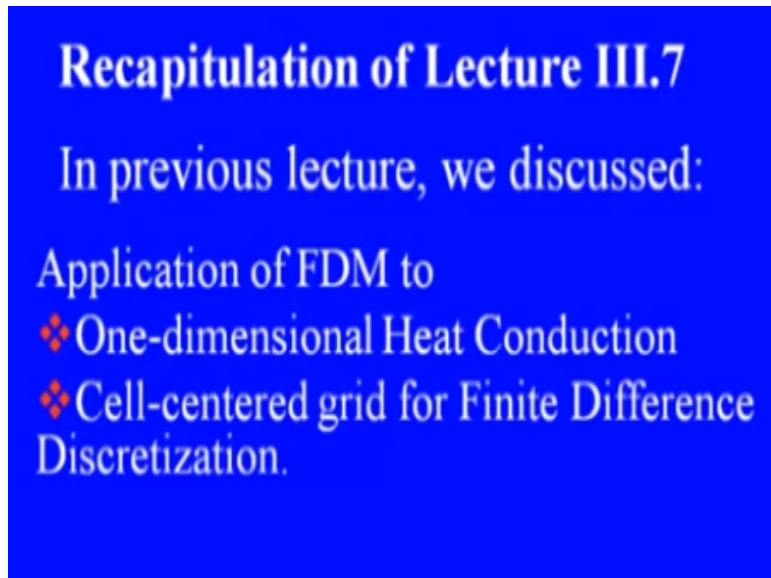


Computational Fluid Dynamics
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Lecture – 17
Applications of FDM to Scalar Transport Problems-2

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A blue rectangular slide with white text. The title 'Recapitulation of Lecture III.7' is at the top. Below it, the text 'In previous lecture, we discussed:' is followed by 'Application of FDM to' and then a bulleted list with two items: '❖ One-dimensional Heat Conduction' and '❖ Cell-centered grid for Finite Difference Discretization.'

Recapitulation of Lecture III.7

In previous lecture, we discussed:

Application of FDM to

- ❖ One-dimensional Heat Conduction
- ❖ Cell-centered grid for Finite Difference Discretization.

Welcome once more to our lectures based on application of finite difference method to scalar transport problems. This is our module outline and we had been working on the last topic that is applications of finite difference method to scalar transport problems. In the previous lecture, we discussed application of our difference to one dimensional heat conduction which was based on what we call node or a vertex centered finite difference formulae.

We introduced a cell centered grid for finite differences discretization and we looked at how do we modify the boundary conditions? The boundary conditions have to be taken care of by what we is called ghost cell, we have to incorporate ghost cells from ghost nodes, to incorporate boundary conditions, we did one part that is the incorporation of the Dirichlet boundary conditions and in this lecture this where we are going to continue form.

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LECTURE OUTLINE

- ❖ Cell-centered grid for Finite Difference Discretization (continued)
- ❖ Application of FDM to
 - ❖ Two-dimensional Heat Conduction
 - ❖ Transient Heat Conduction
 - ❖ Advection-diffusion Problem
- ❖ Computer Implementation Aspects

So, this is our second lecture in applications of domain, over all lecture 8 and 5 difference application of FDM to scalar transport problems, part 2, so we will continue with our cell centered grid for finite difference discretization from where we left in the previous lecture and then you would have a look at application of finite difference method to 2 dimensional heat conduction, then transient heat conduction and advection diffusion problem.

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One Dimensional Heat Conduction

Let us consider steady state heat conduction in a slab of width L with thermal conductivity k and heat generation. Governing equations and boundary conditions are:

$$k \frac{\partial^2 T}{\partial x^2} + q_g = 0$$

$$T(0) = \bar{T}$$

$$-k \left. \frac{dT}{dx} \right|_{x=L} = h(T - T_a)$$

If time permits, we will take up the computer implementation aspect in this lecture, so now let us get back to what we were doing in last class, we wanted to solve it using finite difference this one dimensional heat conduction problem with heat generation, so the governing equation for $k \frac{\partial^2 T}{\partial x^2} + q_g = 0$. At the left edge of the slab, that is at $x=0$, we had temperature specified and we saw in footway, we can incorporate this temperature specified our Dirichlet boundary condition.

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... One Dimensional Heat Conduction

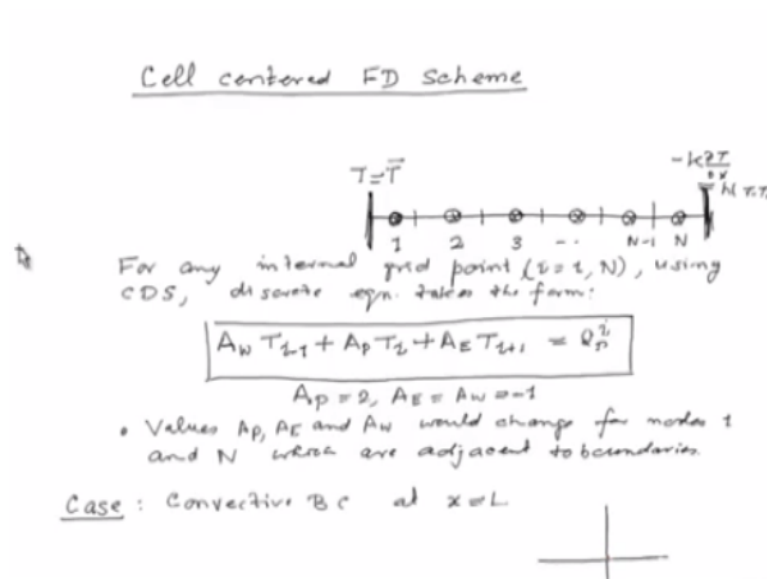
Cell-centred finite difference discretization

- ❖ Consider cell centred uniform grid
- ❖ 3-point CDS scheme for FD approximation at internal grid points
- ❖ Central difference (CDS) for BC at right boundary.

At the right edge of the slab, that is $x = L$, we have got a convective boundary condition that is $-k \frac{dT}{dx}$ at $x = L = H * T - T_a$, so now we need to find out how do we take care of this derivative boundary condition and in what way that is change our discrete equations. So, once again we would continue with the cell centered uniform grid and of course now in this case all our grid points are the nodes they are internal.

So, we would as usual use 3 points CDS scheme for finite difference approximation and we have to modify only this nodes or the equation for the nodes which are close to the boundaries, we have already seen one part and we would again try to use central difference for incorporation of the boundary conditions which involves derivative at the right boundary. So, let us see, how do we incorporate the derivative boundary condition?

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Cell centered finite difference scheme, let us draw our grid, our nodes are located at this centroids of each of these cells node 1, 2, 3 and so on, N-1 and N, this is our right boundary where we have a conductive boundary condition specified and we had at left boundary $T = T_{\text{bar}}$, here we have $-k \frac{\Delta T}{\Delta x} = H * T - T_a$, so they mentioned earlier as for; since all these grid points happen to be internal.

So, at each grid point we would replace of governing equation by a discrete counterpart using central difference approximation, so for any internal grid point in fact; please note that now all of our grid points are internal to the problem domain it is $i = 1, 2, N$ using CDS discrete equation takes the form $A_W T_{i-1} + A_P T_i + A_E T_{i+1} = Q_P^i$, for the time being, we are going to prefer using that I index $A_E T_{i+1}$ and this we said we are going to write Q_P^i .

This is the same as what we had done earlier with the vortex best scheme absolutely no difference, our A, the way rearrange the terms our A_P was equal to 2, $A_E = A_W = -1$. Now, the values of these coefficients were change for values of A_P, A_E and A_W or change for nodes 1 and N, which are close to boundaries or which are adjacent to boundaries, so we have already seen one change.

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Case 1: Convective BC at $x=L$

Use 2nd order accurate CDS for discretization derivative $\frac{dT}{dx}$.

$\left(\frac{dT}{dx}\right)_{x=L} \approx \frac{T_{N+1} - T_N}{\Delta x} \quad (2)$

B.C. $-k \left(\frac{dT}{dx}\right)_{x=L} = h [T_L - T_a] \quad (3)$

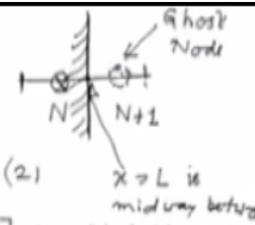
Use simple average to approximate T_L i.e.

$T_L = \frac{1}{2} (T_{N+1} + T_N) \quad (4)$

From eqns. (2), (3) and (4):

$-k \frac{(T_{N+1} - T_N)}{\Delta x} = h \left[\frac{1}{2} (T_{N+1} + T_N) - T_a \right]$

* Objective is to obtain an expression for T_{N+1}



That is we have seen the effect of the Dirichlet boundary condition at node 1, there was Dirichlet boundary condition specified at the left hand and how does it affect these coefficients for node 1 that we saw earlier, so now we will take case 2, that is the incorporation of convective BC at $x = L$, so once again we would introduce our ghost node, so this is our actual boundary, let us put the internal parts as said it, okay.

This is our internal shell whose middle point is our computational node with the index N, now let us introduce a ghost cell which is outside of it and the centroid of the ghost cell let us put this by dotted line is call or give it an index N+1. Now, with this arrangement a boundary point that happens to be the midpoint between these nodes; actual node N and the external ghost node, so this is our so called ghost node.

So, boundary point is midway, this is a boundary $x=L$ is midway between nodes N and N+1, so that tells us that we can now use of us second order accurate central difference scheme, so let us use second order accurate CDS for discretization of derivative dT / dx , so what do we get? dT/dx at $x=L$, this we can approximate as T of N+1- T_N divided by Δx because the distance between nodes and N+1 would be the same as our normal greater spacing Δx .

Now, let us have a look at our boundary condition, so BC was $-k dT / dx$ at $x = L$, this was equal to h times $T - T_a$, so on the right hand side we have got it on the term, that is our T setting here, so this T is at $x=L$, so we need to approximate this T_L as well. So, let us use simple average, so use simple average to approximate T_L that is our T_L becomes half of T of N+1+ T_N .

So, now next we substitute or we use these equations 2, 3 and 4, so from equations 2, 3 and 4 what we will get? On the left hand side, we have $-k$ and approximation for dT/dx would be given by T of $N+1 - T_N$ divided by Δx , on the right hand side we have got h times $1/2 T$ of $N+1 + T_N - T_a$. Let us try to simplify this expression, our main purpose is to eliminate, so what we are looking for? Our objective is; our objective is to obtain an expression for T_{N+1} .

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... Cell centered FDM (Derivative BC)

$$T_{N+1} - T_N = -\frac{h \Delta x}{k} \left[\frac{1}{2} (T_{N+1} + T_N) - T_a \right]$$

$$\Rightarrow T_{N+1} \left[1 + \frac{h \Delta x}{2k} \right] = T_N \left(1 - \frac{h \Delta x}{2k} \right) + \frac{h \Delta x}{k} T_a$$

$$\Rightarrow T_{N+1} = \frac{\left(1 - \frac{h \Delta x}{2k} \right)}{\left(1 + \frac{h \Delta x}{2k} \right)} T_N + \frac{\frac{(h \Delta x)/k}{\left[1 + \frac{h \Delta x}{2k} \right]} T_a}{\left(1 + \frac{h \Delta x}{2k} \right)} \quad (5)$$

↑ contains the effect convective bc.

Consider discretized obtained using CDS for node N:

$$A_W T_{N-1} + A_P T_N + A_E T_{N+1} = Q_P^N \quad (6)$$

Eliminate T_{N+1} using eq. (5):

$$A_W T_{N-1} + A_P' T_N = Q_P^{N'}$$

This T_{N+1} is just intermediate variable which we have introduced for our formulation; it has got no other purpose to serve okay. So, we can write our left hand side as T of $N+1 - T_N$, remaining terms let us transfer to the right hand side, so we get $-h \Delta x$ divided by k and inside we have got by $1/2 T_{N+1} + T_N - T_a$. Let us transfer the remaining term in T_{N+1} to the right sorry left hand side and bring T_N to the right hand side.

So, we get T of $N+1$ within brackets $1 + h \Delta x / 2k$, we have just transferred the first term here $1/2 T_{N+1}$ multiplied by $-h \Delta x / k$ to the left hand side, this is equal to T_N times within brackets $1 - h \Delta x / 2k$ plus $h \Delta x / k$ times T_a , so now this gives us an expression for this intermediate on T_{N+1} which we have introduced as $1 - h \Delta x / 2k$ divided by $1 + h \Delta x / 2k$, the numerator divided by $1 + h \Delta x / k$ multiplied by $T_N + h \Delta x / k$ divided by $1 + h \Delta x / 2k$ times T_a , whole thing multiplied by T_a .

So, now this expression for T_{N+1} , it essentially contains our boundary condition, so this contains the effect of convective boundary condition. So, now let us go to the discrete equation for; consider the discrete equation or other discretized equation obtained using CDS for node N,

so this $A_W T_{N-1} + A_P T_N + A_E T_{N+1} = Q_P N$, so all that we need to do is now we need to eliminate T_{N+1} from here using equation 5.

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↑ Contains the effect convective BC.

Consider discretized obtained using CBF for node N:

$$A_W T_{N-1} + A_P T_N + A_E T_{N+1} = Q_P N \quad (6)$$

Eliminate T_{N+1} using eq. (5):

$$A_W T_{N-1} + A'_P T_N = Q'_P N$$

↑ modified eqn. for node N.

$$A'_P = A_P + A_E \frac{(1 - h \Delta x / 2k)}{(1 + h \Delta x / 2k)}$$

$$Q'_P N = Q_P N + (-A_E) \frac{(h \Delta x / k) - T_a}{[1 + \frac{h \Delta x}{2k}]}$$

2. Implementation of BCs is more complex than usual node based FDM. What are advantages, if any?

- We have used 2nd approximations for all derivatives.

So, eliminate T_{N+1} using equation 5 and this will give us A_W times T of $N-1$, let me write or introduce a new term A_P prime $T_N = Q_P N$ Prime, so this becomes our modified equation for node N; node N, where our A_P prime would be our original $A_P + A_E$ times $1 - h \Delta x$ divided by $2k$ divided by $1 + h \Delta x$ divided by $2k$; sorry this should be $2ks$ everywhere and similarly our Q_P and Prime is the original value of $Q_P N$ + the additional term which comes from the effect of convective boundary condition.

So, it would be $-A_E$ times okay, now you transferring the contribution to the right hand side $h \Delta x / k$ divided by $1 + h \Delta x$ divided by $2k$ times T_a , so what we can say is with cell centered finite differences, the light became bit difficult the implementation boundary condition that required some effort but there is a foot, translate into any gain in computational efficiency or numerical accuracy, so this is what the questions we need to ask ourselves.

The question is implementation of BCs; of BCs is more complex than usual node based FDM, so what are advantages if any? We have spent some good amount of effort on the implementation of these boundary conditions, so it will complicate our coding effort as well, we will require few more computations so what is the gain? One thing which you can guess, we have used, so note here, we have used second order approximations for all derivatives okay.

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Perceived advantage:

- * Hopefully, we should get more accurate numerical solution.

System matrix with cell-centered scheme

$$[A] = \begin{bmatrix} A_P^M & A_E & & & \\ A_W & A_P & A_E & & \\ & \ddots & \ddots & \ddots & \\ & & A_W & A_P^{N/2} & \\ & & & & 0 \end{bmatrix} \quad \boxed{A_E = A_W = -1}$$

- * Matrix A obtained from cell-centered FD discretization is "symmetric"

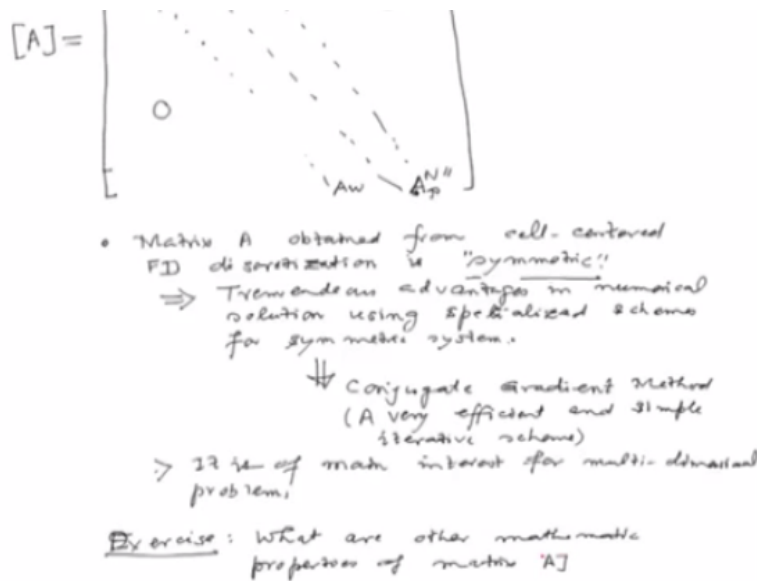
We use central difference scheme for the discretization of $d^2 T / dx^2$ term in our governing equation and we also used a central difference approximation for evaluation of dT/dx term in the boundary condition, so what we said? Is; first thing is perceived advantages hopefully, we should get more accurate numerical solution either any other benefit, for that let us have closer look at the complete system when we assemble.

So, let us write our just system matrix, so system matrix with cell centered scheme, if you remember the case one, what we had they were change only in a diagonal term that is A_P , A_W dropped out, so the first row we are left with 2 terms that is A_P one, let us call it, use a symbol prime or rather to make it clear let us call it A_P^M that is modified coefficient M at node 1 and then usual value of A_E , now this A_E would be the same for remaining terms.

In the next row, we get A_W , then usual value of A_P and A_E , so this is our system matrix A and so on, we can keep writing it, we get only these 3 diagonal terms, the rest of the terms would be zero. Now let us come to the last row which corresponds to node N, so what we found from the previous equation which we had derived, they were changed only in A_P , A will not adjust, this is a last diagonal, so we will get A_P and double prime.

So, this is a modified term A_W remains same and note that the way we have written our A_E and A_W they are both equal and their value was -1, so what you can see from this matrix, now this matrix is; see matrix A obtained from cell centered finite difference discretization is symmetric, so this is stark contrast with our previous formulation, where our nodes were aligned with the boundary.

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The first node was in the left boundary, the last node that is $N+1$ and that node was on the right boundary, there we saw that system matrix is not symmetric but here we have got a symmetric system matrix which has got scores of advantages in numerical solution okay. So we have got tremendous advantages in numerical solution because we have got specialized schemes for symmetric systems, using specialized schemes for symmetric systems.

For instance, if you want to use an iterative scheme you have got a very beautiful reiterating scheme which is applicable that is our conjugate gradient method which is a very very simple and it very powerful iterative scheme, a very efficient and simple to program iterative scheme and of course this advantage or like this observation is pertinent for the case of multidimensional problems, for one D problem where we have got only a tri diagonal structure.

We are happy with TDMA; TDMA matrix is symmetric or not symmetric, so this advantage is basically it is of main interest for multidimensional problems though we derived or we showed this matrix to be symmetric only starting with a one D problem but exactly same structure we would obtain if we had a 2D or 3D problem, if you want you can verify it yourself and the procedure for implementation of boundary conditions would remain exactly the same which we have discussed for all our simple one D case.

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- Matrix A obtained from cell-centered FD discretization is "symmetric!"
 \Rightarrow Tremendous advantages in numerical solution using specialized schemes for symmetric systems.
 \Downarrow Conjugate Gradient Method
 (A very efficient and simple iterative scheme)
 \Rightarrow It is of math interest for multi-dimensional problems.
- Exercise: What are other mathematical properties of matrix [A] which will help in choice of numerical schemes for soln. of [A] ϕ = [Q]?
 Find out if A is positive-definite.

I would like to leave certain things as an exercise for you, I just mentioned this matrix is symmetric. Can you check with a linear algebra book, what are other mathematical properties of matrix A which will help in choice of numerical schemes for solution of our $A\phi = Q$ this system which we had, we want to solve it numerically, so are there any other properties which of; which would be very helpful.

In particular, find out, if A is positive definite okay, I will just close this cell centered approximations with a remark that this scheme we use exclusively in the solution of Navier stokes equations, so we will have what we call a pressure Poisson equation, pressure elliptic equation and for the solution of pressure Poisson equation, we will choose pressure nodes to be at the centres of our cells.

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Two Dimensional Heat Conduction

Steady state heat conduction in a two dimensional domain without heat source or sink is governed by Laplace equation

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$$

And the resulting system matrix would be definitely symmetric and that will help us in the solution for pressure Poisson equation. Now, let us have a look at a two dimensional heat conduction problem and see what sort of discretization we can do for this. So let us consider for the sake of simplicity a steady state heat conduction in a two dimensional domain without heat source or sink.

If the heat source or sink is present that can be taken care of very easily, the way we have seen with one dimensional problem, so this particular problem where there are no sources or sinks is governed by our Laplace equation that is $\Delta^2 T / \Delta x^2 + \Delta^2 T / \Delta y^2 = 0$, so you have got second order derivatives and we have already learned multidimensional formulae for second order derivatives.

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.. Two Dimensional Heat Conduction

Finite difference discretization:

- ❖ Let us consider uniform grid
- ❖ 5-point CDS scheme for FD approximation at internal grid points

$$\frac{T_{i+1,j} + T_{i-1,j} - 2T_{i,j}}{\Delta x^2} + \frac{T_{i,j+1} + T_{i,j-1} - 2T_{i,j}}{\Delta y^2} = 0$$

In generic discrete form

$$A_P T_P + A_E T_E + A_W T_W + A_N T_N + A_S T_S = Q_P$$

So, what do we do? For finite difference discretization, we will consider a uniform grid of the size Δx in x direction and Δy in y direction and let us adopt a 5 point CDS molecule for finite difference approximation at the internal grid point, so if you do that what happens? Now let us draw our computational molecule to clarify the things a bit now.

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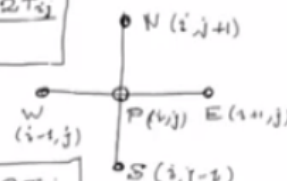
Two dimensional heat conduction

$$\left(\frac{\partial^2 T}{\partial x^2} \right)_{i,j} \approx \frac{T_{i+1,j} + T_{i-1,j} - 2T_{i,j}}{\Delta x^2}$$

Similarly,

$$\left(\frac{\partial^2 T}{\partial y^2} \right)_{i,j} \approx \frac{T_{i,j+1} + T_{i,j-1} - 2T_{i,j}}{\Delta y^2}$$

Discretized equation at internal node P:

$$T_{i+1,j} + T_{i-1,j} - 2T_{i,j} + \frac{\Delta x^2}{\Delta y^2} (T_{i,j+1} + T_{i,j-1} - 2T_{i,j}) = 0$$


Two dimensional heat conduction and what we are doing the way, we are proceeding now that can be easily extended to 3 dimensional problems, so 5 point CDS molecule we are just dealing with the stencil, so these nodes could be at the cell centre, so that these could be at the edges, we do not need really need to worry about it, so our node P ij system neighbour Ei+1, j western neighbour Wi-1,j its northern neighbour in y direction, it will be ij+1.

And then this is for southern neighbour would be given as ij-1, so at point P, that is at point given by the indices i and j, our $\frac{\partial^2 T}{\partial x^2}$, remember what we said if you want to write I want to find out the approximate shown formulae for multidimensional derivative, look at the variable with respect to which we want to differentiate. So, it here it is x; x means only I indices will change in our formulae in which we had derived for one dimensional problems.

Suppose, here we were using CDS, so we will use central difference scheme; P is our central node valued at W and E and P those are the ones which would be involved in approximation of the derivative $\frac{\partial^2 T}{\partial x^2}$. It is simply given as $T_{i+1,j}$ that is the value at eastern neighbour + $T_{i-1,j}$ value at the western neighbour - $2T_{i,j}$ divided by Δx^2 . So, this is the approximation for the first second order derivative in our governing equation.

Similarly, the second derivative which we had $\frac{\partial^2 T}{\partial y^2}$ at the grid point I, j but again use your CDS approximation, so now the values at grid point P N and S, those will be involved because now we have to differentiate with respect to y, so i indices will be kept same in our numerator terms only j indices will change, so $T_{i,j+1} + T_{i,j-1} - 2T_{i,j}$ divided by Δy^2 square, then what would be the discrete equation at the node P?

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$$\begin{aligned}
 & \left(\frac{\partial^2 T}{\partial y^2} \right)_{i,j} \approx \frac{T_{i,j+1} + T_{i,j-1} - 2T_{i,j}}{\Delta y^2} \quad \text{Eq. (3)} \\
 & \text{Discretized equation at internal node P:} \\
 & T_{i+1,j} + T_{i-1,j} - 2T_{i,j} + \frac{\Delta x^2}{\Delta y^2} (T_{i,j+1} + T_{i,j-1} - 2T_{i,j}) = 0 \\
 & \text{Let } \beta = \frac{\Delta x}{\Delta y} \\
 & \Rightarrow \boxed{-T_{i-1,j} + T_{i,j} (2 + 2\beta^2) - T_{i+1,j} - \beta^2 T_{i,j+1} - \beta^2 T_{i,j-1} = 0} \\
 & \Rightarrow \boxed{A_W T_W + A_P T_P + A_E T_E + A_N T_N + A_S T_S = Q_P} \\
 & A_W = A_E = -1, \quad A_P = 2(1 + \beta^2) \\
 & A_N = A_S = -\beta^2 \\
 & \bullet \text{ Nodes at boundaries handled e.}
 \end{aligned}$$

So, discretized equation, substitute the approximation of these derivatives in governing equations, so we get discretized equation at internal node P and this would be given by $T_{i+1,j} + T_{i-1,j} - 2T_{i,j}$, multiplied by Δx^2 to simplify the things of it, so we get a ratio of $\Delta x^2 / \Delta y^2 * T_{i,j+1} + T_{i,j-1} - 2T_{i,j} = 0$, we can introduce a shorthand notation, so let us use the symbol alpha or rather let us use beta.

Beta = Δx divided by Δy , so we can write the preceding quiz in bit more compact form as $T_{i-1,j} + T_{i,j}$ within brackets $2 + 2\beta^2 - T_{i+1,j} - \beta^2 T_{i,j+1} - \beta^2 T_{i,j-1} = 0$, so this can be easily recast in our generic form that is $A_W T_W + A_P T_P + A_E T_E + A_N T_N + A_S T_S = Q_P$, we can easily compare the coefficients and write these values here that $A_W = A_E = -1$, our $A_P = 2(1 + \beta^2)$ and $A_N = A_S = -\beta^2$.

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$$\begin{aligned} \text{Let } \beta &= \frac{\Delta x}{\Delta y} \\ \Rightarrow & \boxed{-T_{i-1,j} + T_{i,j}(2+2\beta^2) - T_{i+1,j} - \beta^2 T_{i,j+1} - \beta^2 T_{i,j-1} = 0} \\ \Rightarrow & \boxed{A_W T_W + A_P T_P + A_E T_E + A_N T_N + A_S T_S = Q_P} \\ & A_W = A_E = -1, \quad A_P = 2(1+\beta^2) \\ & A_N = A_S = -\beta^2 \end{aligned}$$

• Nodes at boundaries handled exactly in the same as we did for 1-D problem to incorporate boundary conditions.

Handling the boundary conditions is exactly the same as we had done previously in the case of one dimensional problems, so nodes at boundaries handled exactly in the same way; the same way as we did for one D problem to incorporate boundary conditions and once you have incorporated the boundary conditions, we can easily obtain discrete system of equations by assembling the things at all the nodes.

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.. Two Dimensional Heat Conduction

Implementation of BCs:

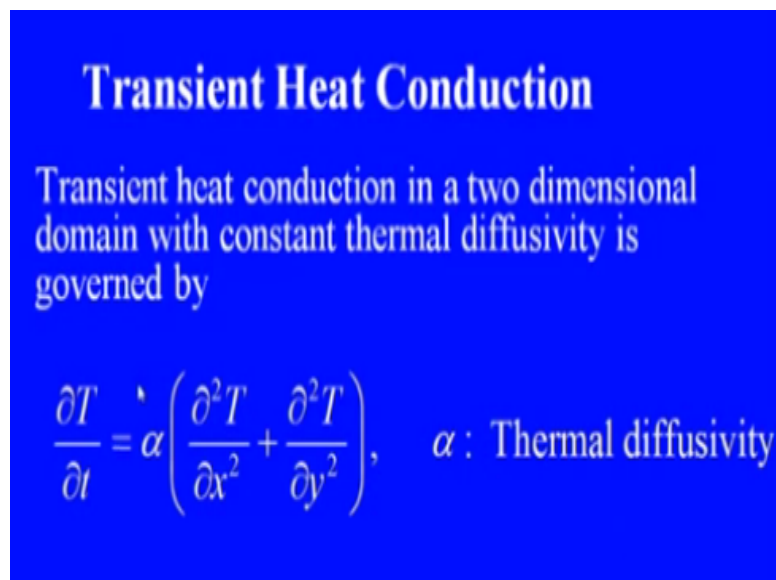
- ❖ Dependent on choice of grid
- ❖ Usual node based: One-sided difference (BDS) for derivatives in BC at any boundary.
- ❖ Cell-centred: Introduce concept of ghost cell
 - ❖ Use simple average for Dirichlet BCs
 - ❖ Central difference (CDS) for derivatives in BC at any boundary.

And you can observe for yourself that we will get a penta diagonal system okay, this is what we had our generic discrete form for two dimensional heat conduction problem, so implementation a BC that will depend on our choice of grid that is to say whether we have taken vertex centre computational node or a cell centered computational node. So, if you have got usual node base that is vertex best schemes.

We have to use one sided difference formula BDS or FDS as appropriate for derivative boundary conditions at any boundary. Dirichlet slip boundary conditions are taken care of without any problem, for cell centered scheme, we will proceed exactly the way we did in one D, that is we will introduce the concept of ghost cell and we will use simple average for Dirichlet basis as how we will incorporate and eliminate the values corresponding to the ghost cell.

And thereby include the specified boundary condition in the discrete equation for the node close to Dirichlet BC. Similarly, we can use central difference scheme which involves value of the variable at the ghost cell, use your boundary condition to obtain that expression for that variable at ghost cell, substitute that in this discrete equation for the node adjacent to this derivative boundary and we are done with introduction of boundary conditions.

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Transient Heat Conduction

Transient heat conduction in a two dimensional domain with constant thermal diffusivity is governed by

$$\frac{\partial T}{\partial t} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right), \quad \alpha : \text{Thermal diffusivity}$$

Next suppose, we had the instead of steady or problem where transient one, so say for example a transient heat conduction problem in a two dimensional domain with constant diffusivity in the the case of variable diffusivity can be taken care of algebra it would become bit more involved but as far as finite difference approximation is concern and these steps would be fairly similar.

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.. Transient Heat Conduction

Finite difference discretization:

- ❖ Let us consider uniform grid
- ❖ 5-point CDS scheme for FD approximation at internal grid points

$$\left(\frac{dT}{dt} \right)_{i,j} = \alpha \left(\frac{T_{i+1,j} + T_{i-1,j} - 2T_{i,j}}{\Delta x^2} + \frac{T_{i,j+1} + T_{i,j-1} - 2T_{i,j}}{\Delta y^2} \right)$$

So, now let us take the case of constant diffusivity, so $\frac{dT}{dt}$, very small Δt of time variable is equal to $\alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right)$, if we had a 3 dimensional problem, we will have one more term $\frac{\partial^2 T}{\partial z^2}$ and here where α denotes thermal diffusivity, so for finite difference discretization let us consider a uniform grid of grid size Δx and Δy , 5 point CDS scheme for finite difference approximation at internal grid points.

So, this is what we have already seen earlier for 2D case; 2D, 3D case we derived this as a central difference approximation. What happens in the left hand side? Now, $\frac{dT}{dt}$ as a partial derivative of capital T with respect to time now that becomes an ordinary derivative, so that is why I have used symbol $\frac{dT}{dt}$ at grid point $ij = \alpha$ times this bracket terms $\frac{T_{i+1,j} + T_{i-1,j} - 2T_{i,j}}{\Delta x^2} + \frac{T_{i,j+1} + T_{i,j-1} - 2T_{i,j}}{\Delta y^2}$ is divided by Δy square.

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.. Transient Heat Conduction

In generic discrete form:

$$C_P \left(\frac{dT}{dt} \right)_P + A_P T_P + A_E T_E + A_W T_W + A_N T_N + A_S T_S = Q_P$$

Collection of discrete equation at all nodes leads to ODE in time given by

$$\mathbf{C} \left(\frac{d\mathbf{T}}{dt} \right) + \mathbf{K}\mathbf{T} = \mathbf{B}$$

which must be solved using a time integration scheme.

So, in generic discrete form, we introduce our symbols A_P A_N and so on and you can write by introducing a new symbol C_P for the time being of course was the way we have written it $C_P = 1$, so $C_P dT/dt$ at point P with $+A_P T_P + A_E T_E + A_W T_W + A_N T_N + A_S T_S = Q_P$, this Q_P might be present in case if we had some stroke terms coming from somewhere.

Now, if you collect such discrete equation at all nodes, so in this case we will get an ordinary differential equation in time, so all these C s coefficients they will be combined in this matrix C , so this capital C matrix is basically a diagonal matrix, so capital C times d capital T/dt + capital $K * T = B$; now these bold symbols, bold capital T indicates or it is a vector of the temperature values at all the grid points.

And capital B denotes what we call the load vector, so in finite difference finite volume of finite element terminology specifically in the case of finite elements this matrix C is also referred to what we call a capacitance matrix, matrix k is called a stiffness matrix and B is called the load vector, so same term is also borrowed and used very often in finite difference and finite volume literature for transient heat conduction problems.

So, this is a simple system of ordinary differential equations one; it contains only first derivative and this has to be solved using a time integration scheme which we will learn in a later module, so until then let us wait and learn few more techniques of finite difference discretization for convective transport problem which we will do in the next lecture and we will discuss some computer implementation aspect also in the next lecture.

And then we will take one by one; the first we will consider in the next module the solution of algebraic equations and then in the module after that we will take; take up the case of solution of these ODE or ordinary differential equations in time