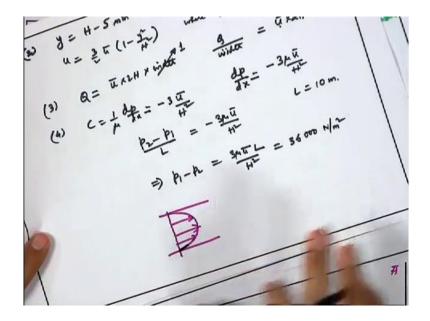
Introduction to Fluid Mechanics Prof. Suman Chakraborty Department of Mechanical Engineering Indian Institute of Technology, Kharagpur

Lecture – 54 Navier-Stokes equation- Part – IV

(Refer Slide Time: 00:17)



So, we will consider a second example of exact solution of the Navier-Stokes equation through something which is very important in fluid mechanics this is called a Couette flow.

(Refer Slide Time: 00:34)

Consider two parallel plates with relative motion; that means, let us say that the bottom plate is stationary and the top plate is moving towards the right with a velocity u_1 . The gap between the plates is small and the flow is fully developed.

 \rightarrow Steady, \rightarrow Incompressible, $\rightarrow 2-D$ In fully developed flow, v=0 x-momentum $0 = -\frac{dp}{dx} + \mu \frac{d^2u}{dy^2}$ $\frac{d^2 u}{dv^2} = \frac{1}{u} \frac{dp}{dx}$ Ex. $p_1 = p_2$ $\frac{dp}{dx} = \frac{P_2 - P_1}{L} = 0 \rightarrow pure$ Couette flow $\frac{d^2 u}{d v^2} = 0$ $\Rightarrow \frac{du}{dv} = C_1$ $\Rightarrow u = C_1 y + C_2$ B.C.s (1) At y=0, u = 0, (2) At y=H, u=u₁ $(1) C_2 = 0$ (2) $u_1 = C_1 H \Longrightarrow C_1 = \frac{u_1}{H}$ $u = \frac{u_1 y}{H}$

(Refer Slide Time: 11:03)

Ex. 2 Consider steady incompressible fully developed flow of water at 20⁰ C between two horizontal parallel plates with the gap between the plates is 2 cm. A constant pressure gradient $\frac{dp}{dx} = -900Pa/m$. The upper plate moves with a uniform speed whereas, the lower

plate is stationary. Find the velocity of the upper plate. $(\mu = 10^{-3} Pa.s)$

$$0 = -\frac{dp}{dx} + \mu \frac{d^2 u}{dy^2}$$

Solution:

$$\frac{d^2u}{dy^2} = \frac{1}{\mu}\frac{dp}{dx} \Longrightarrow \frac{du}{dy} = \frac{1}{\mu}\frac{dp}{dx}y + C_1 \Longrightarrow u = \frac{1}{\mu}\frac{dp}{dx}\frac{y^2}{2} + C_1y + C_2$$

B.C. (1) At y=0, u =0 \Rightarrow C₂ = 0

(2) At y=H, u=u₁
$$\Rightarrow$$
 $u_1 = \frac{1}{\mu} \frac{dp}{dx} \frac{H^2}{2} + C_1 H \Rightarrow C_1 = \frac{u_1}{H} - \frac{1}{\mu} \frac{dp}{dx} \frac{H}{2}$
 $u = \frac{1}{2\mu} \frac{dp}{dx} (y^2 - yH) + u_1 \frac{y}{H}$

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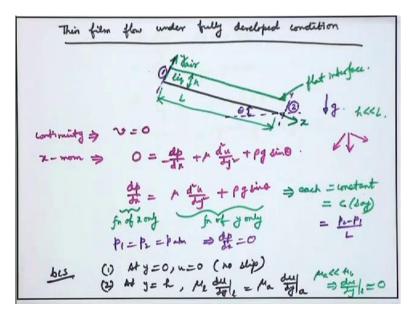
$$\begin{split} & \bigoplus_{ij \in I} = \int_{0}^{ij} u \, dy = \int_{ij}^{ij} \frac{dy}{dx} \int_{0}^{ij} (j-y) \, dy + \int_{0}^{ij} u_{ij} \frac{dy}{dx} \, dy \\ & \bigoplus_{ij \in I} = \int_{0}^{ij} \frac{dy}{dx} \left[\frac{H^{3}}{3} - \frac{H^{3}}{2} \right] + \frac{H}{H} \frac{H^{2}}{2}. \\ & = -\int_{12\mu}^{ij} \frac{dy}{dx} + \frac{H^{3}}{4} + \frac{H}{H} = 0 \\ & u_{1} = +\int_{0}^{ij} \frac{dy}{dx} + \frac{H^{3}}{4} = -60 \, \text{M/s}. \end{split}$$

$$(32) \quad U_{1} = +\int_{0}^{ij} \frac{dy}{dy} + \frac{H^{2}}{4} = -\frac{1}{2\mu} \frac{dy}{dx} \left[(2d-H) + \frac{H}{H} \right]_{y=H}. \\ & = \int_{12\mu}^{ij} \frac{dy}{dx} + \frac{H}{H} = 0 \quad \Rightarrow u_{1} = -\frac{H^{2}}{2\mu} \frac{dy}{dx} = -180 \, \text{M/s}. \end{split}$$

$$\frac{Q}{width} = \int_{0}^{H} u dy = \frac{1}{2\mu} \frac{dp}{dx} \int_{0}^{H} (y^{2} - yH) dy + \int_{0}^{H} u_{1} \frac{y}{H} dy$$
$$\frac{Q}{width} = \frac{1}{2\mu} \frac{dp}{dx} \left[\frac{H^{3}}{3} - \frac{H^{2}}{2} \right] + \frac{u_{1}}{H} \frac{H^{2}}{2} = -\frac{1}{12\mu} \frac{dp}{dx} H^{3} + \frac{u_{1}H}{2} = 0$$
$$u_{1} = +\frac{1}{6\mu} \frac{dp}{dx} H^{2} = -60m/s$$
$$(2) \tau_{w}|_{y=H} = \left| \mu \frac{du}{dy} \right|_{y=H} = \frac{1}{2\mu} \frac{dp}{dx} \left[(2y - H) + \frac{u_{1}}{H} \right]_{y=H}$$

$$\frac{1}{2\mu}\frac{dp}{dx}H + \frac{u_1}{H} = 0 \Longrightarrow u_1 = -\frac{H^2}{2\mu}\frac{dp}{dx} = 180m/s$$

(Refer Slide Time: 24:00)



Thin film flow under fully developed condition

Continuity
$$\Rightarrow v = 0$$

 $x - momentum \Rightarrow 0 = -\frac{dp}{dx} + \mu \frac{d^2 u}{dy^2} + \rho g \sin \theta$
 $\frac{dp}{dx} = \mu \frac{d^2 u}{dy^2} + \rho g \sin \theta \Rightarrow each = const = C(say) = \frac{P_2 - P_1}{L}$

(Refer Slide Time: 30:23)

$$\mu \frac{d^2 u}{dy^2} + \rho g \sin \theta = 0$$

$$\Rightarrow \frac{d^2 u}{dy^2} = -\frac{1}{\mu} \rho g \sin \theta$$

$$\Rightarrow \frac{du}{dy} = -\frac{1}{\mu} \rho g \sin \theta y + C_1$$

$$\Rightarrow u = -\frac{1}{\mu} \rho g \sin \theta \frac{y^2}{2} + C_1 y + C_2$$

B.C.s (1) At y=0, u =0(no slip)

(2) At y=h,
$$\mu_l \frac{du}{dy}\Big|_l = \mu_a \frac{du}{dy}\Big|_a$$

$$\mu_a \ll \mu_l \Longrightarrow \frac{du}{dy}\Big|_l = 0$$

B.C.s (1) At y=0, u =0 \Rightarrow C₂ = 0

(2) At y=h,
$$\frac{du}{dy} = 0$$

$$\Rightarrow 0 = -\frac{\rho g h \sin \theta}{\mu} + C_1 \Rightarrow C_1 = \frac{\rho g \sin \theta}{\mu}$$

$$u = -\frac{\rho g \sin \theta}{\mu} \left(\frac{y^2}{2} - yh \right)$$

(Refer Slide Time: 35:19)

So, we will consider steady, laminar incompressible, fully developed, flow through a circular pipe, this is called as Hagen Poiseuille flow.

Fully developed flow, $v_r = 0$

Z-momentum eqn $0 = \frac{1}{r} \frac{d}{dr} \left(\mu r \frac{dv_z}{dr} \right) + \left(-\frac{dp}{dz} \right)$

$$\frac{1}{r}\frac{d}{dr}\left(r\frac{dv_z}{dr}\right) = \frac{1}{\mu}\frac{dp}{dz}$$

(Refer Slide Time: 39:12)

$$\frac{1}{2\pi} \frac{d}{d\pi} \left(n \frac{dv_{\Phi}}{d\pi}\right) = C$$

$$\frac{n}{dv_{\Phi}} \frac{dv_{\Phi}}{d\pi} = \frac{cn^{2}}{2\pi} + C_{1}$$

$$\frac{Bc}{d\pi} \left(0 \frac{dt}{d\pi} = 0, \frac{dv_{\Phi}}{d\pi} = 0 \Rightarrow C_{1} = 0. \Rightarrow \frac{dv_{\Phi}}{d\pi} = \frac{ch}{2}$$

$$\frac{v_{T}}{v_{T}} = \frac{ch^{2}}{4} + C_{2}$$

$$(2) \frac{dt}{d\pi} = R, \quad v_{F} = 0 \Rightarrow C_{2} = -\frac{cR^{2}}{4}$$

$$\frac{v_{T}}{v_{F}} \frac{v_{F}}{u_{F}} = \frac{ch^{2}}{4} \frac{ch^{2}R^{2}}{rR^{2}} \frac{2\pi h dh}{rR^{2}} = \frac{ch^{2}R^{2}}{rR^{2}}$$

$$\frac{v_{F}}{v_{F}} \frac{d}{rR^{2}} = \frac{cR^{2}}{2} \frac{\sqrt{r}}{rR^{2}}$$

$$\frac{v_{F}}{v_{F}} = \frac{cR^{2}}{2} \frac{\sqrt{r}}{rR^{2}}$$

$$\frac{1}{r}\frac{d}{dr}\left(r\frac{dv_z}{dr}\right) = C$$

$$r\frac{dv_z}{dr} = \frac{cr^2}{2} + C_1$$
At r=0, $\frac{dv_z}{dr} = 0 \Rightarrow C_1 = 0 \Rightarrow \frac{dv_z}{dr} = \frac{cr}{2}$

$$v_z = \frac{Cr^2}{2} + C_2$$
At r=R, $v_z = 0 \Rightarrow C_2 = -\frac{CR^2}{4}$

$$v_z = \frac{C}{4}\left(r^2 - R^2\right)$$

$$\overline{u} = \frac{\int_{0}^{R} v_z 2\pi r dr}{\pi R^2} = \frac{\frac{C}{4}\int_{0}^{R} (r^2 - R^2) 2\pi r dr}{\pi R^2}$$

$$\overline{v} = \frac{C}{2R^2}\left(\frac{r^4}{4} - \frac{R^4}{2}\right) = -\frac{CR^2}{8}$$

$$\frac{v_z}{\overline{v}} = 2\left(1 - \frac{r^2}{R^2}\right)$$

(Refer Slide Time: 44:52)

$$C = -\frac{9}{R^{2}} = -\frac{1}{R} \frac{dp}{dz}$$

$$-\frac{ap}{R} = -\frac{8}{R^{2}} \frac{dp}{dz}$$

$$-\frac{ap}{L} = -\frac{8}{R^{2}} \frac{ap}{R^{2}}$$

$$-\frac{ap}{L} = \frac{8}{R^{2}} \frac{ap}{R^{2}}$$

$$-\frac{ap}{R} = \frac{8}{R^{2}}$$

$$\frac{R}{R} = \frac{8}{R^{2}}$$

$$\frac{R}{R} = \frac{1}{R}$$

$$C = -8 \frac{\overline{v}}{R^2} = \frac{1}{\mu} \frac{dp}{dz}$$

$$\frac{\Delta p}{\Delta z} = -\frac{8\mu\overline{v}}{R^2}$$

$$\Delta p = \frac{8\mu\overline{v}L}{R^2}$$

$$h_f = \frac{8\mu\overline{v}L}{\rho g R^2}$$

$$h_f = \frac{8\mu QL}{\rho g \pi R^4}$$

 $h_f = \frac{128\mu QL}{\rho g \pi D^4} \leftarrow Hagen$ Poiseuille eqn.

(Refer Slide Time: 49:54)

Darry fields futer:
$$k_{f} = \bigoplus_{l=1}^{\infty} \frac{\overline{v}_{l}^{2}}{2g}$$
.
 $k_{f} = \frac{8\mu\overline{v}L}{P_{\overline{s}R^{2}}} = \frac{8\mu8L}{R_{\overline{s}R^{2}}}$
 $= \frac{5L}{9}\frac{\overline{v}_{1}^{2}}{2g}$.
 $\Rightarrow f = \frac{8\mu\overline{s}K}{P_{\overline{s}R^{2}}} \times \frac{aK_{12}g}{K_{\overline{s}K}}$
 $f = \frac{64}{P\overline{v}D} = \frac{64}{R_{2D}}$.

Darcy friction factor: $h_f = f \frac{L}{D} \frac{\overline{v}^2}{2g}$

$$h_{f} = \frac{8\mu\overline{\nu}L}{\rho gR^{2}} = \frac{8\mu QL}{\pi\rho gR^{2}} = f\frac{L}{D}\frac{\overline{\nu}^{2}}{2g}$$
$$f = \frac{8\mu\overline{\nu}L}{\rho gR^{2}} \times \frac{2R \times 2g}{L\overline{\nu}^{2}}$$

$$f = \frac{64}{\frac{\rho \overline{\nu} D}{\mu}} = \frac{64}{\text{Re}_D}$$