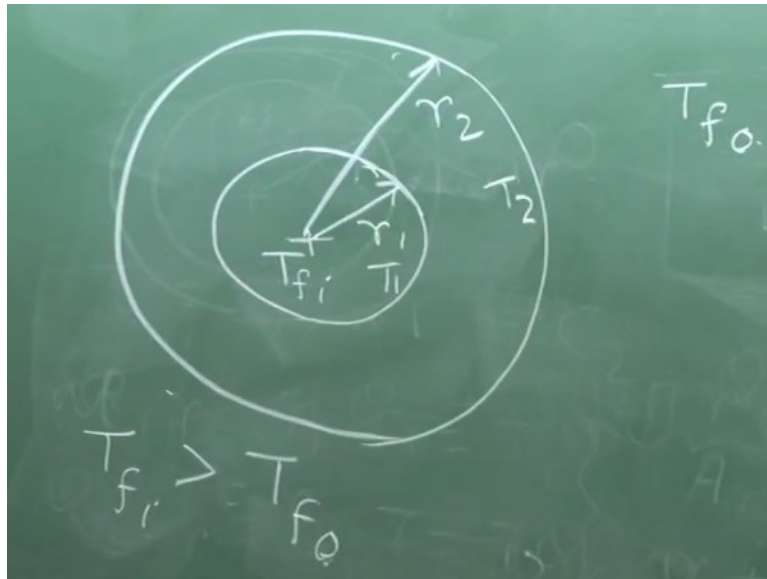


Conduction and Convection Heat Transfer
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Lecture 15

Now next similar to the plane wall, we can have a convective boundary conduction, means that this if I draw this convective that will be in arctic or plane.

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Instead of prescribing the inner surface than outer surface temperature, we prescribe the fluid temperature, inner fluid temperature which may be T_{fi} and outer fluid temperature which may be T_{fo} . That means the heat comes from the inner fluid through this, let us consider T_{fi} fluid temperature inner is greater than T_{fo} . Then first by convection heat will come to the inner surface and it will have a temperature T_1 , which is not prescribed.

And heat will flow by the conduction to the outer surface, which will attain some temperature T_2 , and from T_2 by convection it will go to outside fluid T_{fo} . For example, heat is lost from a hot fluid flowing through the pipe, flowing through the pipe. So, in that case T_1 , if T_1 and T_2 are not prescribed only T_{fi} T_{fo} , then what we can do we know that conduction heat transfer between T_1 and T_2 are the inner and outer surface temperature, which may not be prescribed but I take as temperature denoted as T_1 , T_2 .

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$$\frac{\ln\left(\frac{r_2}{r_1}\right)}{2\pi L K}$$

$$= h_i 2\pi r_1 L (T_{f_i} - T_1)$$

$$= h_o 2\pi r_2 L (T_2 - T_{f_o})$$

I already know that this is equal to $\ln r_2$ by r_1 divided by $2\pi LK$, and same heat Q is coming through, because of steady state the same thing is flowing by convection from the inner hot fluid to the surface, and if I prescribe H_i as the heat transfer coefficient of the inner fluid and H_o that of the outer fluid, then by our definition of the heat transfer coefficient in convection heat transfer.

It can be written as heat transfer coefficient into area, twice $\pi r_1 L$, inner surface area into T_{fi} minus T_1 and that is same as that those out from the outer surface to the outer fluid environment, which is taken to the cold here less, therefore this will be twice $\pi r_2 L$ into T_2 minus T_{fo} . So, in the similar way as we did earlier, we can express the T_1 , T_2 , Q times this. T_{fi} minus T_1 is Q times this, Q divided by this, and T_2 minus T_{fo} is Q divided by this, and this will sum it up.

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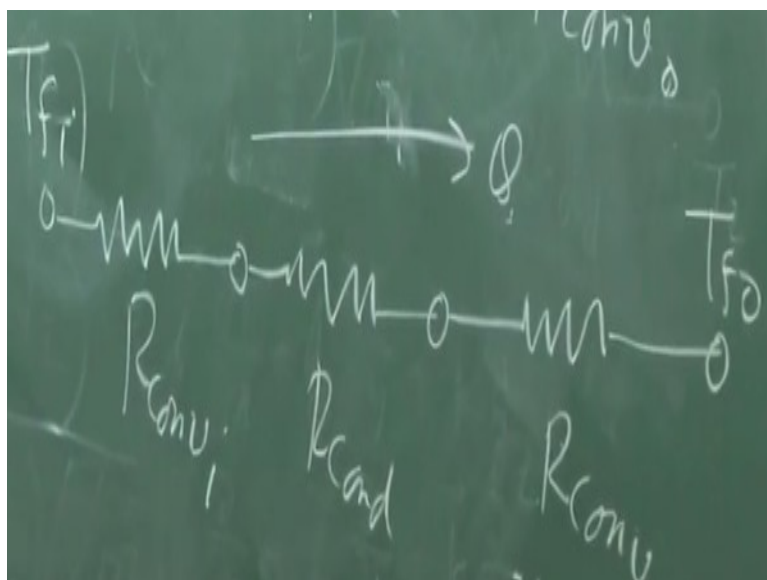
$$Q = \frac{(T_{fi} - T_{fo})}{\frac{1}{2\pi r_1 L h_i} + \frac{\ln\left(\frac{r_2}{r_1}\right)}{2\pi L K} + \frac{1}{2\pi r_2 L h_o}}$$

$R_{conv,i}$ R_{cond} $R_{conv,o}$

Then we get Q is equal to in terms of the extreme temperature difference, we here prescribe that is Tfi minus Tfo divided by 1 by 2 pi r1 h1 plus ln r2 by r3 divided by twice pi LK, r1 l, sorry twice pi, I am sorry, twice pi r1 L hi plus 1 by twice pi r2 L ho, extremely simple. So, it is the r1 and it is r2, ln r2 by r1, I have written r3, sorry, very good. Now this is same as the flat plane thing.

That means it is the sum of these three-series resistance. This is convection resistance, heat convection, inner surface i, this is R conduction, and this is R convection outer surface.

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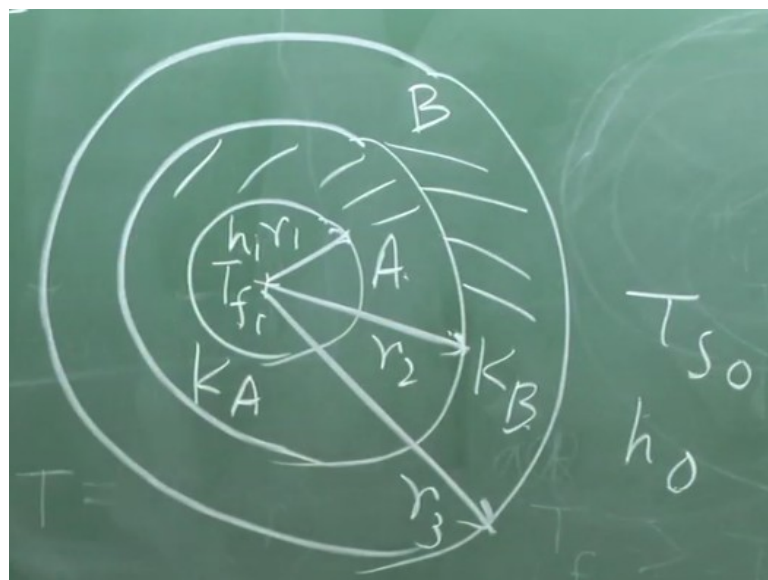
That means extremely simple, series resistance are in parallel, through which the same heat is flowing, and the electrical analogous circuit is like this, Tfi and Tfo. The same heat is flowing Q, with this is R convection i, whose value is 1 by 2 pi r1 L h1, and this is conduction and

this is R convection, same thing. We can also think of composite cylinder or composite cylindrical wall, which may be composed of different thermal conductivity.

Then, we will have the different conduction resistance in series, different conduction resistance in series. So, it will be nothing great if you solve problems, then you will see the application of this. That means instead of one cylindrical wall, we may have a composite cylindrical wall. That means we have another cylindrical layer of material, of different thermal conductivity.

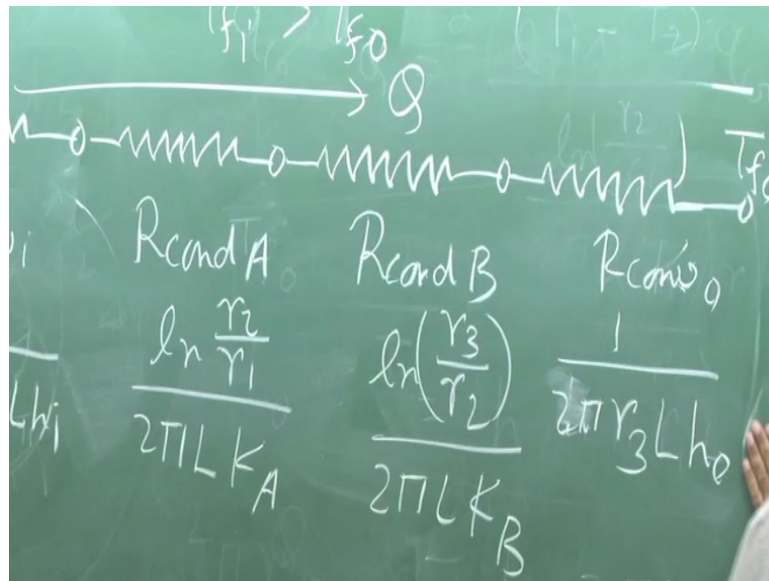
Then we will be adding another conduction resistance like this, that will be from r_2 to r_3 . That means if we have another, just like this I give you a picture like this and it will be very simple to deduce.

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It will be very simple to deduce, like this if we have two cylindrical wall, the radius is r_1 , r_2 and r_3 . Then r_1 to r_2 , this material, this is A, thermal conductivity K_A , and this r_2 to r_3 , this material is B with thermal conductivity K_B and if we have similar T_{fi} and T_{fo} , with h_o and h_i , heat transfer coefficient, then your circuit will be the same with another added resistance, which will be very simple to conceive and we can draw the network like this.

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One convective resistance, then two conduction resistance and another one convective resistance, so that the two terminals have the extreme potentials T_{fi} , Q flows like this. T_{fi} is greater than T_{fo} and we get this convection. What is that? 1 by twice $\pi r_1 L h_i$ then this is conduction for material A, that is $\ln r_2$ by r_1 , outer to inner radius divided by twice $\pi L k_A$. Similarly, this is R conduction B, which is $\ln r_3$ by r_2 outer to inner radius of this cylindrical wall divided twice $\pi L k_B$.

And this is finally R convection o, that is outer 1 by twice π , this I write first r_3 , the area, L into h_o , so this is so simple. Therefore, this is the thing, that means composite cylindrical wall with convective boundary condition are tackled like that. How do we get this distribution? We solve the temperature distribution by developing an expression from the energy balance that is by heat balance, energy balance in the conducting medium by taking a small elemental volume.

Or you can start with the general heat conduction equation as I have told, then you solve it for the special case. If there is heat generation, then heat generation format have to be taken is dependent with the spatial coordinate have to be taken if thermal conductivity depends on temperature, then the dependent has to be taken, and the problem becomes mathematical that means whatever is involved is mathematics.

So, there is no other heat transfer concept, but one very important case, which sometimes many books forget to tell that for a variable area, plane area problem, if you start from the general energy, general heat conduction equation, you will be lost. You have to develop that

equation by taking the, that I told in the last class, energy balance. Because the concept of variable area is not there.

Because it is integrated over a cross section to get a new temperature effect or the temperature being uniform, but area is varying that part will not be manifested. If you step forward take from the heat conduction equation, this is a very general mistake the student does, I tell you. A teacher always tells his experience from students end. The students always jump to the general energy equation.

He finds that okay, we make steady state, $\frac{dT}{dt} = 0$, we make $Q = 0$, we make everything 0, then you get that $\frac{d^2 T}{dx^2} = 0$, T has to be linear in x. Unfortunately, in a one-dimensional heat conduction is an approximation of four, for a varying area T is never linear. It is $A \frac{dT}{dx}$, it is constant, so $\frac{dT}{dx}$ is inversely proportional to A, that constant has to be cleared, but in cylindrical coordinate system.

Because of the coordinate system itself that area, it is inherent to the coordinate system that the area normal to heat flow, for example in the r direction heat is varying with that, it is directly proportional with r, so therefore from the general heat conduction equation, it is x a special, it will be the same as we derived by taking a simple element one dimensional Q_r and $Q_r + \frac{dQ_r}{dr} dr$ like that. Both the things are same.

I think for you people these two things have to be kept in mind, otherwise you will be in problem. That even a variable area, you will draw a linear temperature profile, then come to the teacher and tell why in a steady state one dimensional constant thermal conductivity, temperature is linear, why I have not got the marks, so this is very important. So, today I will stop here.

Well, this is little before the time, but the next thing is the critical thickness of insulation. That I will take in the next class. Now, I tell you, just wait. I give you a clue now before starting the next topic that when this heat flux is given by this, one thing you see that if you increase the outer radius, then two things happen in contrasting nature. We increase the outer radius, the conduction resistance increases, but the convection resistance decreases.

This is because the area, surface area of heat transfer increases. You understand, which is not the case for a plane area. If there is a heat transfer from a wall, if you go on adding material to increase the wall thickness in the direction of heat flow, you are sure that you are putting more conduction resistance and the heat flux will be arrested. That means, it will be reduced, obviously, because the dT/dx is getting reduced, but in a cylindrical geometry to increase the area.

If you increase the radius by more material, that means you are increasing the radial path for conduction and conduction resistance increases, but at the same time mathematically the convection resistance decreases means, the surface area, from which the convection heat transfer takes place increases and convection is directly proportional to surface area. Do you understand me?

So, therefore the two counteracting heat results in a very interesting problem as critical thickness of insulation, that means if you insulate a cylindrical pipe by giving insulating material, adding insulating material, the thermal conductivity is relatively much lower than common conducting material, does not always mean that we are going to reduce the heat loss. Ironically, you will see that you are increasing the heat loss.

Because they are two contradictory things. Conduction resistance increases, but the convection resistance decreases