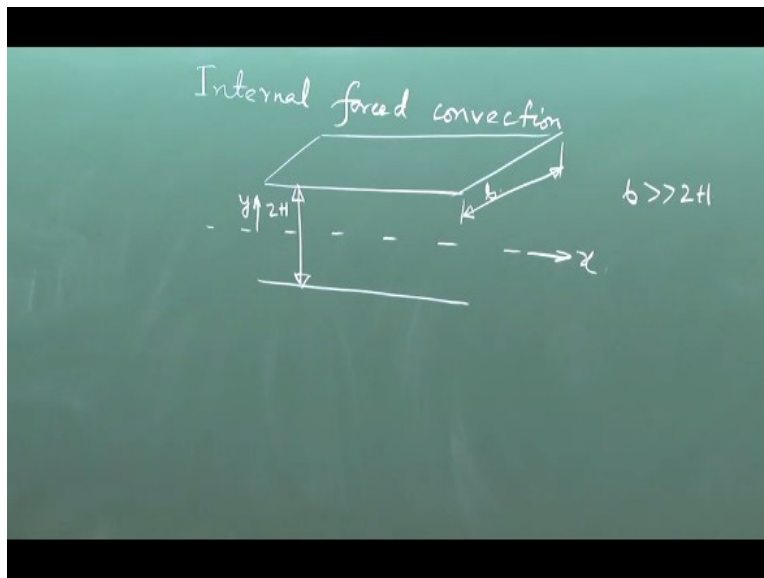


Conduction and Convection Heat Transfer
Prof. S.K. Som
Prof. Suman Chakraborty
Department of Mechanical Engineering
Indian Institute of Technology – Kharagpur

Lecture - 45
Internal Forced Convection – I

In the previous lecture, we were discussing about flow and heat transfer over a flat plate. Now, today we will be discussing about internal flows. So, when we will be discussing about internal flows, we will briefly discuss about the important of fluid mechanics issues and then of course, we will give some more time on heat transfer issues with internal flows.

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So first, we will try to understand what basically happens with internal flows. So, we are now studying internal forced convection. So, let us for simplicity consider something which we call as parallel plate channel. So, what is a parallel plate channel? Parallel plate channel is essentially 2 parallel plates where the width of the plate is like infinitely large as compared to its other dimensions.

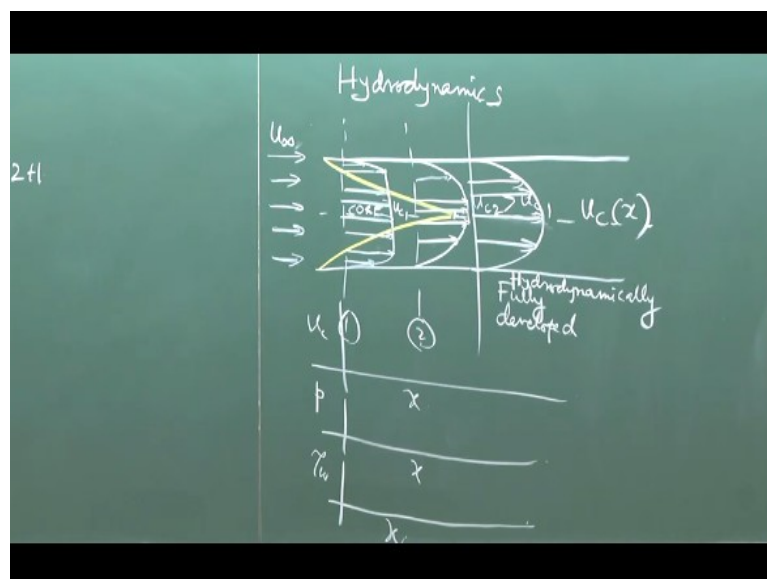
So, if you have a channel like this. So, this dimension let us call it b , let us call this as $2H$, so b is much greater than $2H$. So that it is basically a flow taking place in the x y plane. The z direction being infinitely large. It means that the gradient in the z direction is much negligible as compared to the gradients in the x and y direction. Now, this is a simplified paradigm, but it gives a very important physical insight.

Now, in reality even for rectangular channels, if the width of the rectangular channel is much larger than the height we can consider it like a parallel plate channel, although it is not physically 2 parallel plates, but in effect if the width is much larger than the height then it is like a parallel plate channel.

So, we will discuss about parallel plate channels and circular tubes or circular pipes, which are of importance in engineering and although the mathematics involved with the circular pipes will be different from that of a parallel plate channel simply because of the change of coordinate systems from Cartesian to the cylindrical polar coordinate system. But essentially, the concept, the physics is almost the same.

So, we will try to understand that carefully. So, first we will consider the hydrodynamics.

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Let us say that fluid enters this channel with a velocity u infinity and temperature T infinity, but I am not writing the temperature issue here. Because here we are discussing only the hydrodynamics first. So, just as in case of flow over a single flat plate, for flow over, flow within a parallel plate channel. Essentially it is like flow confined between 2 individual plates.

So, the boundary layers will develop on individual flat plates. So, the boundary layers are developing like this and because of symmetry with respect to the centre line, the boundary layers will meet somewhere on the center line of the channel. Now, let us try to figure out the

velocity distribution in here. Let us say 2 sections 1 and 2. So, you can see that within the boundary layer the velocity profile will be there then the velocity will be uniform.

So, the region where the velocity is uniform, this is called as the core region, outside the boundary layer - CORE region. Now, if you try to draw the velocity profile in section 2, what will happen? Now, let us say in the core region at section 1, the velocity is $u_c 1$. Now, my question is that in the core region of section 2, if the velocity is $u_c 2$. Is $u_c 2$ equal to $u_c 1$? Is it greater than $u_c 1$ or is it less than $u_c 1$?

So, let us assume that it's a constant density flow. So, what remains constant between the sections 1 and 2 is the volume flow rate. The mass flow rate is constant, but if ρ is constant that is equivalent to volume flow rate is constant. How do you get the volume flow rate? You get the volume flow rate by integrating the velocity profile. You get the volume flow rate by integrating the velocity profile.

So, integral of the velocity profile here must be same as the integral of the velocity profile here. Now here there is a greater region over which the fluid is slowed down. Here the fluid is slowed down only over this distance. Here the fluid is slowed down, over a greater distance. So, when the fluid is slowed down by a greater distance, what will happen? To compensate for this slowing down, the core velocity $u_c 2$ must be greater than $u_c 1$.

To make up for this slowing down over a larger distance right. So, one important thing we can follow is that one very key difference between internal and external flow is: In external flow, there is a u_{∞} which is a constant. Here, there is no constant u_{∞} . There is a centre line velocity or the core velocity, the core velocity is continuously changing with x . So, u_c is a function of x . Alright, so it is not like u_{∞} which is a constant.

Now, let us try to schematically draw u_c versus x , P versus x and τ_{wall} versus x . So, u_c versus x we have seen that the core velocity increases as you are moving along x but to what extent? How long? There is a situation when the boundary layers merge. After the boundary layers merge, if you want to get the velocity profile. The velocity profile becomes something like this.

This velocity profile is called as fully developed velocity profile because we are going to discuss about 2 different boundary layers: thermal and hydrodynamic. This is more specifically characterized as hydrodynamically fully developed flow. So, when the flow hydrodynamic becomes hydrodynamically fully developed, I mean it may appear that just when the boundary layers merge it becomes like that.

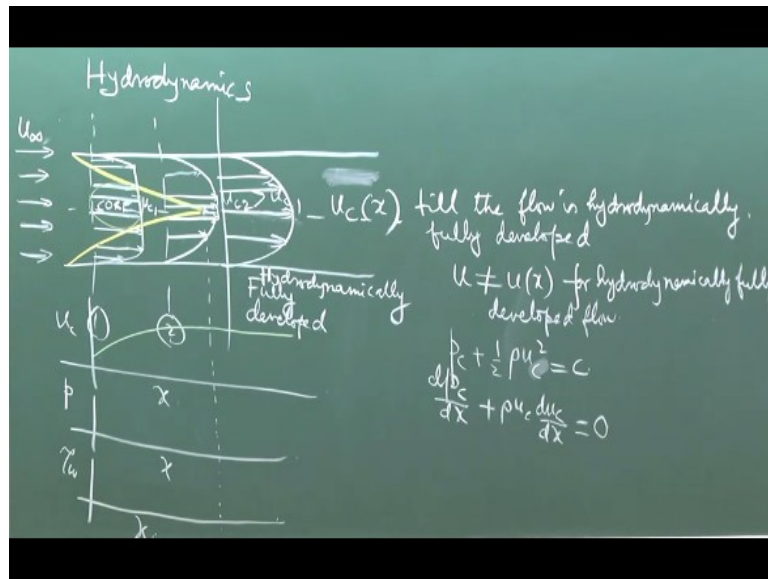
But in practice it takes a little bit of distance from there to become hydrodynamically fully developed, but at least for the under-graduate level without going into that complexity we will assume that after the boundary layers are merged the flow has become hydrodynamically fully developed. So, what is the big essence of hydrodynamically fully developed flow? So, here in the core region what happens?

The effect of the presence of the wall is not propagated. The effect of the presence of the wall is propagated only up to this distance. But, when you come to hydrodynamic fully developed flow, the entire fluid fills the effect of the wall, ok. And because the entire fluid now fills the effect of the wall. The velocity profile from now onwards does not change any more with x . So, hydrodynamically fully developed u_c is a function of x till the flow is hydrodynamically fully developed

And u is not a function of x for hydrodynamically fully developed flow. So, with this concept now let us try to draw this graph of u centre line versus x . So, how will the graph look like? Let us assume that the flow has become hydrodynamically fully developed here. So, u centre line versus x . How will the graph look like? Or u_c versus x ? How will the graph look like? The core velocity increases till the flow becomes fully developed.

After it has become fully developed, it does not change any more right. What happens with pressure versus x or $\frac{dp}{dx}$ versus x , whatever? So, remember that in the core region, we can use the Bernoulli's equation. Because the core region does not feel the effect of the viscous force, right. So, this is for the core region.

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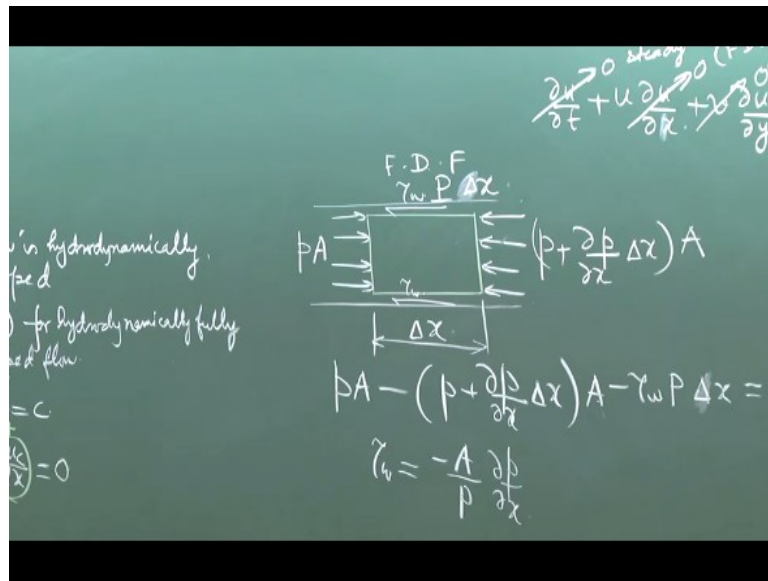
So, if you now differentiate with respect to x , $\frac{dp}{dx}$ right. So, you can see what is this? What is $\frac{du}{dx}$? positive or negative? Positive, u is positive. That means $\frac{dp}{dx}$ is negative. So, it shows that the pressure continuously decreases as the fluid enters the channel. Remember that this pressure may include gravity. So, this is here we have not considered the effect of gravity assuming that it is not important or we have put the gravity within the p .

So, the p is p plus $\rho g z$ that is called as piezometric pressure, ok. So, this p versus x is the piezometric pressure versus x , it may include the gravity part. That is why in the Bernoulli's equation separately the potential energy term, we have not reaching. Because it may be clubbed with the pressure term, so pressure versus x . Now, after the flow has become fully developed what is the situation? $\frac{du}{dx}$ will be 0. So, $\frac{dp}{dx}$ will be 0.

That means p will be - so p will be yes, why are you accepting what I am saying? This is the. see, I am saying that when the flow has become fully developed, this will be 0 and you are accepting it. When the flow has become fully developed the viscous effect has penetrated to the centre line. So, the Bernoulli's equation is no more valid, ok. So, you cannot use this equation after the flow has become fully developed.

This equation is only till the flow has become flow is becoming developed. So, when the flow has become fully developed what happens? So, let us try to make a talk about the fully developed flow.

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The mathematics of the fully developed flow, the exact solution of the Navier-Stokes equation has already been worked out by Professor Som. I am not getting into the exact solution of the Navier-Stokes equation for fully developed flow, but I am trying to give you some physical and qualitative understanding which may be useful for our discussion. So, let us take a small volume of fluid.

Let us say if this is the channel so we have got convinced that we should not use this equation when the flow has become fully developed because viscous effects now penetrate to the core. So, you cannot use the Bernoulli's equation any more. Otherwise, it gives something upside. You see if this is 0 then $\frac{dp}{dx}$ is 0. That means p is constant. If the pressure is constant how will it drive a flow? Right.

So, if you take a fluid element like this. So, here if the pressure is P let us say the cross-sectional area is A , what is the pressure here? P plus let us say this length is Δx . P plus $\frac{dp}{dx} \Delta x$ into Δx into A . This is the force due to pressure. What are the forces acting on this? This is the fully developed flow. What are the forces which are acting on this? So, a fully developed flow means what? So, if you look into the acceleration of flow.

If it is a 2-dimensional flow so $\frac{\partial u}{\partial t}$ let us say it's a steady flow. So, steady flow this term will be 0. So, this is the acceleration term right. ρ into this is the mass into acceleration per unit volume in the Navier-Stokes equation. So, this is 0 for steady flow. What about $\frac{\partial u}{\partial x}$? $\frac{\partial u}{\partial x}$ is equal to 0 for fully developed flow. When we say fully developed we are meaning here hydrodynamically fully developed.

When we come to thermal boundary layer, you have to be care full in distinguishing between hydrodynamically fully developed flow and thermally fully developed flow. They are 2 different concepts all together. Now what about this term? So, we can evaluate this term by looking into the continuity equation. So, this is 0 for fully developed flow. That means v is not a function of y . So, if v not a function of y , what can you say about v ?

So, if you consider the y direction, consider this figure. What is the value of v at y equal to h ? 0. y equal to minus h also it is 0. That means because v is not a function of y , if you can find out the value of v at a particular value of y that should be true for all values of y right. That means v is 0 for all values of y . So, but if there were holes in the plate, there are technological situations in which you make holes in the plate. Then v is not 0 at the wall.

So, assuming that there is no penetration at the plates or no penetration at the solid boundaries, you will have v equal to 0 at wall. So v is equal to 0 at wall, this means v is equal to 0 for all y . So, if v is 0 then this term is 0. So, the entire, in the Navier-Stokes equation, the left-hand side becomes identically 0. So, the non-linearity of the Navier-Stokes equation is gone.

So, it becomes a linear equation which is also called as the Stokes equation which you can solve by analytical tools. Now when the, so physically what is happening? Physically the flow is not accelerating. So, a fully developed flow physically is not accelerating. Until and unless there is a penetration at the solid boundary. If there is no penetration at the solid boundary that means a fully developed flow is not accelerating.

So, if the fully developed flow is not accelerating then what is happening? All forces are balanced that is why it is not accelerating. So, what are the forces acting on it? one is due to, so if you take an element like this a control volume like this one force is due to the pressure, other force is due to the wall shear stress. So, these 2 forces they are balance each other, so that there is no net acceleration.

That is the physics of a fully developed flow. So, if you have τ_{wall} as the wall shear stress. So, you can write the force as τ_{wall} into perimeter into Δx , right. So, for example if it is for the circular pipe what is the shear force? Wall shear stress into $2\pi r$ into l , right. So,

the perimeter is $2\pi r$. So, to make it general, so that you can apply it for any cross section we are writing τ_{wall} into perimeter into length. Perimeter for a circular pipe is $2\pi r$.

That is easy to visualize. So, now these forces are balanced. So, P into A minus P plus. So, you can write τ_{wall} , right. Now, how do you calculate τ_{wall} for a fully developed flow? For a fully developed flow, you get a velocity profile which is a function of y for a rectangular or a parallel plate channel and its function of, or for a circular pipe. So, depending on whether it's a parallel plate channel or a circular pipe.

You have to calculate $\mu \frac{du}{dy}$ at the wall or $\mu \frac{du}{dr}$ at the wall. So, that will give you τ_{wall} . So, question is, Is it a constant or not a constant? So, u is a function of y for a fully developed flow. So, $\frac{du}{dy}$ is a function of y . When you put the value of y equal to y at the wall then that becomes a constant right. So, if the velocity is the function of y only then τ_{wall} is the constant.

If velocity is the function of y only then τ_{wall} is the constant. That means this is also a constant. That means for fully developed flow $\frac{dp}{dx}$ is the constant. That means $\frac{dp}{dx}$ becomes $\frac{dp}{dx}$. So, p versus x is linear. So, p versus x when the flow is not fully developed is non-linear, but when the flow is fully developed it is linear, so this is linear. τ_{wall} versus x , the wall shear stress should be constant for a fully developed flow.

Because τ_{wall} is $\mu \frac{du}{dy}$ at the wall, u is a function of y only. So $\frac{du}{dy}$ at the wall is the constant. So, fully developed flow it's a constant, this is constant. This is also constant. In the developing region, now there are two possibilities, one is it increases to this constant value or it decreases from a different value to this constant value. So, what it will be? So, τ_{wall} scales with μu_c by δ right.

$\mu \frac{du}{dy}$ is order of magnitude wise, μ into u centre line or u core by δ . Where δ is the local boundary layer thickness. This is δ . So, the interesting thing is u_c increases with x right in the developing region, that we have seen. δ also increases with x right. The boundary layer grows. So, what happens to this ratio? Right. You have a ratio where the numerator increases with x , the denominator also increases with x .

So, what happens to this ratio? See, that you can tell from a very intuitive thing, that when you start entering the channel what is δ ? δ is tending to 0, but u_c is finite. So, τ_{wall} will be very large as you enter the channel. After the both δ and u_c are finite. That means it should asymptotically decrease from a very large value to this value as. So, this is large. Large τ_{wall} then it comes to a constant.

See these 3 graphs, I will tell you that it is very important that as students of fluid mechanics, you should be able to sketch those qualitatively. See, you may be very strong in solving complex differential equations. That is very important but that is not all in learning fluid mechanics. So, this we totally develop these concepts by looking into the physics of the fully developed flow.

Without getting into the Navier-Stokes equations their exact solution and all these. At this kind of physical insight, you should try to develop in a... like understanding the fluid mechanics and heat transfers.