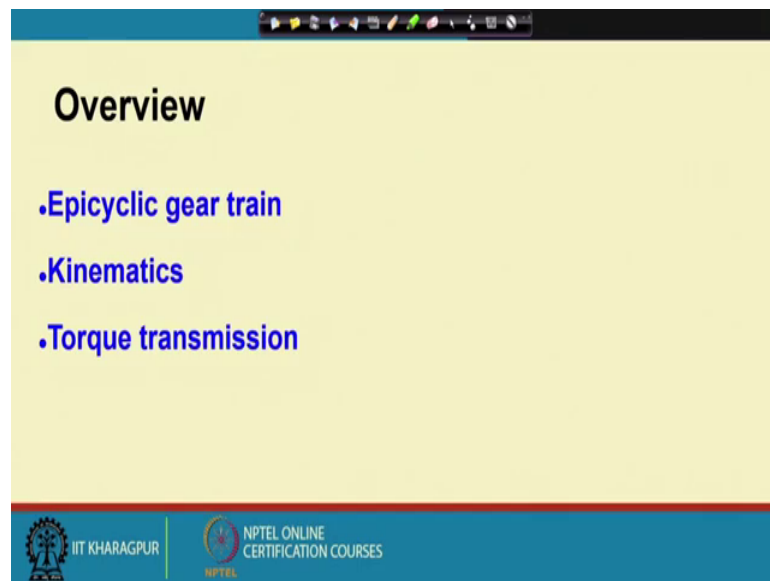


Kinematics of Mechanisms and Machines
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Indian Institute of Technology, Kharagpur

Lecture - 39
Gear Trains – II

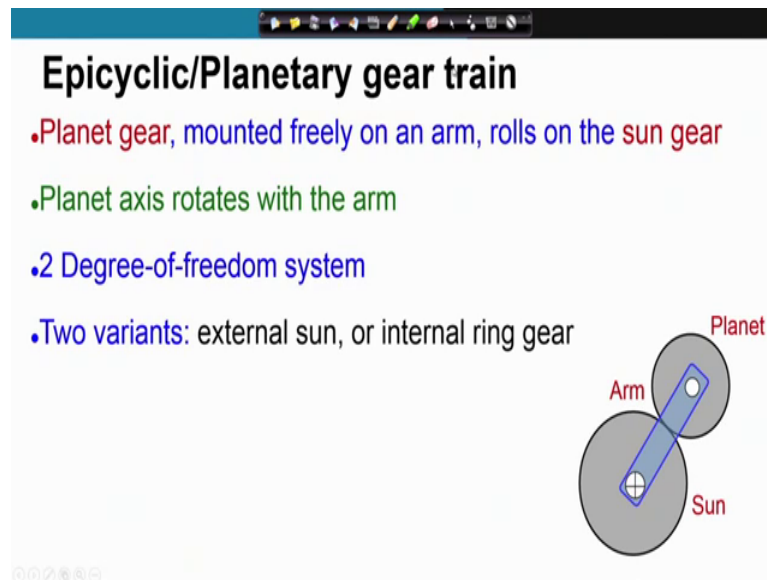
We will continue our discussion on Gear Trains.

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In this lecture, I am going to discuss about epicyclic gear train; their kinematics and torque transmission.

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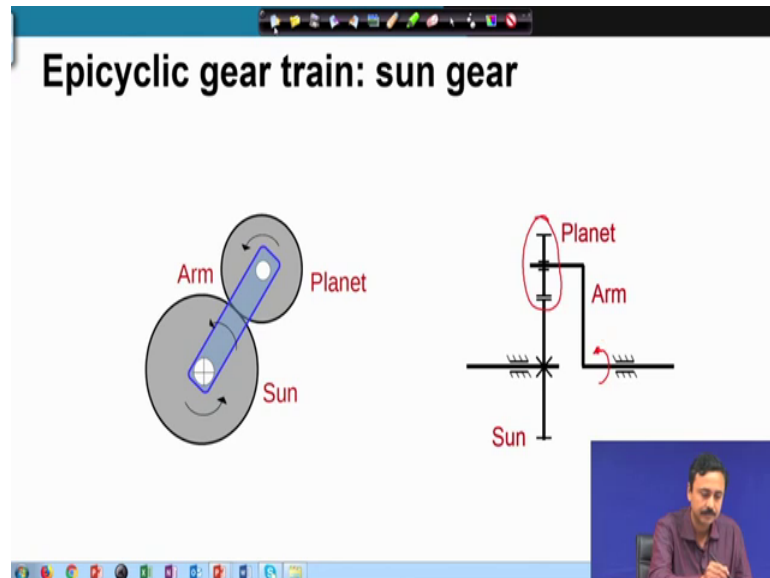
Then, epicyclic gear train as I have mentioned that there are gears whose centres can move or rotate in space. This is unlike the simple and the compound gear trains where their centres are fixed. The epicyclic gear train has these components, it has got planet gear which is mounted freely on an arm and it rolls on what is known as the sun gear. This is the analogy is from our solar system.

So, here I have sun gear on which there is this planet gear which meshes with the sun gear. The sun gear axis is fixed which is indicated by this cross at the centre; while the planet can roll freely on the sun gear. In order to keep the planet in place we have the arm. So, that keeps the planet in its place as it rolls on the sun gear. So, the planet axis rotates with the arm as it is shown here. This system has 2 degrees-of-freedom, let us understand this.

If I want to fix the configuration of the sun planet system, sun planet and arm system; then, suppose I fix the angle of the arm; I fix the angle of the arm. So, that is 1 degree-of-freedom, I can arbitrarily choose the angle of the arm. Suppose, I fix this; then still the sun and the planet can rotate with respect to one another; therefore, if I fix the sun at a particular angle then the planet also gets fixed. Therefore, I can fix the arm and the angle of the sun to fix the whole system. So, this has 2 degrees-of-freedom since we require two variables to fix up the configuration.

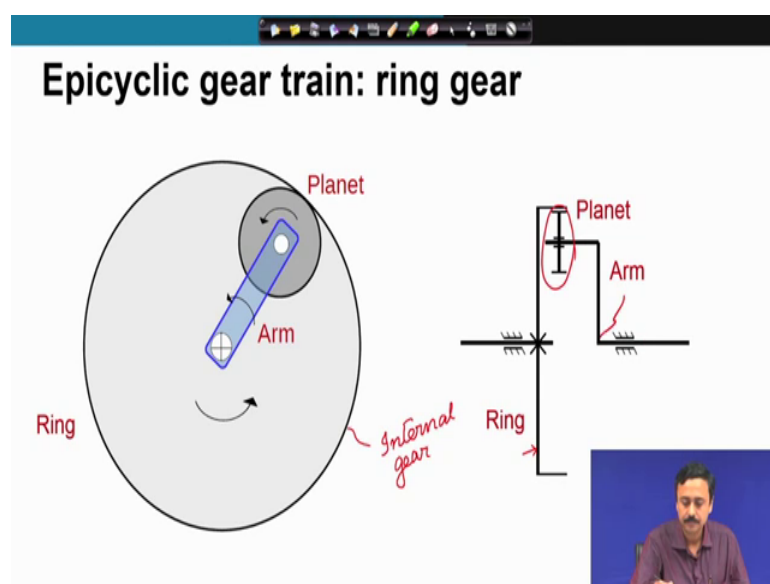
Now, there are two variants as we will soon see, we have this external sun external gear which is the Sun or an internal gear which is a ring gear.

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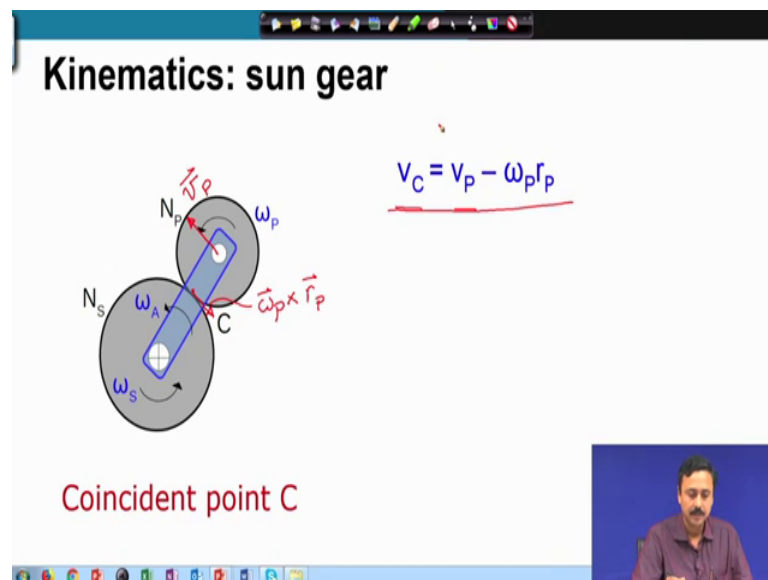
Here, is an epicyclic gear train with the sun gear, if you look at the representation; a schematic representation of this, the Sun gear axis is fixed where as the planet is mounted freely on the arm, the arm can rotate. So, therefore, the arm carries the planet as the planet measures on roles on the Sun.

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This is the second type in which we have a ring here. So, this is an epicyclic gear train with a ring gear this is an internal gear, so, the ring gear is an internal gear. If you look at the schematic representation, this is the ring gear and we have the planet mounted freely on the arm.

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Let us now look at the kinematics of the epicyclic gear train. In order to derive the relation between the input and output, we know that there are 2 inputs and 1 output just 2 degrees-of-freedom. Therefore, we consider this contact point C of the pitch circles of the sun and the planet gears and trying to do a velocity matching at the contact; this is for pure rolling.

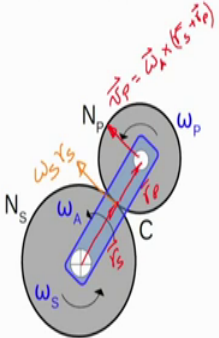
Now, if you look at the velocity of the point C as seen from the planet gear side, this can be written as velocity of the contact on the planet is equal to velocity of the centre of the planet and plus $\omega_p \times r_p$. Let us look at these vectors one by one. V_P which is the velocity of the planet centre, this is the velocity of the planet because of the rotation of the arm. So, this velocity V_P is because of the rotation of the arm.

Then we have because of the rotation of the planet itself about its centre, we have this is $\omega_p \times r_p$. And if you do this calculation and finally, write out this vector equation, then it turns out that because these two vectors are in a position. So,

velocity of the centre of the contact point velocity of the contact point C of the planet is equal to velocity of the centre of the planet minus omega P times r P.

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Kinematics: sun gear



$$v_C = v_P - \omega_P r_P$$

$$= \omega_A (r_S + r_P) - \omega_P r_P$$

Also,

$$v_C = \omega_S r_S$$

Equating

$$\omega_S r_S = \omega_A (r_S + r_P) - \omega_P r_P$$

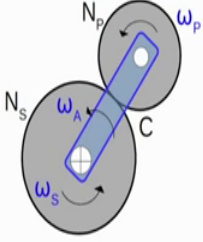
Coincident point C

Now, velocity of the centre of the planet this vector V P which I had drawn this is V P. As I have mentioned that this is because of the rotation of the arm. So, this must be equal to, so, omega of the arm cross the length of the arm which is summation of these two vectors; one is radius of the radius vector of the sun and this vector the radius of the planet.

Therefore, if you express velocity of the centre of the planet, it will be omega A times sum of the radii of the sun and the planet and minus omega P r P. If you look from the sun side, then velocity of the contact from the sun side is equal to omega of the sun times the radius of the sun. So, this is omega of the sun times radius of the sun. So, that is the velocity of the contact when you calculate it from the sun gear side. Now, these two must match because these two pitch circles are in pure roll.

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Kinematics: sun gear



$$\omega_s r_s = \omega_A (r_s + r_p) - \omega_p r_p$$

$$(\omega_s - \omega_A) r_s = -(\omega_p - \omega_A) r_p$$

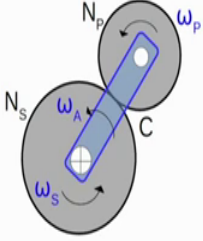
$$\frac{\omega_p - \omega_A}{\omega_s - \omega_A} = -\frac{r_s}{r_p} = -\frac{N_s}{N_p}$$

If you do that, then $\omega_s r_s$ must be equal to $\omega_A r_s$ plus r_p minus $\omega_p r_p$. Now, if you simplify this expression, you can write this as $\omega_s r_s$ minus $\omega_A r_s$ is equal to minus of $\omega_p r_p$ minus $\omega_A r_p$. So, therefore, now I can take the ratio let us say ω_p minus ω_A by ω_s minus ω_A that is equal to minus of r_s by r_p and this you also know is equal to minus of N_s by N_p .

So, this relation that we have obtained relates ω_p of the planet ω_s of the sun and ω_A of the arm in terms of the number of teeth on the sun and the number of teeth on the planet.

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Kinematics: sun gear



$$\omega_s r_s = \omega_A (r_s + r_p) - \omega_p r_p$$

Simplifying

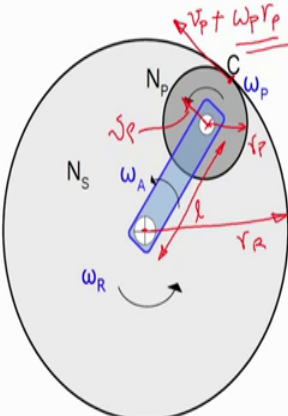
$$(\omega_p - \omega_A) / (\omega_s - \omega_A) = -r_s / r_p$$

$$(\omega_p - \omega_A) / (\omega_s - \omega_A) = -N_s / N_p$$

So, this I write out for you. So, this is the final expression of the motion relation. From here given let us say omega of the arm and omega of the sun, you can find out omega of the planet or given the omega of the planet and omega of the sun, you can find out omega of the arm.

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Kinematics: ring gear



$$\omega_R r_R = \omega_A (r_R - r_p) + \omega_p r_p$$

$$v_p = \omega_A l = \omega_A (r_R - r_p)$$

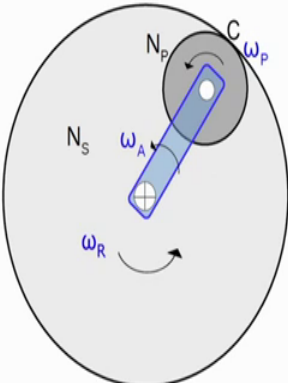
Let us now look at the other case where you have a ring gear. So, here you have this relation from similar considerations that omega of the contact as seen from the planet side, this must be equal to velocity of the centre of the planet. Now, plus omega planet

times radius of the planet, so, from the planet side if you calculate, velocity of C is equal to velocity of the centre of the planet plus omega P times r P. Velocity of the planet is nothing but omega arm times this length, this is the velocity of the planet, this vector is V P.

What is V P? Now, V P is equal to if I call this l, V P is equal to omega arm times this length l. Now this length l can be written as radius of the ring gear minus the radius of the planet gear. Radius of the ring gear minus radius of the planet gear and that has been substituted here, this term comes from here and we match the velocity of the contact from the ring gear side which is omega R times radius of the ring gear.

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Kinematics: ring gear



$$\omega_R r_R = \omega_A (r_R - r_P) + \omega_P r_P$$

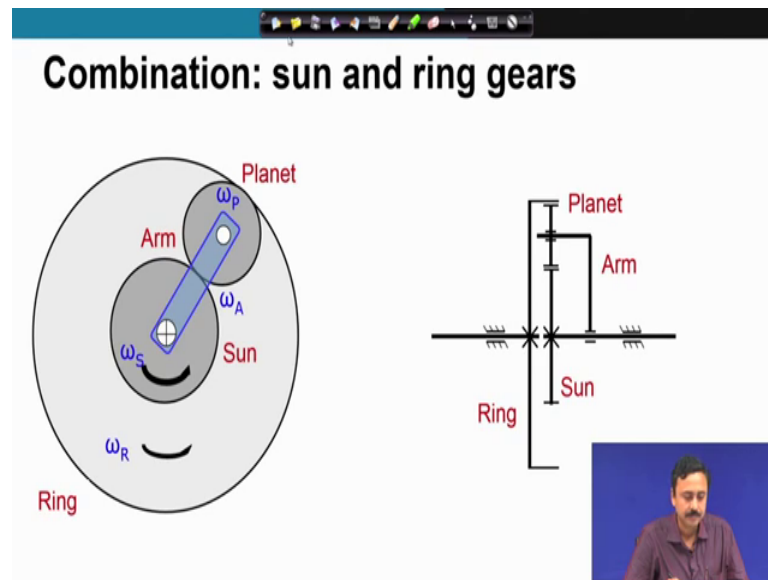
Simplifying

$$(\omega_P - \omega_A) / (\omega_R - \omega_A) = r_R / r_P$$

$$(\omega_P - \omega_A) / (\omega_R - \omega_A) = N_R / N_P$$

If you simplify this expression, we have this relation and you can write this ratio of the on the right hand side r R by r P as N R by N P. Here you should notice that because this ring gear being internal gear, the sign here is positive. This is unlike the relation we obtained when we had a sun gear. So, that completes the kinematics of the epicyclic gear train.

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Let us now look at the combination of both sun gear and a ring gear with a planet. Now this is the fundamental unit that is used in automatic transmission as we will discuss. This is the schematic representation of the gear train with this combination of ring and the sun.

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The slide is titled "Combination: kinematics". It features a schematic diagram of a planetary gear set with the Sun, Planet, Arm, and Ring components. The diagram includes labels for angular velocities (ω_R , ω_A , ω_S) and gear tooth counts (N_R , N_S , N_P). Handwritten notes include $\omega_A = 0$ and $\frac{\omega_S}{\omega_R} = -\frac{N_R}{N_S}$. The slide presents the following kinematic equations:

- Sun-planet: $(\omega_P - \omega_A)/(\omega_S - \omega_A) = -N_S/N_P$
- Ring-planet: $(\omega_P - \omega_A)/(\omega_R - \omega_A) = N_R/N_P$

The word "Dividing" is written in blue. A red box contains the resulting equation after dividing the two equations:

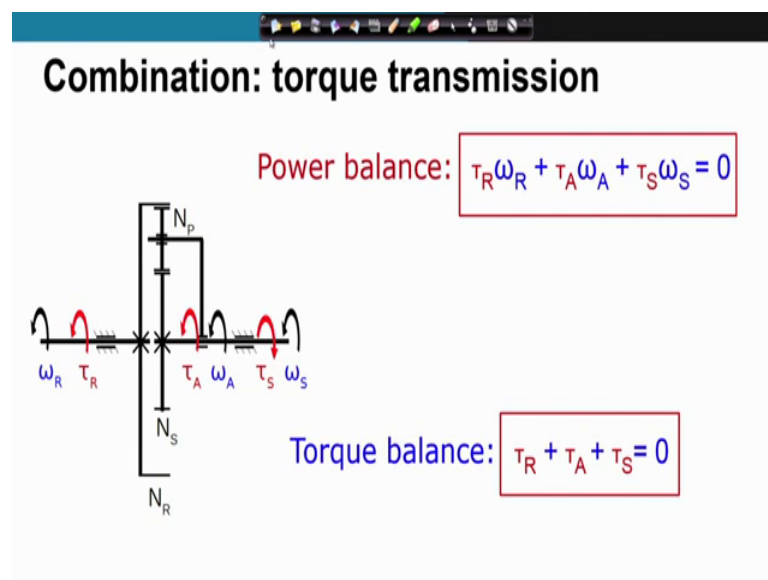
$$(\omega_S - \omega_A)/(\omega_R - \omega_A) = -N_R/N_S$$

Let us now look at this kinematics relations and go in pairs we will discuss we will look at these this combination in pairs. First let us look at the sun planet pair which means we are looking at this system in which we have the sun-planet and the arm. We have derived

the kinematic relation which is of this form. Next we look at the ring-planet combination; this is the ring-planet combination.

So, we had the ring gear, the planet gear and the arm and the kinematics for this, we have derived is written out here for you. You can clearly note the difference in these two relations. Now if you divide one by the other, then you can find out this relation between omega sun, omega arm, omega ring in terms of the teeth number of teeth on the ring and the sun. You will notice that this does not involve the planet anywhere. So, we have a relation between the angular speed of the sun the ring and the arm in terms of the number of teeth on the ring and the number of teeth on the sun.

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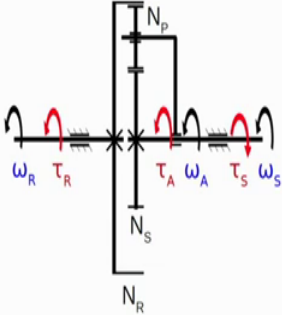


Now, let us look at torque transmission, here I have drawn out the torques that are acting tau R is the torque on the ring gear; tau A is the torque on the arm and tau S is the torque on the sun. If you do a power balance, then this is the relation we have been looking at this relation; if you do a power balance, then the net rate of work done on the system must vanish. There are 3 inputs, so, to say you have the power input at the ring, the power input at the arm and the power input at the sun and the total power input must add up to 0 that gives us the work power balance.


And we also have the torque balance relation because the whole thing is in equilibrium we are assuming that whole thing is in equilibrium; there is no dynamic forces acting, so, everything is in steady state.

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Combination: input-output calculations



- Two motion inputs and one output
- 3 equations, 6 variables: Multiple possibilities

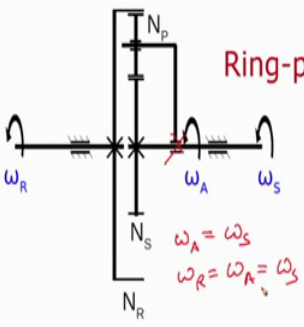


So, what do we have finally? We have 2 motion inputs and 1 output and we have obtained 3 equations in 6 variables. So, what are these three equations? One equation was the kinematic relation between the omega sun, omega ring and omega arm in terms of the number of teeth on the sun and the ring. The other equation was of power balance. So, the power input at the sun, power input at the arm and the power input at the ring. They must add up to 0 and the torque balance. These are the three equations we have in 6 variables, the 6 variables are shown in this figure; omega R, tau R, tau A, omega A and tau S, omega S. Now if we are given 3 of these variables and we can solve for the other 3.

If you quickly go back and look at this motion relation let us say, if we are given the omega of the ring and omega of the arm; then, from this relation we can solve for omega of the sun, so, we can solve the omega of the sun. Let us look at some very special cases. Let us say that I fix up omega of the arm as 0. Let me take some special cases; one special case can be omega arm is 0, which means my arm is fixed, it is not rotating. If omega arm is 0, then we have this relation omega S by omega R is minus of N R by N S which means its a simple transmission between the sun and the ring, I mean what we have for two external gears. On the other hand, if you let us say fix the arm with one of the gears.

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Combination: kinematics



Sun-planet: $(\omega_P - \omega_A)/(\omega_S - \omega_A) = -N_S/N_P$

Ring-planet: $(\omega_P - \omega_A)/(\omega_R - \omega_A) = N_R/N_P$

Dividing

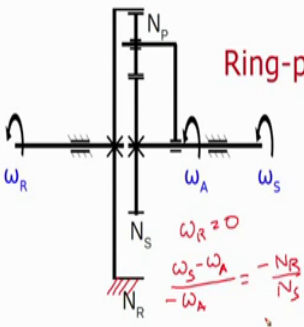
$$\frac{(\omega_S - \omega_A)}{(\omega_R - \omega_A)} = -N_R/N_S$$

Handwritten notes: $\omega_A = \omega_S$, $\omega_R = \omega_A = \omega_S$

Let us say omega arm is equal to omega sun. Suppose I fix the arm on to the sun which means I fix this, then omega arm and omega sun, they are equal. If that be so, then this whole thing vanishes, this becomes 0. Therefore, in order to have this relation valid this also must be 0 which means that the omega of the ring gear must be equal to omega of the arm and that is equal to omega of the sun, therefore, all of them are match. Therefore, if I fix the arm on to let say the sun, all the shafts move on at the same angular speed.

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Combination: kinematics



Sun-planet: $(\omega_P - \omega_A)/(\omega_S - \omega_A) = -N_S/N_P$

Ring-planet: $(\omega_P - \omega_A)/(\omega_R - \omega_A) = N_R/N_P$

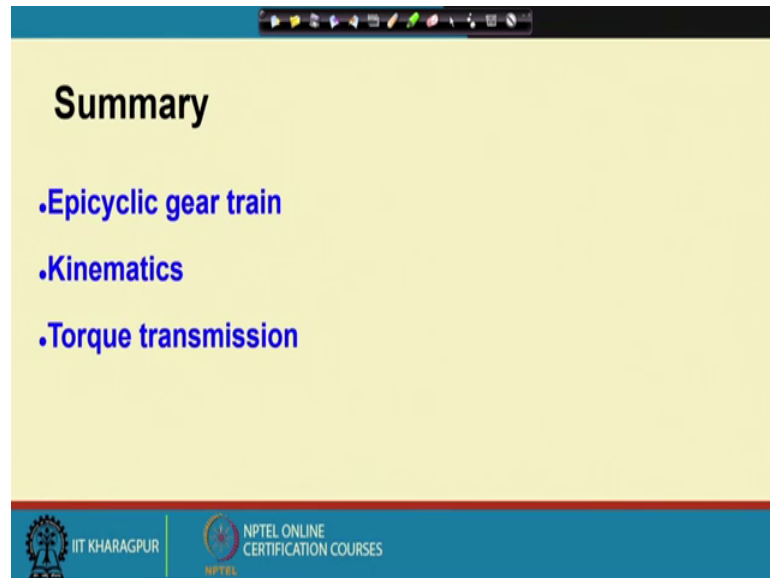
Dividing

$$\frac{(\omega_S - \omega_A)}{(\omega_R - \omega_A)} = -N_R/N_S$$

Handwritten notes: $\omega_R = 0$, $\frac{\omega_S - \omega_A}{-\omega_A} = -\frac{N_R}{N_S}$

So, ω all the gears move at the same angular speed ω_R is equal to ω_A is equal to ω_S . If I let us I fix the ring gear; let us say if I fix the ring gear which means I do not allow this to rotate, then I have this relation $\omega_{\text{sun}} - \omega_{\text{arm}}$ by minus ω_a is minus N_R by N_S . So, now various combinations you can calculate the relation between the gears the angular speeds of the gears.

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So, let me conclude by summarising what we have discussed. We have looked at the epicyclic gear train their kinematics considering both a sun-planet gear and a planet-ring gear and a combination of these two. You have calculated the motion transmission and the torque transmission ratios. So, with that I will close this lecture.