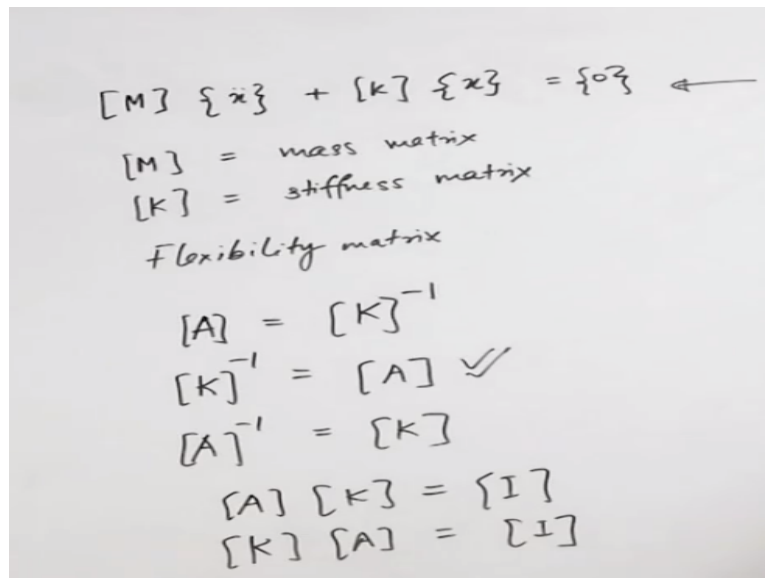


Introduction to Mechanical Vibration
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Lecture - 38
Flexibility Influence Coefficients

So welcome to the lecture on multi-degree of freedom system. We will discuss today the flexibility influence coefficients. So what is flexibility as flexibility is reciprocal of the stiffness and we know that in any vibrating system, we have mainly three elements spring, mass and damper system. So for spring, mass system that is undamped multi-degree of freedom system, we have already derived the equation of motion that comes into the form of a matrix.

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Handwritten notes on a slide:

$$[M] \{\ddot{x}\} + [k] \{x\} = \{0\} \leftarrow$$

$[M]$ = mass matrix
 $[k]$ = stiffness matrix
Flexibility matrix

$$[A] = [k]^{-1}$$
$$[k]^{-1} = [A] \checkmark$$
$$[A]^{-1} = [k]$$
$$[A] [k] = [I]$$
$$[k] [A] = [I]$$

So the equation of this motion that is $M \ddot{x} + kx = 0$ and here I said that this M is mass matrix and here this k is stiffness matrix. Now what is the flexibility matrix? So here because flexibility is inversely proportional that is the reciprocal of the stiffness. So here the flexibility matrix let us say A that is equal k inverse and similarly k inverse = A or A inverse = k .

So here we can also write that A into k that is equal to an identity matrix or k into A is equal to identity matrix. So here we have this equation $M \ddot{x} + kx = 0$.

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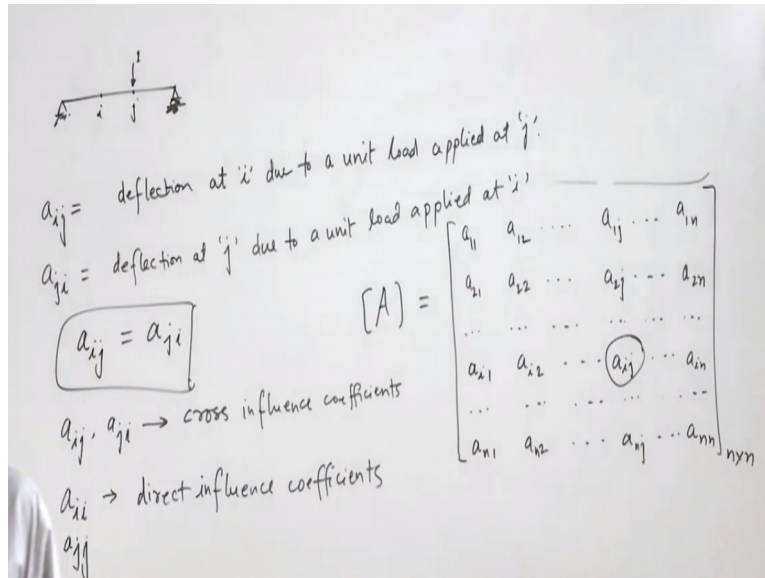
$$\begin{aligned} & \leftarrow [K]^{-1} [M] \{\ddot{x}\} + [K]^{-1} [K] \{x\} = \{0\} \\ & [A] [M] \{\ddot{x}\} + \{x\} = \{0\} \\ & [A] = \begin{bmatrix} a_{11} & a_{12} & \dots & a_{1j} & \dots & a_{1n} \\ a_{21} & a_{22} & \dots & a_{2j} & \dots & a_{2n} \\ \dots & \dots & \dots & \dots & \dots & \dots \\ a_{i1} & a_{i2} & \dots & a_{ij} & \dots & a_{in} \\ \dots & \dots & \dots & \dots & \dots & \dots \\ a_{n1} & a_{n2} & \dots & a_{nj} & \dots & a_{nn} \end{bmatrix}_{n \times n} \end{aligned}$$

Now we multiply with k inverse so we will have k inverse M x double dot + k inverse k x = 0. Now here k inverse is we can write the flexibility matrix so this is A m x double dot + here k inverse into k is i and when we multiply i with x it is x so that is 0. So finally our equation of motion results to b in the form of mass matrix and flexibility matrix. So therefore if we can make we can prepare the flexibility matrix.

We can also write the equation of motion directly using the flexibility matrix. So flexibility matrix A has its coefficients. So here we have like a₁₁, a₁₂, a_{1j}, a_{1n}, if it is n into n; here a₂₁, a₂₂, a_{2j}, a_{2n}; we have here a_{i1}, a_{i2}, a_{ij}, a_{in}; here we have a_{n1}, a_{n2}, a_{nj}, a_{nn}. So we have this is n into n matrix that is flexibility matrix and the elements of this matrix are known as flexibility influence coefficients.

So if we take this a_{ij}, one element a_{ij}, so how we will define this a_{ij} and how we will obtain a_{ij} because if we know all these elements we can prepare a flexibility matrix for that problem. Now a_{ij} means what? So we will define here a_{ij}.

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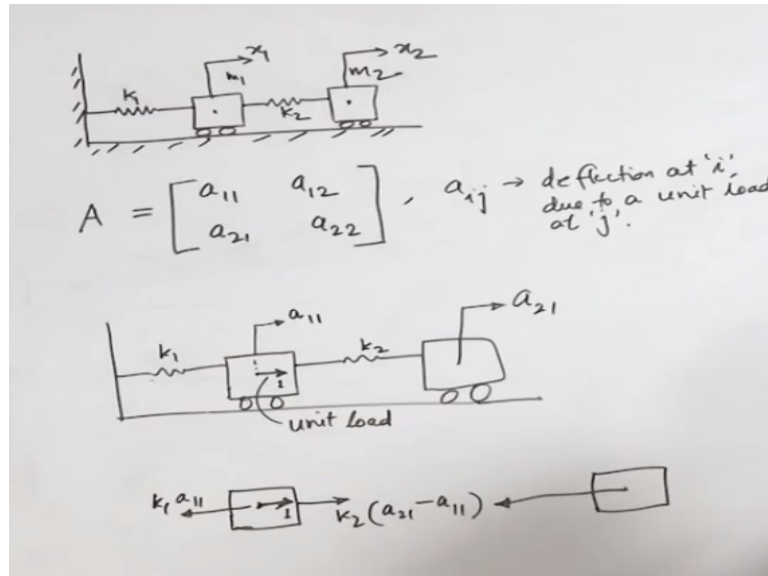


So suppose we have some member here and here are two points that is i and j. So a_{ij} is defined as the value of deflection at i due to a unit load applied at j. So if we have this flexibility influence coefficient a_{ij} defined as the deflection at i when we apply a unit load j at j that is unit load and we measure what is the deflection that is coming here and that is a_{ij} . Similarly, a_{ji} is the deflection at j due to a unit load applied at i, so here we are applying a unit load at i and measuring deflection at j.

So now the Maxwell's reciprocal theorem states that this $a_{ij} = a_{ji}$. So it means that the deflection at i due to unit load at j is equal to the deflection at j due to unit load at i. Now here we have a_{ij} , a_{ji} and we have also a_{ii} so ii means we have the deflection at i and unit load at i so at the same point. So we are applying the load at the same point unit load and measuring the deflection at the same point so a_{ii} are a_{jj} .

So these are called the direct influence coefficients and these are called the cross influence coefficients. Now as we have defined what is the flexibility matrix? What are the flexibility influence coefficients? Now if we want to prepare this flexibility, how we will do it. So I take one example and we can apply these rules that we have already studied these equilibrium equations and we will find these coefficients.

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So now we take one problem and we try to derive these flexibility coefficients. So here we have two degree of freedom system and comprising the two masses m_1 and m_2 and two stiffness elements that is k_1 and k_2 . We assume that the surface on which these masses are resting, the friction is negligible or 0. So we are not considering the friction. And now we have to find the flexibility matrix.

So because we have this two degree of freedom system, so our flexibility matrix will be square matrix having 2 into 2. So we will have A , the flexibility matrix that is having a_{11} and a_{12} and a_{21} and a_{22} . So now we have to find the values of these coefficients and so we will find the flexibility matrix. So now if we want to find this a_{11} , a_{21} so let us now we do like this. So now what we are doing because the flexibility coefficients are defined as the deflection, so a_{ij} is defined as deflection at i due to a unit load at j .

So it means, we have to apply a unit load at one point and measure the deflection at other points. So if I apply here so this is one and this is two so this is first mass, so I apply a unit load here like this so this is unit load. So this is unit load here. And now I want to measure the deflection so deflection here and deflection here so what will be deflection here that will be a_{11} .

Because I am applying a unit load at 1 and I am measuring deflection at 1 so I am applying the load at j so here $i = j$ is 1. Now what will be the displacement at mass two, so I am applying load 1 so here I am applying and measuring at 2 so a_{21} so I am applying load at 1

and measuring deflection at 2. Now we have to make the free body diagram to find the equilibrium equations.

So here we have this mass first mass and this first mass we have load here unit load then because we have some deflection here we will have spring force here that is k_1 because this is k_1 and this is k_2 . So k_1 into a_{11} because a_{11} is the deflection and k_1 is the stiffness. So the spring force acting due to the movement is k_1 into a_{11} in the opposite direction. Now there is spring k_2 and this will apply a force, so k_2 into this is moving a_{21} this is a_{11} .

So here $a_{21} - a_{11}$ so the net force that is due to spring is the relative displacement of this spring so that is a_{21} if we assume greater than a_{11} . So $a_{21} - a_{11}$ into k_2 . Now on the second mass, we have to make this free body diagram of this mass so this mass is m_2 . On this mass we do not have any external load as in this case we have unit load. So this mass is only subjected to force due to the spring k_2 and that is the same magnitude, but the direction is opposite one.

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Handwritten derivation of equilibrium equations for a two-mass spring system:

$$\begin{aligned}
 k_1 a_{11} - 1 - k_2 (a_{21} - a_{11}) &= 0 \quad \text{--- (i)} \\
 k_2 (a_{21} - a_{11}) &= 0 \quad \text{--- (ii)} \\
 \text{from Eq. (ii)} \\
 a_{21} &= a_{11} \quad \text{--- (iii)} \\
 \text{From Eq. (i)} \\
 k_1 a_{11} - 1 - k_2 \cdot 0 &= 0 \\
 k_1 a_{11} - 1 &= 0 \\
 k_1 a_{11} &= 1 \\
 \Rightarrow a_{11} &= \frac{1}{k_1} \\
 \text{From Eq. (iii)} \quad a_{21} &= a_{11} = \frac{1}{k_1}
 \end{aligned}$$

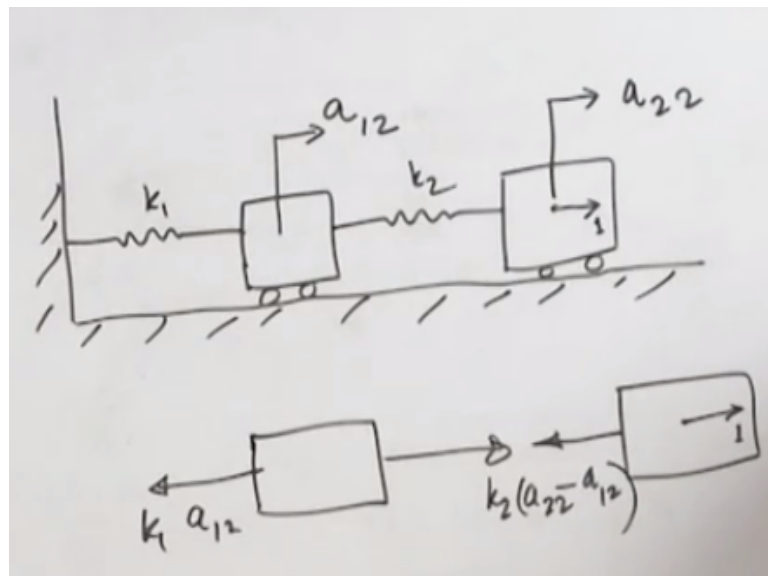
So now we have to balance these equations so for this equation number one, these two forces in this one direction and this is opposite direction. So we will have $k_1 a_{11} - 1 - k_2 a_{21} - a_{11} = 0$. So the net total sum of the forces are 0. Similarly, for the second mass, we will have $k_2 a_{21} - a_{11}$ so only this force and so that is equal to 0. So from this equation so this is equation number one and this is equation number two.

So from equation number two, we will have $a_{21} = a_{11}$ because here this is 0 and k_2 cannot be 0 because it is finite stiffness of this spring two and therefore we will have $a_{21} = a_{11}$, let us say this is equation number three. Now from equation number one, $k_1 a_{11} - 1 - k_2$ into $a_{21} - a_{11}$, $a_{21} - a_{11}$ is 0 so into 0 and equal to 0. So we will have $k_1 a_{11} - 1 = 0$. This means $k_1 a_{11} = 1$ and this implies that $a_{11} = 1$ by k_1 .

So we have got this influence coefficient a_{11} that is when the unit load is applied at one and the displacement is being measured at 1. Now from equation three, we have $a_{21} = a_{11}$ and therefore it is also equal to 1 by k_1 . So we have got the second influence coefficient a_{21} that is when the load is applied at 1 and displacement is measured at 2 and they are equal. So we have got these two influence coefficients.

Now we have other coefficients that we need to find out and therefore we will apply the similar process. So now in the previous case, we applied a unit load at 1, now we will apply a unit load at mass two.

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So we will have this spring k_1 k_2 and this is mass m_1 and m_2 . Now in this case, we are applying a unit load here so let us we apply a unit load here and we measure the deflection at other places. So here deflection at this place will be a_{22} means we are applying a load at mass two and we are measuring deflection at two and this one will be a_{12} . So we are applying unit load at 2 and measuring the deflection at 1.

Now we make the free body diagram of this load system. So we will have this first mass, so we will have and this is the second mass. So on the second mass, we have this unit load + this is spring force so we will have this spring force k_2 into $a_{22} - a_{12}$. So this is k_2 into $a_{22} - a_{12}$ and similarly this force will also work on this mass because the spring is connected to both, only the direction will be different. Now we have here due to a_{12} movement, there will be a force k_1 into a_{12} .

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$$\begin{aligned}
 k_1 a_{12} &= k_2 (a_{22} - a_{12}) \quad \text{---(i)} \\
 k_2 (a_{22} - a_{12}) &= 1 \quad \text{---(ii)} \\
 a_{22} - a_{12} &= \frac{1}{k_2} \\
 k_1 a_{12} &= k_2 \cdot \frac{1}{k_2} = 1 \\
 \Rightarrow a_{12} &= \frac{1}{k_1}
 \end{aligned}$$

Now we apply the equilibrium equations, so here $k_1 a_{12} = k_2 a_{22} - a_{12}$, this is equation number one and then for this $k_2 a_{22} - a_{12} = 1$. So here $a_{22} - a_{12}$ so this is equation number two and from here we will get 1 by k_2 , this $a_{22} - a_{12}$. Now we put this value $a_{22} - a_{12}$ into this equation number one, so this $a_{22} - a_{12}$, so we write $k_1 a_{12} = k_2$ into $a_{22} - a_{12}$ is 1 by k_2 and so this will cancel out and it is equal to 1 .

So this implies $a_{12} = 1$ by k_1 . So we have got this influence coefficient a_{12} when a unit load is applied at 2 and we are measuring deflection at 1 .

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From Eq (ii)

$$k_2 (a_{22} - \frac{1}{k_1}) = 1$$

$$a_{22} = \frac{1}{k_2} + \frac{1}{k_1}$$

$$a_{22} = \frac{k_1 + k_2}{k_1 k_2}$$

Now we put the value of a_{12} in equation number two so from equation two, if we put this value a_{12} here so $k_2 a_{22} - 1 \text{ by } k_1 = 1$. So now we will have $a_{22} = 1 \text{ by } k_2 + 1 \text{ by } k_1$ and so it is $k_1 + k_2 \text{ upon } k_1 k_2$. So this is another influence coefficient.

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$$a_{21} = a_{12} = \frac{1}{k_1}$$

$$a_{11} = \frac{1}{k_1}$$

$$a_{22} = \frac{k_1 + k_2}{k_1 k_2}$$

So we know that from the reciprocal theorem, $a_{21} = a_{12}$ and so that is we see a_{12} is $1 \text{ by } k_1$ and a_{21} is $1 \text{ by } k_1$. So even if we know from here a_{21} , we do not need to calculate a_{12} , we already can use this as the value of a_{12} and here $a_{11} = 1 \text{ by } k_1$ and $a_{22} = k_1 + k_2 \text{ by } k_1 k_2$.

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$$[A] = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}, a_{ij}$$
$$[A] = \begin{bmatrix} \frac{1}{k_1} & \frac{1}{k_1} \\ \frac{1}{k_1} & \frac{k_1 + k_2}{k_1 k_2} \end{bmatrix}$$

So now we know all the elements of this matrix so we can write this matrix, so $A = a_{11}$ that is $1/k_1$ and a_{12} that is $1/k_1$ and a_{21} is also $1/k_1$ and a_{22} is $(k_1 + k_2)/k_1 k_2$. So this is the flexibility matrix that we can obtain. So I stop here and I thank you for attending this lecture, see you in the next lecture.