

Radiative Heat Transfer
Prof. Ankit Bansal
Department of Mechanical and Industrial Engineering
Indian Institute of Technology - Roorkee

Module - 5
Lecture - 24
Discrete Ordinate Method (DOM)

Hello friends, in the last lecture we discussed the spherical harmonics method P N, for the solution of radiative transfer equation. The method included approximation of the intensity. In today's lecture, we will discuss the method of discrete ordinates, the S N approximation method. The method is very similar to the method of spherical harmonics in the sense that we convert the algebra, the integro differential equation into sort of partial differential equations.

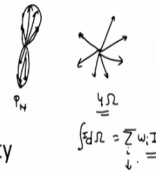
We approximate the intensity in angular direction. And the method has similar accuracy as that of the spherical harmonics method. However, there is a difference between the 2 methods. As opposed to continuous distribution of intensity in spherical harmonics, where we represented the intensity in terms of a series of harmonics. Here we represent intensity as discrete values in different directions.

So, in a sense, the discrete ordinate method finds equivalents in finite difference method of CFD. So, just like we have finite difference method in CFD, this method also relies on discretizing the angular direction using finite angular directions, discrete directions. We also have 1 method which is not we are going to discuss. And the method is finite volume method, where we discretize the angular direction using the finite volume approach. So, this discrete ordinate method is very much similar to what we have the CFD in CFD the finite difference method. So, the objective is same.

(Refer Slide Time: 02:32)

Discrete Ordinate Method (S_N Approximation)

- ❖ Transform RTE into a set of simultaneous PDEs
- ❖ Carried out to any arbitrary order and accuracy
- ❖ Unlike P_N method
 - ❖ Discrete representation of directional variation of Intensity
- ❖ Integrals over solid angle (4π) approximated by numerical quadrature



We have to transform our RTE, the integro differential equation into a set of partial differential equations. We can choose as many discrete directions as we want. Of course, the directions have to be decided judiciously. And we have to integrate over the solid angles for 4π . So, just to explain the difference between the method of spherical harmonics and discrete ordinate method. In spherical harmonics method at any point, we represented the intensity as a continuous function or a series of function.

So, we had a continuous function over theta, in both + direction and – direction. So, that was the P_N method. And we can retain as many terms as we want, leading to higher accuracy. So, we have P_1 method, the first order spherical harmonics method. We have P_3 method, the third order spherical harmonics method. However, in the discrete ordinate method, the intensity is not a continuous function of theta.

Rather, at any point, we take only discrete directions. So, we choose only discrete directions along which we will solve the RTE. So, we are basically discretizing the angular domain of 4π . So, this angular domain, angular solid angle, total solid angle we are discretizing using finite number of discrete directions. And then, we will integrate over all these directions using numerical quadrature.

So, what we will do is basically, we will integrate over the entire solid angle using some numerical scheme, numerical quadrature scheme, where we have w , the weights and intensity. If you are integrating over intensity, then we will have intensity in only those discrete

directions. Where I represents the discrete directions chosen using a suitable scheme. And then, we use numerical quadrature to integrate over the solid angles.


So, that is the difference between the spherical harmonics method and the discrete ordinate method that I basically is continuous function of intensity versus theta or azimuthal angle. And here we have a discrete function. And we use numerical quadrature to integrate over solid angle using these discrete values of intensity.



(Refer Slide Time: 05:12)

S_N Approximation

- ❖ RTE

$$\frac{dI}{dS} = \hat{s} \cdot \nabla I(\mathbf{r}, \hat{s}) = k(\mathbf{r})I_b(\mathbf{r}) - \beta(\mathbf{r})I(\mathbf{r}, \hat{s}) + \frac{\sigma_s}{4\pi} \int_{4\pi} I(\mathbf{r}, \hat{s}') \Phi(\mathbf{r}, \hat{s}', \hat{s}) d\Omega'$$
- ❖ Boundary conditions

$$I(\mathbf{r}_\omega, \hat{s}) = \epsilon(\mathbf{r}_\omega)I_b(\mathbf{r}_\omega) + \frac{\rho(\mathbf{r}_\omega)}{\pi} \int_{\hat{n} \cdot \hat{s}' < 0} I(\mathbf{r}_\omega, \hat{s}') |\hat{n} \cdot \hat{s}'| d\Omega'$$




3

So, we will start the development of this method from the radiative transfer equation. So, for radiative, for absorbing, emitting and scattering medium, we have radiative transfer equation in a given direction s. Radiative transfer equation can be written as the kappa times I b. That is the emission term – extinction by scattering and absorption. And then, in-scattering, that is augmentation by scattering, in-scattering.

And this radiative transfer equation is subjected to boundary condition at the wall, where we have at the wall 2 components, the emission from the wall and reflection from the wall. Reflection will have reflectance rho times irradiation from all the directions. So, we have to integrate over the solid angle for all the intensities coming. So, we are interested in intensity coming from all directions and reflected in a given direction.

And that this direction is s cap. And this, all the directions are basically represented by s cap prime. So, these are the governing equations. We have observed them many times before. Now, how do we approximate in the discrete ordinate method? That is, N S N approximation,

we replace the quadrature or the angular integration over solid angles with appropriate quadrature, numerical quadrature.

(Refer Slide Time: 06:48)

S_N Approximation

- ❖ RTE solved for a set of n different direction \hat{s}_i
- ❖ Numerical quadratures: $i = 1, 2, \dots, n$

$$\int_{4\pi} f(\hat{s}) d\Omega \approx \sum_{i=1}^n w_i f(\hat{s}_i)$$

w_i = weight
 $f(\hat{s}_i)$ = value of f
in discrete direction
 \hat{s}_i

- ❖ RTE

$$\hat{s}_i \cdot \nabla I(\mathbf{r}, \hat{s}_i) = k(\mathbf{r}) I_b(\mathbf{r}) - \beta(\mathbf{r}) I(\mathbf{r}, \hat{s}_i) + \frac{\sigma_s(\mathbf{r})}{4\pi} \sum_{j=1}^n w_j I(\mathbf{r}, \hat{s}_j) \Phi(\mathbf{r}, \hat{s}_i, \hat{s}_j)$$

- ❖ Boundary condition

$$I(\mathbf{r}_w, \hat{s}_i) = \epsilon(\mathbf{r}_w) I_b(\mathbf{r}_w) + \frac{\rho(\mathbf{r}_w)}{\pi} \sum_{\hat{n} \cdot \hat{s}_j < 0} w_j I(\mathbf{r}_w, \hat{s}_j) |\hat{n} \cdot \hat{s}_i|, \quad \hat{n} \cdot \hat{s}_i > 0$$

IIT KHARAGPUR
 NPTEL ONLINE
CERTIFICATION COURSE

4

So, if we have a function f , now in this case f will be intensity. So, if we have a function f that we want to integrate over solid angles. Then this integral is replaced by numerical quadrature. So, we replace it by summation $i = 1$ to n . w_i , where w_i is weight. And $f(\hat{s}_i)$ is value of f in discrete direction, \hat{s}_i . So, we have chosen certain directions. And along those directions, we are solving the RTE.

And the integral over solid angles appearing in the RTE is approximated using numerical quadrature. So, now our governing equation, the radiative transfer equation becomes purely differential equation. So, integration does not appear in this equation. We are evaluating intensity in discrete direction \hat{s}_i . And their integration has been replaced by numerical quadrature.

So, we have w_j intensity coming from all directions \hat{s}_j . The scattering phase function which is now dependent on discrete directions. So, although the scattering phase function is a continuous function, but we have approximated the scattering phase function Φ with a discrete function given from 2 directions \hat{s}_i and \hat{s}_j . Similarly, our boundary conditions now is no more an integral equation.

Boundary conditions also simplifies by replacing the integral in the boundary condition with the summation using numerical quadrature. So, the integration in the boundary condition here

for irradiation h is now replaced by a summation for all the incoming directions. So, n cap dot s_j cap is < 0 means, we are interested in only incoming directions. So, this has to be, the summation is for all incoming directions over which the reflection has to be accounted for.

(Refer Slide Time: 09:01)

S_N Approximation

- ❖ First-order linear PDEs for the unknown $I_i = I(\mathbf{r}, \hat{\mathbf{s}}_i)$
- ❖ Radiative heat flux (inside the medium or at a surface)

$$\mathbf{q}(\mathbf{r}) = \int_{4\pi} I(\mathbf{r}, \hat{\mathbf{s}}) \hat{\mathbf{s}} d\Omega \approx \sum_{i=0}^n w_i I_i(\mathbf{r}) \hat{\mathbf{s}}_i$$

- ❖ The Incident radiation

$$G(\mathbf{r}) = \int_{4\pi} I(\mathbf{r}, \hat{\mathbf{s}}) d\Omega \approx \sum_{i=0}^n w_i I_i(\mathbf{r})$$

So, using numerical quadrature, we have simplified the governing equations. The integro differential equation has been converted into first order linear partial differential equation in unknown intensity I subscript i . So, there will be number of discrete directions. So, we have to solve a number of equations. Number of equations depend on how many directions, discrete directions we have chosen in our analysis.

Now, once the intensity is known, we can calculate the radiative heat flux. So, radiative heat flux is intensity times the direction vector s cap integrated over all solid angles. Now, we can replace I with I_i and we integrate over the solid angle using the quadrature. So, our flux becomes summation i is $= 0$ to n , $w_i I_i$ subscript i s_i . Similarly, the incident radiation is integration of intensity over the solid angle.

And this can be written as simply summation $w_i I_i$ subscript i . So, once the discrete intensity or the intensity in discrete direction I subscribe i is known, the quantities of our interest heat flux and irradiation are easily calculated using this summation in the quadrature.

(Refer Slide Time: 10:24)

Discrete Ordinate Directions

- ❖ Directions and weights are completely symmetric
- ❖ Satisfy zeroth, first, and second moments

$$\int_{4\pi} d\Omega = 4\pi = \sum_{i=1}^n w_i$$

$$\int_{4\pi} \hat{s} d\Omega = 0 = \sum_{i=1}^n w_i \hat{s}_i$$

$$\int_{4\pi} \hat{s} \hat{s} d\Omega = \frac{4\pi}{3} \delta = \sum_{i=1}^n w_i \hat{s}_i \hat{s}_i \quad \left[\begin{array}{ccc} \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \end{array} \right]$$

Now, how these directions are chosen? So, we have to choose a certain number of directions. But how do we choose these directions? It has to satisfy certain conditions. The condition basically includes zeroth, first and second moments over the solid angle. So, for example, the total solid angle over 4π gives, should give you total intensity. So, the summation of the weights all the weights $i = 1$ to n should be $= 4\pi$.

Similarly, the first moment over the solid angle $\int \hat{s} d\Omega$ should be $= 0$. That is, the flux from all the directions should add up to 0. So, it becomes in summation, that summation $i = 1$ to n , $w_i \hat{s}_i$ should be $= 0$. And similarly, the second moment, $\int \hat{s} \hat{s} d\Omega$ should be $= \frac{4\pi}{3} \delta$, where δ is basically the matrix, identity matrix. And this should be $= \sum_{i=1}^n w_i \hat{s}_i \hat{s}_i$.

So, this value should be $=$ the identity matrix times $\frac{4\pi}{3}$. So, when we choose directions, our directions, chosen directions should satisfy these rules. And based on this, the directions can be chosen.

(Refer Slide Time: 12:01)

Discrete Ordinate Directions

 S_N

Order of Approximation	Ordinates			Weights
	ξ	η	μ	w
S_2 (symmetric)	0.5773503	0.5773503	0.5773503	1.5707963
S_2 (nonsymmetric)	0.5000000	0.7071068	0.5000000	1.5707963
S_4	0.2958759	0.2958759	0.9082483	0.5235987
	0.2958759	0.9082483	0.2958759	0.5235987
	0.9082483	0.2958759	0.2958759	0.5235987
S_6	0.1838670	0.1838670	0.9656013	0.1609517
	0.1838670	0.6950514	0.6950514	0.3626469
	0.1838670	0.9656013	0.1838670	0.1609517
	0.6950514	0.1838670	0.6950514	0.3626469
	0.6950514	0.6950514	0.1838670	0.3626469
S_8	0.1422555	0.1422555	0.9795543	0.1712359
	0.1422555	0.5773503	0.8040087	0.0992284
	0.1422555	0.8040087	0.5773503	0.0992284
	0.1422555	0.9795543	0.1422555	0.1712359
	0.5773503	0.1422555	0.8040087	0.0992284
	0.5773503	0.5773503	0.5773503	0.4617179
	0.5773503	0.8040087	0.1422555	0.0992284
	0.8040087	0.1422555	0.5773503	0.0992284
	0.8040087	0.5773503	0.1422555	0.0992284
0.9795543	0.1422555	0.1422555	0.1712359	

$$\hat{s} = \xi \hat{i} + \eta \hat{j} + \mu \hat{k}$$

❖ N in S_N denotes number of directions used for each principle direction

❖ Total direction $N(N+2)$ } $2 \times (2+2) = 8$

Now, for different values of approximations. So, we are talking about S_N approximation, where subscript N represents the order of the method. If $N = 2$, we have second order discrete ordinate method. If $N = 4$, we have fourth order discrete ordinate method and so on. Now, this N represents number of directions used for each principal directions. So, suppose we have taken 2 values of zeta, now any direction can be represented by its direction cosines.

So, S direction can be represented as $\xi \hat{i} + \eta \hat{j} + \mu \hat{k}$, where ξ , η and μ are constants. So, we have taken 2 values. If we have taken 2 values of zeta, then it will be called second order discrete ordinate method. Now, we will have total 8 directions in this case. So, total directions will be $2 \times 2 + 2$, that is total 8 directions. So, for a 2 values of zeta, we will have total 8 directions.

But we will just call it second order discrete ordinate method. Similarly, if we choose 3 values of zeta, we will have $3 \times 3 + 2$, 15 directions in all. So, as opposed to spherical harmonics method where we have first order and third order; even order terms were not there. Here we have even order for the method, that is S_2 , S_4 , S_6 , S_8 and so on. S_3 and S_5 method is not basically done here. The weights of these ordinates is also given in this table.

(Refer Slide Time: 13:46)

ONE-DIMENSIONAL SLAB

- ❖ Isotropic scattering

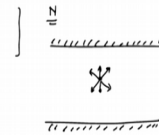
$$\phi = 1.0$$

$$\mu_i \frac{dl_i}{d\tau} = (1 - \omega)I_b - I_i + \frac{\omega}{4\pi} \sum_{j=1}^n w_j I_j$$

in a given discrete direction

- ❖ Intensity is independent of azimuthal angle

$$\mu_i \frac{dl_i}{d\tau} + I_i = (1 - \omega)I_b + \frac{\omega}{4\pi} G$$



Now, let us apply this method of discrete ordinate to 1-dimensional slab with isotropic scattering. So, once we have isotropic scattering, the value of phi will be = 1. So, our directional radiative transfer equation in direction mu i will be simply = mu i d I subscript i d tau is = 1 – omega I b – I i + omega upon 4 pi sum of the over all the quadrature weights, j is = 1 to n, w j i j. So, this is in a given direction, in a given discrete direction, the radiative transfer equation.

Now, for 1-dimensional slab, the intensity is independent of azimuthal angle. It depends on only on mu. And we observe that the method basically can also be written as first term remaining the same, the last term omega upon 4 pi j is = 1 to n w j i j. Now this summation is where nothing but incident radiation G. So, we replace it by G. So, what we get is the last term in the equation as omega G by 4 pi. Where omega is single scattering albedo.

Now, we have this governing equation. Total number of direction is N. This is in a given direction. So, total number of directions is N. So, in plane parallel slab, N by 2; if you are interested in finding intensity at a given point. So, let us say we have certain number of directions. So, N by 2 directions will be in the upward direction and N by 2 directions will be in the downward direction.

So, those directions which are going in upward direction are basically originated from the bottom plate. And intensity direction going in the downward direction are basically originated from the top late. So, we can assume that, out of N directions, N by 2 will be in the upward

moving direction and $N/2$ will be in the downward moving direction. So, based on that we can write down the intensities

(Refer Slide Time: 16:02)



ONE-DIMENSIONAL SLAB

❖ N different intensities

❖ $\rightarrow I_1^+, I_2^+, \dots, I_{N/2}^+ \quad \tau = 0 \text{ (with } \mu_i > 0)$ $\mu_i > 0$ I_1, \dots, I_N

❖ $I_1^-, I_2^-, \dots, I_{N/2}^- \quad \tau = \tau_L \text{ (with } \mu_i < 0)$

$$\left. \begin{aligned} \mu_i \frac{dI_i^+}{d\tau} + I_i^+ &= (1 - \omega)I_b + \frac{\omega}{4\pi}G & \mu_i > 0 \\ -\mu_i \frac{dI_i^-}{d\tau} + I_i^- &= (1 - \omega)I_b + \frac{\omega}{4\pi}G & \mu_i < 0 \end{aligned} \right\}$$



9

So, unknown intensities I_1^+, I_2^+ and so on up to $I_{N/2}^+$. Here, $+$ represents the intensity in the upward direction. That is, $\mu_i > 0$. And I_1^-, I_2^- and so on up to $I_{N/2}^-$ represents intensity in the downward direction at the plate, $\tau = \tau_L$ with $\mu_i >, < 0$. Okay. So, we have total N unknowns. So, unknowns are total N , I_1 up to I_N . Out of these unknowns $N/2$ intensities are in the upward direction and rest $N/2$ are in the downward direction.

So, the radiative transfer equation for this 1-dimensional case can be written for $\mu_i > 0$ as, $\mu_i \frac{dI_i^+}{d\tau} + I_i^+ =$ the source term. And similarly, for $\mu_i < 0$, that is downward movement, $-\mu_i \frac{dI_i^-}{d\tau} + I_i^- =$ the source term.

(Refer Slide Time: 17:09)

ONE-DIMENSIONAL SLAB

❖ Boundary conditions

$$\tau = 0: \quad I_i^+ = \frac{J_1}{\pi} = I_{b1} - \frac{1-\epsilon_1}{\pi\epsilon_1} q_1$$

$$\tau = \tau_L: \quad I_i^- = \frac{J_2}{\pi} = I_{b2} - \frac{1-\epsilon_2}{\pi\epsilon_2} q_2$$

❖ q and G are related to the directional intensities



$$q = \sum_{i=1}^{N/2} w_i' \mu_i (I_i^+ - I_i^-)$$

$$G = \sum_{i=1}^{N/2} w_i' (I_i^+ + I_i^-)$$

Since the intensity does not depend on azimuthal angle, summing weights $w = \sum w$

$q \sim \int I \mu d\Omega$

$G \sim \int I d\Omega$



10

The boundary conditions can be written at the bottom wall. At the bottom wall we have $\tau = 0$ and intensity is moving in the upward direction. So, we write it as I_i^+ , certain discrete directions. And this intensity will be written, J_1 upon $\pi = I_{b1} - 1 - \epsilon_1$ upon π i ϵ_1 q_1 . So, we can write down the boundary condition either in terms of radiosity J_1 upon π or we can write down in terms of emission and reflection.

So, first term is reflection, I_{b1} emission I_{b1} and second term is basically the reflection part. Similarly, at the top boundary, the boundary condition can be written. At top boundary, $\tau = \tau_L$. We have certain discrete directions. And in these discrete directions, the intensity will be J_2 upon π . And this value should be $I_{b2} - 1 - \epsilon_2$ upon π ϵ_2 q_2 . Now, q and G , as we have done many times for the approximate methods and P1 method.

So, q and G are related to these intensities. So, we can write down q . So, q is basically = summation of intensity $\mu_i d\Omega$. So, we can simply write down this as summation i is = 1 to N by 2 $w_i \mu_i (I_i^+ - I_i^-)$. And G is =, similarly, G is defined as integration over $I d\Omega$. So, we can write down this as summation i is = 1 to N by 2 $w_i - w_i$ prime $I_i^+ + I_i^-$.

So, we can write down our radiative heat flux and incident radiation in terms of the variables that we are solving the radiative transfer equation, that is I^+ and I^- . So, in terms of I^+ and I^- , the radiative heat flux q and G can be written using or approximating this integral using summation as has been done here.

(Refer Slide Time: 19:29)

ONE-DIMENSIONAL SLAB

$\tau = 0$:

$$q_1 = q(0) = \epsilon_1 \left(E_{b1} - \sum_{i=1}^{N/2} \omega'_i \mu_i I_i^- \right)$$

$\tau = \tau_L$:

$$q_2 = -q(\tau_L) = -\epsilon_2 \left(E_{b2} - \sum_{i=1}^{N/2} \omega'_i \mu_i I_i^+ \right)$$



So, once we do that finally, our boundary condition can be written at q is $= \tau$ is $= 0$. That is, q_1 is $= \epsilon_1 E_{b1} -$ the reflected part of the radiation i is $= 1$ to N by 2 w_i ; this is w_i prime $\mu_i I_i^-$. And similarly, at the top boundary q_2 is $= -q_{\tau L}$. And this will be $= -\epsilon_2 E_{b2}$. And then, sum over N by 2 weight $\mu_i I_i^+$. So, this is the expression for the heat flux at the boundaries. Now, let us apply this method to solve 1 problem.

(Refer Slide Time: 20:15)

Problem

Problem: Consider two large, parallel, gray-diffuse and isothermal plates, separated by a distance L . One plate is at temperature T_1 with emittance ϵ_1 , the other is at T_2 with ϵ_2 . The medium between the two plates is a gray, absorbing/emitting and linear-anisotropically scattering gas ($n = 1$) with constant extinction coefficient β and single scattering albedo ω . Assuming that radiative equilibrium prevails, determine the radiative heat flux between the two plates using the S_2 -approximation.

$$\nabla \cdot \mathbf{q} = 0$$

$$T_2, \epsilon_2$$

$$\beta$$

$$T_1, \epsilon_1$$



So, we have 2 large parallel gray-diffuse plates. The bottom plate, the first plate has temperature T_1 and emittance ϵ_1 . The other plate is at temperature T_2 emittance ϵ_2 . The medium between 2 plates is gray, absorbing and emitting. And linearly isotropically scattering gas; so, we take a extinction coefficient β for the medium. And assuming radiative equilibrium prevails, that is, $\nabla \cdot \mathbf{q} = 0$, we have to find out radiative heat flux between the 2 plates using the S_2 approximation method.

So, S 2 approximation method as we have discussed, is based on single direction. So, let us apply this method to solve this problem. So, we have to take the governing equation first. Our governing equation is given by these 2 equations, μ_1 ; so, these are our governing equation. So, let us write down these equations for the case.

(Refer Slide Time: 21:28)

Solution $\omega=0$ non-scattering

$$\mu_1 \frac{dI_1^+}{dz} + I_1^+ = \frac{1}{4\pi} G \quad \text{--- (1)}$$

$$-\mu_1 \frac{dI_1^-}{dz} + I_1^- = \frac{G}{4\pi} \quad \text{--- (2)}$$

Boundary condition \Rightarrow $z=0 \quad I_1^+ = \frac{J_1}{\pi}$
 $z=L \quad I_1^- = \frac{J_2}{\pi}$

$$\Rightarrow \begin{aligned} G_1 &= 2\pi(I_1^+ + I_1^-) \\ q &= 2\pi\mu_1(I_1^+ - I_1^-) \end{aligned}$$

$$\frac{dq}{dz} + G_1 - G_2 \Rightarrow \frac{dq}{dz} = 0 \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{Radiation equilibrium}$$

$$\mu_1 \frac{dG}{dz} + \frac{q}{\mu_1} = 0$$

$$G = C - \frac{1}{\mu_1^2} qz \quad \text{--- (3)}$$

IT KOOKEE NPTEL ONLINE CERTIFICATION COURSE 13

So, we have $\mu_1 \frac{dI_1^+}{dz} + I_1^+ = \frac{1}{4\pi} G$. And this will have a 1 more term for scattering. So, for the time being, we will just solve a simplified problem assuming $\omega = 0$. So, let us just solve this problem for a non-scattering case that will give us a simple solution. So, assume let us say there is no scattering. So, $\omega = 0$. Our equation now becomes simply this $\mu_1 \frac{dI_1^+}{dz} + I_1^+ = \frac{1}{4\pi} G$. Okay.

So, there will be only 1 direction. Okay. So, only 1 direction will be there for the S 2 method given by μ_1 . Similarly, the second equation can be written as $-\mu_1 \frac{dI_1^-}{dz} + I_1^- = \frac{G}{4\pi}$. This is our second equation. Okay. The boundary conditions, the boundary condition can be written as; at $z = 0$ $I_1^+ = \frac{J_1}{\pi}$ and at $z = L$, $I_1^- = \frac{J_2}{\pi}$. So, these are the boundary condition. Okay.

Now we have only 1 direction μ_1 . μ_1 is given by 0.57735. So, remember μ_1 is nothing but $\cos \theta$. Okay. So, this is a given direction. And the value of μ_1 is 0.57735. Okay. As is given in this table also. So, this value we are taking S 2 symmetric; So, there are 2 versions of second order discrete ordinate method, symmetric and non-symmetric. So, we are taking this symmetric method.

And the direction is 0.5773503. And w , the weight is 1.5707963. Okay. So, once we do that, now, let us solve this equation 1 and 2. So, we write the expression for G we derived here. Okay. So, G is = summation i is = 1 to N by $2 w_i \text{ prime } I_{i+} + I_{i-}$. And similarly, for q ; so, we write G is = $2 \pi I_1 + I_1 -$. And q is = $2 \pi \mu_1 I_1 + - I_1 -$. Okay. So, what we are trying to do is, we are trying to convert our equation 1 and 2 from I_1 to in terms of G and q . Okay.

So, once we do that, our equation is transformed as dq by $d\tau + G$ is = G . Or simply, d by $d\tau$ is = 0. So, that is radiative equilibrium. So, this is a redundant equation. Because it reiterates the statement of the problem, that is radiative equilibrium. Okay. So, this equation of no use. The second equation can be written as, $\mu_1 dG$ by $d\tau + q$ by μ_1 . q by μ_1 is = 0. Okay. So, this is our second equation. So, let us solve this.

This is simple ordinary differential equation. We can easily solve it. And we get G is = a constant $C - 1$ by μ_1 square times $q \tau$. So, this is a solution for G in terms of q of course. Okay. So, G is = C , $C - 1$ upon μ_1 square $q \tau$. Okay.

(Refer Slide Time: 26:03)

Solution



$$\begin{aligned} z=0 \quad I_1^+ &= \frac{1}{4\pi} \left(G + \frac{q}{\mu_1} \right) = \frac{J_1}{\pi} \quad \Rightarrow 3 \\ z=z_L \quad I_1^- &= \frac{1}{4\pi} \left(G - \frac{q}{\mu_1} \right) = \frac{J_2}{\pi} \quad \Rightarrow 4 \end{aligned}$$

$$\begin{aligned} @ z=0 \quad G > L \\ 4J_1 &= G + \frac{q}{\mu_1} = C + \frac{q}{\mu_1} \quad 5 \\ 4J_2 &= G - \frac{q}{\mu_1} = C - \left(\frac{1}{\mu_1^2} \right) q z_L - \frac{q}{\mu_1} \quad 6 \end{aligned}$$

Eliminate C from 5 and 6

$$\psi = \frac{q}{J_1 - J_2} = \frac{2\mu_1}{1 + \left(\frac{1}{\mu_1^2} \right) \mu_1 \frac{z_L}{2}} = \frac{2\mu_1}{1 + \frac{z_L}{2\mu_1}}$$

$$\psi = \frac{2\mu_1}{1 + \frac{z_L}{2\mu_1}}$$



14

Now, we apply the boundary condition. So, boundary condition in solving this at τ is = 0. We have $i_1 + i_s = 1$ upon $4 \pi G + q$ by μ_1 is = J_1 upon π . So, we have written the intensity in terms of G and q . So, I_{i+} and τ is = τL . The intensity I_{i-} is = 1 upon $4 \pi G - q$ upon μ_1 is = J_2 upon π . Okay. So, we have to solve for these quantities. So, let us substitute. So, this equation, let us call it equation 3 and 4. Okay.

And together with this solution G . So, we have this equation. Let us call this equation 1. We have already; let us call it 2 prime. So, substituting the value of G in the boundary condition, we can solve for q . And the unknown coefficient C . So, what we do is, we write like this: $4 J_1 = G + q \mu_1$. Substituting for G ; so, at $\tau = 0$, from this equation, at $\tau = 0$, G is simply C .

$G = C$. So, this will become $C + q \mu_1$. So, $4 J_1 = C + q \mu_1$. So, this is the 1 equation. And similarly, at $\tau = \tau_L$, we get $4 J_2 = G - q \mu_1 = C - q \mu_1$. Okay. And then, $- q \mu_1$. Okay. Now, we have obtained the final equations 5 and 6. The unknown here is q . So, we can eliminate C from 5 and 6. So, eliminate C from 5 and 6.

We can write down non-dimensional heat flux as, in terms of radiosities; q by J_1 by J_2 as $2 \mu_1$ upon $1 + \tau_L \mu_1$; be this 1 upon μ_1^2 . So, this will be 1 upon μ_1^2 , $\mu_1 \tau_L$ by 2 . Or simply this will be $= 2 \mu_1$. μ_1 is canceled. So, we have $1 + \tau_L \mu_1$ by $2 \mu_1$. Okay. So, this is the expression for the non-dimensional radiative heat flux. $\Psi = 2 \mu_1$ upon $1 + \tau_L \mu_1$.

So, this is the expression for the radiative heat flux for the case of 1-dimensional medium using the S_2 approximation. Now, how do we implement it in CFD codes. So, together with spherical harmonics method P_1 , the spherical ordinate method is one of the most popular method used in CFD codes.

(Refer Slide Time: 29:46)

Implementation in CFD Codes

$$\hat{s}_i \cdot \nabla I(\mathbf{r}, \hat{s}_i) = k(\mathbf{r})I_b(\mathbf{r}) - \beta(\mathbf{r})I(\mathbf{r}, \hat{s}_i) + \frac{\sigma_s(\mathbf{r})}{4\pi} \sum_{j=1}^n w_j I(\mathbf{r}, \hat{s}_j) \Phi(\mathbf{r}, \hat{s}_i, \hat{s}_j) \left. \vphantom{\frac{\sigma_s(\mathbf{r})}{4\pi}} \right\}$$

$$\xi_i \frac{\partial I_i}{\partial x} + \eta_i \frac{\partial I_i}{\partial y} + \mu_i \frac{\partial I_i}{\partial z} + \beta I_i = \beta S_i \quad \hat{s}_i = \xi_i \hat{i} + \eta_i \hat{j} + \mu_i \hat{k}$$

$$S_i = (1 - \omega)I_b + \frac{\omega}{4\pi} \sum_{j=1}^n w_j I_j \Phi_{ij} \left. \vphantom{\frac{\omega}{4\pi}} \right\}$$

So, many commercial packages like Ansys have implementation of spherical harmonics as well as discrete ordinates method. The accuracy of the 2 method is more or less the same. Both the methods, spherical harmonics and this discrete ordinal method give good results in optically thick case. But the accuracy is relatively low in optically thin case. Now, how do we implement?

The implementation of spherical harmonics method was relatively easy as we discussed in the previous lecture. However, the implementation of discrete ordinate method is little difficult. So, what we do is, we start again the discretized radiative transfer equation in a direction I. So, this is the radiative transfer equation in a given direction I. Now the given direction I can be written in terms of the direction cosine. Okay.

So, we write the left-hand side of this radiative transfer equation by expanding the left-hand side. We get $\xi_i \frac{\partial I_i}{\partial x} + \eta_i \frac{\partial I_i}{\partial y} + \mu_i \frac{\partial I_i}{\partial z}$, where ξ_i , η_i and μ_i are direction cosines for a given direction I. Now, we have to, this is, the second term is basically the absorption term and the right-hand side is the source term, where we have source term given by $1 - \omega I_b + \omega$ upon 4π and summed over all the discrete direction.

So, this is the summation over all the discrete directions. And Φ_{ij} is the scattering phase function. Now, what we will do is, we have to discretize the partial derivatives appearing in this equation.

(Refer Slide Time: 31:38)

Two Dimensional Finite Volume Method

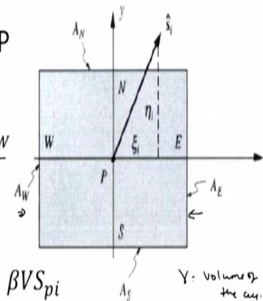
$$\frac{\partial I_i}{\partial z} = 0$$

❖ Integrating over the finite volume around P

$$\int_V \frac{\partial I_i}{\partial x} dV = \int_E I_i dA - \int_W I_i dA = I_{Ei} A_E - I_{Wi} A_W$$

❖ Governing equation

$$\xi_i (I'_{Ei} A_E - I'_{Wi} A_W) + \eta_i (I'_{Ni} A_N - I'_{Si} A_S) + \beta V I_{pi} = \beta V S_{pi}$$



So, we will take a special case of 2-dimensional method. 2-dimensional domain. The method can easily be extended to 3-dimension. Just we are understanding how it is implemented in 2-dimension. We take a special case where we have, $\frac{\partial I}{\partial z} = 0$. That means, in 2-dimensional problem, the intensity does not vary in the z direction. Because the z direction is infinite. So, the intensity will not change with respect to z direction.

And this term will be 0. Now, as we do in any finite volume scheme, we first integrate the terms over a finite volume. So, we integrate, let us say the first term $\frac{\partial I}{\partial x}$ over a finite volume. And then, we approximate using the Gauss theorem. We convert the volume integral into a surface integral. So, $\frac{\partial I}{\partial x}$ is converted into intensity $I_{i,d}$ – integration over phase w $I_{i,d} A$.

So, the intensity at any point we are interested in, the point is P. In the finite volume cell, we are interested in finding the intensity at point P. So, this $\frac{\partial I}{\partial x} dV$, that is integral over this volume, has been converted into flux of intensity at phase E. So, E represents the phase with area A_E east phase. And w represents the west phase with area A_W . And we can write down this as $I_{Ei} A_E - I_{Wi} A_W$.

Where A_E and A_W are the phase areas. And I_{Ei} and I_{Wi} are intensities averaged over these phase areas. So, over the entire phase, this the average intensity I_{Ei} and I_{Wi} . This is similar to what we do in any finite volume discretization scheme. So similarly, we can discretize the second term $\frac{\partial I}{\partial y}$. And then, we put $\frac{\partial I}{\partial z}$ as 0. And our

governing equation is now converted as, ζ_i the discretize derivative with respect to x ; η_i , discretize derivative with respect to y .

And then, integrated over the volume, the intensity at point P, I_{pi} ; so, I_{pi} is the average intensity over the volume over the finite volume, $I_{pi} = \beta \frac{1}{V} \int_V S_{pi} dV$. Where S_{pi} is again now average source term over the volume. And V is the volume of the cell. In finite volume method, V represent; so, here we have unknowns I_{Ei} , I_{Wi} , I_{Ni} , I_{Si} and I_{pi} . So, we have introduced more unknowns.

And in finite volume method, we connect this unknowns at the phase to values at the center. So, that is typically what we do in finite volume method. We connect the phase values with the phase, with the center.

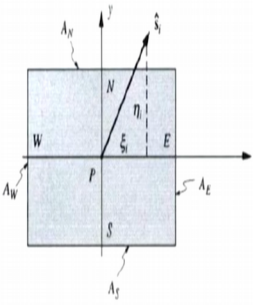
(Refer Slide Time: 34:49)

Two Dimensional Finite Volume Method

- ❖ Relating cell edge intensity to volume averaged intensity
 - ❖ Linear scheme (Diamond scheme)

$$\frac{1}{2}(I_{Ei} + I_{Wi}) = \frac{1}{2}(I_{Ni} + I_{Si}) = I_{pi}$$
- ❖ Governing equation

$$\int_V \frac{\partial I_i}{\partial x} dV = \int_E I_i dA - \int_W I_i dA = I_{Ei}A_E - I_{Wi}A_W$$



So, we can take a linear scheme. In linear scheme, we connect; this phase is in the x direction I_{Ei} and I_{Wi} . So, average of these 2 intensities is nothing but the intensity at the center. And similarly, North and South intensities are related to the cell center well intensity using an average value. This particular interpolation scheme in finite volumes method; we call it interpolation scheme.

This particular interpolation scheme is linear and it is called diamond scheme in radiative transfer. So, this is called diamond scheme, where we are interpolating the intensities linearly. Okay. So, our governing equation now has become relatively simplified. And we can easily

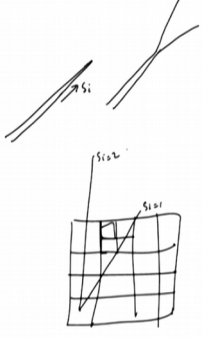
implement this in any finite volume framework. We have to repeat this for all the directions. So, what we have discussed is, in a given direction.

But, this we have to repeat for all the discrete directions. So, in a sense, we are implementing the finite volume method in space. But, we are implementing finite difference method in angular direction. We can also implement finite volume method in a angular space. Then, the method is called finite volume method, rather than the discrete ordinate method. The finite volume method of radiative transfer discretize the angular directions also in finite volume schemes.

(Refer Slide Time: 36:17)

Limitations

- ❖ False Scattering:
 - ❖ Spatial discretization error
 - ❖ Single collimated beam gradually widens (smear)
- ❖ Ray effect:
 - ❖ Angular discretization
 - ❖ Energy transfer occurs in discrete directions only
 - ❖ Some cells do not receive radiation



IT KOOBEE NPTEL ONLINE CERTIFICATION COURSE 18

There are certain limitations of this method such as false scattering and ray effect. And this is again what we observe in a typical finite volume method. False scattering is analogous to numerical diffusion in finite volume schemes. So, it is a result of spatial discretization error. Because we have approximated our phase center intensities with cell center intensities. We have assumed that the intensity is averaged over the phase.

So, we get spatial discretization error on intensity. And this is called false scattering. Now, how it basically looks like. We have let us say a pencil of rays in a discrete direction S_i . Now, as this ray move, it will basically smear out. That means, it will scatter the radiation. So, we will have some kind of scattering effect in the radiation. So, the wave or the ray will kind of widens. It will smear in angular direction. It will not be sharp.

It will basically smear in the angular direction. It will not be confined to small solid angle, rather it will be smeared over a range of solid angles. So, this is called false scattering. Similarly, where we have a discretization error in angular direction. In angular direction, we have used finite difference method. And there are only discrete directions. So, let us take a 2-dimensional case.

We are interested in finding how the radiation is transferred between 1 cell to another. Let us say there is 1 ray we are modelling in a direction S_i . Okay. So, what we see is, if this cell is let us say divided into 4 cells, this cell is not touched by this intensity. Because it is only in discrete directions. Okay. So, let us say this is $S_i = 1$ and this is $S_i = 2$. The angular directions that we are discretizing.

So, there may be some cells in the region which are not basically touched by or affected by the discrete intensity directions. Okay. So, this is called angular discretization error. And it is called ray effect. Okay. Because the energy transfer is taking place in discrete directions only, some cells do not receive radiation. And we get some kind of error. Now, definitely this error can be minimized if we increase the number of directions.

That is, more number of points in finite difference scheme results in smaller error. Same thing we can do here also. Or we can go for finite volume method, where the ray effect is minimized. So, this is all on the discrete ordinate method, is a powerful method and finds lot of applications in a radiative transfer in combustion. Many commercial packages come with this method.

In the next lecture, we will discuss the zone method, which is not a solution method for radiative transfer equation, but rather is based on principle of energy conservation. Thank you for your time. We will continue in the next lecture.