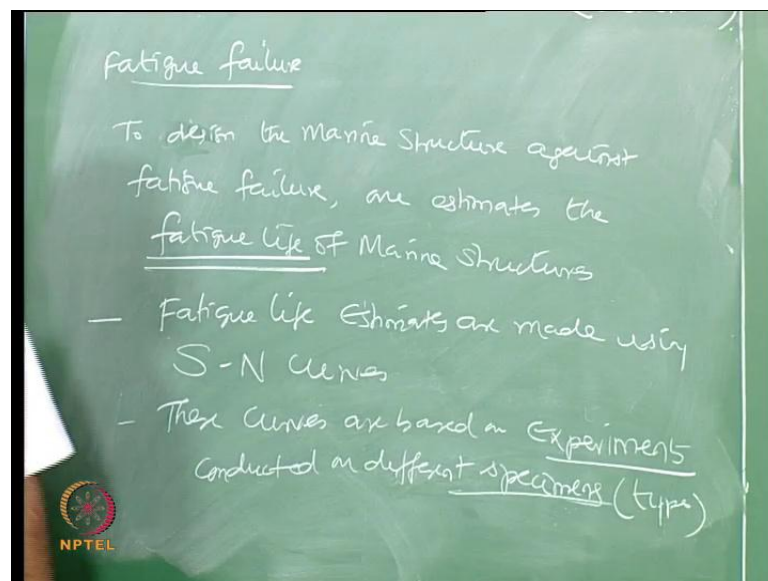


Advanced Marine structures
Prof. Dr. Srinivasan Chandrasekaran
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Lecture - 2
Fatigue failure

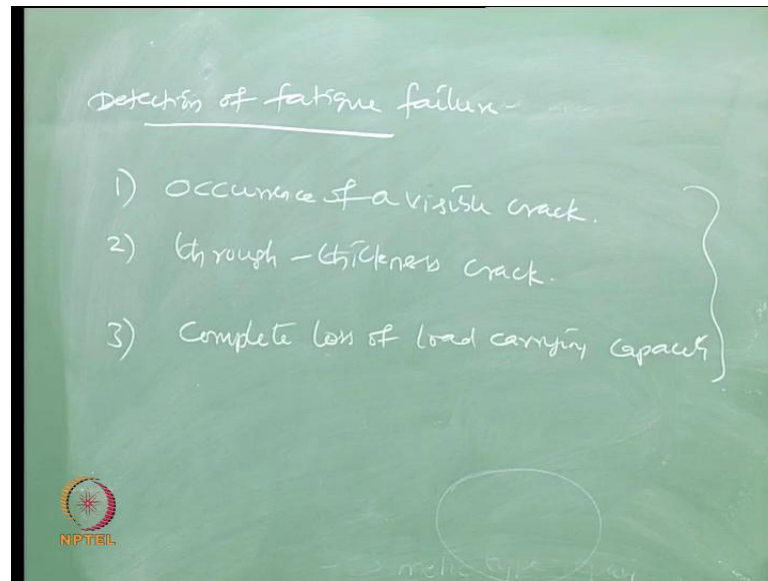
So, in the last lecture, we discussed about fatigue and failure. We said that those a construction of a material, are the construction material used for manufacturing a machinery compared that of an. Let us say construction of a marine structure, may be steel material is common. But still assessing the fatigue failure and understanding the fatigue damage or designing for a fatigue behavior, will be different in both these cases. Because, though the material is similar in both the cases, but in the case of machinery, you will know that the stress variation or fluctuations or in a specific state of or state on a specific range. And this is cost by the range of stresses applied on the material or on the machinery for a given design life. And one can easily estimate to limit, by limiting the stress levels within the endurance limit, whereas this concept cannot be applied to marine structures. Because in marine structures, there is a mixture of different kinds of stresses and fluctuations happening and therefore, one must estimate in a different manner.

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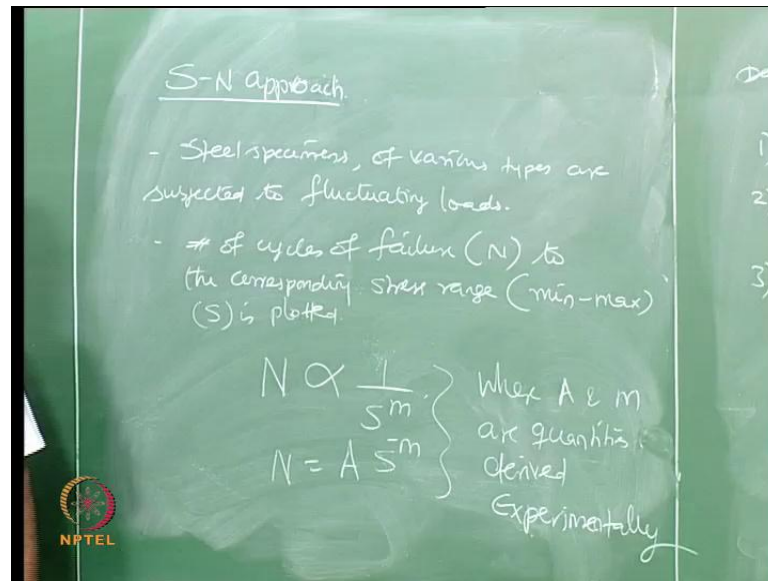
Now, to design the marine structure, against fatigue failure or fatigue damage, one estimates the fatigue life of marine structures. So, we estimate fatigue life. Usually, the fatigue life estimates are done, are made using S N curves. These curves are based on experiments conducted on different specimens. We can even say different types of specimens to be very specific.

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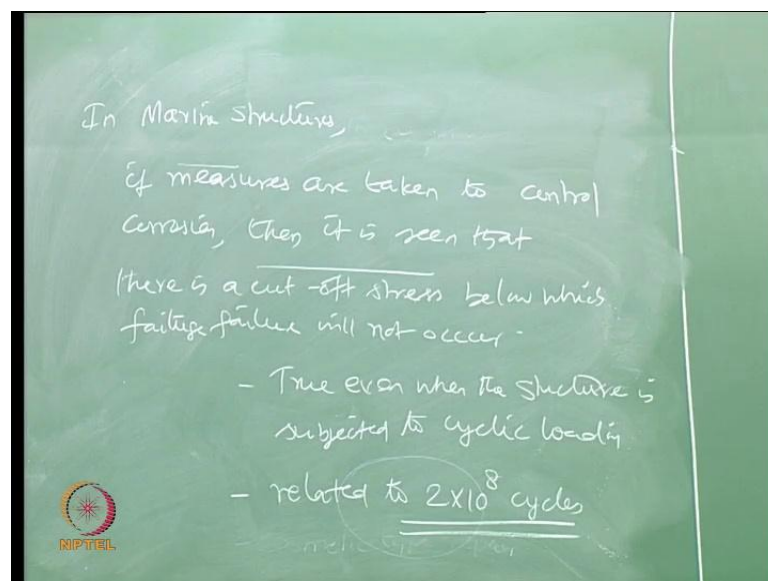
How one can detect fatigue failure? How one can detect that the material or the member of the structure failed to be fatigue? Fatigue failure can be detected by three ways and can detect fatigue failure by looking observation 3 ways. When, you notice an occurrence of a visible crack, when you notice a visible crack or, if you notice through a thickness crack and you notice a complete loss of load carrying capacity. Then we can infer that the material or the member or the structure is failed by fatigue. So, these are detections of a fatigue failure of a structural member.

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Now, let's talk about the S-N approach. In the S-N approach, steel specimens of various types are subjected to fluctuating loads, usually tensile in nature. The number of cycles of failure, which we call as N, is plotted against the corresponding stress range. The stress range, I am talking about, is the values from minimum to maximum. It is not a specific stress value, it is a range. This is always plotted, which we call as S-N curves. So, N seems to be proportional to some power of m. So, N is equal to some constant A, so where A and m are quantities derived experimentally, suppose in marine structures.

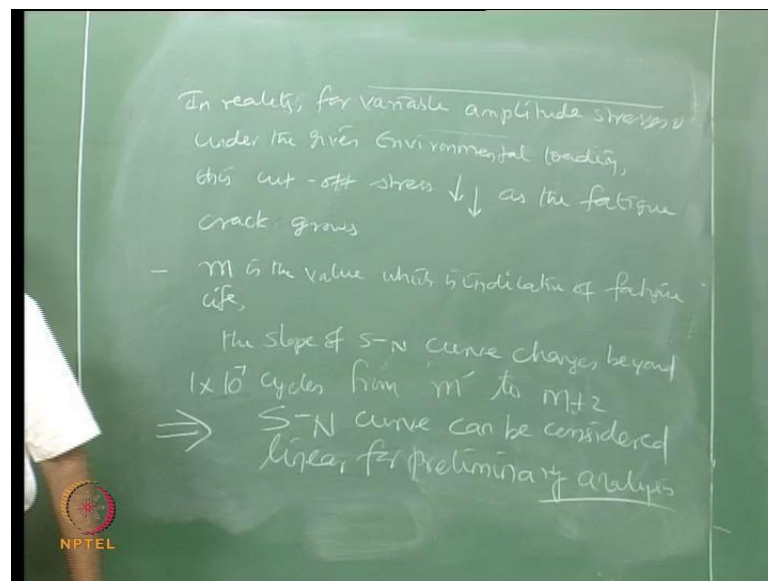
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In marine structures, if we take measures to control corrosion. There are many techniques by which control corrosion can be controlled. If I adopt, all those measures to control corrosion in a marine structure. Then it is seen that, there is a cut off stress below which fatigue failure will not occur, this is true even when the structure is subjected to cyclic load. And that cut off stress is related to 2×10^8 cycles. So, that cut off stress corresponding to 2×10^8 cycles in a same curve is the threshold value.

If you are able to employ a measure to control corrosion and the stress level is below. This, which is corresponding to 10^7 cycles, then fatigue failure will not be initiated in marine structures. So, the stress level should be kept to that cut off value and that corresponds to 10^7 cycles in a; in a same curve. This is true, only when measures to control corrosion are adapted, without that it is not correct. If you are able to do that, then this is the value.

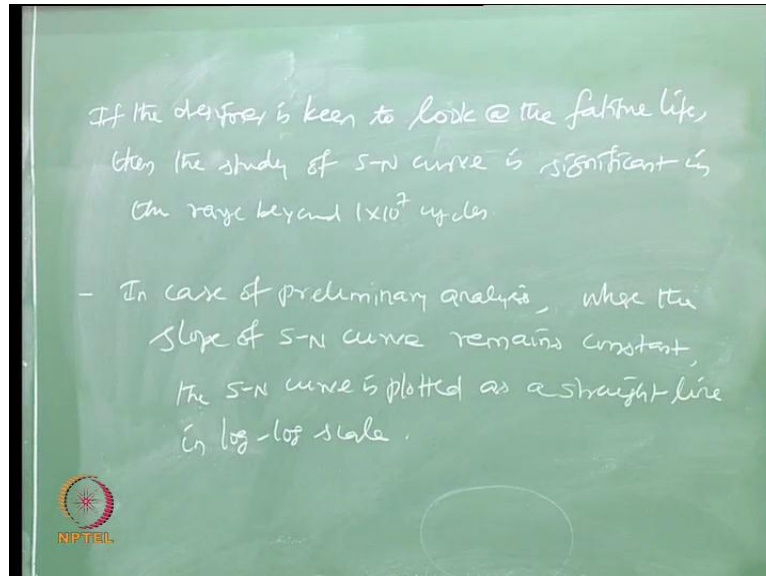
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Now, in reality for variable amplitude stresses and under the given environmental loading, this cut off stress decreases, as the fatigue crack grows. So, there will be reduction in this stress carrying capacity, or a stress range capacity, when they are subjected to real environmental loading. And it is subjected to variable amplitude stresses. Interestingly, as m is the value, which is indicative of fatigue life, the slope of the S N curve, actually changes, beyond 10^7 cycles from m to $m+2$, the slope changes, what does it mean is that. The S N curve can be considered. Linear for preliminary analysis, it changes only

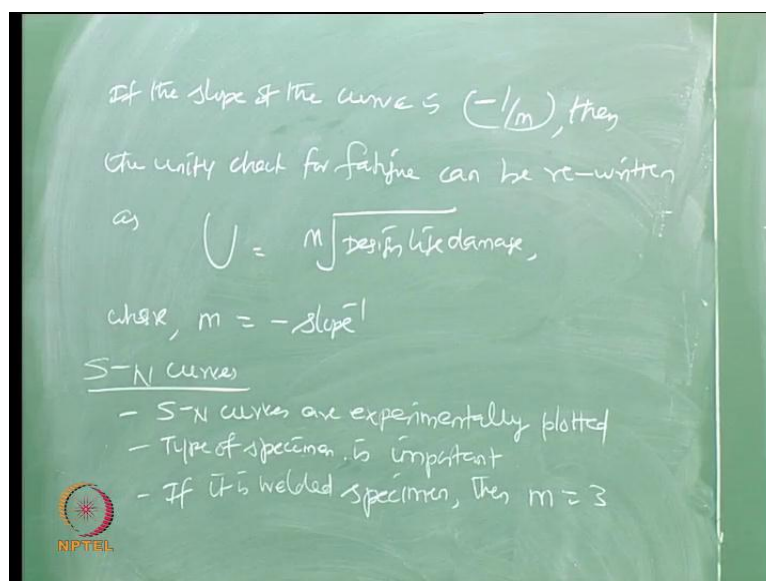
beyond a specific number of cycles. Until, then it remains the straightline. So, it can be consider as linear.

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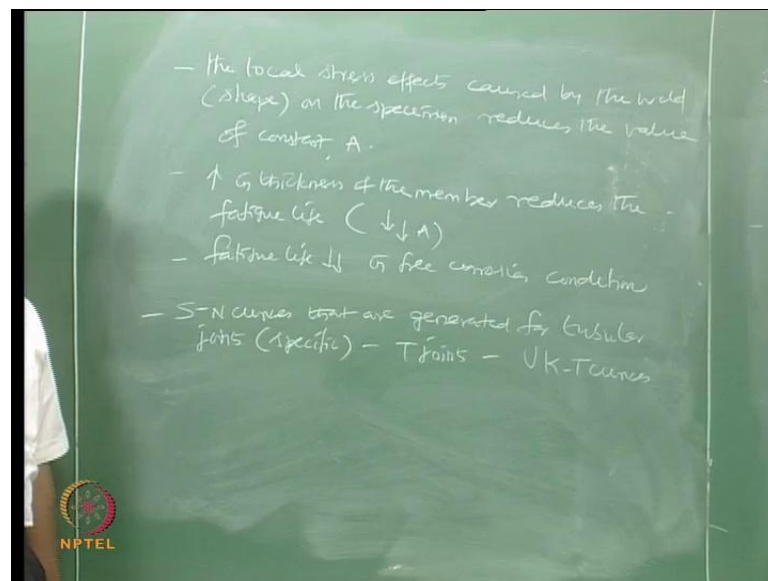
If the designer is interested, look at the fatigue life, then the study of S N curves is significant. In the range beyond, $10^{power 7}$ cycles. Now let us look at in case of preliminary analysis, where the slope of the S N curve remains constant, that is what they have said here. The S N curve is plotted as straight line.

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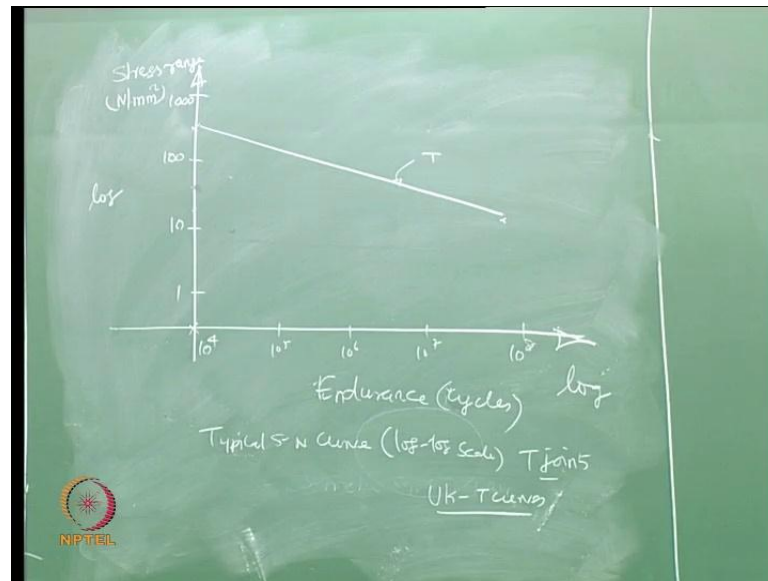
In a log scale, slope of the curves minus 1 by m. Then the unity check for fatigue can be written as $U = m \cdot S^{-1}$, where m is minus of slope inverse, in this equation. If the slope is corrected to be S^{-1} by m . Now, let us look more about the S-N curves. Before you plot one and show how they look like. S-N curves are experimentally plotted. That is the first observation, which we must know. In the type of specimen, which is used to plot is important, because this can also govern the slope of the S-N curve. For example, if it is a welded structure, then m is 3.

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Now, interestingly the local stress effects caused by the weld or I should say by the shape of the weld on the specimen reduce the value of constant A . A is a constant. We saw in the equation earlier. Next point is increase in thickness of the member also effects S-N curve. It reduces the fatigue life, that is it reduces A significantly. The value of A , A is a constant. And as we all know fatigue life is decreased in free corrosion condition. Many international codes are focused S-N curves to be very specific on tubular joints, because as you know S-N curves are influenced by the type of specimen, and they have also influenced by the shape of the weld. So, there are specific curves generated by conducting experiment on T joint or tubular joints. So, there are S-N curves that are generated for tubular joints very specifically, especially for T joint. For example, one can look at, what we call as UKT curves. A typical T curve or UK T curve looks like this.

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So, log log scale is also log scale. This is also a log scale. So, let us say this value is 10 power of 4. Let us say, this is 10 power 8567110100. Let us say 1000, so typical curve 40 joints, so typical curve. So, typical S N curve plotted on a log log scale, which is for T joints source UK T curves.

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$$N = A S^{-m}$$

$$N = \begin{cases} A S^{-m} & \text{for } S > S' \\ \infty & \text{for } S \leq S' \end{cases} \quad (2)$$

alternatively,

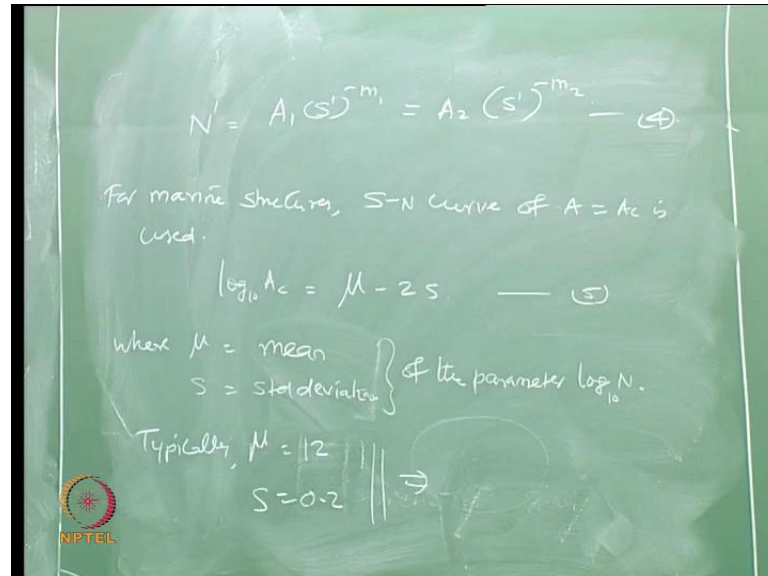
$$N = \begin{cases} A_1 S^{-m_1} & \text{for } S > S' \\ A_2 S^{-m_2} & \text{for } S \leq S' \end{cases} \quad (3)$$

where (N', S') is the point of intersection of the two curves given by Eqn (3).

So, we know that, N is equal to AS power minus m, N also be AS power minus m for S greater than S dash, which is equal to infinity for S less than S dash. Let us see equation number 2. Alternatively, N can be also written as A1 Sm1 or A2 m2 for S greater than S

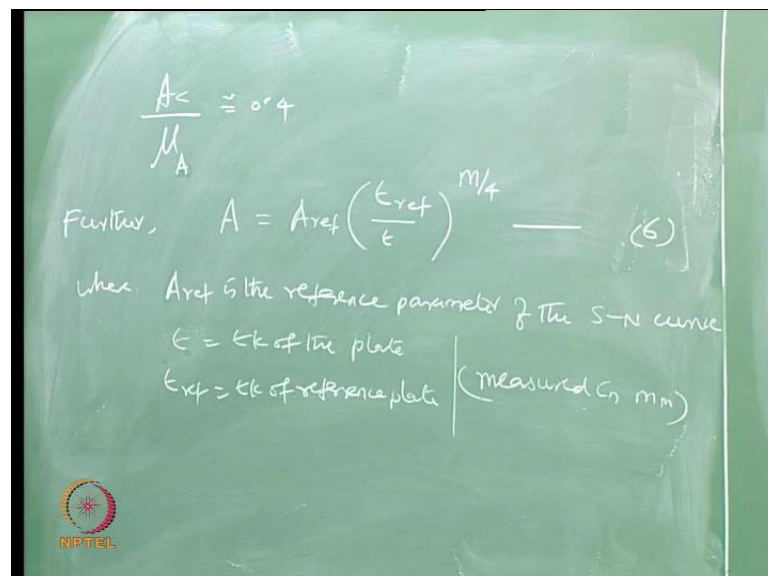
dash. For S less than equal to S dash. Where N dash S dash is the point of the intersection of the 2 curves shown in equation 23, we can also.

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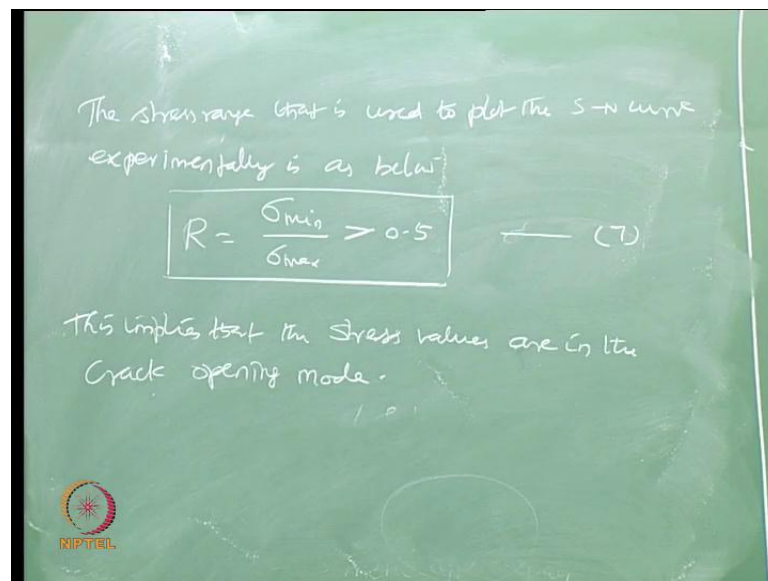
Write N dash can be $A_1 S$ dash minus m_1 . That is also equal to $A_2 S$ dash minus m_2 . For marine structures, your common equation, which defines S N curve of A equal A_c is used. Whereas the equation connects A_c is given by, where μ is the standard deviation, sorry mean. And S is the standard deviation of parameter $\log N$ the base 10, typically μ is 12 and S is 0.2, which gives me.

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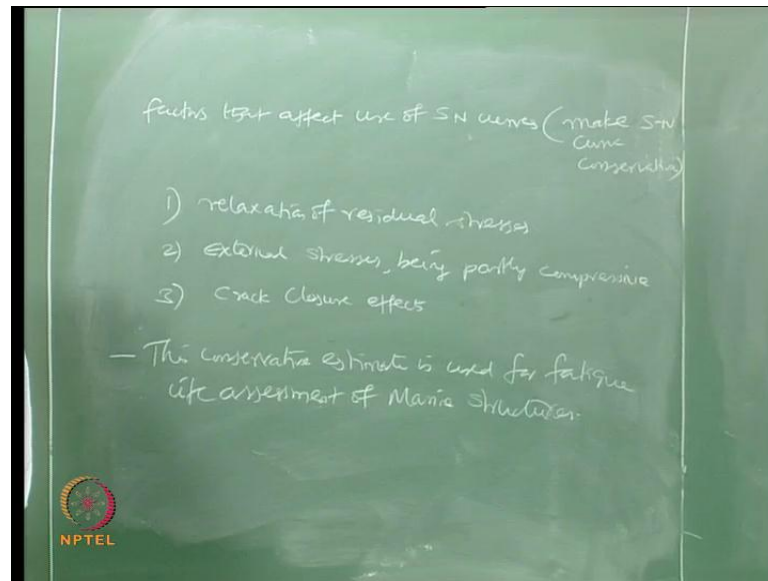
A_c by μA is it not, μA , that is deviation of σ is approximately 0.4. Further, we already know that A is influenced by the thickness of the material of the member. Therefore, A is also given by a reference t reference by t raise to the power of m by 4, equation number 6. Where $A_{reference}$ is the reference parameter of the S-N curve. T is the thickness of the plate, which is being used for study. And $T_{reference}$ is thickness of the reference plate based on which S-N curve is plotted both of them are measured in millimeters.

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Now, we already said that, S-N curves are experimentally generated or plotted on different types of specimen for a specific stress range. So, the stress range that is used to plot the S-N curve experimentally is as below. R is the range which is stress min to stress max, which is greater than 0.5, that is the stress range we have been used generally to plot S-N curves. This implies that the stress values are in the crack opening mode. Having understood that the stress strain or say S-N curves are plotted experimentally, shape of the specimen, type of the specimen, shape of the weld, thickness of the reference member, all influences S-N curve then.

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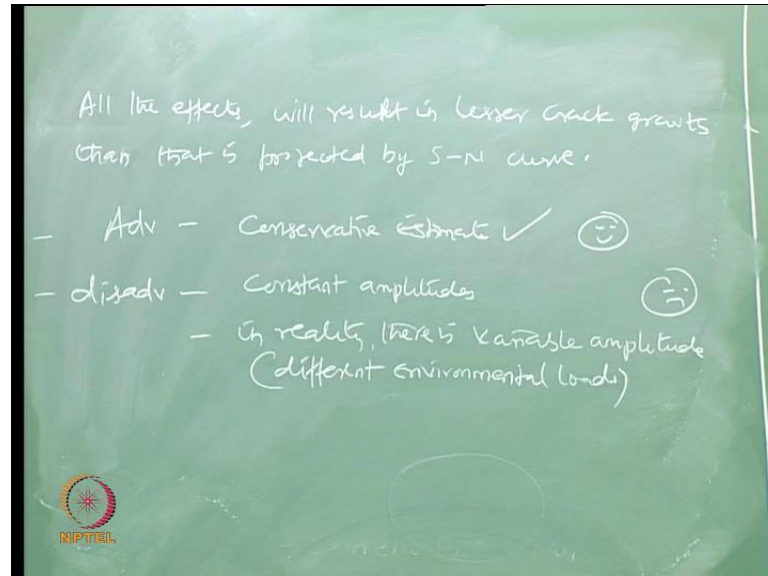
Let us quickly see, what are the factors that affect use of S N curves? Are the factors which make, the factors that make S N curves conservative, I mean safe, the for most factor is relaxation of residual stresses. That is the first factor which makes S N curves plotted as conservative got S. The second one is external stresses being partly compressive. See whenever a crack is formed or propagated or initiated. Let us say, if I apply for that tensile stresses, there is a probability that the crack will get propagated or extended or expanded. When you apply a partially compressive stress rate, there is a possibility that the propagation of cracks will not be as fast as that of tensile stress.

In reality, if you see this always reversal of forces. So, the stress does not remain always tensile, it can also become compressive. Therefore, S N curves which are plotted based on stress ranges purely tensile will become conservative stresses. The third point, which is addressing the crack closure effects, there can be some parameters, which can influence the closing of crack also, which is completely ignore, because the stress range which our construing in S N curves plots, or essentially on the crack opening modes.

So, you are compulsory casting range of stress, which results in opening of cracks. But in reality, there can be a possibility that closure effect cracks can be there, which we do not consider in the experimental manner of plotting S N curves. Therefore, if use S N curves, to find out the fatigue life for a given stress range, how many number of cycles the structure can withstand. The values what you get from the conventional S N curve given

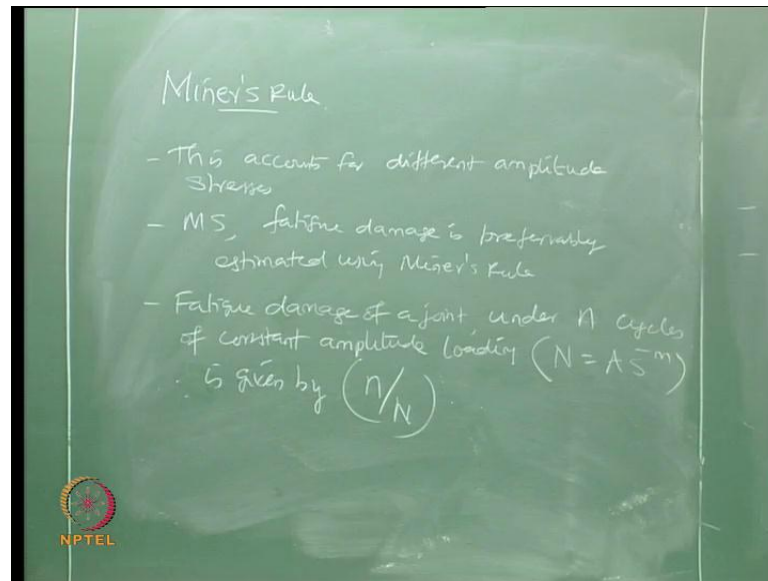
in the code will become a conservative estimate. And therefore, this conservative estimate is used for fatigue life assessment of marine structures.

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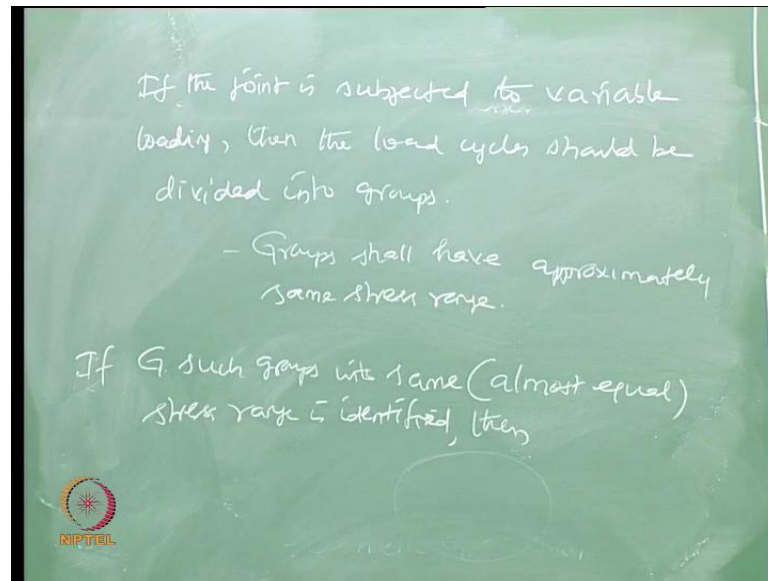
So, all these effects; all these effects will result in lesser crack growth, than that is projected by a conventional S N curve. So, all S N curves are generally considered to be conservative estimates. Now, there are some specific problems associated with S N curve. One advantage, S N curve has is, it is a conservative estimate. That is good, the other disadvantage what we have is, S N curves are generally plotted for constant amplitude. But in reality, there is variable amplitude which is essentially caused by different environmental loads, so that is a demerit. Now, how to handle this issue minus rule has been applied is a correction to the S N curve that is a last topic what we will discuss today in this lecture.

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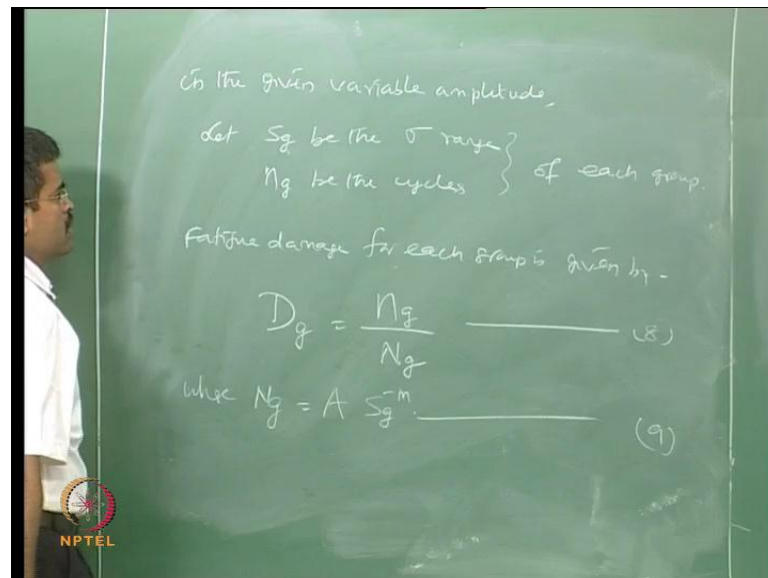
So, there is something called a miners rule, which is applied as a correction factor to the estimate of time from S N curves. So, this accounts for different amplitude stresses which conventional S N curve does not. Therefore, for marine structures, fatigue damage is preferably estimated using miners rule. Let us see, what is a miners rule? If you are looking for fatigue damage of a joint, under N cycles of constant amplitude loading, which could be N is equal to $A S^m$. That is the estimate we already know from the S N curve estimate based on this equation. Where m is the slope or minus 1 by m is the slope of the curve. So, the fatigue damage of a joint and the N cycles of constant amplitude loading which can be given by this equation. Let us put it as small n here, is given by simply n by N .

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If the joint is subjected to variable loading, as the case of marine structures under environmental loads, then the load cycles should be divided into groups. These groups shall have approximately the same stress range. If that is the case, if G such groups with same or almost equal stress range is identified, then.

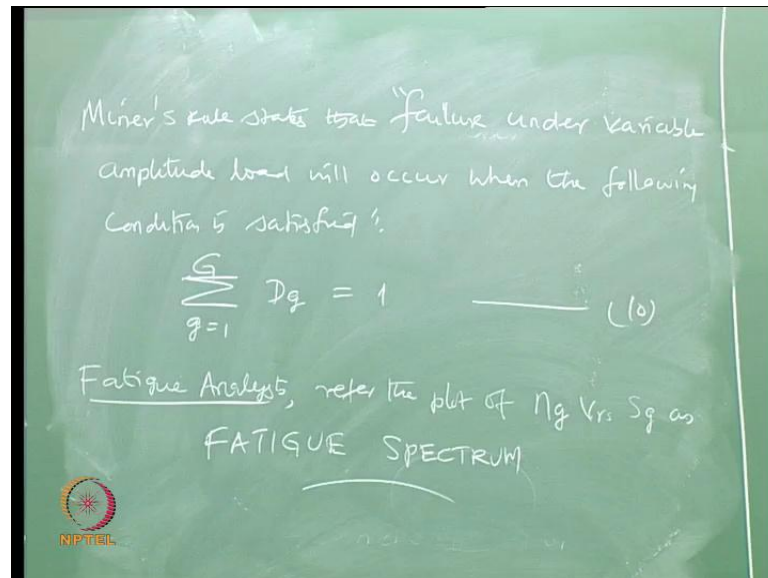
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In the given variable amplitude, let S_g be the stress range. And n_g be the cycles of each group. Fatigue damage for each group is given by D_g . D_g of each group is simply n_g / N_g . Where, what is equation number here fine where what is that? 8, where n_g is $A S_g^m$

minus m and I calls this equation number 9. So, you have got g 's as groups. Each group you know the stress range s_g and the number of cycles for the stress range n_g . So, for each group the fatigue damage is simply with this number. But I want to find the fatigue damage of the whole structure or the member for submitted to every well amplitude in that case.

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Miner's rule states that failure and the variable amplitude load will occur. When, the following condition is satisfied. The condition is now interestingly, the fatigue analysts refer, the plot of n_g versus s_g as fatigue spectrum. So, in this lecture, we have understood that, how the fatigue assessment or the fatigue failure on marine structure can be estimated. Why S-N curves from a very major part in estimating the fatigue life of a marine structure, even though; marine structure can be constructed which steel is a material, which is similarly, to that of missionary where indolence limit is always consider as one of the criteria to find of the cut of stresses.

Because here the main component is, the stress variation range is very large. And we are getting mixture of small and large amplitude low defects on the members. Whereas in the other cases in missionary. This kind of variety of amplitude variation does not occur. So, S-N curves play a very important role. In estimating the fatigue life say estimate the S-N curves remains linear up to a specific number of cycles, which has been seen by experimental experiments conducted on test specimens.

And we have also seen, what are the factor with that influence S N curves formation. And if a marine structure is controlled under corrosion, or against corrosion. Than one can say that, the stress range correspond a specific number of cycles, if the stress range is not reached or not exceeded. Let us say, then the fatigue damage will not be cost to the marine structure. However, when the variety of combination of loads and variation or variable in this loads occur are load effects occuron marine structures. The constants which form a part of the S N curves, which remains linear of to a specific value or 10 power 7 cycles, where the slop changes from m to m plus 2.

As it is been seen in experiments, the constants A and m the slop and the constant get seriously affected by variety of parameters. Two important parameters could be thickness of the member or the material, which you are assessing. And other could be even the shape of the weld. Therefore, S N curves can be used only as a pulmonary analysis of fatigue failure or fatigue damage or essentially to estimate fatigue life. Butin reality in marine structures, we have got composition or mixture of variables of load effects, whereas S N curves are plotted on a specific manner on type of specimen. Where, essentially the forces are remaining as tensile stresses. Buthere we have got other information's, where the stresses can be compressive as well and as a mixture.

So, the S N curve conventionally available, though they remain conservative, cannot be applicable to marine structures. Therefore, minus rule is an modification on S N curves, which is applied for estimating fatigue life of marine structures. Man; marines rule say that yougrouped, the stress range and the corresponding number of cycles of each group, separately from a given stress history or stress range time history. And for the each group estimate the fatigue damage. By this equation, if you really wanted to know. What is the fatigue damage of the entire structure, which is having different group of such groups than you have to fulfill this condition? If this comes to around one are closer to one it is showed that the groups of the stress ranges will result in fatigue damage of the member.

In the next lecture, we will talk about the fatigue assessment, on time history scale as well as frequency response in the next lecture. That will be our focus on the following lecture. Do you have any questions here, in this lecture? The experiments cannot match in the real time, but here experiments. Yes, you meant to say, why it is so. I repeat again the same explanation, what I gave as you correctly said. Yes, the experiments conducted on the lab scale to estimate fatigue damage cannot map exactly the behavior and the

environmental loads on real time structures. Agreed, but S N curves are done under control environment, experimentally on various types of specimen only to estimate the preliminary damage or the preliminary fatigue life of a given member.

So, only you to estimate the preliminary fatigue life, one can use S N curves as a design phenomenon. If you really wanted to look at, the fatigue estimate on the design prediction of the structure into cyclic loading. One should look for the non-linear component of the variations of slopes components in S N curves. Where the S N curves does not remain on the same slope, are will not acquire the same slope. So, in the lab scale the experiment conducted to estimate S N curves cannot directly map the behavior and reality. But still to a greater agreement, international codes to recommend fatigue life estimates based on S N curves.

Thank you.