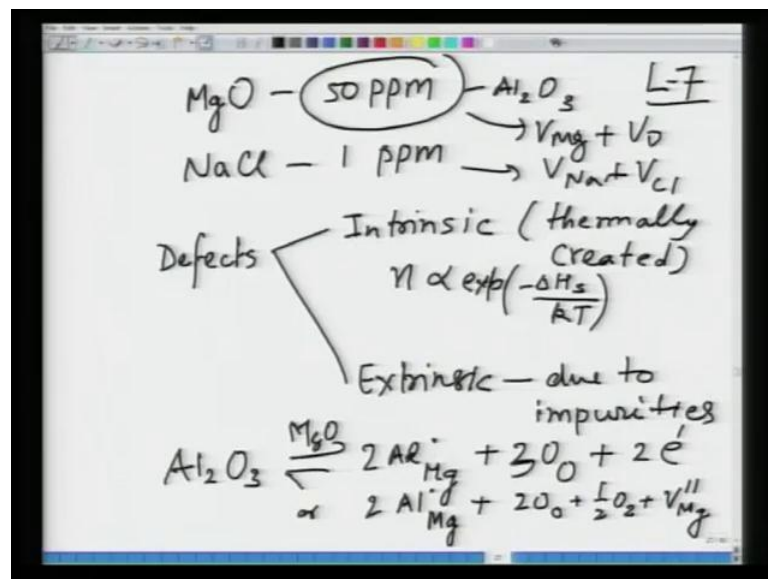


Electroceramics
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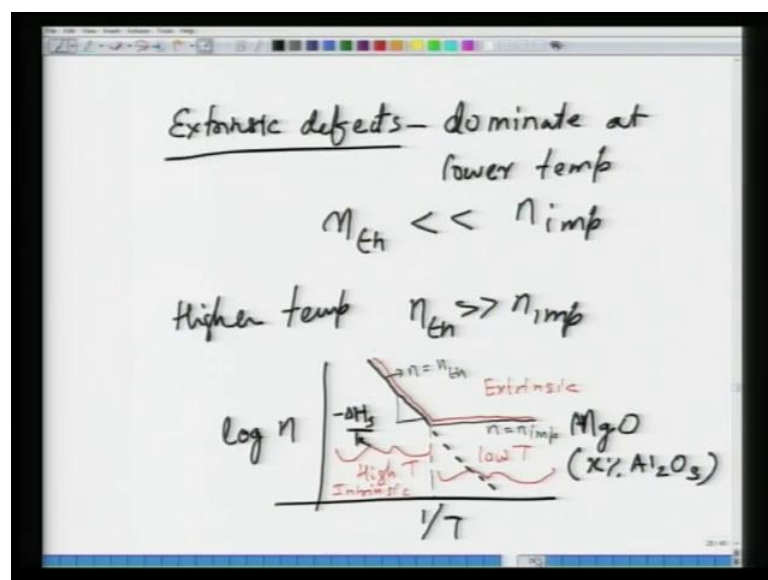
Lecture - 8

So, welcome to this new class. So, we will just review the last class in which we discussed first the intrinsic, extrinsic defects.

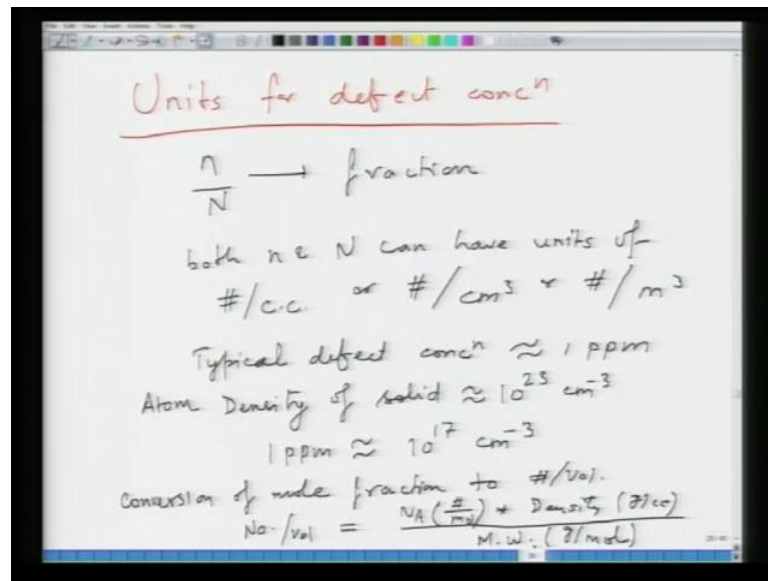
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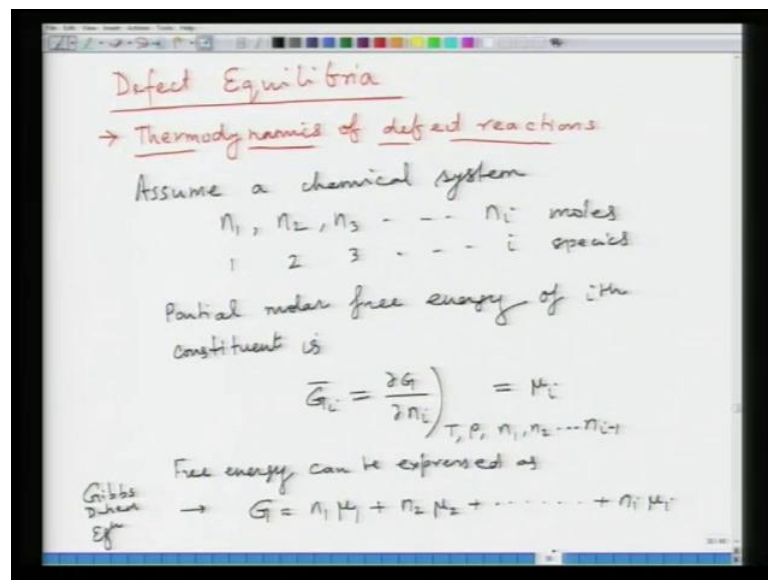


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The temperature dependence and then we looked at what are the possible units for defect concentration.

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And then we moved on to a important topic of defect equilibria, which is basically the purpose of this, showing this was to basically establish the criteria that we can treat these defect reactions just like chemical reactions. So, the thermodynamics or defect reactions can be treated in a similar way as thermodynamics of a chemical reaction, in dilute solutions. So, let us say you have a chemical system with various number of species with

their respective moles, and then we worked out what was that Gibbs Duhem equation; following that we could work out what was the, we could work out that the K , which is the reaction constant, which is nothing but ratio of product of products, product concentrations divided by ratio or activities divided by product of concentrations of reactants.

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For an open system

$$dG_{T,P} = \mu_1 dn_1 + \mu_2 dn_2 + \dots + \mu_i dn_i$$

$$\sum_i \mu_i dn_i = \mu_1 dn_1 + \mu_2 dn_2 + \dots + \mu_i dn_i = dG_{T,P}$$

Assume a chemical reaction as following

$$aA + bB \rightleftharpoons cC + dD$$

$$\Delta G = (c\mu_C + d\mu_D) - (a\mu_A + b\mu_B)$$

At equilibrium

$$\Delta G = 0$$

$$\mu_i = \mu_i^\circ + RT \ln a_i \rightarrow \text{activity of } i$$

$$a_i = \gamma_i \cdot n_i$$

for an ideal solution $\gamma_i = 1$

$$a_i = n_i$$

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$\Delta G = \Delta G^\circ + RT \ln K$

$$K = \left(\frac{a_C^c \cdot a_D^d}{a_A^a \cdot a_B^b} \right) \text{ equilibrium constant}$$

$$= \frac{n_C^c \cdot n_D^d}{n_A^a \cdot n_B^b}$$

$$\Delta G = \Delta G^\circ + RT \ln \left(\frac{n_C^c \cdot n_D^d}{n_A^a \cdot n_B^b} \right)$$

$\Delta G^\circ = -RT \ln K$ as $\Delta G = 0$

$$\Delta G^\circ = (c\mu_C^\circ + d\mu_D^\circ) - (a\mu_A^\circ + b\mu_B^\circ)$$

Further

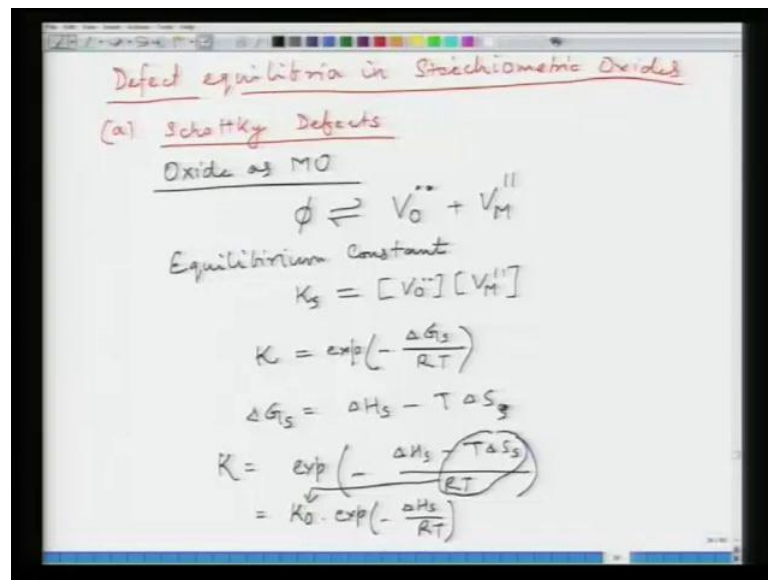
$$\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ = -RT \ln K$$

$$K = K_0 \exp\left(-\frac{\Delta H^\circ}{RT}\right) \quad K_0 = \frac{\Delta S^\circ}{R}$$

Now so, this is K but, we also saw that K is also equal to k is also equal to k naught exponential minus H naught by kT or RT which explains the temperature dependence

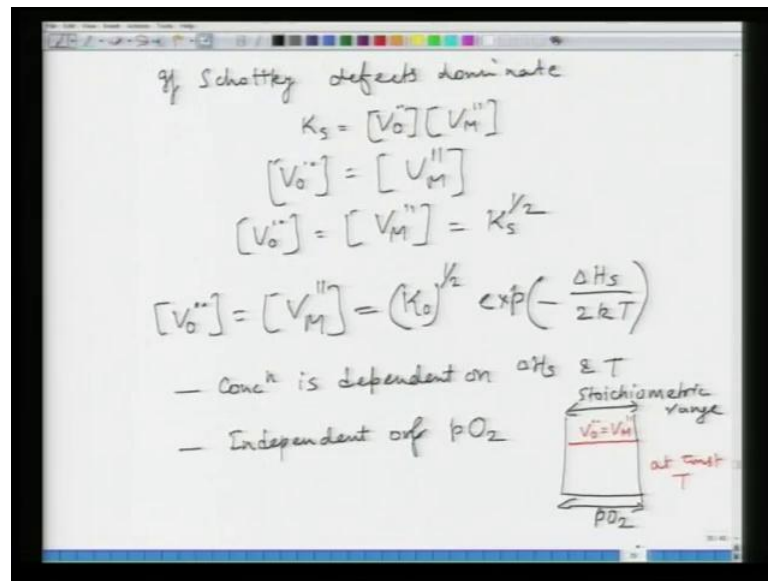
of k . So, this helps us in establishing the relations later on and we want to make a defect so, so you can see the defect concentration now, not only will depend upon the temperature and now, we will establish that it also depends upon things like oxygen partial pressure.

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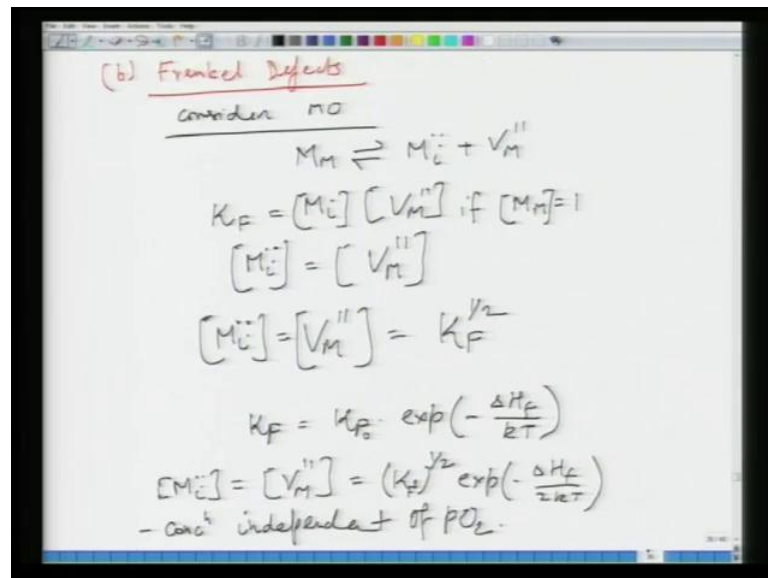
So, then we look at the defect equilibria and stoichiometric oxides considering defect reactions like chemical reactions, where we assume that defects are very small in numbers hence these can be considered as solute in a solvent or dilute solution, solid can be considered as a dilute solution, where solvent is the host lattice and solute is the defect. So, first we took the case of Schottky defects and considered an example of MO and in that we worked out the reaction constant and we find that there is no temperature dependence of concentration in case of Schottky defects and concentration is purely dependent upon temperature and magnitude of ΔH_S .

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So, and this typically happens at intermediate partial pressures for oxygen and in these ranges your V O is equal to V M.

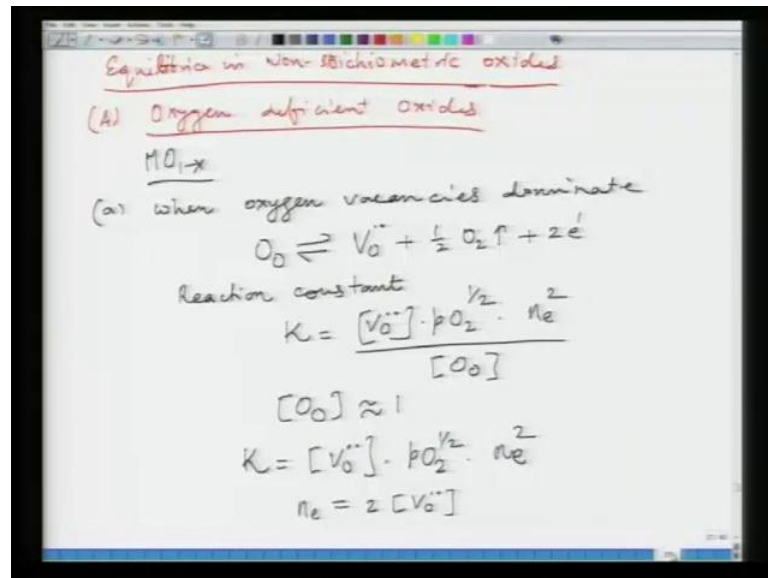
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So, similarly, at the same was true for Frenkel defects as well, again the concentration is independent of partial pressure of oxygen and it is dependent upon temperature and defect formation energy. So, both the formalisms are similar with the conclusion that in case of Schottky in case of stoichiometric solids the defect concentration does not depend upon the partial pressure of oxygen, it only depends upon the temperature

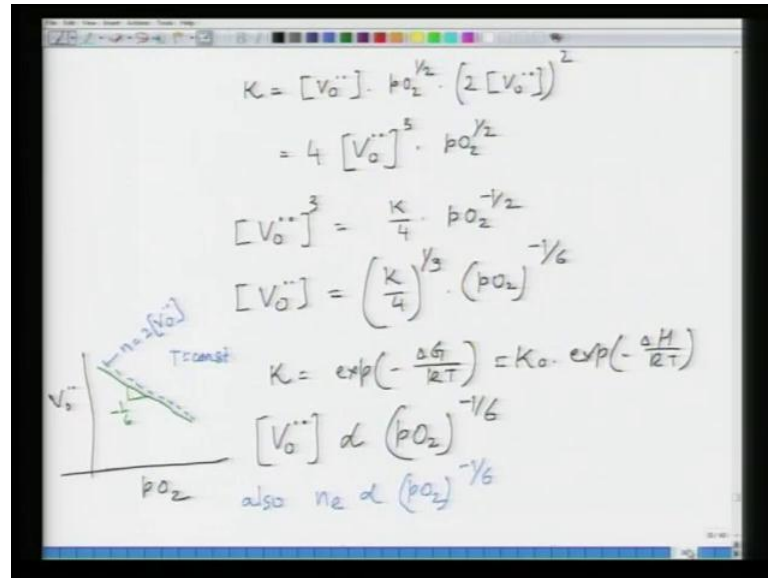
because and then we looked at what is the equilibrium in equilibrium concentration in non-stoichiometric solids.

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So, first we considered the case of oxygen deficient oxides. Example of let us say taking example of MO_{1-x} so, some oxygen is missing from the host lattice, those sites are empty. So, when oxygen so first case we took was when oxygen vacancies dominate in such a situation your the defect reaction can be written as like this and so O_O gives rise to $V_O^{..}$ plus half O_2 plus 2 electrons and then we worked out that using the charge neutrality condition n_e is equal to $2[V_O^{..}]$ and we can also write the defect we can also write the reaction constant which has dependence not only on concentrations and also on partial pressure of oxygen.

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Handwritten mathematical derivations and a graph on a whiteboard:

$$K = [V_{O^{\bullet\bullet}}] \cdot p_{O_2}^{1/2} \cdot (2[V_{O^{\bullet\bullet}}])^2$$

$$= 4 [V_{O^{\bullet\bullet}}]^3 \cdot p_{O_2}^{1/2}$$

$$[V_{O^{\bullet\bullet}}]^3 = \frac{K}{4} \cdot p_{O_2}^{-1/2}$$

$$[V_{O^{\bullet\bullet}}] = \left(\frac{K}{4}\right)^{1/3} \cdot (p_{O_2})^{-1/6}$$

Graph showing $V_{O^{\bullet\bullet}}$ vs p_{O_2} with a slope of $-\frac{1}{6}$. A dashed line labeled $n_e = 2[V_{O^{\bullet\bullet}}]$ is also shown.

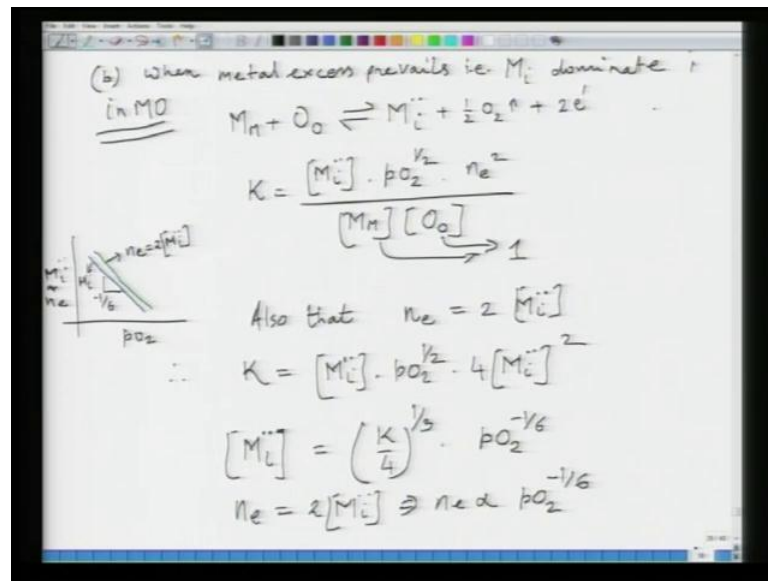
$$K = \exp\left(-\frac{\Delta G}{RT}\right) = K_0 \cdot \exp\left(-\frac{\Delta H}{RT}\right)$$

$$[V_{O^{\bullet\bullet}}] \propto (p_{O_2})^{-1/6}$$

also $n_e \propto (p_{O_2})^{-1/6}$

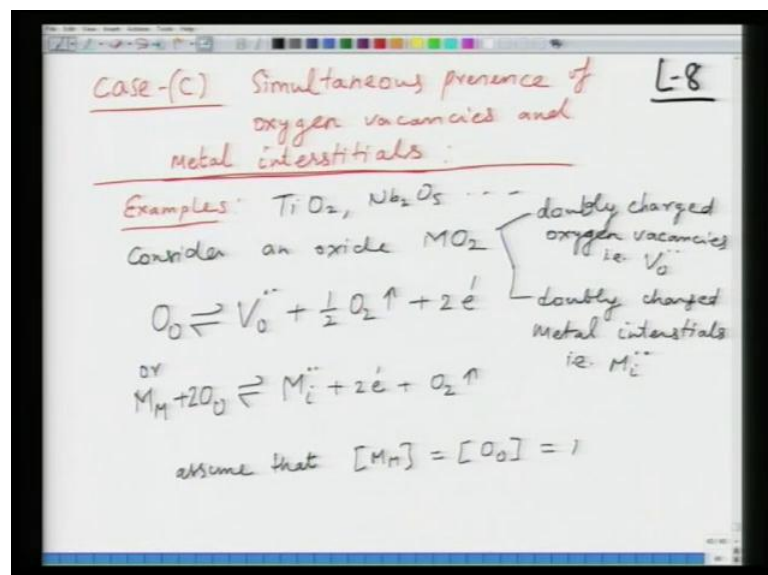
And if we just interchange various equations what we work out is the concentration of defects or electrons is proportional to p_{O_2} to the power minus 1 by 6. Temperature dependence is of course, given by K now, at a fixed temperature what it means is that so, not only the concentration will depend upon K that is temperature as exponential minus 1 by 2 to the power 2 to the power 1 by 3, it will also depend upon partial pressure of oxygen to the power minus 1 by 6 so, if you plot these so $V_{O^{\bullet\bullet}}$ is plotted as a line with slope of minus 1 by 6, we know from n_e charge equality that n_e is equal to twice of $V_{O^{\bullet\bullet}}$. So, n_e line would lie just on top of this $V_{O^{\bullet\bullet}}$ line and that will be 2 of $V_{O^{\bullet\bullet}}$ and then we did the similar analysis for conditions when metal excess prevails for an oxygen deficient solid in such a condition your M_i is dominant.

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And again you can write the equation for k and again you can see that n_e is proportional to $p_{O_2}^{-1/6}$ and $[M_i^{..}]$ is also proportional to $p_{O_2}^{-1/6}$. And again you can plot the charge concentration, if defect concentration as a function of partial pressure of oxygen so, we were here now now the next case that we will take is in this lecture.

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The next case now we will take is, case three or c I do not know what we used let us see if we used in the previous slide c so I will just rub three case c okay. So, in in this case we will take simultaneous presence of now so, far we have considered that only one kind

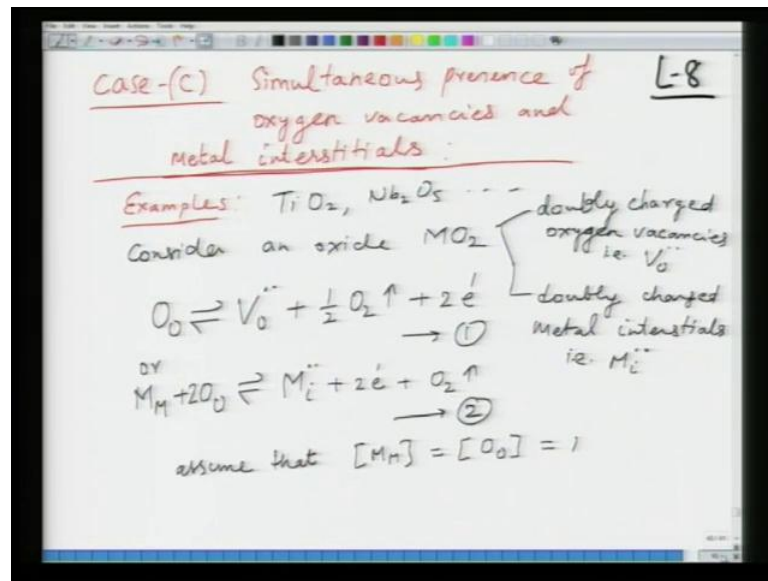
of defect can be present at a time now in this case you will consider simultaneous presence of 2 defects, which is oxygen vacancies and metal interstitials. So, this is the again for oxygen deficient solid now, examples of such a scenario this is a very practical scenario so, examples of such a such scenario is oxides like the TiO_2 or Nb_2O_5 so all these oxide shown not only oxygen vacancies but, also metal interstitials and this is simply because metal ions tends to be smaller titanium is a smaller cation so, as a result it tends to go to vacant interstitial sites.

Now so, we will take an example of so consider an oxide let us say MO_2 and this oxide has doubly charged oxygen vacancies, that is $\text{V}_\text{O}^{\bullet\bullet}$ and it has doubly charged metal interstitials, that is $\text{M}_\text{i}^{\bullet\bullet}$. So, we have not taken completely charged metal interstitials for a convenience and I will explain you what the convenience would be, because if you take this $\text{M}_\text{i}^{4\bullet}$ then you may not appreciate the exercise that we are going to do.

So, so this is the situation so for the first scenario when you have so, what is the defect reaction for the formation of these vacancies. So, oxygen at oxygen side goes out giving rise to 2 vacancies plus half of oxygen going out and as a result you create 2 electrons so, this is the reaction for oxygen going out or other reaction in case of metal interstitials would be $\text{M} + 2\text{O} \rightarrow \text{MO}_2$ because it is MO_2 . So, you have M_i metal going to interstitial side. oh sorry I just take so, it is not completely ionised I will only take 2 electrons so, compensating that you will have 2 electrons and both the oxygens go out so, that maintains the side balance so this is the situation.

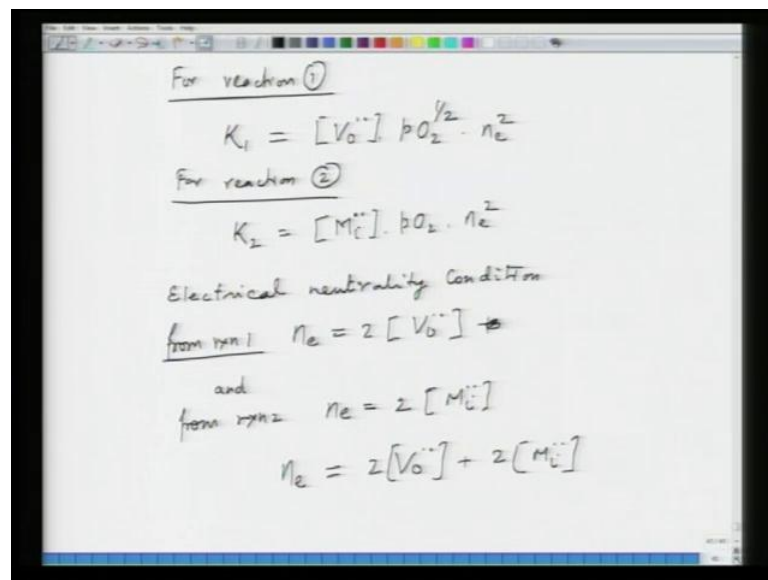
Now, let us say that defects are a smaller in number as compared to host lattice, assume we can assume that M_i is equal to V_O is equal to 1, assuming that it is a dilute solution. So, now we can write the defect reactions for we can write the reaction constant and now reaction constant assuming that M_i and O were equal to 1. k_1 for the first reaction would be so, I can write this as $k_1 \text{V}_\text{O}$. Let us say, just to avoid the confusion I will just let us go to previous slide.

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So, this is let us this is this is let us say reaction one and this is reaction two. So that makes it better.

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So, for reaction one we can write k_1 and k_1 will be equal to V_O multiplied by $p_{O_2}^{1/2}$ multiplied by n_e^2 and for reaction two you will have k_2 which is equal to M_i multiplied by p_{O_2} multiplied by n_e^2 . So, these are two expressions that we get. Now, what is the electrical neutrality condition? That says that end of reaction one number of electrons n_e is equal to 2 of V_O and for the second case so, this

will total basically and for the second case so, from this is from reaction one and from reaction two n_e is equal to $2 M_i$, right. So, if both for simultaneously present then n_e would be equal to $2 V_O$ plus $2 M_i$ so, the concentration of n_e would depend upon the total concentration of these 2 so, let us say we take two limiting cases.

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Limiting case-I $[V_O^{**}] \gg [M_i^{**}]$
 $n_e \approx 2[V_O^{**}]$
 $[V_O^{**}] = \frac{1}{2} n_e = \left(\frac{K_1}{4}\right)^{1/3} (p_{O_2})^{-1/6}$
 from reaction (2)'s ~~rate~~ equilibrium constant
 $K_2 = [M_i^{**}] \cdot n_e^2 \cdot p_{O_2}$
 replace $n_e = 2[V_O^{**}]$
 $K_2 = [M_i^{**}] \cdot 4 \cdot \left(\frac{K_1}{4}\right)^{2/3} (p_{O_2})^{-2/3} \cdot p_{O_2}$
 $[M_i^{**}] = \frac{K_2}{4} \cdot \frac{4^{2/3}}{K_1^{2/3}} p_{O_2}^{-2/3}$
 $= \frac{K_2}{(2K_1)^{2/3}} p_{O_2}^{-2/3}$

Limiting limiting case one now, this limiting case one is so you can have both V_O and M_i in various proportions so, we are taking two extreme conditions one condition is when V_O is large in quantity another condition is when M_i is in is in large quantity so, we will take first case which is V_O is much larger as compared to M_i in concentration. So, if that is the case then we of course, the reaction one would be more appropriate reaction so, that gives us the concentration of V_O is equal to half n_e is equal to because from the electrical inequality condition in that in such a situation n_e will be equal to $2 V_O$ so, V_O will be half n_e which will be equal to your k_1 you can work out from that is expression k_1 to the power $1/3$ to the in multiplied by p_O to the power minus $1/6$.

So, you just go to previous expression so, this is what you have k_1 is equal to $V_O p_O$ to the power half n_e square, you replace the expression for n_e which is equal to $2 V_O$ so, it will become $4 V_O$ square so, if you take $p_O p_O^2$ on the left hand side and just invert the equation then then it will become V_O cube is equal to k_1 by 4 multiplied by p_O to the power minus $1/2$ and then you just so, V_O cube was equal to that. So, when

when you want to take for V_O the right hand side will become to the power $1/3$ so, this is the expression for V_O you get here. Okay.

Now, what will be the concentration of now, let we are saying that V_O is very large in number, but still what is the concentration of M_i so, M_i concentration will still be given by reaction two, but in that reaction now, n_e is governed by concentration of V_O so, n_e is no longer a function of M_i . So, from reaction two we know from reaction two's rate constant or reaction constant or equilibrium constant, we know that k_2 was equal to M_i into n_e square multiplied by p_{O_2} so, here this. So, you replace n_e is equal to $2 V_O$ because in this condition n_e is not dependant upon M_i it is only depended upon V_O because V_O is much larger than M_i now, k_2 will become M_i dot dot multiplied by what is n_e n_e square so, it will become 4 into k_1 to the power $2/3$ into p_{O_2} to the power minus $2/6$ into p_{O_2} .

Now, all you have to do is that you have to rearrange so, M_i will become k_2 divided by 4 into so, this will become $1/3$ so, this will be p_{O_2} the power $2/3$ which on the other side if it goes it will become p_{O_2} to the power minus $2/3$ and this so, k_2 k_2 k_2 divided by 4 and then this becomes 4 to the power $2/3$ divided by k_1 to the power $2/3$. So, I have just taken everything on the other side and later next question for M_i M_i dot dot, which will reduce to k_2 divided by $2 k_1$ to the power $2/3$ so, this is basically 4 to the power $1/3$ so, 4 to the power 1 minus 4 to the power will be 4 to the power $2/2$ will be equal to 2 to the power $2/3$.

So, so k_2 and k_1 so, M_i so in this regime when V_O is much larger than M_i then V_O is equal to k_1 by 4 to the power $1/3$ into p to the power minus $1/6$ so, V_O varies $\log V_O$ varies as with the slope with respect to p_{O_2} with the slope of minus $1/6$ on the other hand M_i varies with the slope of minus $2/3$ and what is the boundary condition? The the condition beyond which this is valid so, we are saying that if you want to determine that partial pressure of oxygen beyond which this is valid in that case we are saying that since V_O is greater than M_i so, what is V_O ? V_O is k_1 by 4 to the power $1/3$ into p_{O_2} to the power minus $1/6$ is greater than k_2 divided by $2 k_1$ to the power $2/3$ multiplied by p_{O_2} to the power minus $2/3$.

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since $[VO] \gg [Mn]$

$$\left(\frac{K_1}{4}\right)^{1/3} \cdot pO_2^{-1/6} \gg \frac{K_2}{(4K_1)^{1/3}} \cdot pO_2^{-2/3}$$

$$\Rightarrow pO_2 \gg \left(\frac{K_2}{K_1}\right)^2$$

Case - II - when $[Mn] \gg [VO]$

$$K_2 = [Mn] \cdot n_e^2 \cdot pO_2 \quad \text{and} \quad n_e = 2[Mn]$$

$$[Mn] = \frac{1}{2} n_e = \left(\frac{K_2}{4}\right)^{1/3} \cdot pO_2^{-1/3}$$

for calculating $[VO]$,

$$K_1 = [VO] \cdot n_e^2 \cdot pO_2^{1/2}$$

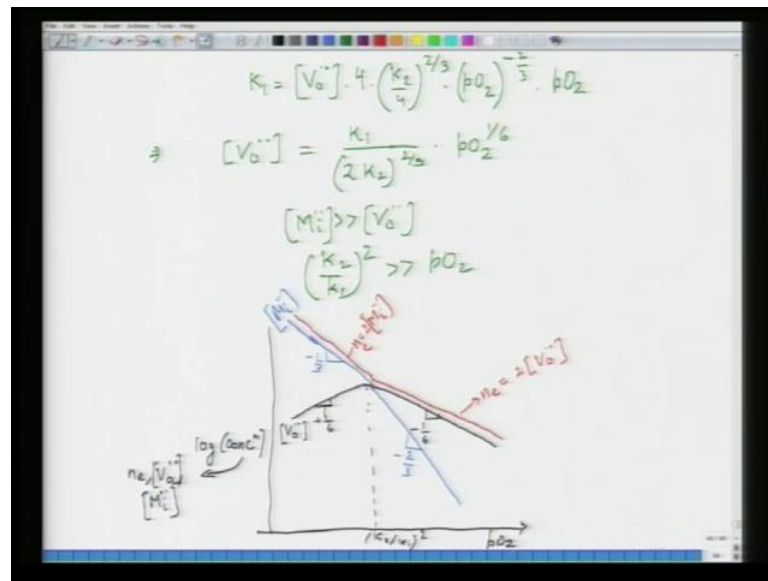
$$\rightarrow n_e = 2[Mn]$$

So, this is the condition that we establish and so, if we now rearrange this what you will find is that pO_2 is greater than K_2 divided by K_1 square so, this is the pressure beyond which this condition will satisfy. So, this was case one, limiting case one when VO is greater than Mn second case we will take is when Mn is greater than VO so, we have to determine this condition so, naturally this condition will prevail under this so pO_2 has to be lesser than K_2 by K_1 square. You can verify that using again this equality when you calculate the concentration.

So, now we know from so, first we will calculate what is Mn now so, from reaction two we know K_2 was equal to Mn multiplied by n_e square into pO_2 so, Mn now will be equal to and under such a condition n_e will be equal to 2 of Mn because it is much more larger than VO so, Mn under such a condition will be equal to half of n_e 3. This now you can do, I am not going to do the whole exercise so, you all you need to do is, that you need to put this expression here and just rework the parameters on either side to work out an expression for Mn in terms of pO_2 .

So, this is one expression and now for calculating VO we know that K_1 was equal to VO into n_e square multiplied by pO_2 to the power half and now, this n_e now is equal to 2 of Mn so, we will just move to next slide.

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So, we know that k_1 is equal to $V O$ into $n e$ $n e$ square so, $n e$ square will be $4 M i$ square and $M i$ square will be k_2 divided by 4 to the power 2 by 3 multiply by $p O$ multiplied by $p O$ to the power minus 2 by 3 multiplied by if you go to previous expression previous page k_1 was $V O$ we have replaced $n i n e$ with two $M i$ and $M i$ is equal to this. So, we have just replaced this so k_2 by 4 to the power 2 by 3 into $p O$ to the power minus 2 by 3 multiplied by 4 multiplied by $p O^2$ now, if you work out the expression in for $V O$ in terms of $p O^2$ what you will find is $V O$ is equal to k_1 divided by $2 k_2$ to the power 2 by 3 into $p O^2$ the power 1 by 6 .

So, we can see here that in this regime i , $m i$ has a pressure dependence of minus 1 by 3 to the $p O$ to the power minus 1 by 3 and $v o$ has a dependence of $p O$ to the power 1 by 6 . So, again now you can calculate the boundary so, we know that since $M i$ is larger than $V O$ I am just putting the value of $V i$ and $M i$ and $V O$ and what you will find is k_2 by k_1 square is greater than $p O^2$ which is nothing but you worked out from the previous expression now, you can so here you can see that $v o$ increases as the partial pressure of oxygen decreases and but at different rate as compared to previous exercise sorry $V O$ increases as you increase the partial pressure of oxygen up to certain point and then it decreases when $V O$ is much larger.

So, we will just now plot this so, this is log of any kind of concentration so, which means concentration will mean your $n e V O$ and $M i$ and this will be your $p O^2$. So, the

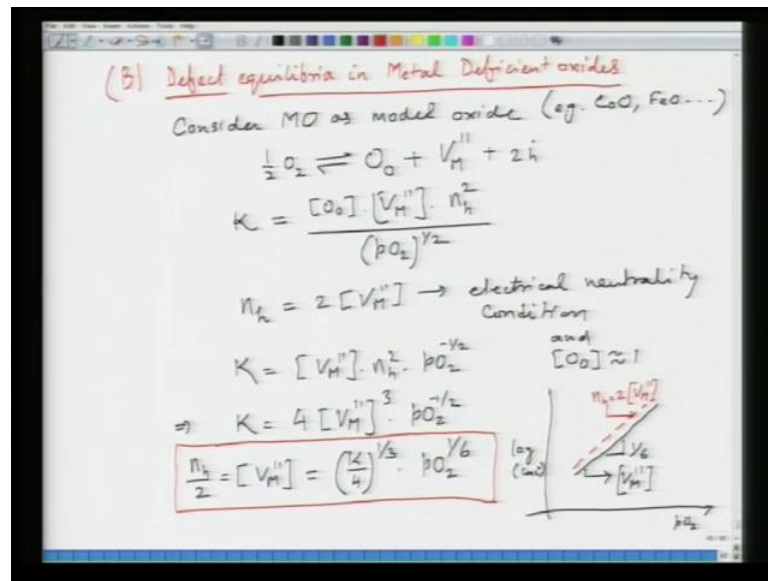
boundary we get it is at so, let us say we start at a arbitrary point and this boundary is equal to k_2 by k_1 square. Now, what we see is that p_{O_2} larger than k_2 by k_1 is when k_2 when k_2 by k_1 square is larger than p_{O_2} which means the smaller p_{O_2} 's in that case what we have is our V_O varies as this so, this will be plus 1 by 6 for V_O and how does V_O varies how does the V_O vary after when p_{O_2} is larger, in that case it varies as like this. So, this will be minus 1 by 6 this is the V_O line now how does let us say blue line now, how does M_i vary? M_i in this region if you go to previous slide it varies as minus 1 by 3 if you go to previous slide it varies as minus 2 by 3.

So, now we just take it so it it varies at minus 2 by 3 here and and this region it varies at minus 1 by 3. So, this will be your M_i and n is nothing but if you want to plot n so, n is nothing but in this region 2 of M_i and in this region it is 2 of V_O . So, up to this point n is equal to 2 of M_i and in this region it is equal to n is equal to 2 of V_O . So, this is kind of an equilibrium diagram where you get a boundary the the transition point and the conditions away from the boundaries in both the directions. In one condition your M_i is a dominating defect in another condition your V_O is the dominating defect and in between both of them exist together.

So, basically what it means is that you start drawing the lines from the far of regions and then let them meet at the at the juncture junction which is nothing but p_{O_2} is equal to k_2 by k_1 square. So, I hope this gives you an idea about how to establish these various equilibrium conditions, you can take single defect situation, you can take multi defect situation and see how they co-exist under various conditions of partial pressures of oxygen.

So, next we will take into account what is the scenario in case of metal deficient oxide. So, far we have considered scenarios of defect we have worked out the defect equilibria only for a stoichiometric only for oxygen deficient oxides and stoichiometric oxides now what is remaining is metal deficient oxides and we will do it very briefly because now, that you understand the fundamentals of how to work out defect equilibria in case of oxygen deficient oxide the approach is similar in case of metal deficient oxide. So, we will only take one case in such a such condition. So, here now let us see how we were we had the numbering so, this is case c so A capital A so, we will take capital B here.

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And we will take defect equilibria in metal deficient oxides. So, again consider for example, M O as model oxide all right. So, as now assuming complete ionization of vacancies for the formation of metal vacancies what you write is half O 2 now, this will happen in for example, example our C O O, F e o etc. So, you write half O 2 is equal to O O so, oxygen has gone to oxygen site in order to maintain the side balance you need to create a metal side.

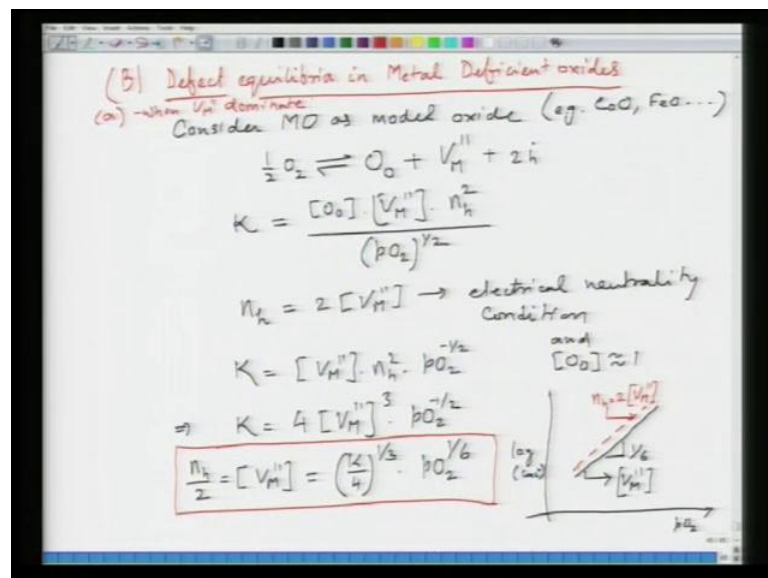
However, there is since it is metal deficient that will be metal vacancy and that would be doubly charged and that would be compensated by creation of 2 holes and the equilibrium constant for this will be k to be equal to O O multiplied by V M double dash multiplied by n p n H square divided by p O to the power half. Now, we know that from electrical neutrality condition n H is equal to 2 of V M so, as a result your k will become and and also assume that and O O is equal to 1 because it is very large in number.

So, as compared to defect concentration so, it becomes k becomes V M double dash multiplied by n H square multiplied by p O 2 and so, now what you can do is that k in such a situation will be n H if you replace by 4 V M cube multiplied by p O 2 sorry p O to the power minus half minus half so, V M double dash. So, just see there was a mistake here it should be so, if it goes there now it will become k by 4 to the power 1 by 3 into p O to the power 1 by 6 so, this is the expression for V M and this is also equal to since n H is equal to 2 V so, this is n H by 2 so, this is the expression for pressure dependence

for whole concentration. So, if you just draw a plot here, plot would be something like this so, you have log of concentration and this pO_2 , so this is your oops sorry it is positive slope so, if this is your V M line then your whole line will be right on top of this V M so, this is how it will vary the scales are arbitrary we will see they are relative to what is beyond or what is after.

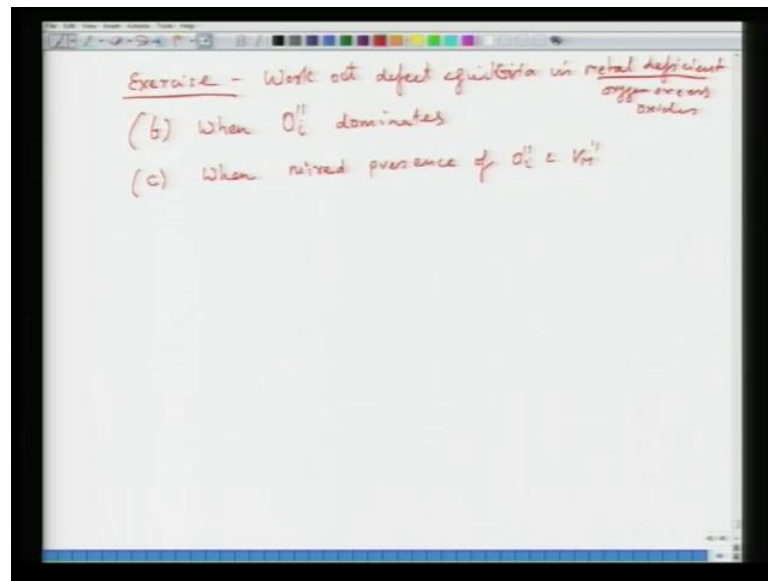
So, what is before, what is after. So, we will see that so, this is the case in case of metal deficient oxides when when metal vacancies are dominating defects you can do the similar exercise for conditions when so I will just leave it to you.

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For example, I will just mention the condition here condition a when V M dominate and I will leave it to you as an exercise, solve it do the defect equilibria calculation for condition 2 when O i dominate and condition c when mixed presence of O i and V M.

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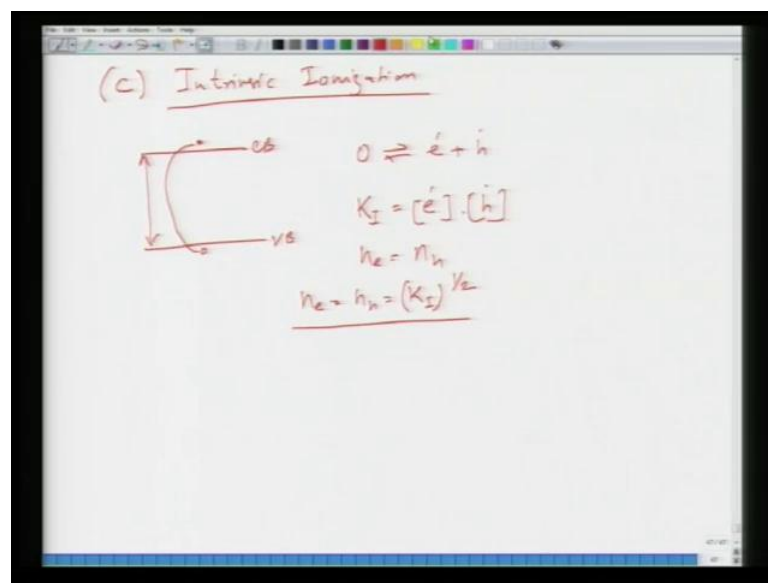


So, the analysis is very similar to what we have done in a previous case for oxygen deficient oxides and this would be similar in case here as well. Now, if you remember in the in the case of if you remember in the case of, yes in this case we choose an oxide MO_2 with when we took simultaneous presence of oxygen vacancies and metal interstitials, we took an oxide MO_2 that was for an purpose. What happens is that in these materials if you had M^{4+} completely ionised which means M^{4+} 4 dots present or if you had taken an oxide MO which is completely ionised defects then you would not see this transition as a result when you make the measurements conduct now these as we will see later on these are all all these plots which I am plotting at the moment they can be obtained by making conductivity measurements as a function of pressure oxygen partial pressure so, when you when you make those conductivity measurements you are not able to ascertain, you you would not be able to get this sort of those sorts of differentiation which you get in these cases.

So, this kind of analysis is applicable in cases where it is very explicit that how what kind of defects are present at what kind of oxygen partial pressures. So, just looking from the analysis or the derivation point of view, it is easy to derive it for cases like these where such as in MO_2 you have M^{4+} dot dot etc, but it does not work the approach similar approach does not work for for instance you want to do for MO , where both the defects are completely ionised or even for MO_2 when where both the defects are completely ionised.

So, one has to be careful, if you if you want to go into details of this you can go you can go through the book of per Kofstad which is known as stoichiometry in oxides which I have listed in the bibliography so, but this is a very useful approach you can see where you can find out the differentiation and where you cannot, so that you can work out yourself by taking various examples of various oxides. So, now so this is as a exercise I left it to you so basically work out defect equilibria in metal deficient slash oxygen excess oxides in under following conditions.

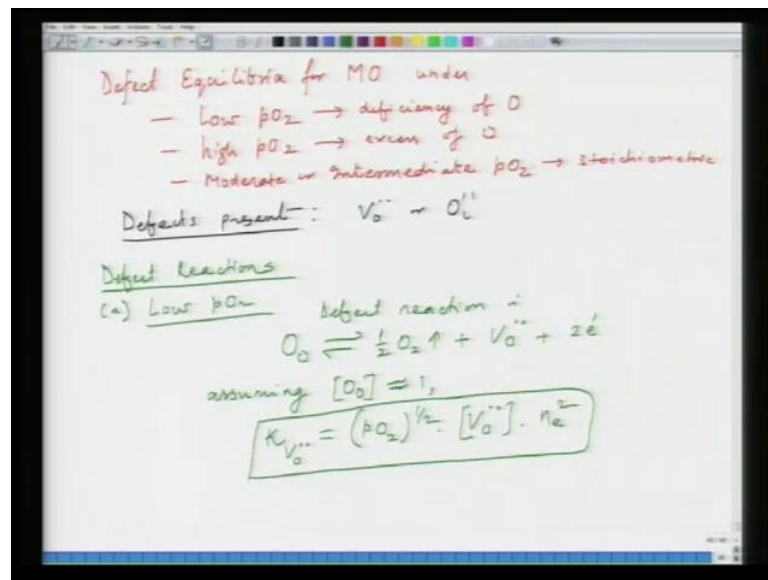
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Now, the third case in this series would be intrinsic ionisation. An intrinsic ionisation as we have seen it has nothing but formation of electrons and holes. So, basically you have this band gap of the material n e oxide so, the electrons from valence band so, this is your valence band this is your conduction band. So, electrons from here jump to valence band gives rise to electron in the conduction band and hole in the valence band so this leads to formation of electron hole pair and the reaction would be null electron and hole and equilibrium constant for this would be e dot h and since n e is equal to n h, n e is equal to n h will be equal to k I to the power half. So, you can see in such a condition when this happens at moderate rate partial partial pressures of oxygen under such conditions you can see that n e or n h is only dependent upon k I which is temperature dependence as you know and it is independent of partial pressure of oxygen.

So, now what we will do is that so far what we have seen is that we have seen oxides of specific kind. We have considered cases of metal deficient, we have considered the cases of oxygen deficient, we have considered the cases of stoichiometric conditions, typically as you can intuitively think that metal deficiency or oxygen excess would tend to occur at higher oxygen pressures. Oxygen deficiency would tend to occur at lower oxygen pressures and intermediate oxygen pressures would determine the stoichiometric condition. Now, what we will do is that we will consider one particular oxide and we will look at the defect equilibria for this particular oxide under three conditions of oxygen partial pressure.

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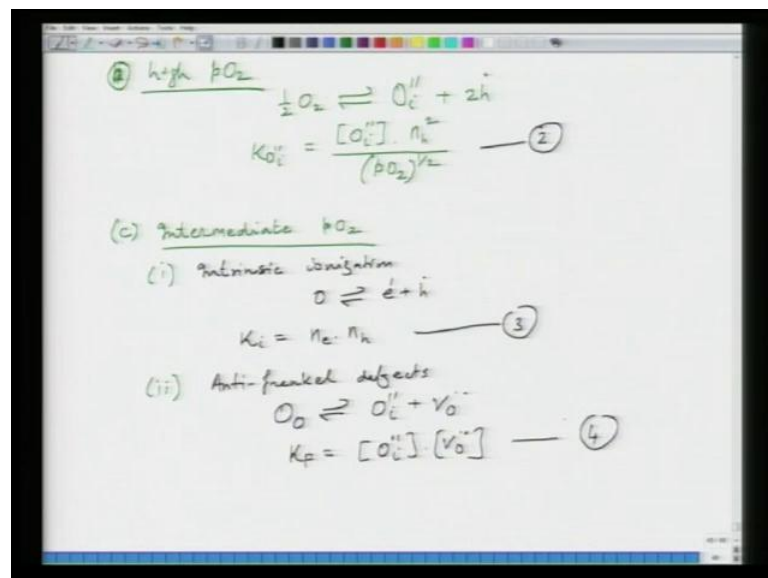


So, the so basically so, we will consider defect equilibria for an oxide M O for M O under number 1 low p_{O_2} number 2 high p_{O_2} , number 3 moderate or intermediate p_{O_2} which is typically in most cases atmospheric pressure intermediate p_{O_2} . So, this condition would typically determine deficiency of oxygen, this condition would typically determine excess of oxygen and this condition would typically determine stoichiometric condition. Now, deficiency of oxygen will also mean excess of metal and excess of oxygen will also mean automatically not automatically but it would be metal vacancy. So, assume that the defects which are presents are either oxygen vacancies or oxygen interstitials and let us say both are doubly charged completely ionised.

So, let us say what are the defect reactions first. So, first we will see just change the colour so, defect reactions so first we will write for low p_{O_2} case so at low p_{O_2} , I am not considering M so if this was V O then you would have complementary defect M i or you can have V M so, we are just considering oxygen at the moment you can consider others as well but let us not complicate let us just simplify otherwise it becomes little complicated so just to simplify, we have chosen only one kind of dominating defect in one region. So, at low p_{O_2} the defect reaction would be $O \rightleftharpoons O_i + 2e^-$ which means oxygen present in the lattice going out giving rise to oxygen vacancy plus two extra electrons.

Now, assuming $O \rightleftharpoons O_i + 2e^-$ was equal to 1 almost equal to 1 and so this would be so, we can write K for this reaction. So, let us say this is K_{O_i} so K_{O_i} would be p_{O_2} to the power half multiplied by $[O_i]$ multiplied by n_e square, I am not writing it in terms of n_e , I am just writing the whole without replacing for n_e so, this is the first expression that you get.

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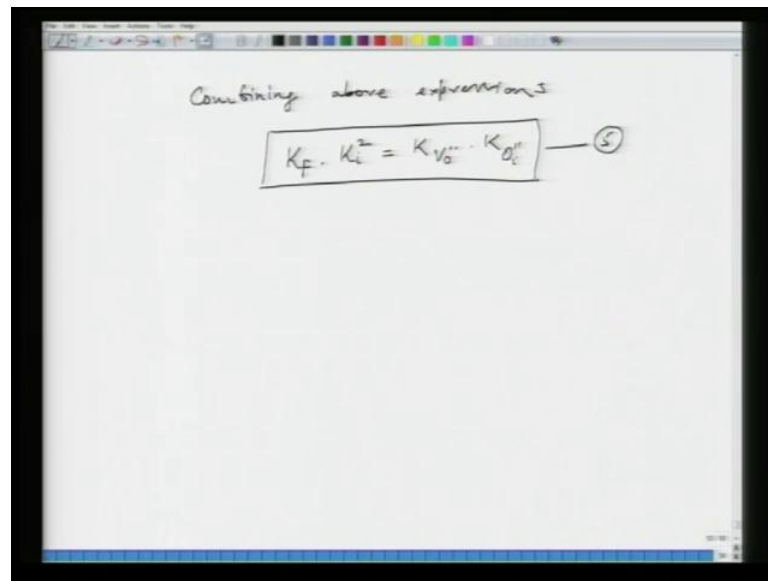
Now, the second expression we will write at at high p_{O_2} so, at high p_{O_2} the defect reaction is $\frac{1}{2} O_2 \rightleftharpoons O_i + 2h$ and as a result the reaction constant you can work out as K_{O_i} to be equal to $[O_i] \cdot n_h^2$ divided by p_{O_2} to the power half and third condition is oops change the order here a this should be b this should be c intermediate, what am I writing then I get p_{O_2} so under intermediate p_{O_2} there are two possible scenarios. Under intermediate scenario is so

number first number 1 is intrinsic ionization, given the two creation of electrons and holes well reaction in this case would be $e + h$. So, under such a condition k_i would be equal to n_e multiplied by n_h and the second condition that is possible is, so either you can have intrinsic ionisation which dominates so, stoichiometric defects could be of electrons and holes or the stoichiometric defects could be Frenkel defect or anti Frenkel defects.

So, the reaction here would be O_O is equal to O_i plus V_O . So, basically what you can see here is the defects that we have considered at higher and lower p_{O_2} is they have to be in accordance with the defects that are going to be present at in stoichiometric conditions as well so, that you get a continuity in defect concentration as a function of partial pressure of oxygen. So, you can see that intuitively now, if you had chosen Schottky defects here Schottky defects would give rise to V_M and V_O so you would have continuity for a V_O but V_M would not have so, either you replace O_i here with the V_M so, if you had Schottky defects dominating in that intermediate pressure range in that case you would have to choose V_M in the higher pressure regime. So, you understand what the logic is? The logic is whatever defects you choose in the intermediate low and high pressure regions there has to be continuity in the defect concentration.

So, if you choose one particular kind of stoichiometric defect in stoichiometric region then that particular defect grows or reduces in the concentration at higher or lower pressures. So, that that makes sense and that also makes our life little easier so, for this reaction we can write k_F is equal to O_i multiplied by V_O and so from these 4 expressions for so this is let us say 1 just let us say it is 2 let us say it is 3 and this let us say is 4 so, if you combine these expressions combining above expressions gives us k_F multiplied by k_i square is equal to k_{V_O} multiplied by k_{O_i} just a second, show you some that is easy to verify. You can do that yourself, so this could be equation number 5.

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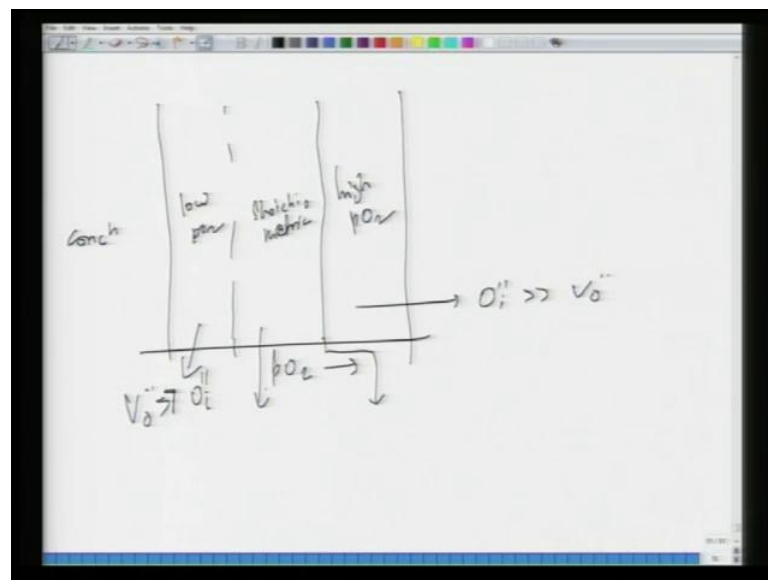


Combining above expressions

$$K_F \cdot K_i'' = K_{V_O''} \cdot K_{O_i''} \quad \text{--- (5)}$$

Now, what we will do is that we will work out the limiting conditions for each of these cases.

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Which means if we are making a plot for example of p_{O_2} versus concentration so, of course, this is the low pressure regime, this is the high pressure regime and this is the stoichiometric regime. So, we know that these are three regions but we do not know where the boundary occurs. So, we need to define the boundaries, where these

boundaries are? So, what basically it would mean is how we would define boundaries are this region would be a region when you have O_i lot greater than V_O .

In this region we will assume that V_O is a lot greater than O_i and in this region we would assume either intrinsic ionization or anti Frenkel defects. We will take both the cases which one each of domination of each of these and we will see how these concentrations then vary, as a function of partial pressure of oxygen and which defects dominate in which region. So, we will finish here we will take these limiting conditions in the next class followed by followed by we will, we will calculate the concentrations of defects in each of these regions based on these limiting conditions and then we will draw the plots of concentration of defects versus partial pressure of oxygen, which are also called as Brouwer's diagram, these are very important diagrams because at any given temperature you can see what the defect concentration versus partial pressures of oxygen is going to look like and these plots also replicate when you measure electrical conductivity versus temperature. You do not know the relation of electrical conductivity with respect of to to partial pressure of oxygen or concentration yet.

But as we will see later on that these plots are very useful to know because you get the similar plots by plotting d c conductivity versus partial pressure of oxygen as a at a given temperature. So, we will do this all this in next class and and then we will move on to next topics after this.

Thank you.