

Automatic Control
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Lecture – 35
Controller Design and Controllability

So, welcome to the lecture on State Space Method. In this lecture we will discuss a problem related to controller design and about controllability.

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NUMERICAL EXAMPLE

- Given the plant, $G(s) = \frac{20(s+5)}{s(s+1)(s+4)}$
- Design the phase variable feedback gains to yield **9.5 %** overshoot and a settling time of **0.74** second.

Ref. N. S. Nise: Control Systems Engineering, 6th Ed., Wiley, 2013

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So, we discussed this problem that we are given a plant that is $G(s)$ equal to $\frac{20(s+5)}{s(s+1)(s+4)}$ and we design the phase variable feedback gains to yield 9.5 percent overshoot and a settling time of 0.74 second.

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$G(s) = \frac{20(s+5)}{s(s+1)(s+4)} = \frac{20s+100}{s^3+5s^2+4s}$

Design $\zeta = 0.74$ overshoot
 $T_s = 0.74 \text{ sec}$

$\zeta = \frac{\sigma}{\omega_n} = \frac{4}{5.4} = 0.74$
 $\sigma = 5.4 = \zeta \omega_n$

$\xi = \frac{-\ln(1/0.01)}{\sqrt{\pi^2 + \ln^2(1/0.01)}}$
 $= 0.6$

$\omega_d = \omega_n \sqrt{1-\zeta^2}$
 $= \frac{5.4}{0.6} \sqrt{1-0.6^2}$
 $= 7.2$

$R(s) \rightarrow G(s) \rightarrow C(s)$

$s^3 + 5s^2 + 4s = 0$
 $s^3 + a_2s^2 + a_1s + a_0 = 0$

$a_2 = 5$, $K = [k_1 \ k_2 \ k_3]$
 $a_1 = 4$
 $a_0 = 0$

$A - BK = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -k_1 & -(4+k_2) & -(5+k_3) \end{bmatrix}$

$y = [100 \ 20 \ 0] x$

$s^3 + (5+k_3)s^2 + (4+k_2)s + k_1 = 0$

So, we were discussing that we have this transfer function $G(s)$ and we have this is the characteristic equation. So, we have this equation that is $s^3 + 5s^2 + 4s = 0$. Now, we can write this as $s^3 + a_2s^2 + a_1s + a_0 = 0$. So, if we compare this we will find the coefficients of this a_2 , a_1 , a_0 .

So, here $a_2 = 5$, $a_1 = 4$ and $a_0 = 0$; so we have the system if we represent this system in the state space we can write $\dot{x} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -4 & -5 \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$ and here we can write reverse order with negative signs which is 0 and this is minus a_1 . So, minus 4 and this is minus a_2 . So, minus 5 , this is matrix A . So, $Ax + Bu$. So, B matrix we have $0 \ 0 \ 1$ and u and here $y = [100 \ 20 \ 0] x$. So, we know that C matrix we can write these by these coefficients.

Now, if we write $A - BK$ matrix. So, $A - BK$ because we assume that there are. So, we there are 3 coefficients a_2 , a_1 and a_0 . So, we need 3 K value. So, $K = [K_1 \ K_2 \ K_3]$. So, here we have K . So, here we have K that is equal to K_1 , K_2 , K_3 . Now, this matrix we can write. So, $A - BK$. So, we can write this as equal to. So, this is 3 by 3 matrix. So, $0 \ 1 \ 0 \ 0 \ 0 \ 1$ and this will be minus. So, here we will have K_3 sorry K_1 minus K_1 because here it is minus a_0 plus K_1 . So, a_0 is 0 . So, it is minus K_1 minus K_1 plus K_2 , so, 4 plus K_2 and minus 5 plus K_3 . So, this is $A - BK$.

Now, the characteristic equation that is this will be changed. So, it is like $s^3 + 5s^2 + 4s = 0$ now here we will have $5 + K_3s^2 + 4 + K_2s + K_1$ that is equal to 0 , this is

the new characteristic equation. Now, what is the design requirement? This is the design requirement. So, we have got two equations this is the first equation and this is the second equation.

So, this is the initial system and this is system we want. So, we want the values of K 1, K 2, K 3, ok. So, we have to select K 1, K 2, K 3 to obtain what objective these objective. So, here we have T s equal to 0.74. So, we know that here T s equal to pi sorry 4 upon sigma d or zeta omega n sigma d or 4 upon zeta omega n. So, that is 0.74. So, we can find sigma d equal to 5.4 or zeta omega n equal to 5.4.

Now, we have percentage overshoot we have to find the damping. So, damping is equal to. So, we have if we are given percent overshoot we can find a damping from here and we have percent overshoot 9.5. So, we put 9.5 and we will get the value of damping equal to 0.6 and here this is zeta omega n. So, here we can also find omega n and omega d equal to omega n root 1 minus zeta square and omega n equal to sigma d upon damping that is 0.6 into root 1 minus 0.6 square. So, we get omega d equal to 7.2.

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Handwritten mathematical derivation for a control system design problem. The derivation includes the following steps:

- Given parameters: $\zeta = 5.4$, $\omega_n = 7.2$
- Pole locations: $s_{1,2} = (5.4 \pm j7.2)$, $s_3 = -5.1$
- Characteristic equation: $C(s) = \frac{20(s+5)}{s^3 + 5s^2 + 4s}$
- State-space representation: $X = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -4131 & -136.08 & -15.9 \end{bmatrix} X + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$
- Output equation: $y = [100 \ 20 \ 0] X$
- Transfer function: $T(s) = \frac{20(s+5)}{s^3 + 15.9s^2 + 136.08s + 4}$
- Characteristic equation for desired poles: $(s-5)(s-5-j7.2)(s-5+j7.2)(s+5.1) = 0$
- Expanded characteristic equation: $(s^2 + 10.8s + 81)(s+5.1) = 0$
- Final characteristic equation: $s^3 + 15.9s^2 + 136.08s + 413.1 = 0$ (ii)
- Comparison of coefficients to find gains:
 - $5 + k_3 = 15.9 \Rightarrow k_3 = 10.9$
 - $4 + k_2 = 136.08 \Rightarrow k_2 = 132.08$
 - $k_1 = 413.1 \Rightarrow k_1 = 413.1$
- Final characteristic equation with gains: $s^3 + (5+k_3)s^2 + (4+k_2)s + k_1 = 0$ (ii)

So, now, we obtain that that we have this sigma d equal to 5.4 and omega d equal to 7.2 it means we to obtain 9.5 percent overshoot and damping equal to. So, that equivalent to damping equal to 0.6 and settling time equal to 0.7 for we need to put the poles at this real part and this imaginary part. So, we want to put this poles here somewhere. So, that we have this is omega d and this is sigma d omega d into j. So, we have 5.4 plus minus j

7.2. So, these are the two poles, where they are the two poles because this system has a cube. So, they are total three poles out of three the two poles complex poles would be this.

So, we have here let us say s_1 and s_2 equal to this now what about s_3 . So, the third pole where should I put. So, we know that here we have $G(s)$ equal to $s^2 + 10s + 5$ upon this system that is. So, this 0 is at 5. So, if we put the third pole near to this 0 the pole 0 cancellation will take place and therefore, the higher order pole will not affect the response of the dominant poles.

So, therefore, let us put this third pole at near 5. So, let us say 5.1. So, now, what should be the resulting equation we have $(s - \sigma_1)(s - \sigma_2)(s - \sigma_3) = 0$. So, this should be the characteristic equation if we have three poles, so, $(s - 5.4 + j7.2)(s - 5.4 - j7.2)$ and here $(s - 5.1)$. So, this is the characteristic equation. This is the desired characteristic equation because we this is the other desired pole locations. So, now, if we solve this equation we will obtain this equation as. So, we can have $(s - 5.4 - j7.2)$ and this is $(s - 5.4 + j7.2)$ and this is $(s - 5.1)$ equal to 0.

So, this we can write $(s - 5.4)^2 + 7.2^2$ into $(s - 5.1)$ that is equal to 0 and so, here we can obtain this as $s^2 + 10.8s + 81$ into $(s - 5.1)$. So, sorry this is plus because here this is minus 1, we are putting at negative side because here the 0 is at s equal to minus 5. So, this s^3 is minus 5.1. So, we have here $(s - 5.1)$. So, it is plus. So, $(s + 5.1)$ that is equal to 0. So, we finally, obtain this as $s^3 + 15.9s^2 + 136.08s + 413.1 = 0$.

So, this is equation number third, let us say now, this is the desired characteristic equation because you that will put the poles at these locations and this is also the desired characteristic equation that will set these values of K_1 , K_2 , K_3 to put the poles at the desired location. So, these two equation can be compared and we can find the values of K_1 required values of K_1 , K_2 , K_3 that will put these poles put the system at this locations.

So, we compare these coefficients. So, here if we compare s^2 so, $5 + K_3$ equal to 15.9 and $4 + K_2$ equal to 136.08 and K_1 equal to 413.1. So, from here we can

obtain that K_3 equal to 10.9 from here we can obtain K_2 equal to 132.08 and the K_1 equal to 413.1 and here we have the 0 is the same.

So, now, what is the new system. So, here the new equation is \dot{X} equal to Ax . So, $\begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}$ and here we have. So, minus 413.1 minus 136.08 and minus 15.9 into x plus $\begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} u$ and y equal to Cx and the transfer function because this is the characteristic equation we can write transfer function. So, transfer function is $\frac{20s + 5}{s^3 + 15.9s^2 + 136.08s + 413.1}$ upon here we have this is the characteristic equation. So, we can write $s^3 + 15.9s^2 + 136.08s + 413.1$. So, these are the systems. So, this is in the state space we have obtained this system and we have obtained the values of feedback gains that will be feedback and they will put all the 3 poles at desired location.

So, here we have taken this third pole at minus 5.1. We can also select this value may be very higher. So, we can put this pole at very far from the dominant real part of the dominant pole maybe at s^3 equal to 30 or 50 and we can find the value of gains that will corresponding this value. So, we can put the poles all these system poles at the desired locations. Here we applied the pole 0 cancellation, but here we could say that condition that the pole third pole is very far. So, it is not affecting much to the dominant poles response and this is the transfer function. So, the system is the same we have two different representation one is a transfer function that is the frequency domain approach and this is the time domain approach that is state space. So, now, we have discussed for these systems how to find this.

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CONTROLLABILITY

- If an input to a system takes every state variable from a desired initial state to a desired final state, the system is said to be controllable; otherwise the system is uncontrollable
- To control the pole location of the closed-loop system, we say that the control signal, u , can control the behavior of each state variable in x
- If any one of the state variable cannot be controlled by u , then we cannot place the poles of the system where we desire
- A system with *distinct eigenvalues* and a *diagonal system matrix* is controllable if the input coupling matrix B does not have any rows that are zero

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So, now, we will discuss the concept of controllability. So, when we define the state variables. So, we said that the state variable is takes the system from one state to other when we apply some input or initial conditions. So, if we input to a system takes every state variable from a desired initial state to some desired final state then the system is said to be controllable. If there is no effect of input on any state variables means if we are giving input, but the state variable is not affected or it is not changed. So, it means the system is uncontrollable. Therefore, to control the pole location because we were trying to place the poles at desired location.

So, if we want to do this we are controlling the pole location of the closed loop system by giving some input you are giving some feedback gain as an input. So, if we say that the control signal u we want to through this control signal if we want to control the pole location, so that we can control the behavior of each state variable in x . If any of the state variable cannot be controlled by u , then we cannot place the poles of the system where we desire.

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$$\begin{Bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{Bmatrix} = \begin{bmatrix} -a_1 & 0 & 0 \\ 0 & -a_2 & 0 \\ 0 & 0 & -a_3 \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \\ x_3 \end{Bmatrix} + \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} u$$

$$\dot{x}_1 = -a_1 x_1 + u$$

$$\dot{x}_2 = -a_2 x_2 + u$$

$$\dot{x}_3 = -a_3 x_3 + u$$

$$\dot{x} = \begin{bmatrix} -a_1 & 0 & 0 \\ 0 & -a_2 & 0 \\ 0 & 0 & -a_3 \end{bmatrix} x + \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} u \Rightarrow \begin{matrix} \dot{x}_1 = -a_1 x_1 \\ \dot{x}_2 = -a_2 x_2 + u \\ \dot{x}_3 = -a_3 x_3 + u \end{matrix}$$

So, for example, we let us take some system like. So, which we have this system \dot{x} equal to minus a 1 0 0, 0 minus a 2 0, 0 0 minus a 3 x plus 1 1 1 u. Now, what is this system? So, if let us say here we write this x_1 , x_2 , x_3 . So, here we can write \dot{x}_1 equal to minus a 1 x_1 plus u here we can write \dot{x}_2 because here it is \dot{x}_1 dot \dot{x}_2 dot and \dot{x}_3 dot. So, here \dot{x}_2 we can write minus a 2 x_2 plus u, then \dot{x}_3 dot equal to minus a 3 x_3 plus u.

So, here we see that if we are giving the input we are getting the state variable is affected by this input, because they are function of u. So, here we can say that the system is controllable because each state variable is getting affected and by the input u. Now, we take another system let us say \dot{x} equal to minus a 4 0 0 0 minus a 5 0 0 0 minus a 6 and here we have 0 1 1 and here is u. Now, if we want to write this equation we can write \dot{x}_1 dot equal to minus a 4 x_1 \dot{x}_2 dot equal to minus a 5 x_2 plus u and \dot{x}_3 dot equal to minus a 6 x_3 plus u. So, here we see that this state variable is not affected from the input. So, x_1 is not controlled by input u and therefore, this state variable is not affected by u and so, the system is uncontrollable.

So, here we see that the system is have distinct Eigenvalues because there that is a diagonal element. So, the Eigenvalues are distinct and so, we can say that a system with distinct Eigenvalues and a diagonal system matrix is controllable if the input coupling matrix b does not have any rows that are 0. So, if we have this kind of system diagonal

system we have if any row of this b matrix because this is b. So, b matrix is 0 then the system is uncontrollable. However, if we have the repetitive poles then if the system has multiple poles it does not have distinct poles, then how to find the controllability of a system. So, there the controllability is defined.

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Controllability Matrix

$$C_M = [B \quad AB \quad A^2B \quad \dots \quad A^{n-1}B]$$

$[A]_{n \times n}$ $\text{Rank}(C_M) = n \rightarrow \text{controllable}$
 $\neq n \rightarrow \text{Uncontrollable}$

$$\dot{x} = \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -2 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix} u$$

So, to find controllability of such a system we have to find the controllability matrix. So, we call it a controllability matrix C_m and C_m equal to $B \ AB \ A^2B$ and here it is $A^{n-1}B$ and if the system is of n th order, so, if our matrix A is n by n matrix. So, our system is of n th order so, the rank of C_m equal to n . So, it is controllable otherwise it is not equal to n then it is uncontrollable. So, for any system we can use this method to find the controllability. So, first we calculate the controllability matrix. So, let us take one example. So, if we have a system like \dot{x} equal to $\begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -2 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix} u$.

Now, we can see that the here at multiple poles at minus 1. So, now, we calculate the C_m .

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Controllability Matrix

$$C_M = [B \quad AB]$$
$$[A]_{n \times n}$$
$$\dot{x} = \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -2 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix} u$$

\downarrow 3×3 \downarrow B
A B

$$A^2 B = \begin{bmatrix} 0 & 1 & -2 \\ 1 & -1 & 1 \\ 1 & -2 & 4 \end{bmatrix}$$

AA

$$|C_M| = -1$$
$$\text{Rank} = 3$$

Controllable matrix

So, we have to calculate the C m. So, this we have to calculate. So, here B is now we can complete this. So, B is this. So, this is A that is 3 by 3. So, A and this is B. So, here we have B 0 1 1 now we calculate A B. So, A into B we can calculate. So, we multiply this A matrix to B matrix and we will get 1 minus 1 minus 2 and when we calculate A square B we have to first calculate A into A and then we calculate this into B. So, we can get A square B. So, A square B we calculate we will get minus 2 1 4. So, so, determinant the C m equal to minus 1 and this rank is 3 because this is it is rank is 3 and that is equal to the order of the system that is n. So, this is controllable matrix. So, here just by saying this row we cannot say because here the first row of the B matrix was 0, but the session is controllable.

So, the examples discussed in this lecture were taken from the book of Norman S. Nise, Control Systems Engineering. So, I thank you for attending this lecture and let us see in the next lecture.

Thank you.