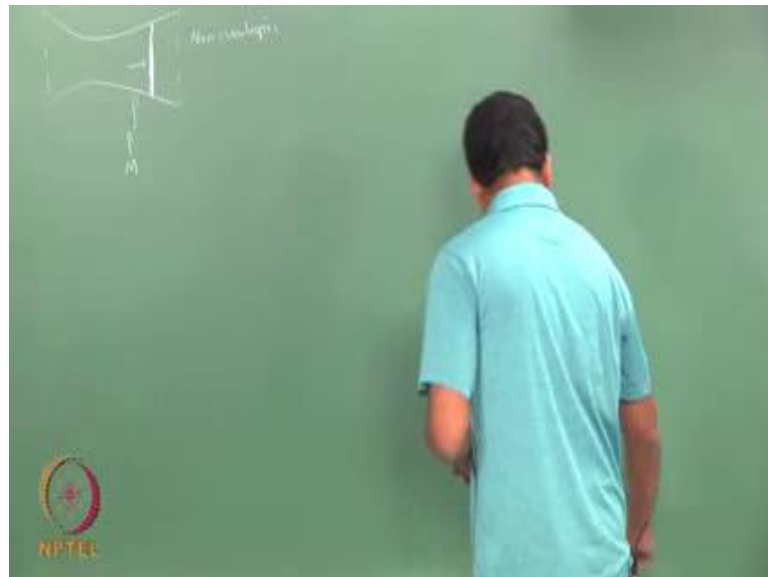


Fundamentals of Gas Dynamics
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Week - 08
Lecture - 29
Introduction to normal shocks

This week we are going to study something on normal shocks. So, normal shocks are non-isentropic process that is happening in the flow.

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So, if I have a nozzle like what we had discussed in the last few classes for some pressure issue, you are going to have non-isentropic solutions. What essentially it means is that you are going to have some kind of shock that is hitting in the diverging section of the nozzle. What do I mean by that? I will show you a video.

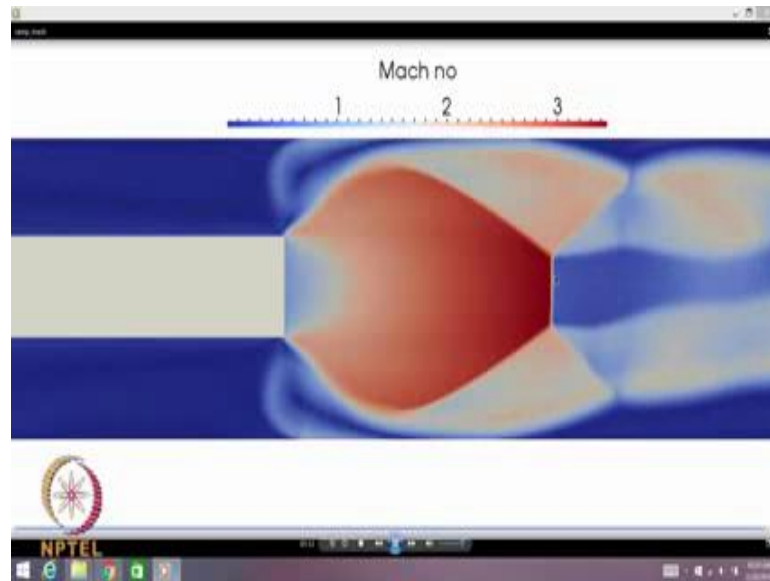
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So, in this video what you see here as this dark lines are the shocks. So, you see a slanting shock here and then, you have the other shocks there. So, I will replay that again. So, this is as a normal shock, this is oblique shock and all those things we are going to discuss in this course. So, as these dark bands are larger density gradient values, so what you see here is something called Schlieren photograph in which the gradients of density is being captured.

This property, this change in your flow pattern at this particular junction or a thin layer, thin region where you have discontinuity in density and pressure and other quantities or typically called as shock, this is a non-isentropic process which essentially would give me flow pattern in this particular case.

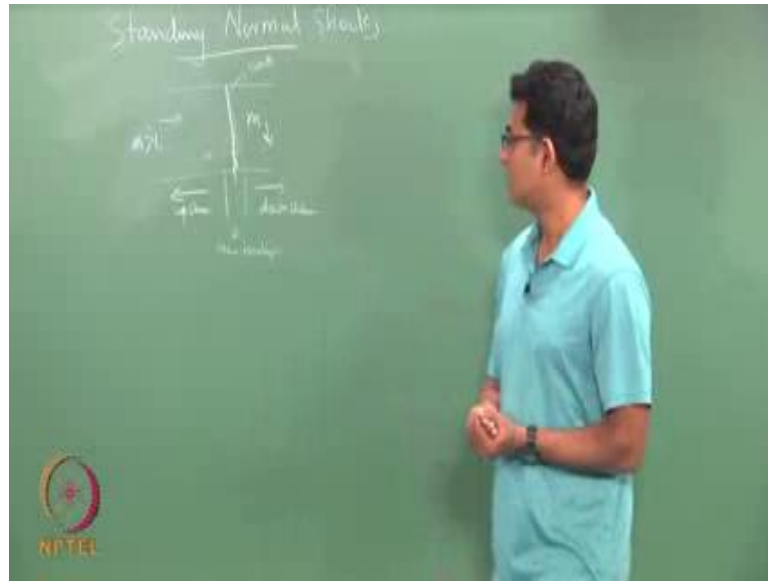
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So, I have a jet that is coming out and this would create a difference in Mach number because my density is now different. So, if you see here, these are larger Mach number regions and the blue regions are your low Mach number regions and in between you see a thin line that is where the jump in Mach number happens and if you see a bit more, these larger Mach numbers once it crosses this thin region, suddenly it turns into a subsonic flow or a blue region. So, the red region is now changed to a blue region once the flow crosses this particular line. So, we are going to see in some special cases. Some within the assumption of 1D steady flow whatever I have shown you is an unsteady flow, but the analysis that we are going to do is something on the steady flow.

So, what do I mean by that? I have a shock that is standing in time and at some location and it is not changing with respect to time. So, we are going to study some location where I have a shock here and this Mach number would be large Mach number comes and something happens here and then, the Mach number reduces. So, your density changes, pressure changes and there are few other quantities that changes and we will see how to analyze this within this particular assumption. We will come back to this once we are discussing supersonic flows. So, whatever we have shown you in the movie, we are going to discuss in detail the oblique shocks and the normal shocks. So, the topic which I am going to discuss now is standing normal shocks.

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So, this unlike what we have seen in the movie, the shock is standing there still and then, we are trying to analyze it. So, what are shocks before we start? So, if I have a fluid particle that is traveling at some velocity, some large velocity at some location, something happens which forces the fluid to decelerate or forces the fluid to stop. Now, if this is M greater than 1, this information cannot be going back or going upstream.

So, if this is my upstream direction and this is my downstream direction with respect to the point we are talking, so at this point something happens, so that the fluid stop suddenly. So, the fluid particle that comes here does not have this information till it reaches that information and that is what we have learned from the propagation of supersonic waves. So, the fluid here comes and stops or decelerates suddenly to a large value, decelerates to a large velocity gradient.

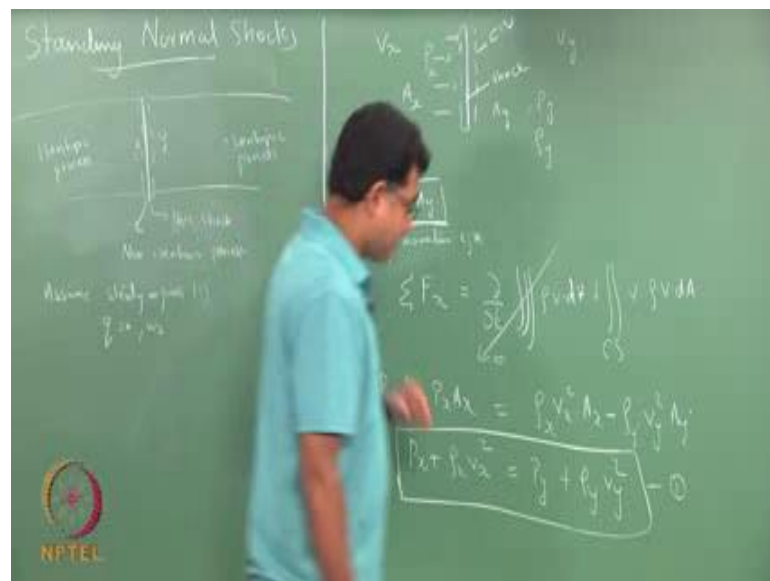
So, the fluid behind does not know this information comes and hit the same fluid and you will have an accumulation of fluid particles at this particular region, at this particular point to coming and hitting and that thin region is called your shock. So, the sound waves are infinite decimally small pressure waves, shock is a finite value pressure wave. So, the large pressure gradient that is moving is here shocks are called shock.

The analogy that is given in a few books which I have read is that if you have few skiing, if you are skiing, a group is skiing down the hill, at some point something happens and the first skier stops suddenly and then, the person skier that is behind him does not know

what has happened comes and hit and the following person comes and hit and there is a sudden havoc. You know change in velocity of the group of the skiers that is professionally something like this, it comes and it stops or decelerates to a very small value. So, the Mach number here would change dramatically at this thin region. So, as soon as it comes and crosses this, the Mach number change because Mach number changes the other property also changes.

Now, we will see what the relation between the Mach number before the wave and before this shock and after the shock and the relation that is connecting these two, ok. So, this particular region is non-isentropic process. So, in this region it is non-isentropic because it involves sudden changes in properties, it involves entropy change and it involves friction and other things. So, it is a non-isentropic process. So, what we will analyze is the following.

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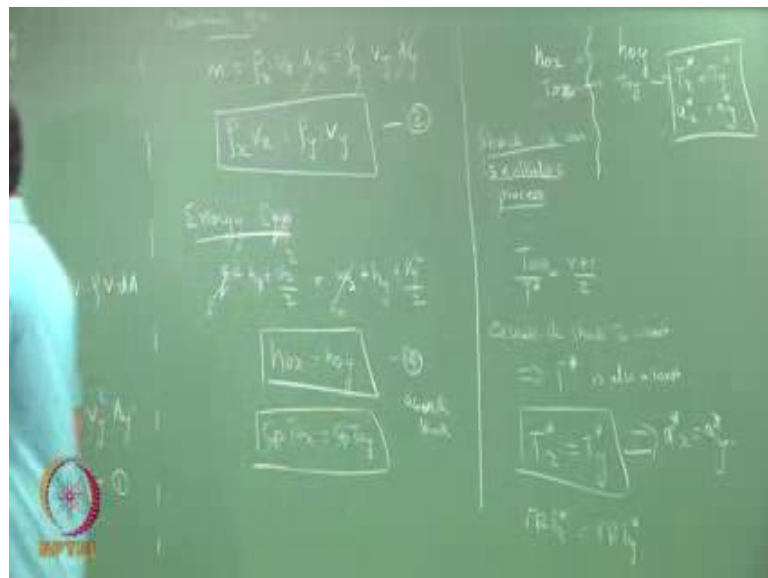


We have a thin shock. So, typically the thickness is of the order of our mean free path. So, I have a shock here, very thin up to this, it is an isentropic process, after this is again isentropic process, but within this thin region you have non-isentropic process. We will also assume steady and quasi 1D as before we will also assume our heat transfer is 0 and shaft work is 0. So, it is an adiabatic process, irreversible adiabatic process steady quasi 1D.

So, if I take the shock alone and the control volume here, so this is my control volume and this thick line is my normal shock. So, there is I call this region just properties before the shock as x and after the shock as y. So, if I say m_x , it is the shock Mach number before the shock m_y is the Mach number after the shock or you still can use one and two, but for convenience, we will use x and y and see how it changes across the shock. So, if this is my control volume, if p_x is acting on the control volume in an area a_x , so this is $p_x a_x$ after the shock is $p_y a_y$ and p_y you have ρ_x and ρ_y approaching with a velocity v_x and v_y .

So, if I assume a_x equals a_y , apply my momentum equation here, we have not used momentum equations in the previous few classes. Now, we are going to use that here. So, this is going to be $\sum F_x$ or $\sum F_x$ equals assuming it to be 1 t, you have $\rho v dv$ of control volume $\rho v dv$ plus control volume $c_s v \rho v da$ assuming steady this term would go 0, f_x is the pressure that is acting on this area. So, it will be $p_y a_y$ minus $p_x a_x$ equals, this would be $\rho_x v_x^2 a_x$ minus $\rho_y v_y^2 a_y$. So, a_x equals a_y , I can cancel out these terms. So, my p_x plus $\rho_x v_x^2$ same as my p_y plus $\rho_y v_y^2$. So, that is our equation 1. So, p_x is the pressure before the shock, p_y is the pressure after the shock density and velocity.

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Now, we will use the continuity, apply continuity equation which is \dot{m} equals $\rho_x v_x a_x$ equals $\rho_y v_y a_y$. So, a_x and a_y are equal. So, I cancel out and my $\rho_x v_x$

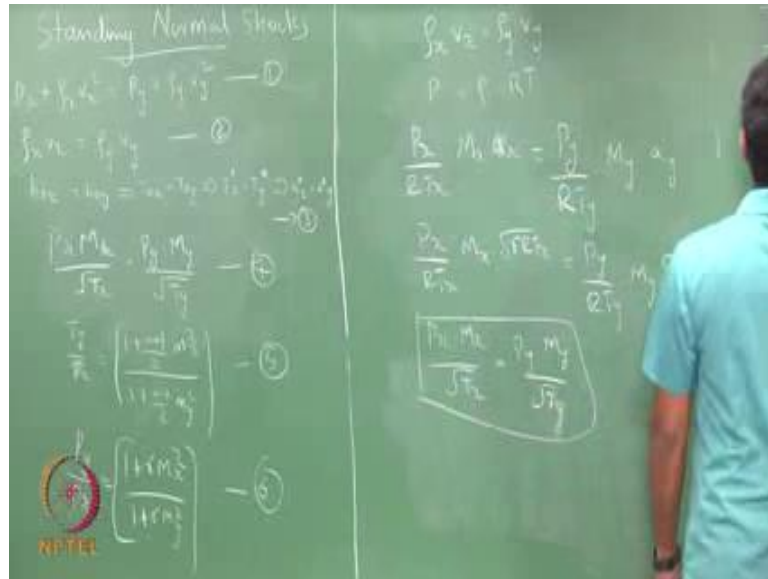
equals $\rho_y v_y$. So, that is equation 2. Now, I apply energy equation which is q plus h one h_x plus v_x^2 by 2 equals w_s plus h_y plus v_y^2 by 2. So, we have assumed q equals 0 and w_s is equal 0. So, we end up with h_{0x} equal h_{0y} . So, these are across the shocks for perfect gas. I can write $c_p t_{0x}$ equal $c_p t_{0y}$ assuming c_p to be constant; you will get t_{0x} equal t_{0y} . So, what I mean by that is, if I have shock here, the enthalpy here is same as my enthalpy after the shock.

So, even though the process is non-isentropic which does not impose this condition to be wrong, we have assumed q equals 0, w_s is equal 0 is enough to have my stagnation temperatures and stagnation enthalpy to be same. So, the process here is isenthalpic process is shock is essentially is an isenthalpic process. So, we just assumed our heat transfer and shaft work to be 0. That is the only assumption we have taken and we have arrived at this particular relation.

Now, we also know that your t_{0x} or t_{0y} by t_{star} is $\gamma + 1$ by 2. Now, across the shock point t_{0} is constant which implies my t_{star} is also a constant. It means my t_{starx} is same as my t_{stary} . We are going further if this is true my $\gamma r t_{starx}$ is same as my $\gamma r t_{stary}$ which implies my a_{starx} is same as my a_{stary} . Across the shock now I have my t_{starx} equals t_{stary} and a_{starx} also equals to a_{stary} .

So, all this from the assumption that q equals 0, w_s is equal 0. Now, we will take this equation 2 and try to substitute that in terms of pressure and see what we get. So, like what we are done before, we will write these equations here, so that we can discuss it at a later point of time.

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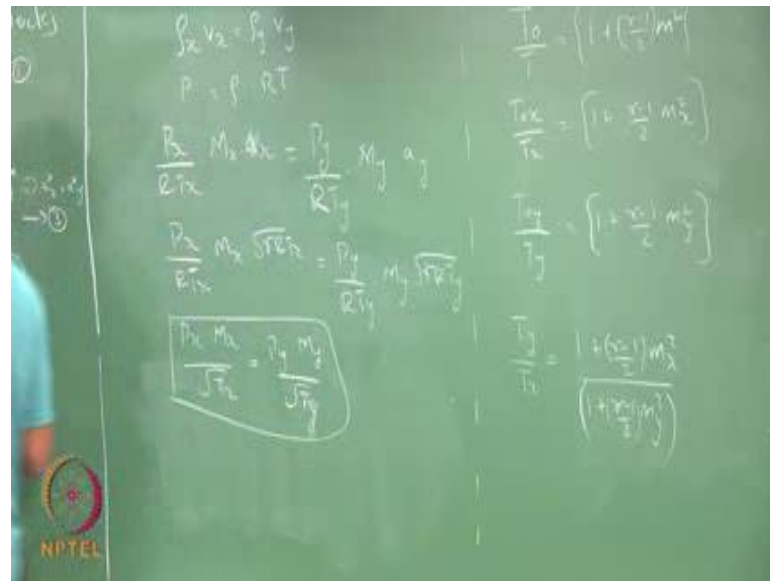


That is equation 1. Equation 2 is this which is continuity equation and then, we have $h_0 x$ equals $h_0 y$ which implies $t_0 x$ equals $t_0 y$ which implies $m t^* x$ equals $t^* y$ which implies $a^* x$ equals $a^* y$. So, we have derived, we have seen these many equations. Now, I am going further in the derivation. So, what I will take is let us number the equation.

So, that is equation 1, this is equation 2 and this set is equation 3. So, what I will do is, I have $\rho_x v_x$ equals $\rho_y v_y$ I would have $m p_x$ equals ρ_x into $r t_x$ or I would rather say my ρ equals $p r t$. I would get ρ_x by ρ_y as v_x by v_y . Now, I will substitute this there. So, this would be ρ_x . Instead of ρ_x , I would substitute as p_x by $r t_x$ into m_x into a_x equals p_y by $r t_y$ into m_y into a_y . Now, also I would substitute in terms of temperature. So, this would be p_x by $r t_x$ into m_x into root of γt_x equals p_y by $r t_y$ into m_y into root of $\gamma r t_y$.

So, I can reduce this to p_x into m_x divided by root t_x equals p_y into m_y by root t_y . So, this is from a simple continuity equation and substituting the ideal gas equation. So, that is my equation 4. So, this quantity is going to be constant across the shock. So, that is my equation 4.

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Now, I can relate t by t_0 by t as $1 + \frac{\gamma - 1}{2} m^2$ which means I can relate my stagnation quantities before the shock and after the shock in terms of Mach number m_x square and m_y square. Now, we know $t_x t_0 x$ and $t_0 y$ are same. So, I can write t_y by t_x equals $1 + \frac{\gamma - 1}{2} m_x^2$ divided by $1 + \frac{\gamma - 1}{2} m_y^2$. So, this is our t_1 minus t_2 . What we have done previously?

So, there is nothing new here for what we had discussed, but just that this is also true across the shock. So, the property t_y and t_x can be related to the Mach number that is happening before the shock and after the shock. So, we will for completeness, we will write that too. Now, what about p_1 by p_2 ? So, I will rub this. So, I take the first equation $p_x + \rho_x v_x^2$ equals $p_y + \rho_y v_y^2$.

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$$\frac{T_0}{T} = \left(1 + \frac{\gamma-1}{2} M^2\right)$$

$$\frac{T_{0x}}{T_x} = \left(1 + \frac{\gamma-1}{2} M_x^2\right)$$

$$\frac{T_{0y}}{T_y} = \left(1 + \frac{\gamma-1}{2} M_y^2\right)$$

$$\frac{T_{0x}}{T_{0y}} = \frac{1 + \frac{\gamma-1}{2} M_x^2}{1 + \frac{\gamma-1}{2} M_y^2}$$

$$P_2/P_1 = P_2/P_1 \cdot \left(\frac{\rho_2}{\rho_1}\right)^\gamma = P_2/P_1 \cdot \left(\frac{T_2}{T_1}\right)^{\frac{\gamma-1}{\gamma}}$$

$$P_2 \left(1 + \frac{\gamma-1}{2} M_x^2\right) = P_1 \left(1 + \frac{\gamma-1}{2} M_y^2\right)$$

$$\frac{P_2}{P_1} = \frac{1 + \frac{\gamma-1}{2} M_y^2}{1 + \frac{\gamma-1}{2} M_x^2} \quad \text{--- (6)}$$

So, yeah I will take $p \times \rho$ substitute the ideal gas equation by $r t x$ into $m x$ into $m x$ square into $a x$ square which is $\gamma r t x$ square $t x$ equals $p y$ plus $p y$ by $r t y$ $m y$ square into $\gamma r t y$. So, this is $p y$ into $1 + \gamma m x$ square equals $p y$ into $1 + \gamma m y$ square. So, I can write $p x$ by $p y$ as this quantity $1 + \gamma r m y$ square divided by $1 + \gamma m x$ square. These are simple algebra, nothing more here.

Just you realize the pressure difference, pressure changes according to your Mach number changes. So, this is my equation 6. So, I gather that and write it here. So, I will write $p y$ by $p x$ $1 + \gamma m x$ square divided by $1 + \gamma m y$ square. So, this is my equation 6. So, these are the property changes across the shock. Now, what I am going to do is, I am trying to see if there is a relation between Mach number x and y . So, I relate if I know my Mach number x $m x$, can I find my Mach number $m y$ that is after the shock. So, I am going to use this equation which is our equation 4. $P x m x$ by root $t x$ equals $p y m y$ by root $t y$ which I can rewrite as $p x$ by $p y$ into $m p x$ by $p y$ into root of $t y$ by root of $t x$ equals $m y$ by $m x$.

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So, I have written this from our continuity equation. I have just taken ρ_x by ρ_y . So, I have taken ρ_x by ρ_y and $\sqrt{t_x}$ by $\sqrt{t_y}$ by t_x . Now, this I know in terms of Mach number which is $1 + \gamma M_y^2$ divided by $1 + \gamma M_x^2$ t_y by t_x . Also I know in terms of Mach number $1 + \gamma M_x^2$ divided by $1 + \gamma M_y^2$ M_y^2 to the power $1/2$ equals M_x by M_y . So, this is from equation 6. This is from equation 5. So, I know this relation. This is the pressure before the shock and this is pressure after the shock. Likewise, temperature after the shock and temperature before the shock, I know these ratios in terms of Mach number before the shock and Mach number after the shock.

Now, I am eliminating these quantities and trying to get a relation between M_x and M_y , if I do this, there is a bit of algebra here. I would get the following equation which I would write it here as M_y^2 equals M_x^2 plus $2(\gamma - 1)$ divided by $2\gamma(\gamma - 1)$ $M_x^2 - 1$. So, this is my final equation. So, if you do from algebra here, you will get a quadratic solution and this is the solution for M_x^2 . So, if I know my shock number, shock Mach number at location before the shock or just before the shock, when I know my Mach number after the shock that is what it means.

Now, let us look at the other equation and try to see what is happening here. So, I have a shock M_x and M_y . I also know that ρ_x into $1 + \gamma M_x^2$ equals ρ_y

into $1 + \gamma M^2$. So, this does not distinguish anything between subsonic or supersonic Mach number. So, let us first consider $M > 1$. So, if $M > 1$, this ratio implies. So, if $M > 1$, you are going to get $M < 1$ here. If you look at this equation implies your $M < 1$ or p_y would be larger than your p_x p_y would be greater than your p_x which means this is a compression process.

So, what happens here is you have a Mach number supersonic. Mach number comes and there is a shock and then, you hit a condition where your $M < 1$ and suddenly your pressure increases to p_y . So, the flow comes and then sees something all your fluids are to one thin region and then you see the Mach number is decreasing and the other side and your pressure is increasing which is essentially your compression process.

Now, if my $M < 1$, if I substitute here $M < 1$, if $M = 1$, what happens? So, let us discuss that first if $M = 1$, if this is $1 + \frac{2}{\gamma} M^2 - 1$, this is 1. So, it is going to be same as let us do that minus 1. So, this would be $\gamma - 1$ $\gamma - 1$ goes. So, this would be $\gamma - 1 + 2$ divided by $2 \gamma - 1$. So, this is $\gamma + 1$ divided by or this would be bracket here. So, this would be $\gamma + 1$ which is 1. So, your $M = 1$.

So, this solution is also present in this particular equation, but this is also the trivial solution which means you have a Mach number and nothing is changing if $M = 1$. Then, your pressure ratio here p_x by p_y is also 1 and hence, your temperature if you look at the equation 5, this will also be 1. So, it is something like you know a flow with nothing is happening. It is a trivial solution. So, that is also a solution to whatever we are discussing here.

Now, our problem is the other one. So, this is also equal to $M < 1$. So, what happens is $M < 1$, if you substitute a value $M < 1$ here, γ is always greater than 1. So, $M < 1$ would give me $M > 1$. Again you can substitute any random value and see $M > 1$ is always going to be greater than 1. So, if $M > 1$, if you look at this equation relating the pressure, your p_y is less than your p_x . So, if I have subsonic flow and if there is something that is happening that to take me to $M > 1$, my pressure is going to decrease which means this is an expansion shock. So, this is a compression shock and this is an expansion shock. So, this

is an expansion shock. Now, this is not possible. We will derive and show that this is not possible.

In the next class or the next lecture, we will show that the entropy change during this process is going to be negative and we will also see what is the relation between that when it comes to this, how does m_y vary with respect to m_x and hence, why this is not possible and only this is possible. We will show that in the next lecture for the time being. So, this is my expansion compression shock and this is my expansion shock. Both of this is possible solution to this equation which relates m_x and m_y . So, for any given m_x , I have a given y and mathematically that is possible. Basically this is not possible. Again we will show it using entropy change and it gives equation. That is for this class.

Thank you.