

Robotics and Control: Theory and Practice
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Lecture – 16
Manipulator Control

Hello viewers, this lecture is on Manipulator Control. So, in this lecture, we will see how to compute the control of your robot manipulator for performing a assigned task. So, in the previous lectures, we have seen how to derive the dynamics equation of a robot manipulator.

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Manipulator Control


Consider the dynamic equation of a n -link manipulator:


$$M(q, \dot{q})\ddot{q} + C(q, \dot{q}) + G(q) = \tau \dots \dots (1)$$

where

$$q(t) = \begin{bmatrix} q_1(t) \\ q_2(t) \\ \vdots \\ q_n(t) \end{bmatrix}, \quad \tau(t) = \begin{bmatrix} \tau_1(t) \\ \tau_2(t) \\ \vdots \\ \tau_n(t) \end{bmatrix}$$

$M_{n \times n}$ is the Inertia Matrix.
 $C_{n \times 1}$ is the centrifugal and Coriolis force vector.
 $G_{n \times 1}$ is the Gravity term.
 $\tau_{n \times 1}$ is the Force/Torque vector.

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So, we have seen that it is written in the form of a system of second order differential equations, like $M \ddot{q} + C \dot{q} + G = \tau$, where q is

the vector containing all the joint variables q_1, q_2, \dots, q_n . So, some of them may be revolute joint some of them may be prismatic.

So, if it is revolute joint q_i denotes the joint angle and if it is a prismatic joint then q_i denotes the linear motion of the joint. Similarly, τ denotes the torque at each joint τ_1, τ_2 up to τ_n . For revolute joint τ_i denotes the torque and for prismatic joint τ_i denotes the linear force applied at that joint.

So, here this $M(q) \ddot{q}$ denotes the inertia matrix and $C(q, \dot{q}) \dot{q}$ denotes the centrifugal and Coriolis force, G is the gravity term and τ denotes the force or torque vector applied at each joint. So, for each robot manipulator, we can derive such a system of differential equation representing, the equation of motion.

Now, the problem is to find the control, control is here the torque vector $\tau(t)$ for a particular task for an assigned task how to find the control torque.

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Manipulator Control

Let $q_d(t)$: $t \geq 0$ be the desired joint trajectory.

If $q(t)$ is the actual joint variable at time t then:

$$e(t) = q(t) - q_d(t)$$

is the error at time t .

To track the desired joint trajectory $q_d(t)$, it is necessary to find the control vector $\tau(t)$ (Force/Torque) such that the error:

$$e(t) \rightarrow 0 \text{ as } t \rightarrow \infty$$

The equation (1) is a system of n second order ODE. It can be converted into $2n$ first order ODE.

Let

$$\dot{q} = v$$

Then

$$\dot{v} = M^{-1}(q, v)[\tau - C(q, v) - G(q)]$$

So, let us assume that q_d denotes the desired joint trajectory. So, joint trajectory means the desired angles or the linear motion of each joint. So, the q of t the desired value is given by $q_d(t)$ and $q(t)$ denotes the actual joint variables. So, the current value of q is given by $q(t)$. So, the error between the current value and the desired value denotes the error at time t . So, it is a vector n dimensional vector. So, the aim is to find the control the torque vector, in such a way that the error converges to 0 as t tends to infinity.

So, in theoretically we say that error should tend to 0 as t tends to infinity, but in practice the error must tend to 0 as quickly as possible ah. So, that the desired trajectory is tracked. Now, we can convert the given system of second order equation into $2n$ first order differential equation.

So, each second order equation can be converted into 2, first order equation by substituting. So, if you define \dot{q} equal to v , then you can write \dot{v} equal to \ddot{q} and the \ddot{q} from this equation 1. If, you keep the \ddot{q} in 1 side and take all the remaining terms to the right hand side, we get \dot{v} is \ddot{q} which is equal to $M^{-1}(\tau - C(q, \dot{q}) - G(q))$.

So, it is the same equation written in 2 first order differential equation form. And, each one is a n equation because q is a vector containing n elements. So, here there are n equations and the second one there are n equations, totally there are $2n$ first order differential equations.

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Manipulator Control

Now we can write these equations in terms of e .

$$e = q - q_d$$

$$\dot{w} = \dot{e} = \dot{q} - \dot{q}_d = v - \dot{q}_d$$

So,



$$\begin{aligned} \dot{e} &= w \\ \dot{w} &= \ddot{q} - \ddot{q}_d \\ &= M^{-1}(e + q_d, w + \dot{q}_d)[\tau - C(e + q_d, w + \dot{q}_d) - G(e + q_d)] \\ &= \bar{M}^{-1}(e, w)[\tau - \bar{C}(e, w) - \bar{G}(e)] \end{aligned}$$

Choose the control $\tau(t)$ to be:

$$\tau(t) = \bar{C}(e, w) + \bar{G}(e) + \bar{M}(e, w)[-Ke - Lw]$$

$\ddot{q}_d(t)$

$\dot{w} = -Ke - Lw$



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Now, according to the notation introduced earlier e is q minus q_d and w , if you call is \dot{e} dot we can write the same equation in the error form. So, \dot{e} is equal to w we can give this notation and \dot{w} is nothing, but \ddot{e} . So, \ddot{e} is from here it is \ddot{q} double

$\ddot{q} - \ddot{q}_d$ or in other words it is $\dot{p} - \ddot{q}_d$. So, we can get \dot{w} is given by from the previous slide, we can write this one \dot{v} is given by this last line.

So, ultimately \dot{w} is given by this expression the $M^{-1}(\dot{e} + \dot{q}_d)$, because \dot{q} means $\dot{e} + \dot{q}_d$ from this equation and $w + \dot{q}_d$ from this equation. Similarly, C of this is \dot{q} and this is \dot{q} and G of q is substituted. Now, when we write the same equation only in terms of e and w we can give this particular notation, instead of writing $M^{-1}(\dot{e} + \dot{q}_d)$ etcetera we can write it in a shorter form as $\bar{M}(e, w)$, a function of e and w . And, similarly C of $\dot{e} + \dot{q}_d$ etcetera can be written in the shorter form as $\bar{C}(e, w)$ and this can be written as $\bar{G}(e)$.

So, the same dynamic equation is converted into a form in terms of the error vector e and its derivative \dot{w} in this way. Now, we have to compute the control, control τ for tracking their desired trajectory $q_d(t)$ is the desired joint trajectory we want to track.

So, we can define this torque or the control in this form, that is $\bar{C}(e, \dot{w}) + \bar{G}(e) + \bar{M}(e, \dot{w})$ multiplied by $-K_e - L_w$. How it is selected it is just the observing the equation, here we have $\tau - \bar{C} - \bar{G}$. So, if you take τ to be $\bar{C} + \bar{G}$ this 2 will get cancelled. So, the remaining term is simply \bar{M} into $-K_e - L_w$.

So, what we will get is if we substitute this particular τ we will get the equation to be the simple 1, the equation the second equation will become after substitution this \bar{M}^{-1} will get cancelled with \bar{M} , and the remaining will be simply \dot{w} will be $-K_e - L_w$. So, only this much we will get.

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Manipulator Control

Then the equation becomes:

$$\begin{aligned} \dot{e} &= w \\ \dot{w} &= -Ke - Lw \end{aligned}$$

For this system, the equilibrium point is $(0,0)$ and it is asymptotically stable.

Proof:

Let $e = e, w = w$

Then $V(e, w) = Ke^2 + w^2$

$$\begin{aligned} \dot{V} &= 2Ke\dot{e} + 2w\dot{w} \\ &= 2Kew + 2w(-Ke - Lw) \\ &= -2Lw^2 \end{aligned}$$

Handwritten notes:

- K and L are $n \times n$ positive definite matrices.
- $K = \begin{bmatrix} k_1 & 0 & \dots & 0 \\ 0 & k_2 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & k_n \end{bmatrix}$
- $L = \begin{bmatrix} l_1 & 0 & \dots & 0 \\ 0 & l_2 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & l_n \end{bmatrix}$

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So, what we get the error system to be \dot{e} is equal to w and \dot{w} is minus $K e$ minus $L w$, it is a very simple system of differential equation. And, we can easily verify that $(0,0)$ is the equilibrium point. If, we equate the right hand side to 0, we will get w equal to 0 and putting it in the second equation, we get e equal to 0. Here, K and L are positive definite matrices.

So, for example, we can take K to be $k_1 \ 0 \ 0$ and $0 \ k_2 \ 0 \ 0$ etcetera. Here n cross n diagonal matrix, where all the diagonal entries are positive numbers k_i is greater than 0, strictly greater than 0, if we take then it is a positive definite matrix a example of a positive definite matrix. So, it this will be very useful in this type of control problems. A positive definite matrix can be it is defined as a matrix whose all eigenvalues are positive.

So, it need not be always a diagonal matrix, but here we can select this K to be like this similarly L to be here, diagonal matrix with all positive diagonal entries. So, so by selecting

like this we can easily see that $0\ 0$ is the equilibrium point for this system. And, we can also show that it becomes asymptotically stable by selecting this k and L suitably so, that we can see through the Lyapunov theory, which was done in the previous lecture.

So, let us assume that the Lyapunov function is taken to be like this, in terms of e and w V of e and w is $K e^2$ plus w^2 . So, first thing is K is positive definite as we have selected and therefore, this function the right hand side is a positive definite function, because it is 0 only at e and w both are 0 and it is positive for all other values of e and w the matrix.

So, when we say because e is a vector here e^2 it means it is not the scalar square, it is the vector $e \cdot e$ the norm of e squares, in similarly w^2 means $w \cdot w$ the scalar product of these vectors. So, when we take the derivative V dot it is $2k$ times $e \cdot$, when e is a vector $e \cdot$ is also a vector, this is the dot product of this vectors, because when we say differentiation d by dt of e^2 . The meaning is d by dt of $e \cdot e$.

So, that is nothing, but 2 times $e \cdot e$ dot ok. The derivative of e and $e \cdot$ so, that is written in this way, similarly w^2 when we differentiate we will get $2 w \cdot$ it means the dot product of w vector and w dot vector. So, now we can take this expression by substituting the values of $e \cdot$ and $w \cdot$ from this 2 equation, we get $2K e \cdot$ is w that is the first term and $2w$ and $w \cdot$ is given by this.

So, it is easy to see that the ultimate value is $2L w \cdot w$ this is nothing, but minus $2L w \cdot w$ vector. So, this is negative definite function, because it is always negative value, this minus sign is there and all the things are positive.

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Manipulator Control

$\Rightarrow \dot{V}$ is -ve definite

as $w = 0 \Rightarrow \dot{w} = 0 \Rightarrow e = 0$ $\dot{V} = 0$
 $\Rightarrow e = 0, \dot{w} = 0$

So $\dot{V} = 0$ only at (0,0)

and $\dot{V} < 0$ for all (e, w)

Hence Proved

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So, it is a negative definite value, even because when w is 0 automatically it will imply that e is also equal to 0, because when w equal to 0 \dot{w} will be 0 and then both w and \dot{w} or 0 from the equation given here, you can say that e is also equal to 0. Because, when w is 0 \dot{w} is 0 $K e$ is equal to 0 and K is positive definite therefore, the vector e is 0 vector.


So, the \dot{V} the scalar is always negative and it is 0 only at the e and e is 0 and w equal to 0 ok, \dot{V} equal to 0 that implies e is 0 and w 0. So, it is negative definite. So, this implies that, the system is asymptotically stable, when we select the control in this way. We get the asymptotic stability of this system; we have shown that the system is asymptotically stable in this way.

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Manipulator Control Example

- Consider the controlled pendulum OA .
- Let $OA = L$ and τ denotes the torque applied.

θ is variable denoted angle with vertical axis.
 M denotes the mass of pendulum.



The diagram illustrates a simple pendulum system. A vertical axis is shown with a red circle at the origin. A blue line of length L extends from the origin to a blue mass M at point A . The angle between the vertical axis and the line OA is labeled θ . A curved arrow indicates a torque τ applied at the joint.

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Now, we take an example of computing the control of a simple 1 arm manipulator ok, single arm manipulate or we can say that a pendulum with control torque, that is applied at the joint here.

So, if you assume that the simple the pendulum single arm manipulator, the length is L and θ is measured from the vertical downward vertical, then and M is the mass of the pendulum.

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Manipulator Control Example

The dynamic equation is:

$$\frac{1}{3}ML^2\ddot{\theta} + \frac{Mg}{2}L \sin \theta = \tau$$

If we want to find a control τ such that:

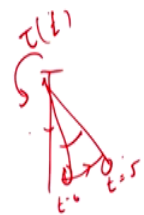
$$\begin{aligned} \theta(0) &= \frac{\pi}{6} \quad \text{and} \quad \theta(5) = \frac{\pi}{3} \\ \dot{\theta}(0) &= 0 \quad \text{and} \quad \dot{\theta}(5) = 0 \end{aligned}$$

Then we can find the desired trajectory as:

$$\theta_d(t) = a_0 + a_1t + a_2t^2 + a_3t^3$$

a_0, a_1, a_2, a_3 can be obtained using the four conditions.

If the actual initial position is:

$$\theta(0) = 0 \quad \text{and} \quad \dot{\theta}(0) = 0$$


Then, we know that the equation is written in this particular form. We have already seen the dynamic equation of the single arm robot manipulator is written like this, where the torque access the control for this one. Now, we want to find the control of this pendulum, in this particular manner. That is a time T equal to 0 the angle is pi by 6, 30 degrees. And, a time t equal to 3 5 unit the angle is 60 degrees.

So, the pendulum is at 30 degree when t equal to 0, when t equal to 5 it is at 60 degrees and the derivative; that means, the velocity of the pendulum is 0 at time t equal to 0 and 5 both.

So, it should start from here and then stop at this point, that is the meaning here. For this how to find a torque the torque is applied at the joint as a function of time.

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So, now after obtaining the desired trajectory as a function of time, we define the error actual angle is θ and desired angle is θ_d as a function of time. These are all functions of time and w is \dot{e} the derivative of e and that is nothing, but $\dot{\theta}$ and $\dot{\theta}_d$ the derivative. Now, we define the system in the form of error and its derivative.

So, let us say \dot{e} is w as given here and \dot{w} is nothing, but $\ddot{\theta} - \theta \ddot{d}$. So, if you substitute that from here we will get this expression \dot{w} is nothing, but $\ddot{\theta}$, $\ddot{\theta}$ is from this equation we can get it is $\tau - M g \frac{L}{2} \sin \theta$ by 2 etcetera. So, we can easily calculate from that expression this one.

So, \dot{w} is given by this expression $\frac{3}{M L^2} \tau - M g \frac{2}{L} \sin \theta + \ddot{\theta}$, that is coming from this equation, this is for $\ddot{\theta}$. I think we have to add this term also because w is given by this $-\theta \ddot{d}$ of t . So, \dot{w} is actually this term, then we can select this τ to be given by this equation.

So, τ if you take the first term this will cancel the term $M g \frac{2}{L} \sin \theta$ of this thing. So, this term is getting cancelled with this term and then we can write $\frac{M L^2}{3}$ into $-\dot{K} e - L \dot{w}$.

So, if you substitute in the place of τ this whole expression, we will simply get the expression to be equal to this will imply \dot{w} is equal to we get simply $-\dot{K} e - L \dot{w}$. So, here one term is missing that is $\ddot{\theta}$.

So, we have to include this $\ddot{\theta}$ in the selection of τ . So, that finally, we will get only this term. So, by selecting this control, what we get is in the form of error \dot{e} equal to w , \dot{w} is $-\dot{K} e - L \dot{w}$.

So, as we did in the previous description, exactly similar equation we are getting. So, by taking a Lyapunov function of this form $\dot{K} e^2 + w^2$ the same thing can be done here, we can show that this system is asymptotically stable. In other words it says that the τ which we have selected here will make the system the pendulum to travel along this particular desired trajectory. As t progresses the error of the desired trajectory and the actual trajectory will tend to 0. So, that is the meaning of this expression.

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Manipulator Control Example

$$\Rightarrow \ddot{w} = -Kw - L\dot{w}$$

$$\Rightarrow \ddot{w} + L\dot{w} + Kw = 0$$

$$w(t) = C_1 e^{m_1 t} + C_2 e^{m_2 t}$$

$$m_1 = -\frac{L}{2} \pm \frac{\sqrt{L^2 - 4K}}{2}$$

If $L^2 - 4K \leq 0$ then the real parts of m_1 and m_2 are $-\frac{L}{2}$
 So $e^{m_1 t}$ and $e^{m_2 t} \rightarrow 0$ as $t \rightarrow \infty$
If L is large then $w(t)$ is close to 0 for small value of t .

Handwritten notes:
 L large.
 $e^{-\frac{L}{2}t}$ is very small for small values of t if L is large.

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Now, we can see here how quickly we can make the error to be 0 by selecting suitably L and K . So, here w double dot is given by this expression minus $K w$ minus $L w$ dot, because from the previous equation, we have w dot equal to minus $K e$ minus $L w$, if we take double dot of this we get this expression.

So, this is nothing, but a second order ordinary differential equation and this expression it gives the roots of this auxiliary equation to be m_1 and m_2 . So, w of t is nothing, but $C_1 e$ to the power $m_1 t$ plus $C_2 e$ power $m_2 t$, where the roots of the auxiliary equation is given by this expression. If, you select L square minus $4 K$ less than or equal to 0, we can see that the real parts of the roots m_1 and m_2 are simply minus L by 2.

So, if we take L very large, then e to the power minus L by 2 tends to 0, L by 2 into t it converges to 0 or it converges to close to 0, in a shorter span of time. So, e power minus L by

2 t this modulus is very small for small value of t, if L is large. So, by selecting a large value of L we can make the error tending to 0 in a shorter period of time. So, in that case we can say that the trajectory will be tracked by using the control given by this formula.

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Manipulator Control Example 2

	θ	d	α	a
1	θ_1	<u>OA</u>	$-\frac{\pi}{2}$	0
2	θ_2	0	0	<u>AB</u>
3	θ_3	0	$\frac{\pi}{2}$	0
4	θ_4	<u>BC</u>	0	0

$OA = 10$
 $BC = 6$
 $AB = 8$
 Tool Length = 1 unit
 One Rotation = $\frac{1}{4}$ units

So, we have the robot manipulator, where OA is this and AB is the second link and BC is the third link with the tool in the as the end effector.

So, here the AB is a revolute joint, first joint is revolute, the second is revolute joint with rotation of this type, the third is revolute joint and the fourth is also a revolute joint. So, the 4 joints all of them are revolute and by using the d h algorithm, we have already seen we can write the coordinate frames and the joint and link parameters in this particular form.

So, here OA is given by this expression this is a joint distance. And, similarly BC is joint distance AB is the link length. According to the parameters theta 1, theta 2, theta 3, theta 4 these are the joint angles, theta 3 and theta 4.

So, with this adjustment of these 4 angles one can perform a desired task using the robot manipulator. So, here in this example it is starting from a initial position and then reaching a position on the ground and inserting the tool at a particular point.

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Manipulator Control Example 2

$${}^0T_4 = \begin{bmatrix} (c_1c_2c_3 - c_1s_2s_3)c_4 - s_1s_4 & -(c_1c_2c_3 - c_1s_2s_3)s_4 - s_1c_4 & c_1c_2s_3 + c_1s_2c_3 & a_2c_1c_2 + d_4(c_1c_2s_3 + c_1s_2c_3) \\ (s_1c_2c_3 - s_1s_2s_3)c_4 + c_1s_4 & -(s_1c_2c_3 - s_1s_2s_3)s_4 + c_1c_4 & s_1c_2s_3 + s_1s_2c_3 & a_2s_1c_2 + d_4(s_1c_2s_3 + s_1s_2c_3) \\ (-s_2c_3 - c_2s_3)c_4 & -(-s_2c_3 - c_2s_3)s_4 & -s_2s_3 + c_2c_3 & d_4(-s_2s_3 + c_2c_3) - a_2s_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_1 \\ r_{21} & r_{22} & r_{23} & p_2 \\ r_{31} & r_{32} & r_{33} & p_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

We get

$$\underline{\underline{2d(t) = \begin{pmatrix} \theta_1(t) \\ \theta_2(t) \\ \theta_3(t) \\ \theta_4(t) \end{pmatrix}}}$$

$$\begin{aligned} c_1(c_2c_3 - s_2s_3)c_4 - s_1s_4 &= r_{11} \\ s_1(c_2c_3 - s_2s_3)c_4 + c_1s_4 &= r_{21} \\ \Rightarrow s_4 &= c_1r_{21} - s_1r_{11} \\ \tan \theta_4 &= \frac{r_{21}}{r_{11}} \\ (-c_2s_3 - s_2c_3)c_4 &= r_{31} \\ \tan \theta_4 &= \frac{r_{31}}{r_{11}} \end{aligned}$$

$$\left\{ \begin{aligned} \theta_1(t) &= \\ \theta_2(t) &= \\ \theta_3(t) &= \\ \theta_4(t) &= \end{aligned} \right. \text{ in terms of } r_{ij}(t)$$

So, for performing this task we can design the problem in the following manner. So, firstly, the arm matrix 0 T 4 as we have seen in the inverse kinematics lecture, the 0 T 4 for this particular manipulator is given by this expression. So, if we know the 0 T 4 for each instant of

time as a function of time, then we can solve the inverse problem for all the angles θ_1 as a function of time θ_2 , θ_3 , and θ_4 .

So, all the angles can be obtained by solving the inverse kinematics problem, in terms of this r_{ij} , these are all functions of time in terms of r_{ij} as a function of time.

So, the main problem here is to give r_{ij} as a function of time and then solving the inverse problem θ_i equal to 1 to 4 as a function of time. So, once this is done this is our Q desired, Q desired as a function of time is given by $\theta_1(t)$ $\theta_2(t)$ $\theta_3(t)$ $\theta_4(t)$.

So, this is calculated by this one. So, main problem here is now to give this r_{ij} as a function of time. So, once it is given we can easily obtain what is Q desired, once Q desired is given we can get the torque as demonstrated in the previous examples.

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Manipulator Control Example 2


Initial position of end effector(t_0) = $\{0, 14, 10\}$
 Position of end effector at $t = 1(t_1)$ = $\{4, 4, 1\}$


$t \in [0, 1]$
 0T_4 at $t = 0$

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 14 \\ 0 & -1 & 0 & 10 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \checkmark$$

0T_4 at $t = 1$

$$\begin{bmatrix} -1 & 0 & 0 & 4 \\ 0 & 1 & 1 & 4 \\ 0 & 0 & -1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \checkmark$$




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So, let us assume that the robot performs a desired task in 2 unit of time.

So, from the interval in the interval 0 to 1, time interval 0 to 1, it performs the job of starting from the initial position and reaching the final position. And, then in the interval z 1 to 2 it is performing the job of rotating the screw for 1 full rotation. So, these are the two segments of the task assigned to the robot.

So, let us assume that at time t equal to 0 the end effector is at this position 0, 14, 10. And, at the final time t equal to 1, it is a deposition 4, 4, 1, that is from the ground the z value is 1 unit above, that is the final position of the end effector. So, initial position is given final position, the origin is at the 0.014, 10 and the x axis of the end effector is $1\ 0\ 0\ 0\ 0$ minus 1 and $0\ 1\ 0$.

So, it this means that the end effector x axis is parallel to x axis of the base. And, it is the negative z axis of the base, the y axis is $0\ 0$ minus 1, it means it is pointing downwards and the z axis is $0\ 1\ 0$ it means the z axis of the end effector is parallel to the y axis of the base. Same way, we can define the required position and orientation of the end effector at t equal 1 is given by this expression.

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Manipulator Control Example 2

In interval $t \in [1,2]$, screw makes one full rotation
End effector position at time t is given by

$${}^0T_4(t) = \begin{bmatrix} \cos \theta(t) & \sin \theta(t) & 0 & 4 \\ \sin \theta(t) & -\cos \theta(t) & 1 & 4 \\ 0 & -1 & 0 & z(t) \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$\theta(1) = \pi$ $z(1) = 1$
 $\theta(2) = 3\pi$ $z(2) = \frac{3}{4}$
 $\theta(t) = \pi + (t-1)2\pi$

${}^0T_4(t) \in [0, 2]$



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So, there are two conditions therefore, we can decide a trajectory as a polynomial of degree 2 degree 1. So, now, during the time 1 to 2, this crew makes 1 full rotation, that is angle 0 2 angle 2 pi it will make a rotation.

So, at time t equal to 1 the angle is pi and at the time t equal to 2 it is 3 pi. And, the height of the tool is at 1 unit at time t equal to 1, after 1 full rotation the screw has gone inside 1 by fourth unit. Therefore, from the ground the height will be 3 by 4 at time t equal to 2.

So, from this information we can easily calculate theta of t should be like this. If, you substitute t equal to 1 we will get pi at t equal to 2 we will get 3 pi.

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Manipulator Control Example 2

$${}^0T_4(t) = a_0 + a_1 t \quad t \in [0,1] \quad \checkmark$$

$$a_0 = {}^0T_4(0)$$

$$a_1 = {}^0T_4(1) - {}^0T_4(0)$$

$$t \in [1,2]$$



$$\theta(1) = \pi \quad z(1) = 1$$

$$\theta(2) = 3\pi \quad z(2) = \frac{3}{4}$$

$$\underline{z(t) = b_0 + b_1 t}$$

$$1 = b_0 + b_1$$

$$\frac{3}{4} = b_0 + 2b_1$$



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Similarly, we can calculate z of t as a function of time, and 0T_4 as a function of time during the interval 0 to 1.

Because, there are 2 conditions given here, these are the 2 conditions at t equal to 0 and 1; we get a polynomial of degree 1. There are 2 coefficients a_0 a_1 which can be easily calculated from this expression. And, z of t is also calculated by using a polynomial with the 2 coefficients. So, it is done using the values z of 1 is 1 and z of 2 is 3 by 4. So, once we get all this information we get 0T_4 as a function of time t belongs to 0 to 2, the total interval of time.

So, for each instant of time we solve the inverse kinematics problem using this formula, various formula is given.. Here θ_4 and θ_1 is solved. Similarly, we can solve for θ_2 and θ_3 using all these values. So, we can obtain q desired as a function of time during

the entire interval. And, then this gives the control using this procedure. As we have seen the procedure for the general robot manipulator we have seen how to select the control. So, this procedure will give the control of the robot manipulator using the designed q value.

So, as we have seen for the general robot manipulator how to calculate the control using the formula given in the last line that is τ equal to \bar{C} plus \bar{G} plus \bar{M} into minus $K e$ minus $L w$.

And, where K and L are selected suitably to make the system asymptotically stable so, using this procedure we can compute the control for the example 2 and we get the desired torque. So, that the assigned task is performed in a robust manner ok.

Thank you.