

Robotics and Control: Theory and Practice
Prof. N. Sukavanam
Department of Mathematics
Indian Institute of Technology, Roorkee

Lecture -14
Manipulator Dynamics Multiple Degree of Freedom

This is the continuation of the previous lecture. In this lecture we will see how to write the dynamic equation of n degree of freedom manipulator.

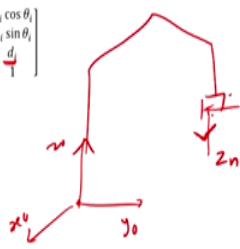
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Manipulator Dynamics
Multiple Degree of Freedom

Let $T = {}^0T_n = {}^0T_1 {}^1T_2 \dots {}^{n-1}T_n$ be the arm matrix of the manipulator. Then ${}^i-1T_i$ is a function of q_i , where q_i is the joint variable (joint angle or joint distance) where

$${}^{i-1}T_i = \begin{bmatrix} \cos \theta_i & -\sin \theta_i \cos \alpha_i & \sin \theta_i \sin \alpha_i & a_i \cos \theta_i \\ \sin \theta_i & \cos \theta_i \cos \alpha_i & -\cos \theta_i \sin \alpha_i & a_i \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$D = \begin{bmatrix} 0 & -\delta_x & \delta_y & d_x \\ \delta_x & 0 & -\delta_x & d_y \\ -\delta_y & \delta_x & 0 & d_z \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$${}^iD = \begin{bmatrix} 0 & -{}^i\delta_x & {}^i\delta_y & {}^i d_x \\ {}^i\delta_x & 0 & -{}^i\delta_x & {}^i d_y \\ -{}^i\delta_y & {}^i\delta_x & 0 & {}^i d_z \\ 0 & 0 & 0 & 0 \end{bmatrix}$$


The diagram shows a manipulator arm with a base coordinate frame x_0, y_0 and a joint variable z_n at the end. Red arrows indicate joint variables and coordinate transformations.

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So, the last lecture we have seen how to write the dynamic equation of a two degree of freedom manipulator with uniformly distributed mass. So, here we consider a general n degree of freedom manipulator, whose arm matrix is written as 0T_n which is the product of

${}^0T_1, {}^1T_2$, etcetera. So, in general this ${}^{i-1}T_i$, it represents the coordinate frame of the i th joint with respect to the $(i-1)$ th coordinate frame so.

So, if you consider a general robot manipulator with n degree of freedom, so, if you consider the 0th frame as x_0, y_0, z_0 that is the base coordinate frame and x_n, y_n, z_n is the end effector coordinate frame then, 0T_n it represents the n th tool frame, end effector frame with respect to the base frame given by this and then it is already known from the DH algorithm that ${}^{i-1}T_i$ can be written like this.

So, if the i th joint is a revolute joint then θ_i it represents the joint angle it is a variable in case i th joint is a prismatic joint then θ_i is a constant and d_i is a variable in that case. Now, the differential transformation; d represents a matrix which contains dx, dy, dz and $\delta x, \delta y, \delta z$. Which are the translational and rotational velocities of a particular joint with respect to the base frame?

And, here d super fix T it represents the translational and rotational velocity with respect to its own the current frame the T frame itself. So, the Jacobean lecture we have seen the relation between d and dt through the arm matrix.

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Let

$$T_i = {}^{i-1}T_i$$



$$\frac{dT_i}{dq_i} = D_i \cdot T_i$$

where

$$D_i = \begin{bmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \dots \dots \dots \text{if joint } i \text{ is revolute}$$

$$D_i = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \dots \dots \dots \text{if joint } i \text{ is prismatic}$$

$q_i = \theta_i$ or d_i

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So, now if you denote ${}^{i-1}T_i$ as T_i then the derivative with respect to the variable q_i because, the i th frame is a function of q_i .

Where q_i is either θ_i or d_i depending on whether the i th frame is a revolute joint or prismatic joint. So, the derivative with respect to the i th variable q_i the partial derivative is given by D_i into T_i . Where D_i is this matrix if it is a revolute joint or this matrix if it is a prismatic joint so, the partial derivative with respect to the variable is given by d_i multiplied by the matrix D_i .

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Manipulator Dynamics
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Thus

$$\frac{dT}{dt} = \frac{\partial T}{\partial q_1} \dot{q}_1 + \frac{\partial T}{\partial q_2} \dot{q}_2 + \dots + \frac{\partial T}{\partial q_n} \dot{q}_n$$

Now consider

$${}^0T_j = {}^0T_1 \cdot {}^1T_2 \dots {}^{j-1}T_j$$

and

$$u_{jk} = \frac{\partial}{\partial q_k} ({}^0T_j) = T_1 \cdot T_2 \dots T_{j-1} \cdot D_k \cdot T_k \dots T_j \quad (\text{if } k \leq j)$$

Let

$$u_{jkl} = \frac{\partial}{\partial q_l} (u_{jk}) \quad ; l \leq j$$

Handwritten notes:
 $\frac{\partial T}{\partial q_1} = \dot{T}_1$
 $\frac{\partial T}{\partial q_k} = D_k T_k$

Handwritten note:
 $\frac{\partial T}{\partial q_1} = \dot{T}_1$

Handwritten note:
 $\frac{\partial T}{\partial q_k} = D_k T_k$

So, the total derivative dT by d small t is given by the standard chain rule; $\frac{dT}{dt}$ by $\frac{dT}{dq_1} \dot{q}_1 + \frac{dT}{dq_2} \dot{q}_2 + \dots$ is the total derivative of the matrix T where $\frac{dT}{dq_k}$ is given in the previous slide. Now, if you consider 0T_j the j th coordinate frame with respect to the base frame which is given by this product and if you denote u_{jk} means, the partial derivative of 0T_j matrix with respect to the variable q_k . Because, 0T_j it contains ${}^0T_1, {}^1T_2, \dots, {}^{j-1}T_j$.

So, when we differentiate 0T_j with respect to a variable q_k ; where k is less than or equal to j we get because, that derivative is effective only with the matrix T_k and the previous slide we have seen that the partial derivative of T_k with respect to q_k is given by D_k multiplied by T_k so, by substituting that we get the derivative to be like this in this way.

Now, if we further differentiate u_{jk} with respect to q_l , where l is say less than or equal to j again then, we can denote it by u_{jkl} the notation u_{jkl} means, we differentiate u_{jk} with respect to q_l that is. So, it is very clear that once again if you differentiate with this term $\frac{\partial}{\partial q_l}$ then wherever T suffix l appears that derivative will be effective in that place. Whether it is after T_k or before T_k wherever T_l appears the derivative should be effective on that T_l the derivative will be D suffix l into s_o , this is $\frac{\partial T_l}{\partial q}$ suffix l .

So, depending on whether it is revolute or prismatic this matrix D can be selected and substituted.

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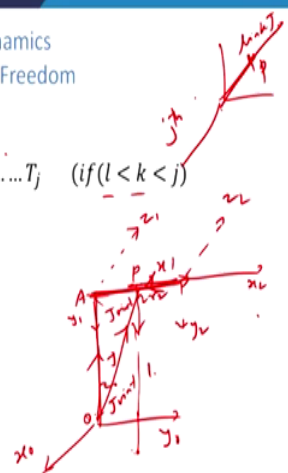
Manipulator Dynamics



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Thus

$$u_{jkl} = T_1 \cdot T_2 \dots D_l \cdot T_l \dots D_k \cdot T_k \dots T_j \quad (\text{if } (l < k < j))$$

Let P be a point on j^{th} link with an element of length dl . Let r_j be the vector representing the point P in the j^{th} coordinate frame, then the vector representing P in the base coordinate frame is:

$$P_j = {}^0T_j \cdot r_j$$




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So, so for example, if you have u_{jkl} it is if j_l is less than k this $D_l T_l$ will appear before $D_k T_k$ or if l is greater than k then it will appear after this T_k . So, in all the cases we can write u_{jkl} notation to be the partial derivative. Now, let us assume that P be a point on the j^{th} link

with respect to j th link. So, if you consider the so, for example, let us say this is the first link this is the second link and the coordinates are x_0, y_0, z_0 and if you assume this is the rotation with respect to z_1 , the revolute joint and we can fix the x_1, y_1 .

So, if we consider this is the point o this is the point a and so, we have two coordinate frames x_0, y_0, z_0 and here we can fix x_1, y_1, z_1 . Now, if I consider this is the first joint this is joint one and this is joint two. So, if I write the joint one with respect to the first frame.

Similarly, j th joint with respect to j th frame it means, the link is for example, here this is the first link and the first coordinate frame is z_1, x_1, y_1 , etcetera that can be fixed. So, with respect to x_1, y_1, z_1 the link one is considered. Similarly, if you have another joint for example, here z_2 and x_2, y_2 , etcetera can be fixed. So, with respect to x_2, y_2, z_2 the link 2 is returned. So, we take a point P general point P on the link 2 with respect to x_2, y_2, z_2 .

Similarly, here according to this let P be a point on the j th link with respect to the j th coordinate frame. So, that is the meaning here. So, now, let r_j denote the vector representing the point P in the j th coordinate frame. So, if you take a particular point P on the second frame and write the vector with respect to x_2, y_2, z_2 it is this vector.

This is the r_2 vector we can say that with respect to the x_2, y_2, z_2 frame for a fixed for a particular point on the second frame. Similarly, if you take a point P on the j th link with respect to j th frame it is coordinate vector we call it as r suffix j here. Now, the same point the point P if you write with respect to the base frame that is called P_j the point with respect to base frame. So, for if the if r_j is the coordinate a vector with respect to the j th coordinate frame then if we multiply in the left side by 0T_j it represent the same point with respect to the base coordinate frame. So, P_j represent the point P with respect to the base frame.

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Its velocity is:

$$V_j = \frac{dP_j}{dt} = \frac{d}{dt}({}^0T_j \cdot r_j)$$



$$= \left[\sum_{k=1}^j \frac{\partial}{\partial q_k} ({}^0T_j) \dot{q}_k \right] r_j$$

$$= \left[\sum_{k=1}^j u_{jk} \dot{q}_k \right] r_j$$

If ρ is the uniform density then the kinetic energy of the element dl is given by:

$$dK_j = \frac{1}{2} |V_j|^2 \cdot \rho \cdot dl$$

Handwritten notes:
 $\frac{d}{dt} ({}^0T_j)$
 $\frac{dl}{\rho}$



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Now, the velocity of the same point means, we have to differentiate the vector P_j with respect to time. So, d by dt of 0T_j into r_j . So, we always keep it mind that r_j is a fixed vector quantity and 0T_j is a function of q_1, q_2 , up to q_j here.

So, we have already seen that the derivative d by dt of 0T_j , how to write it is through the summation? In the previous slide we have seen already the derivative $\frac{\partial}{\partial q_k}$ of 0T_j for different value of k . So, that is substituted here because it is a total derivative in terms of the partial derivative we will write the summation k equal to 1 to j of $\frac{\partial}{\partial q_k}$ of this into the \dot{q}_k by dt . So, it is the same formula as given here the total derivative this thing; instead of n we have j here that is the only difference. So, multiplied by r_j so, by using the notation u_{jk} we can write this can be replaced by u_{jk} . Now, the point P one point P is

considered, if the link is with uniform mass distribution then at a point P if we take a length dl a small element of length dl is taken.

So, the if rho is the uniform density then the kinetic energy of a element of length dl is given by half into mass is rho into dl into velocity square, the velocity of that element is V and its square modulus of velocity can be taken. So, the kinetic energy of the small element of mass can be calculated by this formula.

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Let

$$P_j = \begin{bmatrix} x_j \\ y_j \\ z_j \\ 1 \end{bmatrix} \text{ w.r.t. base}$$

and

$$V_j = \begin{bmatrix} \dot{x}_j \\ \dot{y}_j \\ \dot{z}_j \\ 0 \end{bmatrix} \text{ the velocity vector}$$

Then

$$V_j \cdot V_j^T = \begin{bmatrix} \dot{x}_j^2 & \dot{x}_j \dot{y}_j & \dot{x}_j \dot{z}_j \\ \dot{y}_j \dot{x}_j & \dot{y}_j^2 & \dot{y}_j \dot{z}_j \\ \dot{z}_j \dot{x}_j & \dot{z}_j \dot{y}_j & \dot{z}_j^2 \end{bmatrix}$$

$$\text{Trace}(V_j \cdot V_j^T) = \dot{x}_j^2 + \dot{y}_j^2 + \dot{z}_j^2$$

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So, how to calculate that? We take the point P to be $x_j y_j z_j$ with respect to the base and V_j is given by $\dot{x}_j \dot{y}_j \dot{z}_j$. And, V_j is a column vector V_j^T is row vector the same thing.

If you multiply V_j and V_j transpose we get $x_i x_j$ dot square, $x_j y_j$ dot and x_j dot z_j dot, etcetera. So, directly multiplying V_j and V_j transpose is this. Now the trace of this matrix is the sum of the diagonal elements that is x_j dot square plus y_j dot square z_j dot square. That is the velocity modulus of the velocity square. So, in the place of modulus of velocity square we replace by the it is trace of $V_j V_j$ transpose.

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So

$$dK_j = \frac{1}{2} \text{Trace} \left[\sum_{k=1}^j u_{jk} \dot{q}_k \right] r_j \cdot \left[\sum_{k=1}^j u_{jk} \dot{q}_k \right] r_j^T dm$$

$$= \frac{1}{2} \text{Trace} \sum_{k=1}^j \sum_{l=1}^j u_{jk} r_j \cdot r_j^T u_{jl}^T \dot{q}_k \dot{q}_l dm$$

$$K_j = \int dK_j = \frac{1}{2} \text{Trace} \sum_{k=1}^j \sum_{l=1}^j u_{jk} \int r_j \cdot r_j^T dm u_{jl}^T \dot{q}_k \dot{q}_l$$

$\left(\begin{matrix} u_{jk} & r_j & \dot{q}_k \end{matrix} \right)^T$
 $r_j^T u_{jk}^T$
 $pdL = dm$
 $\frac{L_j}{\Delta L}$

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So, the kinetic energy of the small element dm is half into trace of this is V_j into this whole thing is V_j element and then its transpose V_j transpose. Now, if you multiply two summations here it varies from 1 to j so, there are double summation so, we replace one variable we call it as k and another variable is called as L here.

So, k varies from 1 to j and L varies from 1 to j and if we take transpose of this matrix because r is a vector and here u is a matrix q is a number, it is a joint variable it q dot is the

velocity so, it is a number here so, u when we take the transpose of the product of two matrices, here it is u_{jk} and r_j multiplied by this q_k dot is there if you take transpose of this one and because, this is simply a real value we take the transpose of these two it is r_j transpose u_{jk} transpose.

So, by using that transpose property we can write this product as double summation k equal to 1 to j and L equal to 1 to j of u_{jk} is this and here r_j is as it is then we get r_j transpose, as we are using this one then multiplied by u_{jl} transpose the transpose of this one, multiplied by these two real values q_k dot q_l dot; multiplied by this small mass here. Because ρ into dl it is the small element mass m .

Now, we can calculate the total kinetic energy of the j th link it is the integrally, the j th link has length let us say L_j then we have to integrate from 0 to L_j because, we have taken small element mass length dl and if we integrate from the total length from 0 to L we get the total kinetic energy.

So, we get the same formula can be integrated the integration is effective only on this r_j and r_j transpose because, r_j is the vector in the j th coordinate frame; which is a constant vector similarly, r_j transpose is a constant vector we multiply this two and then integrate from 0 to the length of the particular link.

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$$\int_0^L x \, dl = \bar{x}$$

$$\int_0^L xy \, dl = \bar{xy}$$

$$\int_0^L x^2 \, dl = \bar{x^2}$$

$$r_j \cdot r_j^T = \begin{bmatrix} x_j^2 & x_j y_j & x_j z_j & x_j \\ x_j y_j & y_j^2 & y_j z_j & y_j \\ x_j z_j & y_j z_j & z_j^2 & z_j \\ x_j & y_j & z_j & 1 \end{bmatrix}$$

$$r_j = \begin{bmatrix} x_j \\ y_j \\ z_j \\ 1 \end{bmatrix}$$

$$\int_{\text{Every link } j} r_j \cdot r_j^T dm = \begin{bmatrix} \frac{1}{2}(-l_{xx} + l_{yy} + l_{zz}) & l_{xy} & l_{xz} & m \cdot \bar{x} \\ l_{xy} & \frac{1}{2}(l_{xx} - l_{yy} + l_{zz}) & l_{yz} & m \cdot \bar{y} \\ l_{xz} & l_{yz} & \frac{1}{2}(l_{xx} + l_{yy} - l_{zz}) & m \cdot \bar{z} \\ m \cdot \bar{x} & m \cdot \bar{y} & m \cdot \bar{z} & 1 \end{bmatrix}$$

inertia matrix

So, now, we can write $r_j \cdot r_j^T$ is given by this expression x_j^2 if I write the vector r_j to be $x_j y_j z_j$ then with respect to the j th frame. Now, if you multiply $r_j \cdot r_j^T$ we get this expression and if you integrate from 0 to the length of the particular link we get this expression. So, for example, if we integrate x into y into the length, dl 0 to the total length for example, that is given by I_{xy} the inertia with respect to the xy plane.

Similarly, if you integrate this it is inertia with respect to xz and the because, normally in homogeneous transformation a vector is represented by 4 values, the first 3 represent the coordinate and the last one is a dummy variable 1, ok. So, that the first lecture we have seen how to write the coordinates. So, r_j is so, here sorry, we have to see that everywhere we should write one here. So, that it is a homogeneous coordinate vector, ok.

If we differentiate 1 we will get 0, etcetera. So, we get here 0, 0, 0, etcetera. Here also the same thing r is represented by x y z and 1 here in the end yeah. So, when we do the integration we get inertia with respect to x y plane and here inertia with respect to x z plane, when we integrate this one the last one with respect to 0 to L dl this will give the mass the total mass of the link multiplied by d because, we know that integral x into dm multiplied by the uniform density this gives the value of the x x coordinate of the centre of mass of that particular link multiplied by m here.

So, we get this one integral of x into dm it represent mass into the centre of centre of mass x coordinate. Similarly, the integration of this will give mass into the centre of mass of the y coordinate of the centre of mass and integral L is the z coordinate of the centre of mass multiplied by m . So, the same thing is repeated here.

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$$I_{xx} = \rho \int (y^2 + z^2) dl \quad \checkmark$$

$$I_{yy} = \rho \int (x^2 + z^2) dl \quad \checkmark$$

$$I_{zz} = \rho \int (x^2 + y^2) dl \quad \checkmark$$

$$I_{xy} = \int x \cdot y \, dm$$

$$I_{yz} = \int y \cdot z \, dm$$

$$I_{zx} = \int x \cdot z \, dm$$

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And, here also we can easily see the next slide we can see that I_{xx} is nothing, but the inertia with respect to the X axis.

If you take any point P if you draw up a perpendicular so, this perpendicular to the X axis so, this is nothing, but $y^2 + z^2$, if the point P has x, y, z as the coordinate the length of this point; the if if we draw up a perpendicular to the X axis the length of the m is nothing, but $y^2 + z^2$ length square. So, this gives the inertia with respect to the x coordinate and $x^2 + z^2$ is the square of the distance from P to the Y axis. So, this gives the inertia with respect to Y axis and this is inertia with respect to the Z axis.

So, we can easily see from this one the calculation the integral of only x^2 if you take, into dm that is given by this expression if you substitute for I_{xx} I_{yy} I_{zz} from this quantity divided by 2 will give only the first integral.

So, simply the integral of $r_j r_j^T$ is given by this matrix which is called the inertia matrix. This is a fixed one because, r_j and r_j^T they are not going to change throughout the motion of the robot manipulator. So, once a robot manipulator is given for each joint each link j we can calculate the inertia matrix and it is a fixed one.

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Total Kinetic Energy

where I_j is the inertia of the j^{th} actuator.
Total Potential Energy

So,

$$K = \sum_{j=1}^n K_j$$

$$K = \frac{1}{2} \sum_{j=1}^n \sum_{k=1}^j \sum_{l=1}^l u_{jk} I_j u_{jl}^2 q_k q_l + \frac{1}{2} \sum_{j=1}^n I_j \dot{q}_j^2$$

$$P.E. = \sum_{j=1}^n P_j$$

$$P_j = \sum_{i=1}^n m_j g_j^T ({}^0T_j, r_j)$$

where r_j is the center of mass of j^{th} link

$$L = K - P = \sum_{j=1}^n K_j - \sum_{j=1}^n P_j = \frac{1}{2} \sum_{j=1}^n \sum_{k=1}^j \sum_{l=1}^l u_{jk} I_j u_{jl}^2 q_k q_l + \frac{1}{2} \sum_{j=1}^n I_j \dot{q}_j^2 - \sum_{j=1}^n m_j g_j^T ({}^0T_j, r_j)$$

Handwritten notes:
 $\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_j} \right) - \frac{\partial L}{\partial q_j} = \tau_j$
 $\frac{1}{2} I_j (\text{actuator}) \dot{q}_j^2$
 $j \cdot P_j = 1/2 I_j \dot{q}_j^2$
 $I_j = K - P$
 j^{th} link diagram

Now, the total kinetic energy is summation of all kinetic energies for the link 1 to n. So, we can simply write that the kinetic energy for the j^{th} link is this and we are summing up all the so, it is j equal to 1 to n for all the links and the next two summation it gives the formula which we have given the kinetic energy of the j^{th} link.

And this expression it is nothing, but half into the inertia of the j^{th} actuator multiplied by \dot{q}_j dot square the velocity square so, if the actuator j^{th} actuator is a revolute one if it is revolving with velocity \dot{q}_j then \dot{q}_j dot square multiplied by the inertia of that actuator it gives the kinetic energy of that particular actuator. So, now, if you add the kinetic energy of all the actuators we get this formula. So, total kinetic energy these are the link kinetic energy and then this is link kinetic energy and these are the actuator kinetic energy. Similarly, we take

potential energy potential energy of each link can be calculated mass into gravity into the height.

So, if you take a particular point on the on the link this point so, the height to be calculated with respect to the base actually the we have to consider so, the base is this one and the j th link we let us say this one if P is the point we have to write the gravity vector will be pointing downwards and the height is from the point P to the projection of the point in the $x-y$ plane. So, we have to calculate so, the gravity with respect to the frame we have to write. So, the potential energy is given by mass into the gravity vector with respect to the j th frame.

Because, we are considering the potential energy of the j th frame so, if the j th frame is in different orientation let us say because, throughout the robot motion the frames are moving in different orientation, but the gravity is always pointing downwards. So, when we write the gravity vector in the j th frame then it will have 3 components, ok. It is a vector represented in the j th component it is a constant vector, so, mass into gravity into height the height is given by $0 \text{ T } j \text{ into } r_j$. So, the gravity vector dot product the P vector P_j vector with respect to the base frame so, that gives the height, ok. So, this will give modulus of the gravity vector and this is modulus of P_j into this thing \cos of the angle between these two vectors.

So, it means it is the projection of the gravity vector on the perpendicular vector. So, it gives mass into gravity into height type of thing so, this gives the potential energy formula. Now, if you add if you write the Lagrangian that is kinetic energy minus potential energy of the entire system so, we can write we collect the kinetic energy, collect the potential energy and then take K minus P that is the L Lagrangian.

So, after this we can simply write the equation of motion that is $\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_j} \right) - \frac{\partial L}{\partial q_j} = \tau_j$. If it is prismatic or f_j if it is if it is revolute it is torque, if it is prismatic it is the force. So, the equation of motion can be written from the Lagrangian formula here after doing all the derivatives we can obtain the dynamic equation of this problem which is very lengthy process.

As it is seen here, there are too many summations and too many variables are there if it is a n link manipulator so, it is a really a very lengthy procedure to get the dynamic equation of the n arm robot manipulator. So, this lecture gives only the procedure to find the Lagrangian of the manipulator and the remaining can be calculated using this formula, ok.

Thank you.