

**Foundation of Computational Fluid Dynamics**  
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**Lecture – 24**

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**Week 5 – Syllabus listed for this week**

- **Illustration on the performance by different approximation for convection term**
- Time advancement / Integration methods
- Arrangement of variables
- Pressure velocity coupling

MAC, SIMPLE, Variants of SIMPLE, Projection Methods




Greetings, welcome again to this course on CFD. Today we will be doing fourth module for this week. Syllabus we have listed for this week; illustration on the performance by different interpolation scheme for convection term. And from this class, we will go move onto time advancement, integration methods, arrangement of variables, pressure velocity coupling. There are different methods available MAC, SIMPLE, different versions of SIMPLE, projection methods. We will look into these details and then move onto next module.

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## Arrangement of Variables

- After defining domain and mesh, one needs to select points where variables have to be computed.
- It is critical as it decides the way the governing equations are solved, the programming, the memory size and time requirement.
- There are three approaches – Staggered, Colocated and Semi-staggered.


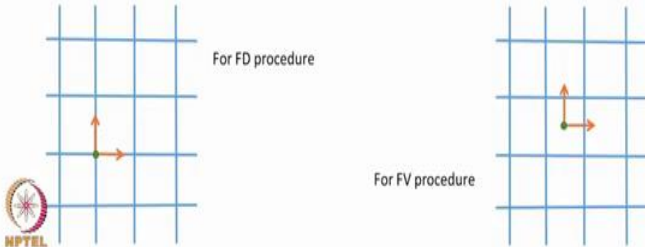


With regards to variables, once you define domain and mesh, then we need to select points where variables have to be computed. It is critical because it decides the way the governing equations are solved, the programming easiness, memory requirement and overall computational time requirement. There are three approaches in general, what is known as a staggered grid, colocated grid, and semi-staggered grid.

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## Collocated grid

- All the variables are stored at the same nodal location.
- Approximation for the derivative terms are straight forward.
  - Programming is easier and memory requirement is minimum
- Used when the boundary conditions and its slope are discontinuous
- Disadvantage: May result in Checker-board problem



Let us look at one-by-one. The first one colocated grid, it is you can also read it as co located. As the name indicate in this system all the variables are stored at the same

location. Approximation for the derivatives are straight forward; programming is easier, memory requirement is minimum. If you look at the mesh arrangement, what is shown here is for the finite difference procedure, and what is shown on the right side is for the finite volume procedure. As you can see here, this is the location, where all the variables are stored. So, in this example, the arrow going from left to right is for the u-velocity, arrow going from bottom to top is for the v-velocity, and dotted point that is marked is actually indicating node or location, where other variables are stored, scalar variables like temperature, pressure or concentration. So, all the three variables for example, u-velocity, v-velocity, pressure are stored at the same location, this is for finite difference arrangement. And you are going for finite volume type of arrangement then you can definition at the centre of the volume as shown here. So, this is the location where scalar variables are stored, and arrow going from left to right for u-velocity, arrow going from bottom to top is for v-velocity.

As you can observe in both the cases, they are defines at the same location. Let say for example, you are trying to find out first derivative  $\frac{du}{dx}$  or the pressure  $\frac{dp}{dx}$ ; both  $\frac{du}{dx}$  and  $\frac{dp}{dx}$  appear in the u-momentum equation and for both you need to find the derivative. And in this case, as you can see here, you are defining only grid, and the grid is same for both u as well as pressure. Hence getting a derivative difference formula is easier, same coding can be used just by change the variables from velocity to pressure, you can obtain first derivative say  $\frac{du}{dx}$  and  $\frac{dp}{dx}$  with much easier, because you are using only same location,  $\Delta x$  is also calculated only once and it can be stored. Hence it is easier and memory requirement is minimum.

It is used when boundary conditions as well as its slopes are discontinuous. So, this co located arrangement of variable extremely helpful when the boundary condition as well as its slope is discontinuous. Like any other method, this also has some disadvantage, what is known as checker-board problem. In the next slide, will explain what is checker-board problem.

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### Checker board problem

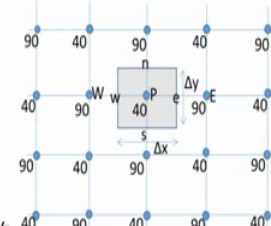
Obtain pressure at face 'e' and 'w' by linear interpolation, the pressure gradient term  $\frac{\partial p}{\partial x}$  in the  $u$ -momentum equation is given by

$$\frac{\partial p}{\partial x} = \frac{p_e - p_w}{\Delta x} = \frac{\left(\frac{p_e + p_P}{2}\right) - \left(\frac{p_P + p_w}{2}\right)}{\Delta x} = \frac{p_e - p_w}{2\Delta x}$$

Similarly, the pressure gradient term  $\frac{\partial p}{\partial y}$  in the  $v$ -momentum equation is given by  $\frac{\partial p}{\partial y} = \frac{p_n - p_s}{2\Delta y}$

It is to be noted that pressure at the central node  $P$  does not appear. Substituting, pressure field information, all the discretized pressure gradients goes to zero.

That means, zero source due to pressure in the discretized momentum equation, even though pressure field exists. This is unphysical in behaviour.



In this slide, what is shown in this figure is a computed pressure distribution on a checkerboard arrangement. A particular control volume or the pressure cell is shown in the shaded portion;  $P$  is the node of interest. For example, west node and west face, similarly east face and east nodes are shown. Similarly, for other side, that is north node, north face, south node and south face, they are also shown.  $\Delta x$  and  $\Delta y$  is a element distance in  $x$  and  $y$  direction respectively. The numbers that is shown in this figure that is 90, 40, 90, 40, this is the pressure field obtained say by ((Refer Time: 06:06)) procedure, let us not worry about what is the procedure. If the pressure field happens to be as shown here, then how we will find out how the derivative of the pressure in  $x$  and  $y$  behave.

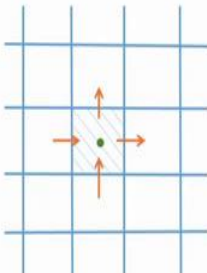
So, obtain pressure at face  $e$  and  $w$  by linear interpolation, the pressure gradient term  $\frac{\partial p}{\partial x}$  for example, in the  $u$ -momentum equation is shown as here. So,  $\frac{\partial p}{\partial x} = \frac{p_e - p_w}{\Delta x}$  for the cell that is shown it is actually  $\frac{p_e - p_w}{2\Delta x}$  that is what it is shown here, because it is  $\frac{\left(\frac{p_e + p_P}{2}\right) - \left(\frac{p_P + p_w}{2}\right)}{\Delta x}$ . Now,  $p_e$  at east face is done by linear interpolation, pressure at node  $P$  – point of interest, and pressure at node  $E$  – the adjacent node are used to get pressure at east face. So, it is shown here  $p_e = \frac{p_e + p_P}{2}$ . Similarly, for  $p_w$  at west face, you take pressure information from node interest  $P$ , and west node and linear interpolation is used  $p_w = \frac{p_P + p_w}{2}$  is there. Now, if you look at this overall, you have  $p_P$  appearing in both the term with the minus in between, so  $p_P$  term gets cancelled. Finally, you have  $p_e - p_w$  by two  $\Delta x$ .

You can obtain similarly the other pressure gradient term  $\frac{dp}{dy}$ , which is appearing in second momentum equation or v-momentum equation. Without going to the details, we can immediately make a guess  $\frac{dp}{dy}$  is equal to  $\frac{p_N - p_S}{2\Delta y}$ . Now, what is to be noted you are interested to find out  $\frac{dp}{dx}$  and  $\frac{dp}{dy}$  and you get expression without the node of interest term appearing. So, it is to be noted that pressure at the central node P does not appear in the final expression for this gradient  $\frac{dp}{dx}$  or  $\frac{dp}{dy}$ . Now, if you substitute the pressure gradient term in discretized Navier-Stokes equation, then all the pressure gradient term will go to zero, which otherwise means there is no source term appearing in the discretized Navier-Stokes equation, which is unphysical. So, that means, the zero source due to pressure in the discretized momentum equation, even though there is a pressure field appearing as shown in this figure. And this is quite unphysical and this is the problem with collocated arrangement.


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Staggered grid

- Locations or nodes for velocities and pressure are different.
- Pressure nodes are at the center. While the nodes for velocity are staggered in line with the direction of the component.
- Strong coupling between velocity and pressure. Helps to avoid oscillations in pressure and velocity field.



The diagram shows a 4x4 grid of blue lines. At the center of the grid is a green dot representing a pressure node. Four orange arrows represent velocity nodes: one pointing right from the center, one pointing left from the center, one pointing up from the center, and one pointing down from the center. The arrows are positioned at the midpoints of the grid lines.



Next arrangement is the staggered arrangement as a name indicate variables are stored at staggering location, location or nodes where velocities and pressure are different, not only pressure any scalar also different. So, here is the figure to explain what is the staggered arrangement, for the same mesh, you can now observe at the centre of the mesh is the pressure or any scalar variable is stored; arrow mark going from left to right is indication for u velocity; and arrow mark going from bottom to top is for the v velocity. So, u velocity variables are stored on the vertical line at this place, which is half

cell distance from the center in the x-direction. Similarly, v-velocity cells are stored on the horizontal line as shown here, which is half- cell distance in the y-direction from the center of the cell as shown here.

So, you have three locations, one for each velocity, and one for pressure or scalar; whereas, in the co-located arrangement, we have the same location. Now, this results in different computation. Pressure nodes are at the center. While the nodes for velocity are staggered in line with the direction of the component. There is one big advantage, there is a strong coupling between velocity and pressure, so as you can interpret from this figure, the pressure at the center is responsible for the u-velocity flow as well as for the v-velocity flow as shown in the figure. Hence there is a natural strong coupling between velocity and pressure, and this avoids oscillations in pressure as well as velocity field.

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### Semi-(partially) staggered

- Velocity variables are stored at the same location, pressure / any scalar quantity is stored at the staggered node - center.
- Combines some advantage of staggered and collocated.
- Good for non-orthogonal grid.
- Still it produces oscillatory pressure or velocity fields.

The figure contains three grid diagrams. The first, labeled 'Colocated', shows a 4x4 grid with a central node (green dot) and two arrows (red and blue) pointing up and right from it. The second, labeled 'Staggered', shows a 4x4 grid with arrows pointing up and right from the midpoints of the grid lines. The third, labeled 'Semi-(partially) staggered', shows a 4x4 grid with a central node (green dot) and arrows pointing up and right from the midpoints of the grid lines.

Third arrangement is what is known as semi or partially staggered arrangement. In this, velocity variables are stored at the same location; whereas, pressure or any other scalar quantity is stored at the staggered node or at the center. So, this is the figure that is explained in for the same mesh arrangement, u-velocity and v-velocity are stored at one same location, whereas, pressure is at the center. So, it is in between colocated and staggered. It combines advantage of staggered as well as colocated and it is found to be good for non-orthogonal grid. Still it produces some oscillatory pressure or velocity fields.

Now, let us look at all the three arrangements together, the left is the colocated arrangement, middle is the semi-staggered or partial arrangement, in the right is the staggered arrangement, so you can immediately get idea the advantage as well as disadvantage. So, in the case of staggered arrangement, because locations are different, you need to compute for each one of them separately hence it involved sometimes and more memory requirement. Whereas, there is natural pressure and velocity coupling in staggered grid arrangement. In the next example, we are going to use only staggered grid arrangement and that is widely used in many codes as well commercial software.

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### Pressure-Velocity Coupling

- There are three governing equations for three momentum (velocity components) and one continuity equation.
- Convection terms are non-linear in nature.
- There are four variables- three velocity components and one pressure. No. of equations and no. of variables are satisfied.
- There is no separate equation for pressure, though it plays an important role in each velocity component equation.
- Velocity variables are very intimately coupled, as each velocity variable term appears in every equation including continuity equation.
- Correct pressure field should be known and to be used in momentum equation, to obtain correct velocity field, which in turn satisfies both momentum equation as well as continuity equation.
- The linkage is set through a procedure called pressure-velocity coupling.



We go to the next important topic what is known as pressure-velocity coupling. What is the background behind pressure-velocity coupling or what do we mean by pressure-velocity coupling. By now we know in general there are three governing equations respectively for three momentum or three velocity components, and there is one continuity equation, this is the minimum requirement for any fluid flow calculations. In each governing equation for momentum, there is a convection term and we repeat it many times before convection terms are non-linear in nature. In total, there are four variables that is there are three velocity components and one pressure. The number of equations equal to number of variables is satisfied.

However, there is no separate equation for pressure, though it plays an important role in all the momentum equation. Velocity variables are; however, very strongly coupled,

because you will observe you know already also that each velocity component appears in every other momentum equation, including the continuity equation that way velocity variables are very intimately coupled. Correct pressure field should be known and that should be used in momentum equation, to obtain correct velocity field, which in turn satisfies both momentum as well as continuity equation. This process of linkage within momentum equation and continuity equation is what is known as a pressure-velocity coupling. Now, this is very important stage in solving Navier-Stokes equation, there are many methods available, we are going to look at specifically three, four method MAC algorithm, SIMPLE algorithm, SIMPLER algorithm, projection methods.

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Marker And Cell (MAC) Method

- Start with guess value for pressure and velocity components.
- Intermediate velocity for the x - direction velocity component can be written as,
 
$$\frac{u^* - u^n}{dt} = -\frac{\partial p}{\partial x} + \left\{ -u \frac{\partial u}{\partial x} - v \frac{\partial u}{\partial y} - w \frac{\partial u}{\partial z} + \frac{1}{Re} \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) \right\}$$

$$u^* = u^n - dt \frac{\partial p}{\partial x} + dt \left\{ -u \frac{\partial u}{\partial x} - v \frac{\partial u}{\partial y} - w \frac{\partial u}{\partial z} + \frac{1}{Re} \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) \right\}$$

Similarly for v and w velocity component in y and z directions

- Calculate error in continuity  $D^* \frac{\partial u^*}{\partial x} + \frac{\partial v^*}{\partial y} + \frac{\partial w^*}{\partial z} = D^*$



Let us look at MAC algorithm first; this is otherwise called Marker and Cell method. For any calculation, once you define mesh and you decide the variable location, you are able to describe boundary conditions, but what about all the internal nodes. All the internal nodes are initialized with some guess values, this step is called initialization. So, you start the solution with the guess value of pressure and velocity component. We will now explain the procedure for u-momentum equation, the procedure is same for v as well as w momentum equation; between time level zero or between one iteration to the next iteration, the velocity is intermediate velocity. Once you know the procedure for discretization then you write down final discretized Navier-Stokes equation. In this case, we mentioned, we will take x-momentum equation and that is what is shown here.



So, the time derivative term is retained on the left side, all other terms are brought to the right side, which means all the terms are supposed to be known right side.  $U^*$  is an intermediate velocity and that is to be determined first then it will be corrected. So,  $u^*$  minus  $u^n$  by  $dt$  that is the time integration; for this case, what is shown here is a first order Euler time integration;  $u$  with the superscript  $n$  refers to previous time level. All the terms on the right side  $\frac{dp}{dx}$  and convection term, viscous diffusion term, we follow any procedure for discretization, finally, we get this discretized equation. So, if you solve this equation, then you get  $u^*$ , we name it as  $u^*$ , because it is an intermediate velocity. The intermediate velocity may not satisfy continuity equation.

So, if you rewrite this equation, take  $dp$  to the other side;  $u^n$  is also known and that is also taken to the other side, and this is the equation for  $u^*$ . So, if you solve, you get  $u^*$ , and this is at one node location, and for one-d, it will run from left to right; for two-d, it will run the entire map. You can write the similar expression for  $v$  as well as  $w$  velocity component for  $y$  as well as  $z$  direction. As we mentioned just now, this  $u^*$ ,  $v^*$ ,  $w^*$  are intermediate velocity component, and they will not satisfy or they may not satisfy continuity equation. So, if you substitute  $u^*$ ,  $v^*$ ,  $w^*$  in continuity then you get what is known as a error in the continuity and it is referred here as  $D^*$ , you write in the form of equation as shown here. So,  $\frac{du^*}{dx} + \frac{dv^*}{dy} + \frac{dw^*}{dz} = D^*$ .  $D^*$  is a error in the continuity.

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### Marker And Cell (MAC) Method


- If the magnitude of  $D^*$  greater than some prescribed value  $\epsilon$ , correction pressure is calculated as  $\delta p = -\beta D^*$ , 
$$\beta = \frac{\omega}{2dt} \left( \frac{1}{\Delta x^2} + \frac{1}{\Delta y^2} + \frac{1}{\Delta z^2} \right)$$
- The velocity components and pressure are corrected as
 
$$u_{(i,j,k)}^* = u_{(i,j,k)}^* - \frac{dt}{\Delta x} \delta p,$$

$$u_{(i+1,j,k)}^* = u_{(i+1,j,k)}^* + \frac{dt}{\Delta x} \delta p,$$

$$p_{(i,j,k)}^* = p_{(i,j,k)}^* + \delta p$$

Similarly for  $v$  and  $w$  velocity component

- Repeat above steps for all cells until no cells has the magnitude of  $D^*$  greater than the prescribed value.



And this  $D^*$  is used to obtain what is known as a correction in the pressure. And you prescribe a limit for  $D^*$ ; if  $D^*$  is greater than some prescribed value  $\epsilon$ , for example,  $10^{-3}$  or  $10^{-5}$  that is the tolerance level you can accept. This limit is set by you, and it will change from problem to problem. You can also change in one calculations itself between different time level of the calculation. So, if the magnitude  $D^*$  is greater than some prescribed value  $\epsilon$  then you setup pressure correction as shown,  $\Delta p$  is correction in pressure equal to minus  $\beta D^*$ . And what is  $\beta$ ,  $\beta$  is defined as shown here,  $\omega^2 \Delta t^2 / (\Delta x^2 + \Delta y^2 + \Delta z^2)$ . Now,  $\omega$  in this case is what is known as relaxation parameter, we will talk about relaxation parameter later. So, once you calculate  $\beta$ , because all the quantities are known then you can calculate  $\Delta p$ ,  $\Delta p$  is the change in pressure or correction in pressure.

Velocity components and pressure are corrected as given here. What is shown here is again only for  $u$  velocity component, so  $u_{i,j,k}^*$ , we are writing it for three dimension, hence we get three subscripts equal to  $u_{i,j,k}^* - \Delta t \Delta p$ . The adjacent node also should be corrected that is  $u_{i+1,j,k}^*$  you can see  $i+1, j, k$  equal to the old one plus the correction in pressure. Similarly, the pressure is also corrected. So, in this equation,  $u^*$  that is on the left side is the new velocity,  $p^*$  is the new pressure, you can use them as a  $u^*$  or you can write it as  $u$  itself, it is immaterial. What is to be noted is this is the corrected value and corrected pressure.

One can repeat this procedure for other two component  $v$  as well as  $w$ . Now, repeat this step now for all the cells in computational domain until no cells has the magnitude greater than  $D^*$  that you have specified. So, this procedure is what is known as Marker and Cell method, and this is again a popular method. So, this class we have specifically seen arrangement of variables, three arrangement of variables, advantage and disadvantage associated with them. Then we understood the need for pressure-velocity coupling. We explained one procedure what is known as a Marker and Cell method. In the next class, we will take another important method what is known as a SIMPLE method.

Thank you and see you all again next class.