

Conduction and Convection Heat Transfer
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Lecture - 37
Review of Fluid Mechanics – V

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Kronecker Delta $\delta_{ij} = 1$ if $j=i$
 $= 0$ otherwise $B_i = B_j \delta_{ij}$

$$C_{ijkl} A_i B_j C_k D_l = \alpha A_i B_i C_k D_k + \beta A_i C_i B_j D_j + \gamma A_i D_i B_j C_j$$

$$= \alpha A_i B_j \delta_{ij} C_k D_k \delta_{kl} + \beta A_i B_j C_k \delta_{ik} D_l \delta_{jl} + \gamma A_i B_j C_k \delta_{jk} D_l \delta_{il}$$

$$C_{ijkl} = \alpha \delta_{ij} \delta_{kl} + \beta \delta_{ik} \delta_{jl} + \gamma \delta_{jk} \delta_{il}$$

Now, how many properties have come? Magically from 81 properties, you are having three properties alpha, beta and gamma. Now, we can reduce the number of properties even further by noting that τ_{ij} deviatoric is equal to τ_{ji} deviatoric.

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$\tau_{ij} \text{ deviatoric} = \tau_{ji} \text{ deviatoric}$

$$\alpha \delta_{ij} \delta_{kl} + \beta \delta_{ik} \delta_{jl} + \gamma \delta_{jk} \delta_{il}$$

$$= \alpha \delta_{ij} \delta_{kl} + \beta \delta_{jk} \delta_{il} + \gamma \delta_{ik} \delta_{jl}$$

$$\beta = \gamma$$

$$C_{ijkl} = \alpha \delta_{ij} \delta_{kl} + \beta \delta_{ik} \delta_{jl} + \beta \delta_{jk} \delta_{il}$$

Because the stress tensor is symmetric the individual hydrostatic and deviatoric component are also symmetric. So, we will swap i and j . So, first we will write C_{ijkl} so $\alpha \delta_{ij} \delta_{kl}$ plus $\beta \delta_{ik} \delta_{jl}$ plus $\gamma \delta_{jk} \delta_{il}$ is equal to now we swap i and j . So, if we swap i and j this will become $\alpha \delta_{ji} \delta_{kl}$ but δ_{ij} and δ_{ji} are the same. Δ is a symmetric tensor.

So, you can write δ_{ij} again δ_{kl} plus $\theta \delta_{jk} \delta_{il}$ plus $\gamma \delta_{ik} \delta_{jl}$ from here what we can conclude. We can conclude, that β is equal to γ , right. You can see that it will be $\beta \delta_{ik} \delta_{jl}$ minus $\gamma \delta_{jk} \delta_{il}$ equal to zero. So that means you have β equal to γ . So, you can write C_{ijkl} equal to $\alpha \delta_{ij} \delta_{kl}$ plus $\beta \delta_{ik} \delta_{jl}$ plus $\gamma \delta_{jk} \delta_{il}$.

So now how many properties are there? Two properties α and β . We will try to get a physical interpretation of these two properties.

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The image shows a chalkboard with the following handwritten equations:

$$\begin{aligned} \tau_{ij}^{\text{deviatoric}} &= C_{ijkl} \epsilon_{kl} \\ &= (\alpha \delta_{ij} \delta_{kl} + \beta \delta_{ik} \delta_{jl} + \beta \delta_{jk} \delta_{il}) \epsilon_{kl} \\ &= \alpha \epsilon_{kk} \delta_{ij} + \beta \epsilon_{ij} + \beta \epsilon_{ji} \\ &= \alpha (\nabla \cdot \mathbf{v}) \delta_{ij} + \beta \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \end{aligned}$$

Below this, the hydrostatic component is defined as:

$$\tau_{ij}^{\text{hydrostatic}} = -p \delta_{ij}$$

So, τ_{ij} deviatoric is equal to C_{ijkl} into ϵ_{kl} . So, what is that? Now you tell δ_{ij} these are i and j are free indices because it is there in both left-hand side and right-hand side. So, you really do not change i and j because you already have i and j in the left-hand side so right-hand side i and j is the same as whatever is there in the left-hand side that you cannot change until or unless you change the left-hand side indices. Only indices that you play with are k and l .

So, δ_{kl} is equal to zero except when l equal to k that is the definition of δ . So, when l equal to k this will be equal to 1 so ϵ_{kl} will become ϵ_{kk} . So, $\alpha \epsilon_{kk}$ plus β

δ_{ik} will become one when k is equal to i . So, when k equal to i this will become i and δ_{jl} will become one when l equal to j . So, one into one into E_{ij} plus beta, δ_{jk} equal to one when k equal to j and δ_{il} equal to one when l equal to i so it will become E_{ji} .

So now what is E_{ij} this we have defined as half $\delta u_i \delta x_j$ plus $\delta_j \delta x_i$. So, what is E_{kk} ? E_{kk} is E_{11} plus E_{22} plus E_{33} . E_{11} is $\delta u_1 \delta x_1$. E_{22} is $\delta u_2 \delta x_2$ and E_{33} is $\delta u_3 \delta x_3$. So, $\delta u_1 \delta x_1$ plus $\delta u_2 \delta x_2$ plus $\delta u_3 \delta x_3$. This in short form we can write $\delta u_k \delta x_k$, right. But what is physically this? This is the divergent of the velocity vector.

So, this as we have discussed earlier relates to volumetric deformation of the fluid. This relates to volumetric strain the rate of change of volume per unit volume. So, α is related to the volumetric deformation plus beta. What is E_{ij} and what E_{ji} ? See E_{ij} and E_{ji} are the same so E_{ij} plus E_{ji} is basically $\delta u_i \delta x_j$ plus $\delta u_j \delta x_i$. So just to write the same notation we write here $\delta u_k \delta x_k$.

Now physically what is this? Physically this relates to the relationship between the deviatoric stress and rate of volumetric deformation. So, this is known as volumetric dilation coefficient in most of the books this is given symbol λ that is why I am just changing from α to λ it does not matter. But since most of the books, used λ as the symbol that I why I am just changing it from α to λ .

This is called as volumetric dilation coefficient because it is very clear that it relates the stress with the volumetric deformation. Now what is this? Can you recall from kinematics of flow that what is this? This is rate of deformation if i is not equal to j that is sheer deformation and if i equal to j that is linear deformation. But it is in general rate of deformation. So, you have the stress proportional to the rate of deformation.

What is this proportionality constant called? Viscosity of the fluid so this beta physically is viscosity. So, this is τ_{ij} deviatoric. What is τ_{ij} hydrostatic? Hydrostatic stress is due to the pressure acting on the fluid element because the hydrostatic stress is the only component of stress when the fluid is at rest. So, if the fluid is at rest the components of stress that is acting on it is the normal component of stress and that the normal stress is minus p .

Why it is minus p? Because by nature pressure is compressive whereas tensile stress is considered to be positive stress. So, pressure is by nature a compressive stress where by sign convention we take tensile stress as a positive normal stress. So, we write this as minus p into delta i j. Why delta i j? Because this is normal stress this is one only if j is equal to i. J is equal to I means it's a normal component. When the two indices are the same it is a normal stress.

When j is not equal to i this will be zero. So, you can combine tau i j equal to tau i j hydrostatic plus tau i j deviatoric. One term we have missed I forgot to write this delta i j please correct this. I forgot to write this delta i j here. So, this will be this time delta i j. There was a delta i j here. I just forgot to write it here.

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The image shows a chalkboard with the following handwritten equations:

$$\tau_{ij} = \tau_{ij}^{\text{hydrostatic}} + \tau_{ij}^{\text{deviatoric}}$$

$$\tau_{ij} = -p \delta_{ij} + \lambda \frac{\partial u_k}{\partial x_k} \delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$\tau_{11} = -p + \lambda \frac{\partial u_k}{\partial x_k} + 2\mu \frac{\partial u_1}{\partial x_1}$$

$$\tau_{22} = -p + \lambda \frac{\partial u_k}{\partial x_k} + 2\mu \frac{\partial u_2}{\partial x_2}$$

$$\tau_{33} = -p + \lambda \frac{\partial u_k}{\partial x_k} + 2\mu \frac{\partial u_3}{\partial x_3}$$

$$\frac{\tau_{11} + \tau_{22} + \tau_{33}}{3} = -p + \left(\lambda + \frac{2\mu}{3} \right) \frac{\partial u_k}{\partial x_k}$$

Annotations include: "p_m (Mech press)" and "The really name is p_m".

So, minus p delta i j plus lambda delta u k delta x k delta i j plus mu. This is nothing but the Newton's law of viscosity for homogeneous, isotropic and Newtonian fluid. So, at every level whenever you learn certain things you have to understand that like things are possibly much more generalized then what is introduced for the first time. Like for example if you are studying in high school and if you are taught what is a vector? What you will be taught?

Vector is something which has magnitude and direction. Then you go to a little bit higher class somebody will add a vector will have magnitude direction and sense. Then if you go to a little bit higher class somebody will add a vector not only have magnitude, direction and sense. It obeys the commutative law of vector addition either the triangle law of the parallelogram law.

If you go to a class of abstract mathematics in algebra, they will discuss about n-dimensional vector space in a vector in a vector space which does not relate to any magnitude direction or anything. So, the question is which one is the most general one obviously what is taught in linear algebra the n-dimensional vector space is the most general vector space that you talk about. So, always we start with the simplest one.

So, when you first studied Newton law of viscosity, you studied $\tau = \mu \frac{du}{dy}$. Just like for everything there is a version for children, Ramayana for children, Mahabharata for children. So, that is Newton law of viscosity for children. So, when Newton law of viscosity was first introduced that is how it is perceived. Now that can be thought of as a special case of this law. So, what it is basically talking about, it is basically talking about this part.

So, think about a flow when you have say in a two-dimensional fluid is like $\frac{\delta u}{\delta y} + \frac{\delta \theta}{\delta x}$. The common symbol that we use this So, if the flow is unidirectional then you have only u components of velocity and then this is not there. So, then that component of tau is $\mu \frac{\delta u}{\delta y}$ that is what is Newton's law of viscosity that you have learned in your earlier I mean first exposure to fluid mechanics.

But do not think that is the most general form of Newton's law of viscosity. So, for homogeneous isotropic Newton fluids this is what is the Newton's law of viscosity. So, never forget to include this term if you have a two dimensional or three-dimensional flow field. Now we will discuss about the normal components about the stress. So, first $\tau_{11} = -p + \lambda \frac{\delta u}{\delta x} + 2\mu \frac{\delta u}{\delta x}$.

See about viscosity we have many misconceptions and one very common misconception is that viscosity is always related to shear deformation. It is not true, viscosity may also be related to linear deformation. You see here this term. What is this? This is linear deformation, right this has nothing to do with shear but it also has a coefficient which is viscosity. So, normal component of stress may also be related to viscosity.

It is not related to viscosity only when the fluid is at rest. But if the fluid is under motion then the normal component of stress is also related to viscosity. So, it is not true that viscosity is just related to shear stress. Very loosely we say, that viscosity is related to shear stress, yes it

is related to shear stress but it may also be related to the normal components of stress. Then τ_{22} , minus p plus $\lambda \Delta u \Delta k$ plus $2\mu \Delta u \Delta x$.

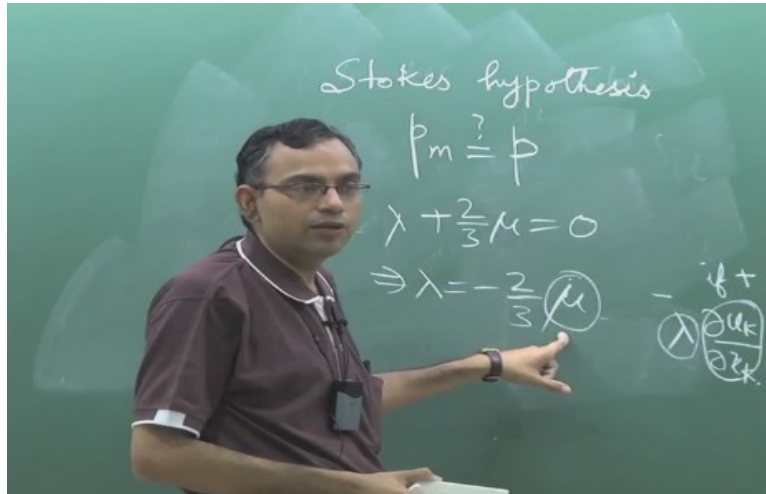
τ_{33} minus p plus $\lambda \Delta u \Delta k \Delta x$ plus $2\mu \Delta u \Delta x$. So, now if we want to find out what is τ_{11} plus τ_{22} plus τ_{33} divided by 3. The average of the normal component of stress that is equal to minus p this three divided by three plus λ , three λ divided by λ plus 2μ into $\Delta u \Delta x$ one plus $\Delta u \Delta x$ plus $\Delta u \Delta x$ plus $\Delta u \Delta x$ that is $\Delta u \Delta k \Delta x$ that divided by three.

So, this three added together will be $\Delta u \Delta k \Delta x$. By definition the left-hand side is called as minus of p_m where p_m is mechanical pressure. So, this is the definition of mechanical pressure, mechanical pressure is by definition the arithmetic average of the negative of the normal components of stress. This p on the other hand is called as thermodynamic pressure. So, what is thermodynamic pressure?

Thermodynamic pressure is the pressure that relates the thermodynamic other parameters through the equation of state. For example, for an ideal gas p is equal to $\rho r t$ that means thermodynamic pressure. So, which relates to other thermodynamic properties through the equation of state. So, mechanical pressure, which relates directly to mechanical forces in general may not be thermodynamic pressure.

Now, still there are many fluids for which our general relationship between mechanical pressure and thermodynamic pressure need to be described. And that was described by something called as Stokes hypothesis.

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So, just like any hypothesis this does not have a proof but this is found to be satisfied for most of the practical fluids. What is that? The Stokes hypothesis is that the mechanical pressure is equal to thermodynamic pressure. Now, the question is that is it true always that the mechanical pressure is equal to thermodynamic pressure? To, understand that we have to appreciate the molecular origin of mechanical pressure and thermodynamic pressure.

Mechanical pressure talks about the translational degrees of freedom whereas thermodynamic pressure includes all possible degree of freedom. Translational, rotational, vibrational degrees of freedom of the molecule. So, when we say that we change a thermodynamic state what happens? The translational, rotational, vibrational all modes change and they eventually get translated in the form of mechanical pressure.

Now, that takes sometime so that the system gets adjusted to the new change. There are certain types of fluids for which of course you can say that mechanical pressure and thermodynamic pressure is identically the same like dilute monatomic gases.

They do not have rotational or vibrational other degrees of freedom. So, they have only translational degrees of freedom. Therefore for dilute monatomic gases Stokes hypothesis is a law it is no more a hypothesis because it can be proved. That for those, for which there is only translational degree of freedom, monatomic, dilute monatomic gases. But for other substances in general this is not equal. Why?

Because every system when you create a change a system takes a time to adapt to the change, right. It is true not just for materials or fluids but for also us as human beings. So, if

somebody wants to change us and we want to change ourselves we cannot do it immediately. Like even if you see in the morning you want to wake up somebody give you a wakeup call or you get the alarming bell still you cannot wake up instantaneously, right.

It takes a time for you to adjust to this disturbance and respond to these changes. This is known as relaxation time of the material. Now typically, the relaxation time is very fast so that the material almost instantaneously responds to the change. But what happens if the material itself is changing at a very high frequency, changing its state at a very high frequency? Let us say that there is a bubble which is expanding and contracting, expanding and contracting very fast at a very high frequency.

Then the bubble when it changes its state from one state to the other before that a new change of state has been imposed. That means the bubbles cannot adjust itself to the change before a new change has come in. So, if you have a bubble which is changing its state very rapidly then if the time scale of the change is faster than it relaxes the time scale. It cannot relax to a new state. So, in that case you do not have mechanical pressure equal to thermodynamic pressure.

So, Stokes hypothesis need not always be valid. But how often, we discuss about such cases of very rapid change possibly very rarely. So, for almost all practical engineering purposes this mechanical pressure is equal to thermodynamic pressure that is why the Stokes hypothesis is such a popular hypothesis. Now for the Stokes hypothesis to be valid, if you have p_m equal to p that means, this term must be zero.

Because this is the volumetric deformation this is in general not equal to zero therefor you must have $\lambda + \frac{2}{3}\mu$ equal to zero. That means λ is equal to minus two third μ . We know that the viscosity of a fluid is positive therefor λ is negative. So, what does it mean? What is the physical interpretation of negative λ ? It means that if there is fluid, you see, the stress is what?

The stress due to the component which is there associated with λ is $\lambda \frac{\Delta u}{\Delta x}$. So, if this is positive that means what? If this is positive that means the volume is expanding. Then λ negative means that the product is negative that means if there is a fluid element which is already expanding then the incremental amount of stress to stretch it

further is actually negative.

That means if it is already expanding you do not require a positive incremental stretch to stretch it further. Because then this component of τ_{ij} is coming to be negative. The other important discussion is that there is a special type of fluid for which you do not care whether the Stokes hypothesis is valid or not that is a case when the flow is incompressible. If the flow is incompressible then because of this equal to zero.

You will have mechanical pressure identical equal to thermodynamic pressure. So, then it does not matter it is an identity you do not care about the discussion on the validity of the hypothesis it become an exact reality. So, on one side you have dilute monatomic gases. On another side, you have incompressible flows for which mechanical pressure is identical to thermodynamic pressure you do not have to put any hypothesis to measure its exactness.

So, we have been successful by the Stokes hypothesis to describe the property of the fluid by just one property which is the viscosity. We had two properties λ and μ but we have shown that λ can eventually be written as a function of μ . So, only property of the fluid viscosity is good enough to describe the state of stress of the fluid. So, with this understanding we will now get back to the Navier equation.

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Navier eq:

$$\rho \left[\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right] = \frac{\partial \tau_{ij}}{\partial x_j} + b_i$$

$$\frac{\partial \tau_{ij}}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_i} \left(\mu \frac{\partial u_k}{\partial x_k} \right) + \frac{\partial}{\partial x_j} \left(\mu \frac{\partial u_i}{\partial x_j} \right) + \frac{\partial}{\partial x_j} \left(\mu \frac{\partial u_j}{\partial x_i} \right)$$

The chalkboard shows the derivation of the Navier equation. It starts with the general form: $\rho \left[\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right] = \frac{\partial \tau_{ij}}{\partial x_j} + b_i$. Then it expresses the stress tensor divergence as $\frac{\partial \tau_{ij}}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_i} \left(\mu \frac{\partial u_k}{\partial x_k} \right) + \frac{\partial}{\partial x_j} \left(\mu \frac{\partial u_i}{\partial x_j} \right) + \frac{\partial}{\partial x_j} \left(\mu \frac{\partial u_j}{\partial x_i} \right)$. The terms are annotated with arrows and circles to show the relationship between the stress components and the velocity gradients.

So, this we derived in the previous lecture. This was the Navier equation and we discussed that this is a very general equation only issue is that there should be no body couple but the problem with handling this equation is that this has too many numbers of unknowns as compared to the numbers of available equations. So, now we will use the Newton's law of viscosity in place of this τ_{ij} . So, what is this τ_{ij} ?

τ_{ij} is equal to this one with λ is equal to minus two third of μ . So, we will substitute that here so we will write $\frac{\partial u_j}{\partial x_j}$. What is $\frac{\partial u_j}{\partial x_j}$? Go to the first term, partial derivative of this with respect of x_j see $\frac{\partial u_i}{\partial x_j}$ equal to one when j is equal to i so x_j will become x_i so it will become minus $\frac{\partial p}{\partial x_i}$. Next term plus $\frac{\partial}{\partial x_i}$ of similarly $\lambda \frac{\partial u_k}{\partial x_k}$ plus $\frac{\partial}{\partial x_j}$ of $\mu \frac{\partial u_i}{\partial x_j}$ plus $\frac{\partial}{\partial x_j}$ of $\mu \frac{\partial u_j}{\partial x_i}$.

Now, we will make a little bit of simplification to this term. What is the simplification first simplification is, it is a homogenous fluid we have considered so μ is not a function of position? If μ is not a function of position this will come out of the derivative. So, you can write this as $\mu \frac{\partial}{\partial x_j}$ of $\frac{\partial u_j}{\partial x_i}$. If the second order partial derivative is continuous then this is as good as $\mu \frac{\partial}{\partial x_i}$ of $\frac{\partial u_j}{\partial x_j}$.

We swap this x_i and x_j because for continuous, partial derivative it does not matter with respect to which you differentiate cost. And then this can be written as $\frac{\partial u_k}{\partial x_k}$. This is a dummy index, this j . So instead of j you can write whatever k it does not make any difference. So, what we are writing it k here you can see own that this term can be clubbed up with this term. Because here also λ , it is not a function of position.

So, you take λ out of this, so $\frac{\partial}{\partial x_i}$ of $\frac{\partial u_k}{\partial x_k}$ plus $\frac{\partial}{\partial x_i}$ of $\frac{\partial u_k}{\partial x_k}$. Here the coefficient is λ and here the coefficient is μ . So, with this we can write the next step.

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$$\rho \left[\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right] = - \frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_j} \left(\lambda \frac{\partial u_k}{\partial x_k} \right) + \frac{\partial}{\partial x_j} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] + b_i$$

- No body couple
- Homogeneous, isotropic, Newtonian fluid
- Stokesian fluid

NAVIER STOKES EQ.

Continuity: $\frac{\partial \rho}{\partial t} + \frac{\partial (\rho u_j)}{\partial x_j} = 0$

$\rho = \rho(p, T) \rightarrow$ Eq of stat.

Unknowns: $p, u_1, u_2, u_3, w_1, w_2, w_3$

So, $\rho \frac{\partial u_i}{\partial t}$ plus $q_j \frac{\partial u_i}{\partial x_j}$ and because λ and μ are not

position dependent we can take them out and inside the derivative without any problem. So, if you now club up these two terms together it will be. So, this $\lambda + \mu$, $\lambda + \mu$ equal to minus two third μ so this will become $\mu/3$. Clearly, the last term is important only for compressible flow. Because for incompressible flow this will be zero.

So, this equation what are the assumption associated with equation? So, first we use the Navier equation there the only assumption was no body couple then so no, body couple of course you also have to add up body force that is there so let us write that no body couple. Then the constructive behavior for that we assume a homogeneous isotropic and Newtonian fluid and finally we have assumed that the Stokes hypothesis is valid.

So, a fluid for which the Stokes hypothesis is valid is known as Stokesian fluid. So, with these assumptions we arrive at this equation of motion which is the celebrated Navier-Stokes Equations. So again, one of the physical implication of various terms. The left-hand side is mass into acceleration per unit volume. So, right hand side is force per unit volume. This is force due to pressure gradient.

This is the viscous force and this is the force due to volumetric dilatation combined with linear deformation. So, for compressible flow this term is already there but for incompressible flow this term is not present and this is any other body force. There are special cases when the left-hand side is equal to zero that means the fluid has no inertia that means the fluid is not accelerating then that equation is known as Stokes equation.

So, this the problem when a scientist does too many things. So, you have Stokes law, Stokes hypothesis, Stokes equation these are all different. Stokes law you have learned in high school physic that if you have a sphere which is in a terminal motion at a very slow velocity in a fluid then what this terminal velocity. How do you calculate the terminal velocity the drag force and so on?

That is Stokes law. Stokes hypothesis, mechanical pressure equal to thermodynamic pressure and Stokes equation is the Navier-Stokes equation with the left-hand side equal to zero. So, all these three are different things. Now let us see how many unknowns and how many equations you have? So, coupled with that you have the continuity equation. So now you tell how many unknowns are there? Unknown?

This equation basically, there are three components I equal to 1, 2, 3. So, how many unknowns? What are the unknowns? ρ , p , u_1 , u_2 , u_3 these are like basically u , v , w . So, you have five unknowns. How many equations you have? Here you have three equations and you have one, four equations. So, these also does not close the system. In a special case when it closes the system it closes the system when the density is the constant or given.

It may be a constant may not be a constant but some given function. So, if ρ is given or ρ is a constant as a special case then this system is closed. So, then you can solve for the velocity field by using the continuity and the momentum equation, momentum equation eventually becomes Navier-Stokes equation. If ρ is not given, then ρ is a function of what? ρ is function of pressure of temperature through the equation of state.

So, ρ is a function of pressure and temperature this is equation of state. But have increased another equation you have got another equation but you have increased another unknown the unknown is temperature. So, you wanted to solve for ρ but to introduce ρ through the equation of state you involved and unknown which is temperature and to solve for the temperature you need to solve for the energy equation.

You get a governing equation of temperature which is the energy equation in convection. So, you require basically the equation starting from fluid flow to the equation of state and the energy equation and sometimes the momentum and the energy equation may be directly coupled because the body force may be a function of temperature and that happens in natural convection and free convection.