the slope, m naught m 2 spectral moments and you already know the value of T, where you are evaluating the D. And A is again the constant of the SN curve, you can find the cumulative damage for a narrow spectrum of the stress cycle, as you see from this expression number six.

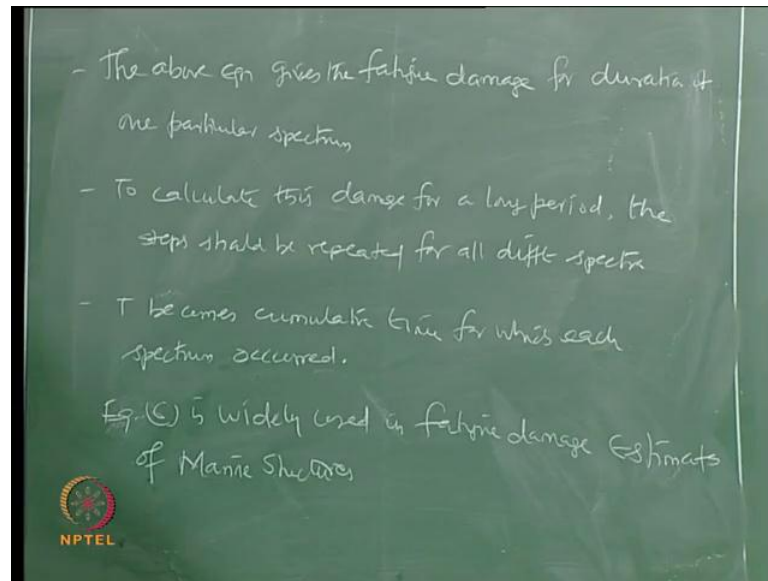
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Now, to calculate m_n spectral moments, the general expression is, to calculate the spectral moments m_n is given by $\int_0^\infty S_{\sigma}(f) f^n df$ and m_2 is given by $\int_0^\infty S_{\sigma}(f) f^2 df$, where I try to plot a spectrum, the frequency is in hertz and this becomes my stress.

Let us say $S_{\sigma}(f)$, the ordinate is nothing but stress square by unit frequency. So, if I get a specific spectrum like this, you want to look at a specific value f is the distance by a plot here, this is f and this is $\times S_{\sigma}(f)$. So, m_0 and m_2 are given by these two equations, and gamma function is already known to you, for m is equal to 3 for m is equal to 3 gamma of 2.5 from the table is 1.33.

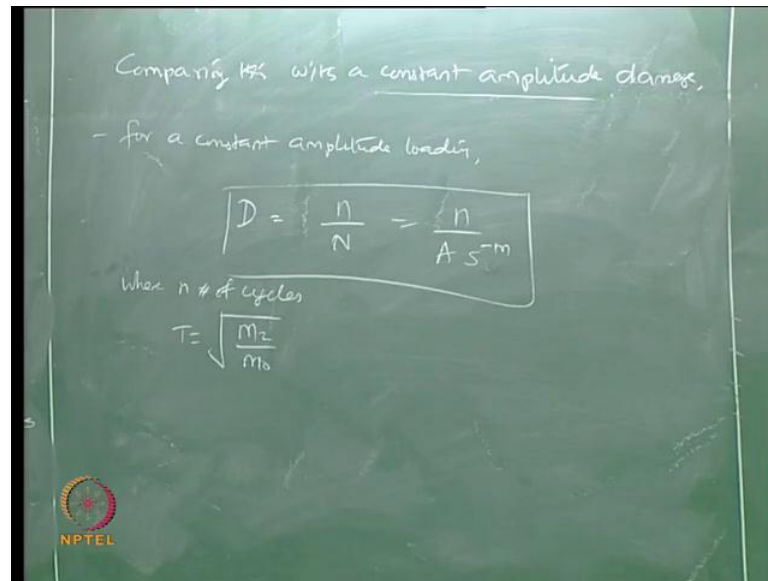
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You know the gamma function here, so the above equation, the above equation what you see here, gives the fatigue damage for duration of one particular spectrum. If you really want to calculate this for a long period, for a longer period, then this should be repeated. The steps should be repeated for all different spectra because you have got a specific spectra S_e title, for all different spectra you will repeat this, that can occur in the marine structure. In that case T then becomes cumulative, time for which each spectrum occurred.

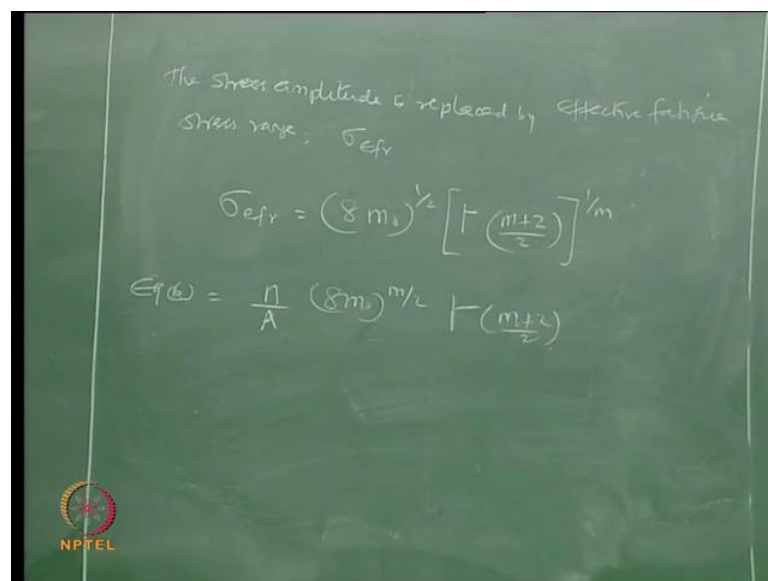
So, T is no more related to one specific value, it becomes a cumulative value. So, equation what was a spectral damage equation, lastly we had? The equation number, equation six is widely used, in fatigue damage estimates of marine structures, if it is a narrow band. Now, let us quickly compare this with the constant amplitude loading because in this case stress cycle is vary, that is why we are plotting the stress cycle spectrum.

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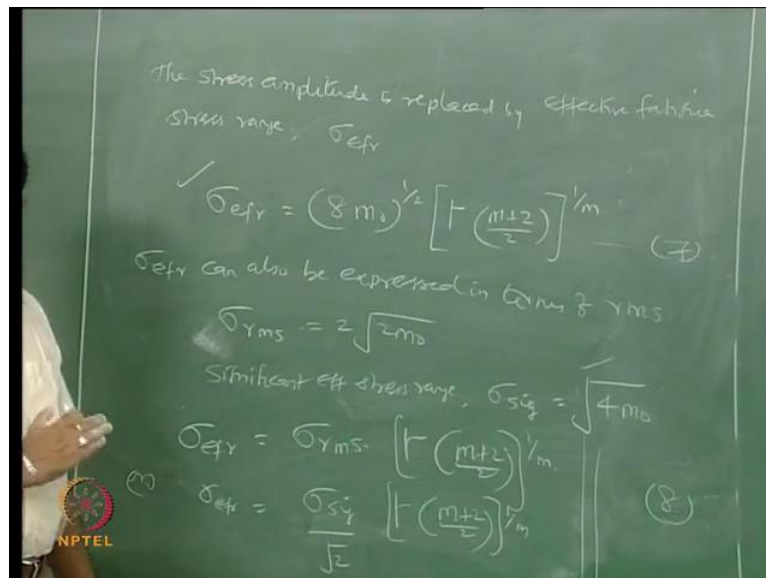
If it is a constant amplitude damage, comparing this constant amplitude damage we know that, for a constant amplitude loading D that is the damage is given by n by N , is it not? We already know this equation which is nothing but n by $A S^{-m}$, where n is the number of cycles and T is of course, square root of m_2 by m_0 . I want to compare this method of estimating damage for a constant amplitude with that of equation seven, that is what I am, six, that is what I am trying to do. So, instead of having a single, simple, amplitude of the stress, I will have a effective stress amplitude.

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So, the stress amplitude is replaced by effective fatigue stress range, which is σ_{efr} . Effective fatigue stress range σ_{efr} , is given by $8 m$ naught to the power half, that is the equation. What I am writing from the equation six is, it not γm plus 2 by 2 raised to the power of 1 by m , is that okay? Look at equation six, equation six I am writing for our understanding, equation six was γm plus 2 by 2 raised to the power of m by 2 γm plus 2 by 2, is it not? I am comparing this, I am trying to find out, what is the equivalency of effective fatigue stress range compared to the standard damage? I get this equation, equation number seven. So, that is what we call a effective fatigue stress range.

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You can also rewrite this effective fatigue stress range can also be expressed in terms of $r m s$ values. So, σ_{rms} , that is root mean square of the stress range is given by, 2 of root of $2 m$ naught. So, significant effective stress range σ_{sig} can be $4 m$ naught. Therefore, I can write σ_{efr} as σ_{rms} 8 can be 4 into 2 , that is 2 root m 2 half is already there. So, I can say this is σ_{rms} , simply γm plus 2 by 2 of 1 by m or σ_{efr} can also be said as σ_{sig} , which I know here, which is $4 m$ naught, which can now be γm plus 2 by 2 to the power of 1 by m by root 2, is it okay?

Because 8 is 2 root, I already have 2 here, so I divided by root 2. So, I can write σ_{efr} as this in terms of $r m s$ or this in terms of significant


because from a given stress spectrum, you will be getting these values. Sometimes you will get these values in the literature, you can find effective stress range. Once you know the effective stress range, I can easily find the fatigue damage as comparable to a single constant amplitude damage like this. Now, let us quickly look at the summary of this. So, for our understanding, let us plot a table for different values of m . m is nothing but the slope of the SN curve, where σ_{efr} by σ_{rms} . σ_{efr} by σ_{rms} significant for different values of m .

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m	$\frac{\sigma_{efr}}{\sigma_{rms}}$	$\frac{\sigma_{efr}}{\sigma_{rms}}$
1		
2	1.00	0.707
3	1.099	$(1.099)^{1/\sqrt{3}}$
4		

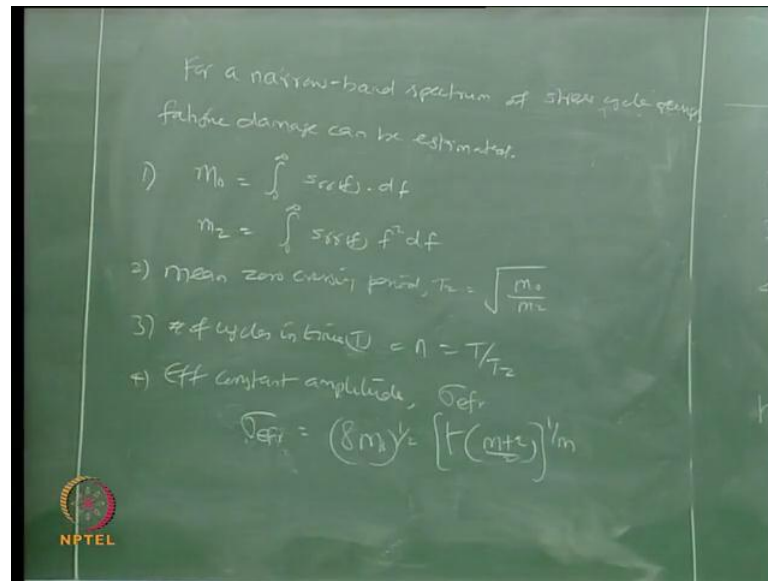
$\Gamma(2.5) = \Gamma(2.5) = 1.33$
 $(1.33)^{1/2}$

$\Gamma(2)$



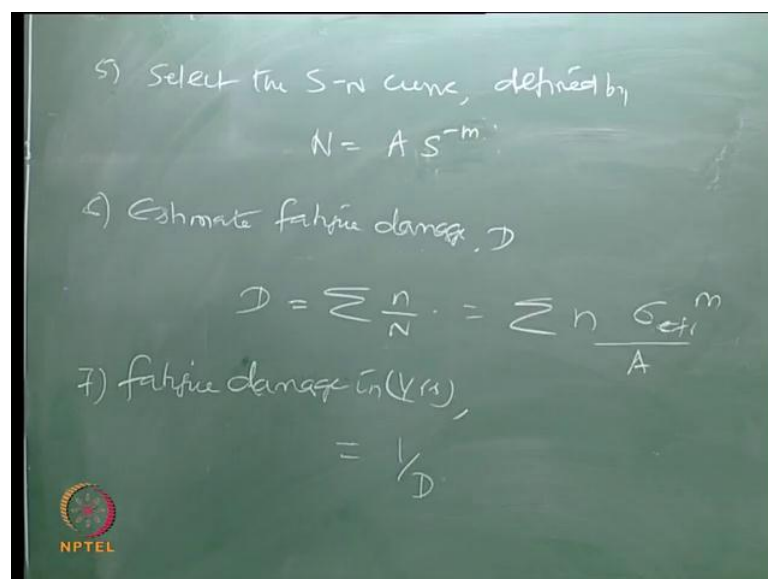
So, for different values of m , I must know how to evaluate the gamma function for values of m . Gamma function equation will be given to you and you know the table also. So, let us plot for... The slope of the curve cannot be 0, slope is having some value, 1, 2, 3, 4. Let us say for example, can you give me the value of σ_{efr} for 2 because 1 you may not have the value. So, if you have substitute m is equal to 2 here, I get gamma function as at 2.5, which is 1.33. 1.33 to the power of 1 by 2 that root of 1.33. So, σ_{efr} with σ_{rms} will be that value, how much is that? Root of 1.33, so this value is going to be 1.15 by root 2 and so on so forth. I can easily find out these values, let us quickly write the summary.

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For a narrow band spectrum of stress cycle range, for a narrow band spectrum of stress cycle range, fatigue damage can be estimated as below. First find out m_0 and m_2 because you need the spectral moments. m_0 is nothing but $\int_0^{\infty} S \sigma f \, df$. m_2 is $\int_0^{\infty} S \sigma f^2 \, df$. Then find the mean zero crossing period, which is T_z , which is nothing but the ratio of m_0 by m_2 , is that okay? Is it right? $T_z = m_0 / m_2$. The number of cycles in time T , which is given by $n = T / T_z$. Once I know this, I find effective constant amplitude, which I call σ_{eff} . σ_{eff} is given by $(8 m_0)^{1/2} \left[\frac{\Gamma(m+2)}{\Gamma(m)} \right]^{1/2}$.

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Now, select the S N curve, select the S N curve defined by N is equal to $A S^m$ minus m . Now, estimate the fatigue damage D , which is given by sum of n by N , which is nothing but sum of $n \sigma_e^m$, that is my stress because instead of S , I am going to use effective stress range, which is going to be divided by A because actually n is $A S^m$ power minus m , it goes off becomes m and S is σ_e . σ_e is already known to me, so if I know m for a given spectrum, which is given by this equation and if you know the values, slope of the curve m , which is approximately 3, I can find σ_e .

σ_e is known to me, I can find the damage. In the next class, we will talk about the broad band spectrum because we discussed about narrow band spectrum here for a stress cycle range. If it is narrow band, I can easily handle this 7 steps, I will get the fatigue damage in years. If I have got a broad band, I will apply some correction and convert that into a narrow band, that is what people have been doing, to find out the fatigue estimation for broad band spectrums. Now, in this lecture we understood that why at all we go for a spectral fatigue damage, why not time series?

In the last lecture we discussed about the time series estimates of fatigue damage, simply by rain flow counting technique, where we understand only the peaks and valleys. In this case I cannot handle because if it is a dynamic loading as in case of wave or wind, the response on the structure excite under this band of near resonance frequency, will not clearly give you a correct picture of the damages. So, I must look for a stress cycles spectrum. It can be narrow it can be broad, if it is narrow I know how to handle it, if it is broad how to handle it? Next lecture we will discuss this.

Thank you.