

Refrigeration and Air Conditioning
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Lecture No. # 14
Vapour Absorption Refrigeration Systems

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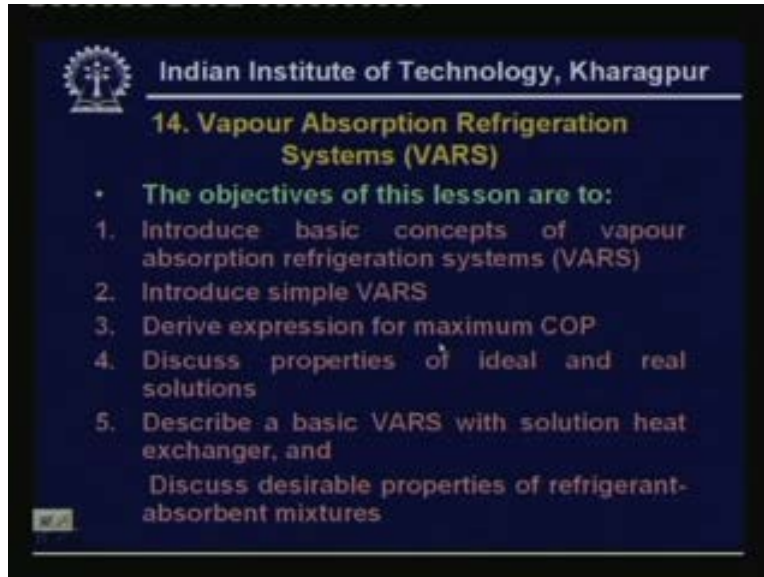
Welcome back in the last few lectures we discussed compression refrigeration systems.

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So in this lecture I shall introduce another very important refrigeration system known vapour absorption refrigeration system.

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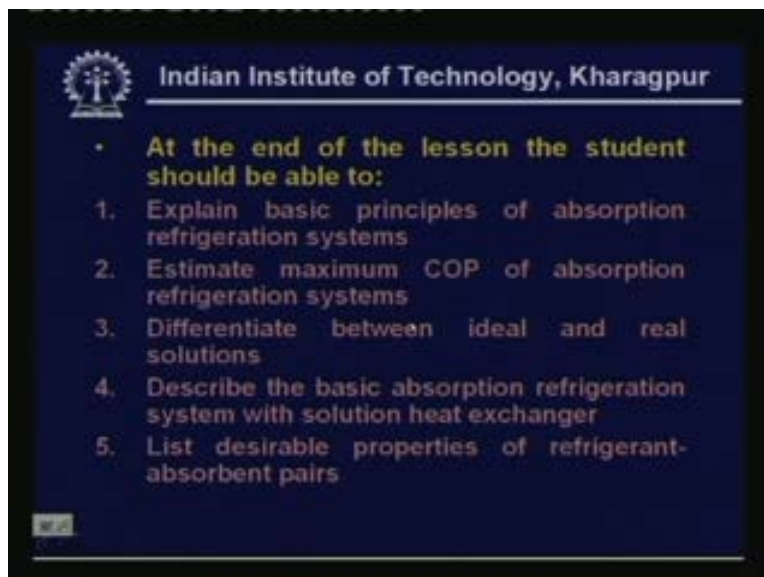
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14. Vapour Absorption Refrigeration Systems (VARs)

- **The objectives of this lesson are to:**
 1. Introduce basic concepts of vapour absorption refrigeration systems (VARs)
 2. Introduce simple VARs
 3. Derive expression for maximum COP
 4. Discuss properties of ideal and real solutions
 5. Describe a basic VARs with solution heat exchanger, and
Discuss desirable properties of refrigerant-absorbent mixtures

So the specific objective of this particular lesson are to introduce basic concepts of vapour absorption refrigeration systems, introduce simple vapour absorption refrigeration system derive expression for maximum COP, discuss properties of ideal and real solutions, describe a basic vapour absorption refrigeration system with solution heat exchanger and finally discuss desirable properties of refrigerant absorbent mixtures.

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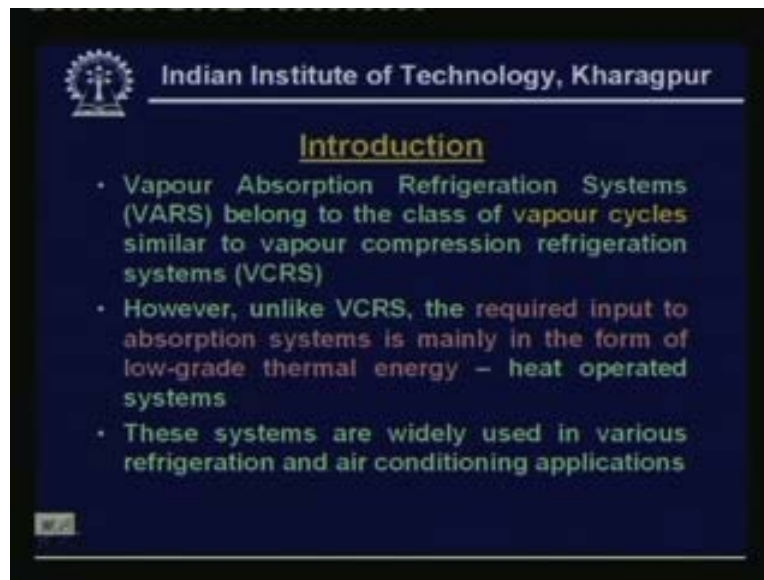
The slide features the IIT Kharagpur logo in the top left corner. The title 'Indian Institute of Technology, Kharagpur' is at the top. Below it, a bullet point states 'At the end of the lesson the student should be able to:' followed by a numbered list of five items.

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- **At the end of the lesson the student should be able to:**
 1. Explain basic principles of absorption refrigeration systems
 2. Estimate maximum COP of absorption refrigeration systems
 3. Differentiate between ideal and real solutions
 4. Describe the basic absorption refrigeration system with solution heat exchanger
 5. List desirable properties of refrigerant-absorbent pairs

At the end of this lesson you should be able to explain basic principles of absorption refrigeration systems estimate maximum COP of absorption refrigeration systems, differentiate between ideal and real solutions, describe the basic absorption refrigeration system with solution heat exchanger and finally list desirable properties of refrigerant absorbent pairs.

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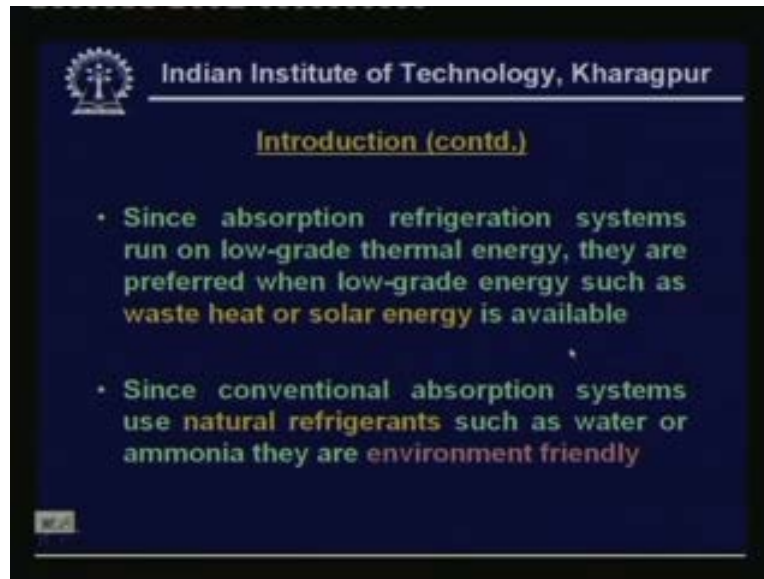


let me give a brief introduction vapour absorption refrigeration systems belong to the class of vapour cycles similar to vapour compression refrigeration systems okay. That means they are just like vapour compression systems these are also vapour cycles. That means as I have already explained the working fluid undergoes a phase change during the cycle. So they are vapour cycles like compression systems but there is one major difference between absorption systems and compression systems what is the difference. Unlike vapour compression refrigeration systems the required input absorption systems is mainly in the form of low grade thermal energy if you remember in the compression system the major input or the input to the system is in the form of mechanical energy to run the compressor okay.

So that is you can call that as a work of evaporator system where as in absorption refrigeration systems the main input to the system is in the form of low grade thermal energy or heat. That is why these systems are also known as heat operated systems or thermal energy driven system okay. This is the major difference between compression system and absorption systems these

absorption systems are also widely used in various refrigeration and air conditioning applications.

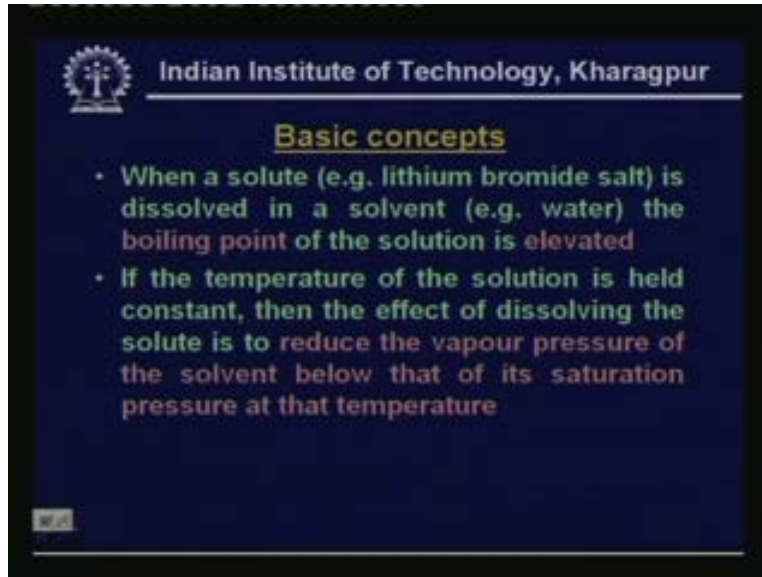
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Since absorption refrigeration systems run on low grade thermal energy they are preferred when low grade energy such as waste heat or solar energy is available. There are many industries and many situations where plenty of low grade thermal energy is either rejected its not used properly okay in such circumstances one can use vapour absorption refrigeration systems by tapping the low grade thermal energy. Our typical example is the waste heat rejected in many of the process plant etcetera or you can also use other low grade energy sources such as solar energy to drive the vapour absorption system.

This is one of the main applications and advantages of absorption systems compare to compression systems. That means you can use low grade energy sources okay. And since the working fluids used in absorption systems are mainly natural working fluid. That means you use either water or ammonia which are natural refrigerants these systems are environment friendly okay. These are two most important advantages of absorption systems compare to vapour compression refrigeration systems. So as I said since conventional absorption systems use natural refrigerants such as water ammonia they are environment friendly.

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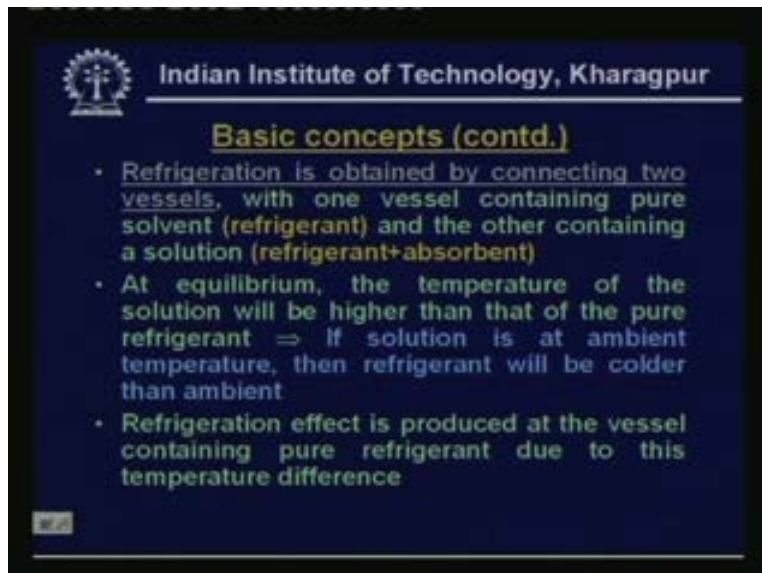
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Basic concepts

- When a solute (e.g. lithium bromide salt) is dissolved in a solvent (e.g. water) the boiling point of the solution is elevated
- If the temperature of the solution is held constant, then the effect of dissolving the solute is to reduce the vapour pressure of the solvent below that of its saturation pressure at that temperature

So let us look at some basic concepts. So first basic concept is that when a solute for example such as lithium bromide salt is dissolved in solvent example water. The boiling point of the solution is elevated okay, this you can also state in another way for example if you are keeping the temperature constant and if you are dissolving the solute in a solvent then the effect of this dissolving is to reduce the vapour pressure of the solvent below that of its saturation pressure at that temperature. This is the basic concept based on which the absorption systems have been built okay. So now let us look at the most basic absorption system.

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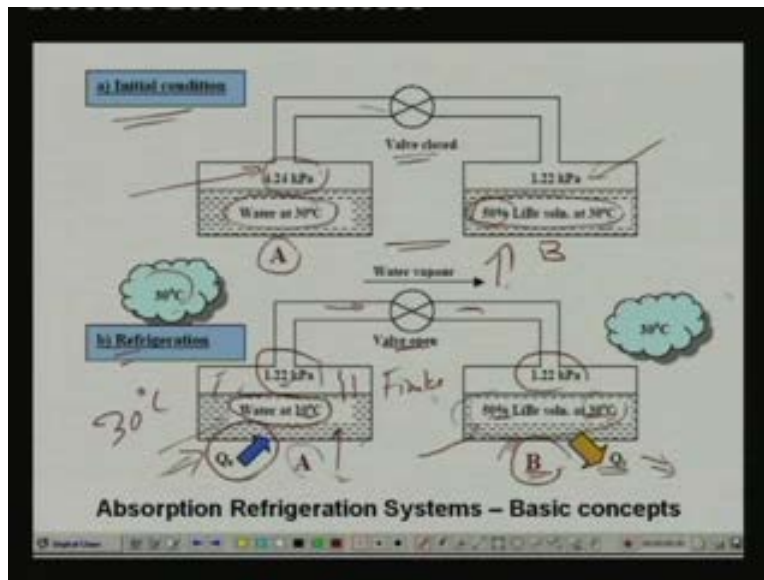
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Basic concepts (contd.)

- Refrigeration is obtained by connecting two vessels, with one vessel containing pure solvent (refrigerant) and the other containing a solution (refrigerant+absorbent)
- At equilibrium, the temperature of the solution will be higher than that of the pure refrigerant \Rightarrow If solution is at ambient temperature, then refrigerant will be colder than ambient
- Refrigeration effect is produced at the vessel containing pure refrigerant due to this temperature difference

In the basic absorption system refrigeration is obtained by connecting two vessels with one vessel containing pure solvent. So we call it as refrigerant and the other containing the solution which is the mixture of refrigerant plus absorbent. At equilibrium the temperature of the solution will be higher than that of the pure refrigerant when the pressures are same obviously. As I have mentioned already the temperature of the solution will be higher than that of the pure solvent and if the solution is at ambient temperature obviously the solvent. That means refrigerant will be at a temperature lower than the ambient. That means there is a temperature difference between the ambient and the solvent. So this is the temperature difference using which you can produce a refrigeration effect. So this is the basic principle. Now let me explain this with the schematic.

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What I have shown here, let us look at the initial conditions initially we have two vessels A and vessel B. Vessel A consists of pure water at thirty degree centigrade and vessel B consists of a solution of water and lithium bromide fifty percent lithium bromide by mass okay. So one is the pure solvent that is water the other one is mixture of water and lithium bromide salt. Let us say that initially the valve is closed and the entire system is in thermal equilibrium with surroundings which is at thirty degree centigrade. So every where you have thirty degree centigrade in vessel B as well as vessel A and vessel A and B are isolated okay. So now what is the vapour pressure in vessel A and what is the vapour pressure in vessel B if you look at the steam tables or steam

charts we will find that at thirty degree centigrade the saturation pressure of water is four point two four kilo Pascal.

That means the pressure inside the vessel A that means this side of the system is four point two four kilo Pascal which is nothing but the saturation pressure of water at thirty degree centigrade. Now what is the pressure on in vessel B since in vessel B we have we do not have pure water. But we have a solution obviously at the same temperature there will be a lower vapour pressure and if you look at the properties of lithium bromide water solution we will find that at fifty percent concentration and at thirty degree centigrade the pressure here is one point two two kilo Pascal.

These are the pressure at equilibrium conditions now you can maintain the pressures at different values because the valve is closed. Now let us say that we have opened the valve okay. Now come to this second part we open the valve initially what happens. Because of the pressure difference the vapour flows from this side to this side and since the solution lithium bromide water solution has an affinity for water vapour the water vapour gets absorbed here okay. So that means the water vapour is absorbed here and the pressure try to tries to be same in both the vessels okay.

So every where you have the uniform pressure now suppose by some means we are able to maintain the concentration and temperature in vessel B okay. Lets the discuss how we can do this a little later but for the time being assume that we are able to maintain the composition and temperature. Then what will be the pressure in the entire system the pressure in the entire system will be one point two two kilo Pascal which is decided by the solution and this is nothing but the equilibrium vapour pressure at this composition and this temperature. So on this side also you have one point two two kilo Pascal okay. If you have one point two two kilo Pascal here what will be the water temperature.

So again if you look at the steam tables or charts you will find that at one point two two kilo Pascal this temperature at equilibrium is nothing but the saturation temperature corresponding to this pressure. That means you will have ten degree centigrade temperature in the vessel A okay.

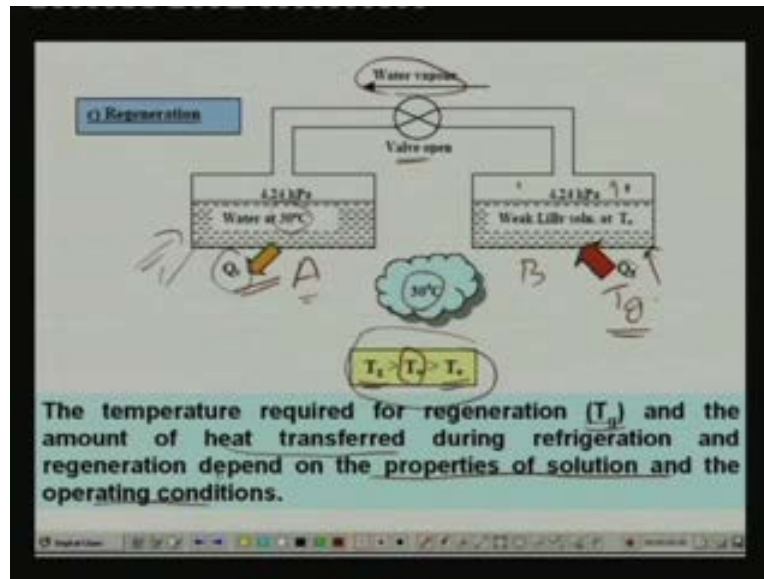
That means by having this combination and by opening the valve I could reduce the temperature from thirty degrees to ten degrees centigrade okay. And as long as you can maintain the conditions in B the conditions in A can be maintained at one point two two kilo Pascal and ten degree centigrade.

Now the outside temperature is thirty degree centigrade and the water is at ten degree centigrade. And let us assume that we do not have we have diathermic valve that means heat can be transferred from outside to the water. So there is heat transfer from the surroundings to the water and as a result of the heat transfer the water will evaporate okay. And this vapour continuously flows from vessel A to vessel B where it gets absorbed now the absorption process is an exothermic process in this case so heat released. And since you want to maintain the temperature at thirty degree centigrade this heat has got to be continuously rejected to the surroundings. That means during this step what we are doing is we are adding heat at vessel A and we are rejecting heat at vessel B.

And you are able to produce refrigeration effect here because you are able to transfer heat from the surroundings to a body at ten degree centigrade okay. That is why you are getting a refrigeration effect here. Now if you have a finite sized vessels let us say, that means A and B are finite sized then you have a finite amount of water in vessel A and finite amount of solution in vessel B and as a result of this water vapour transfer from vessel A to B at a point may come where vessel A may become empty or this may become saturated okay. That means once if this becomes take the first case when this vessel becomes empty means empty of liquid then there will not be any more heat transfer because nothing can evaporate okay. So the refrigeration effect stops here okay.

That means by this means whatever refrigeration effect you are able to produce that is intermittent and it will stop after some point when you are using finite vessels okay. So this is the so what do what we have to do to continue this process to continue this process what we have to do is we have to bring back this system to its original position okay. So how do we do that we do that by reason rating the water vapour okay. So let us see what is the reason rating process okay.

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So this is this picture here shows the process of regeneration during the regeneration process what we do is initially we keep the valve closed and bring the vessels A and B vessel A and B again to equilibrium with the surroundings. So again everything will be at thirty degrees centigrade. Now open the vessel open the valve and supply heat to vessel B okay. Now this due to the vapour transfer in the previous step this solution is weak that means it has more water vapour okay so when you are supplying heat at a particular temperature T_g okay. When you are supplying heat then water is generated at this point and this water vapour flows from this side to this side and if you are able to keep this at thirty degree centigrade. Then the water vapour is coming here it will condense at this pressure and at this temperature.

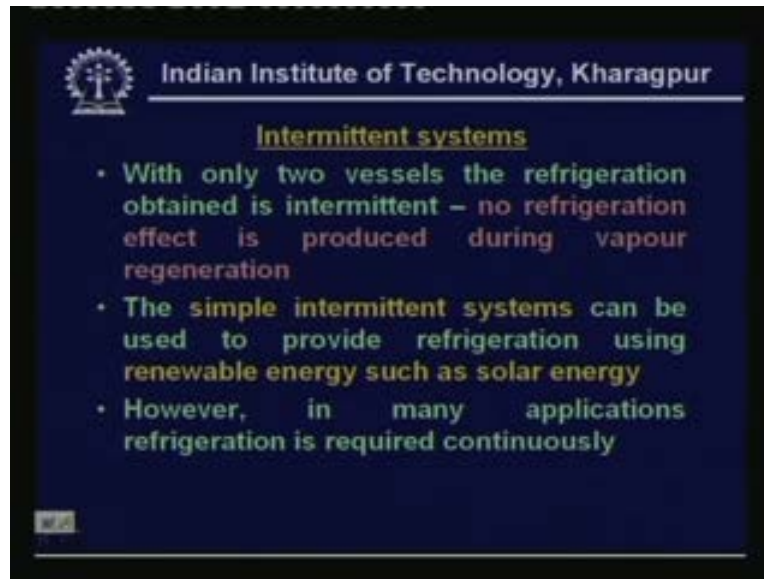
Since this is an exothermic process heat of condensation is rejected to the surroundings okay. That means during the regeneration process what we are doing we are supplying heat at high temperature T_g to the solution. So that vapour is generated and this vapour comes to the solvent side and it condenses by rejecting heat of condensation okay. So by you are transferring the, you are reversing the process and you are transferring water from the solution to the pure solvent side okay. This process will continue till you get the required amount of water on this side okay. Then to complete the process again you have to close the valve and bring these both the vessels to equilibrium with the surroundings at thirty degree centigrade so the process continues okay. So one thing you can notice here is we have so three temperatures here one is the T_g which is

nothing but the temperature at which heat is supplied to the solution for regeneration okay. Let us call that as generated temperature T_g okay.

And we have another temperature called the heat sink temperature. That means the temperature at which heat is rejected during absorption process and during the condensation process okay, T_{naught} and finally we have the refrigeration temperature T_e okay. It is the temperature at which refrigeration produced obviously T_g is greater than T_{naught} is greater than T_e okay. This relation holds good and now how do we decide the, what should be this temperature and how much heat has to be supplied and all that depends upon the temperatures for example the amount of heat transferred these depend upon the properties of solution and the refrigerant and also the operating conditions okay.

So this is the basic principle of a very simple vapour absorption refrigeration system okay. So to summarize what we have done is we have taken two vessels in one vessel we have kept pure solvent and in the other vessel we have a solution okay. So by manipulating the pressures inside the supplying heat or by rejecting heat we could transfer vapour from the pure refrigerant side to the solution side during the refrigeration process and from the solution side to the refrigerant side during the regeneration process okay. And during this entire process we could get refrigeration effect during one step and we have to supply heat at high temperature during the regeneration process. And heat is rejected in both the processes of refrigeration and regeneration okay. So this is an intermittent system that means you are not able to get refrigeration continuously okay. So you call this as an intermittent absorption refrigeration system okay.

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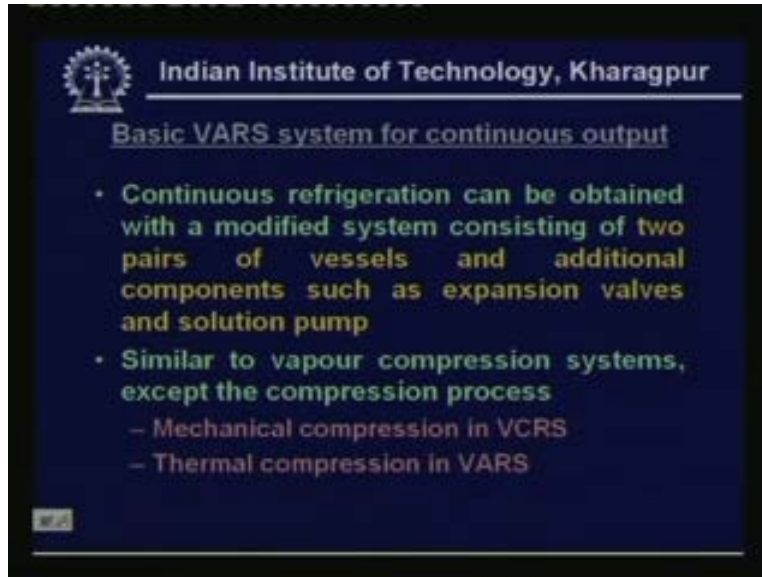
So as I said the you call this as an intermittent system so with only two vessels the refrigeration obtained is intermittent so no refrigeration effect is produced during vapour regeneration and these simple systems also have some applications they can be used to provide refrigeration using renewable energy such as solar energy. For example you would like to produce refrigeration using solar energy okay. So you can have a very simple intermittent system consisting of this simple two vessels and with a valve and connections okay.

What you have to do is during the day time when solar energy is available refrigerant is generated okay. And it is stored as pure refrigerant okay during the day time the, if the, it is the process of regeneration. And during night time what happens is surroundings become cold okay then the process gets reversed. Because the solution becomes cool so the refrigerant in the vessel pure refrigerant vessel can boil by taking heat from the surroundings okay. That means you get refrigeration effect during the night and you have to regenerate the refrigerant during the day time.

Such systems are very good for very remote and rural areas where you do not have any electrical electricity supply or you want a system which is independent of your great power okay. Such systems have been built and there have been used by successfully in many remote areas okay. So they are known as intermittent absorption refrigeration systems. But in practice in most of the applications we require continuous refrigeration okay, when you want a refrigeration

continuously obviously you cannot use this simple system with two vessels. So you have to do certain modifications.

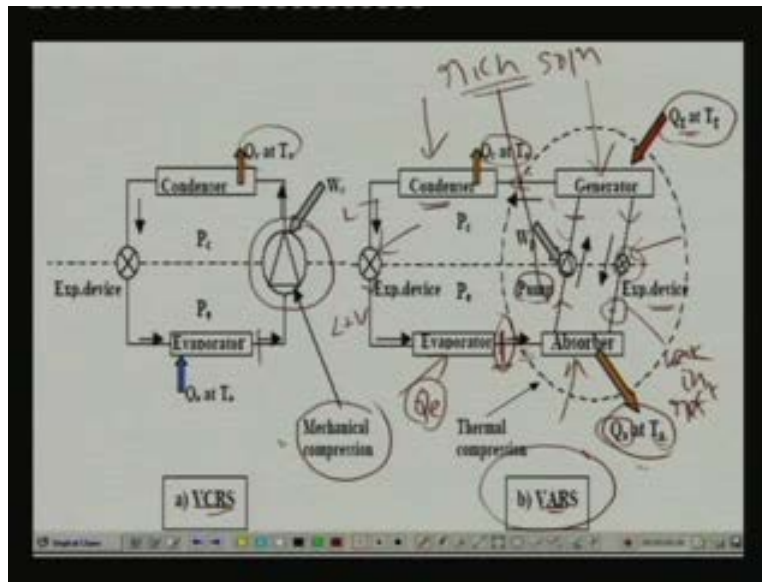
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So this brings us to a basic vapour absorption refrigeration system for continuous output. So continuous refrigeration can be obtained with a modified system consisting of two pairs of vessels and additional components such as expansion valves and solution pump. So you have to have first thing is two pairs of vessels. That means you will have four vessels in addition to that you also have to have some additional components such expansion valves and a solution pump. These systems are similar to compression systems. That means you get continuous output just like a vapour compression system but there are two major differences the major difference is the way the vapour is compressed.

In a mechanical, it is mechanical compression in vapour compression refrigeration system. That means you use mechanical energy supply the mechanical energy to the compressor and compress the vapour mechanically okay. So you call these systems as mechanical compression systems okay. And the in case of absorption system you can call that as thermal compression okay. If you compress the vapour thermally now let me explain the basic system.

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Okay, so here you have the basic vapour absorption refrigeration system. So you have a condenser an expansion device and an evaporator just like a vapour compression system. The only difference between vapour compression system and vapour absorption system lies in the way in which you have compressed the vapour from the evaporator. That means what happens from this point onwards okay. So in vapour compression system what is done this low pressure low temperature vapour is compressed mechanically okay. Mechanically it is compressed to high pressure. So that it is, it can reject heat in the condenser to the external heat sink and it can condense and become a liquid okay.

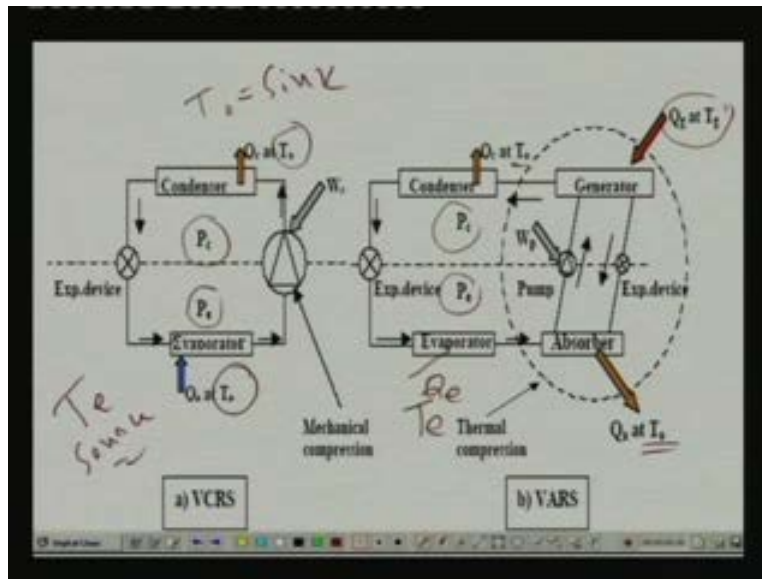
So you call this system, as I said, as a mechanical compression system where as you can see that in the vapour absorption system. You do not have a compressor okay, in place of a single component compressor you have four components one is generator absorber expansion device and a solution pump okay. So the combination of this four components replace the compressor of a vapour compression system okay. So now let me explain the working principle. Let us start again from the point at the outlet of the evaporator we have low temperature low pressure vapour at this point okay. It goes to the absorber in the absorber this refrigerant vapour comes in contact with the solution that is coming from the generator. That means this solution which is weaker in refrigerant okay this is weak in refrigerant. When this solution is weak in refrigerant it has the potential to absorb the refrigerant vapour okay. So when this refrigerant vapour comes in contact with this weak solution then the vapour gets absorbed okay.

Since absorption process is an exothermic process heat is rejected to the atmosphere at temperature T_{naught} and this is the amount of heat rejection during this process okay. So the weak solution and refrigerant vapour are combining heat is rejected. So as a result of this mixing what you have is a rich solution okay this solution is rich solution rich solution means rich in refrigerant. Now this rich solution is pump to the condenser pressure using a solution pump okay. A solution pump is used to compress the vapour from the absorber from the compressor liquid from the absorber to the condenser pressure okay.

And now at this point you have high pressure liquid now this high pressure liquid goes to the generator in the generator what is done is heat is supplied at high temperature. Okay. So when you supply heat at high temperature to the rich solution refrigerant vapour is generated okay. So this refrigerant vapour at high pressure and high temperature goes to the condenser where it rejects the heat to the surroundings condensers and becomes a liquid okay. And this liquid again expands in the expansion device. So you have here a low quality liquid vapour mixer at low, at low temperature and low pressure this enters into the evaporator it takes heat from the surroundings produces the refrigeration effect and becomes the vapour again. So that is how the vapour cycle is completed okay.

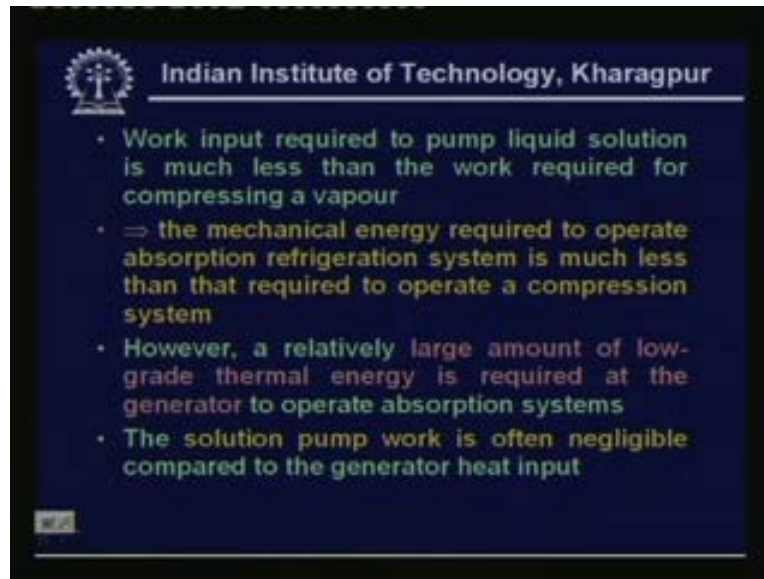
So the only difference you can notice here is instead of compressing it mechanically we have compressed it thermally okay. Now what happens to the solution here remember that we had a rich solution that is entering into the generator. So from that you have stripped off the refrigerant so what you have is a weak solution okay. Now this weak solution is still at high pressure okay. So to complete the cycle for the solution you have to reduce its pressure. So we use an expansion device where the liquid pressure is reduced to that of the absorber or evaporator okay. And then again it comes in contact with this vapour so the solution cycles also completed. So this process goes on continuously as long as you supply heat here you reject heat at absorber and condenser. And you have refrigeration effect continuously okay so this is the principle of very basic vapour absorption refrigeration system.

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And as I said you can see out the similarities just like vapour compression system you have two pressure levels here P_c and P_e here P_c and P_e here okay. However unlike vapour compression system there are three temperatures here. In vapour compression system we have only two temperatures that is this is the T_c is the heat sink temperature and T_e is the low temperature heat source heat source temperature okay. Whereas in absorption system we have three temperatures one is T_e that is low temperature source low source then T_c is the heat sink temperature and T_g is the high temperature heat source okay. At where from which you supply heat to the generator so this is the three temperatures cycle and vapour compression refrigeration system is the two temperatures cycle. Okay. So the major difference is you have seen.

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Now what is the advantage of this i mean you if you look at the components and the schematic you will find that the vapour absorption system is lot more complicated compare to vapour compression system we had only four components in vapour compression systems where as we had seven components in vapour absorption systems okay. And you might have noticed that even though we did not use a compressor we still used a pump in the vapour absorption system. Now the pump requires mechanical energy okay. So both vapour absorption systems as well as vapour compression systems both need the mechanical energy one to run the compressor and in other case you need it for running the pump okay. And in addition to that you also have to supply heat at high temperature okay.

Since mechanical energy is required in both the cases what is the advantage of absorption systems compare to compression systems. The advantage is like this in the compression system you are compressing a vapour okay. So the mechanical energy required to compress the vapour is quite large. Where as in vapour absorption systems you are pumping a liquid and the work required to pump a liquid for the same over the same pressure difference is much less compare to the work required for compressing a vapour okay, this is the major difference. That means the amount of mechanical energy required in vapour absorption systems is very small compare to vapour compression refrigeration systems okay.

In fact it is practically negligible when you compare it with the heat input. So that is why the absorption systems are mainly called as heat operated systems. Because that is the major heat

input is major input is in the form of heat okay. Why do, how do we say that energy required for compressing a vapour is much higher than the energy required for pumping a liquid. Because you have seen that the work input is simply equal to integral V D P. And the V is nothing but the specific volume of the working fluid in one case you have vapour which has a very high specific volume that is why the integral V D P is very high. Where as in absorption system you have a liquid with very small specific volume.

So integral V D P is very small so the mechanical energy requirement is very small okay. So this is the major difference and the major advantage of absorption systems over compression systems okay. So that is what I have mentioned here work input required to pump liquid solution is much less than the work required for compressing vapour. So the mechanical energy required to operate absorption system is much less than that required to operate a compression system.

However of course you have to pay somewhere. So what you do in a instead of mechanical energy you have to supply a large amount of low grade thermal energy to operate the absorption system. And as I said the solution pump work is often negligible compare to the generator heat input.

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- Thus the COPs for compression and absorption systems are given by:

$$\text{COP}_{\text{VCRS}} = \frac{Q_c}{W_c}$$

$$\text{COP}_{\text{VARS}} = \frac{Q_c}{Q_g + W_p} \approx \frac{Q_c}{Q_g}$$

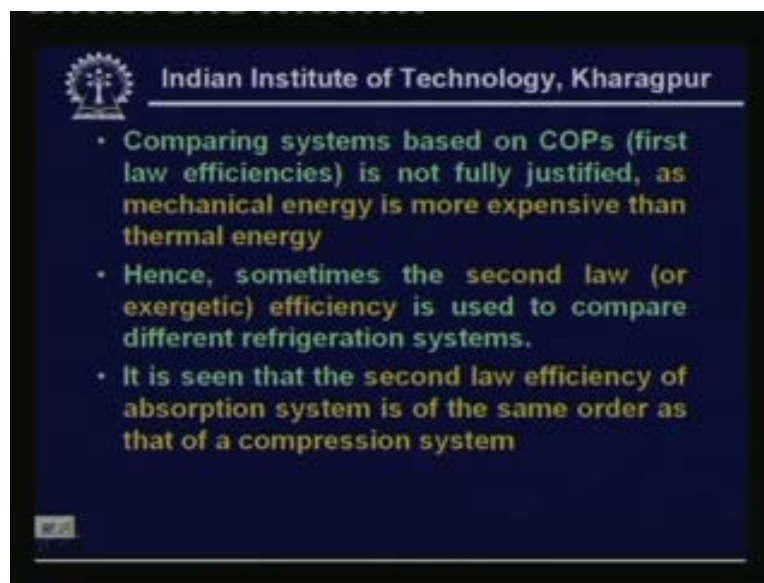
- Since VARS uses low-grade energy as input, COP of VARS is generally much smaller than COP of VCRS

So if you are defining COPs just like the compression system you can see that the COP of the compression system is defined as the refrigeration capacity divided by the power input to the compressor W_c where as the COP of vapour absorption system. You have two inputs and one

output is Q_e input is the heat input Q_g plus work input W_p and as I have said W_p is negligible compare to Q_g so COP of absorption refrigeration system is almost equal to Q_e by Q_g only that means refrigeration capacity divided by the heat input to the generator okay. So this is the major difference between again compression and absorption system in terms of COPs. Since vapour absorption system uses low grade energy as input the COP of absorption system is generally much smaller than COP of compression refrigeration system. Obviously if you are I mean if you are comparing the COPs you get much higher COPs in case of compression systems okay. Because the quality of the energy that you are supplying to the system is much higher okay.

Work is high grade energy compare to heat okay so the COPs are larger okay. But of course comparing the systems based on COP. So you can call also call the COP as the first law efficiency comparing the efficiencies based on COPs is not really justified always because the quality is different and the cost is also different okay.

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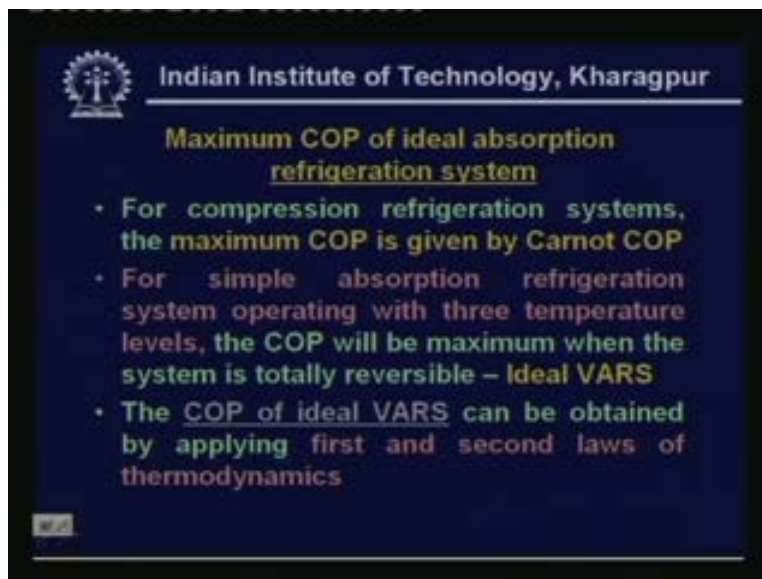
That means comparing systems based on COPs is not fully justified as mechanical energy is more expensive than thermal energy hence sometimes what we do is we define what is known as the second law or exergetic efficiency to compare different refrigerant systems. And you will find that the second law efficiency of absorption system is of the same order as that of a compression system okay. That means if you are comparing the two systems based on COPs then

absorption system is definitely bad because you get very low COP. But as I said since numerator and denominator are of different qualities if you want get the real picture you must convert them into the same quantity okay. That means you have to convert the numerator and denominator in expression for COP into exergy. Let us say then you get what is known as second law efficiency or exergetic efficiency.

When you are doing this you will find that the COP of I am sorry the exergetic efficiency of absorption system is almost same as that of a compression system okay. So it does not look so bad and when you are looking at the exergetic efficiency okay. This you can also justify this in another way for example when you are talking about the COP of the compression system what is the input is the work mechanical energy okay. Most of the time the mechanical energy is derived from the electrical energy that means to run the compressor that is how you supply the electrical energy okay.

And how do you get the electrical energy electrical energy is generated let us say in a thermal power plant okay. And typical efficiency of the thermal power plant could be about forty percent you are not really compare taking that efficiency into account when you are calculating the COP of the vapour compression system okay. So take that efficiency also into account you will find that compression system are not so efficient compared to vapour absorption system or in other words both are equally good or bad okay.

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The slide features the IIT Kharagpur logo in the top left corner. The title is "Maximum COP of ideal absorption refrigeration system". The content consists of three bullet points. The first bullet point states that for compression refrigeration systems, the maximum COP is given by Carnot COP. The second bullet point states that for simple absorption refrigeration systems operating with three temperature levels, the COP will be maximum when the system is totally reversible – Ideal VARS. The third bullet point states that the COP of ideal VARS can be obtained by applying first and second laws of thermodynamics.

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Maximum COP of ideal absorption refrigeration system

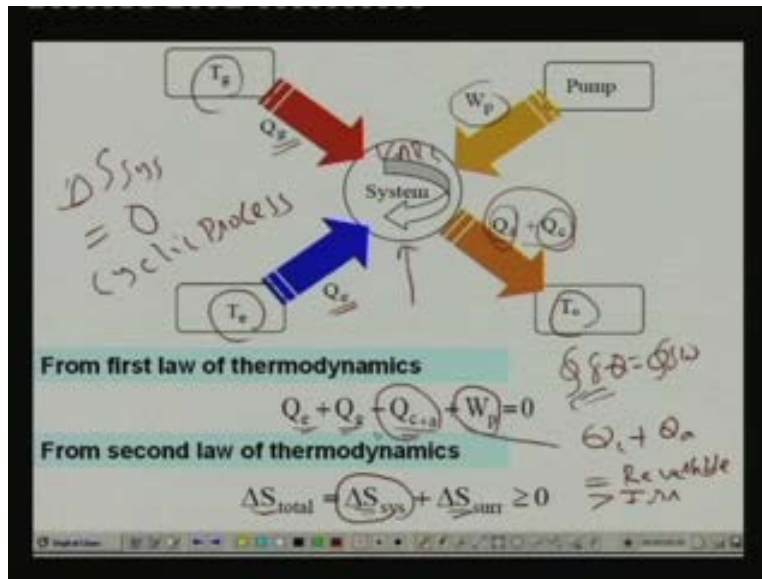
- For compression refrigeration systems, the maximum COP is given by Carnot COP
- For simple absorption refrigeration system operating with three temperature levels, the COP will be maximum when the system is totally reversible – Ideal VARS
- The COP of ideal VARS can be obtained by applying first and second laws of thermodynamics

Now when we discuss vapour compression refrigeration systems how if you remember how did we begin we began with an ideal cycle okay. First we have defined an ideal cycle and we found what is the maximum possible COP of this cycle. That means we found the maximum possible COP of a compression system okay. And if you remember it was the Carnot COP okay. That means the reverse Carnot cycle gives the maximum COP so first we obtained the expression for the COP of the reverse Carnot cycle and then we obtained the expression for the COPs for the real cycles okay.

And if you remember I said that the objective of this is to compare how good is the actual cycle with the best possible or with the ideal cycle okay. So in case of the absorption system also let us first look at what is the maximum possible COP okay. Then we will move on to the actual systems. So as I said for compression refrigeration systems the maximum COP is given by Carnot COP and Carnot COP if you remember is simply given by T_e divided T_c minus T_e where T_e and T_c are evaporator and condenser temperatures. However in simple absorption refrigeration system we have three temperatures. So when you have three temperature levels how do you get the maximum COP okay one thing is for sure that the COP will be maximum when the system is totally reversible.

That means when you have an ideal vapour absorption refrigeration system where it is reversible internally as well as externally okay. That means a total reversible system. So the COP of ideal vapour absorption refrigeration system can be obtained by applying first and second laws of thermodynamics okay. So what we do is we take a ideal system and then you apply the first and second laws of thermodynamics. Let me show how we can do this.

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Okay, what I have shown here is the basic vapour absorption refrigeration system this is the absorption refrigeration system which is operating in a cyclic manner okay. You can see the cycle and here we have three temperatures. As I said generated temperature evaporated temperature and the heat sink temperature and this figure also shows various energy flows okay. For example you take high temperature heat input Q_g to the system near the generator and this system takes low temperature heat input Q_e at refrigeration temperature T_e and it rejects heat to the heat sink.

And heat rejection takes place at the absorber Q_a plus condenser Q_c okay. So heat rejected is Q_a plus Q_c where as heat input is Q_g and Q_e Q_g is at the generator and Q_e is at the evaporator in addition to that we also supply mechanical energy to run the pump okay W_p . So these are the total energy flows in a simple vapour absorption refrigeration system. So if you apply first law of thermodynamics what is the first law of thermodynamics if you remember simply you have okay. And for the cycle the net energy change is zero because the working fluid is undergoing the cyclic process okay. So what is the energy change cyclic energy change you can simply write this as Q_e plus Q_g minus Q_c plus Q_a plus W_p is zero.

This is nothing but this expression where as I said Q_e and Q_g are positive. Because you are supplying them to the system this is negative because this is the heat rejected from the system

and work input required for the pump is also positive. Because that is also supplied okay, so whatever is supplied to the system is positive and whatever is rejected from the system is negative okay. So this is how you get the first law of thermodynamics very simple energy balance now what is the second law of thermodynamics. We write the second law of thermodynamics in the form of entropy change and if you remember the second law of thermodynamics say that the total entropy change.

That means the entropic change of the system plus surrounding will always be greater than or equal to zero. And this equal sign is for completely reversible if everything is reversible and the greater than is for irreversible systems okay. So this is the second law of thermodynamics right now let us write the expression for delta surroundings in terms of Q_e , Q_g and Q_c . Now what is the entropy change of the system obviously entropy change of the system is zero right so delta S system is zero because the working fluid is undergoing a cyclic process okay.

So delta S system is zero right that means ultimately the second law of thermodynamics when you apply to this simply becomes delta S total is equal to delta surrounding which is greater than and equal to zero okay.

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Since the working fluid in the system undergoes a cyclic process; $\Delta S_{sys} = 0$, hence;

$$\Delta S_{SURT} = -\frac{Q_c}{T_c} - \frac{Q_g}{T_g} + \frac{Q_{a+c}}{T_o} \geq 0$$

Combining 1st and 2nd laws:

$$Q_g \left(\frac{T_g - T_o}{T_g} \right) \geq Q_c \left(\frac{T_o - T_c}{T_c} \right) - W_p$$

Neglecting pump work, the COP is given by: $COP \propto \frac{Q_c}{Q_g}$

$$COP_{VARs} = \frac{Q_c}{Q_g} \leq \left(\frac{T_c}{T_o - T_c} \right) \left(\frac{T_g - T_o}{T_g} \right)$$

Now as I said delta S system is zero because this system undergoes a cyclic process okay. Now we write the expression for delta S surroundings means we have three temperature reservoirs one is the low temperature reservoir T_e the other one is at high temperature reservoir T_g and this is

the medium temperature heat sink at T_{naught} okay. And what is the entropy change of these reservoirs the entropy change of low temperature reservoir is this minus Q_e by T_e minus because the reservoir is losing heat okay. And its temperature is constant okay. So ΔS if you remember is ΔQ by T because you are the reservoir is undergoing the reversible change. So you can write this and T is constant. So simply this becomes one Q_2 or whatever it is ΔQ divided by that particular temperature.

So when you are applying this to the evaporator this becomes minus Q_e by T_e when you apply this to the generator this becomes minus Q_g by T_g and when you are applying this to the heat sink this becomes plus because heat sink is taking the energy. And this energy is taken at temperature T_{naught} okay. So this is the expression for the entropic change of the surroundings okay now you combine the first and second law so you get this expression okay. This expression relates the Q_g and Q_e what we are doing is we are eliminating Q_a plus c by using the first law okay. So you that is eliminated and you and then get this expression.

Now if you are neglecting pump work okay. That means you are neglecting pump work and if you define COP as we have seen COP is equal to Q_e divided by Q_g okay. You will find that from this expression COP of vapour absorption refrigeration system is given by this expression okay. That means always less than or equal to T_e divided by $T_{naught} - T_e$ into $T_g - T_{naught}$ by T_g where remember that T_g is the generated temperature which is the highest temperature in the cycle T_{naught} is the heat sink temperature and T_e is the lowest temperature of the evaporator okay.

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For a totally reversible system (ideal VARS):

$$\Delta S = \Delta S_{\text{sys}} + \Delta S_{\text{surr}} = 0$$

$$\Delta S_{\text{surr,rev}} = -\frac{Q_c}{T_c} - \frac{Q_g}{T_g} + \frac{Q_{a+c}}{T_o} = 0$$

Max Possible COP

$$\text{COP}_{\text{ideal VARS}} = \frac{Q_c}{Q_g} = \left(\frac{T_c}{T_o - T_c} \right) \left(\frac{T_g - T_o}{T_g} \right)$$

Hence, the maximum COP of VARS (ideal system) is given by:

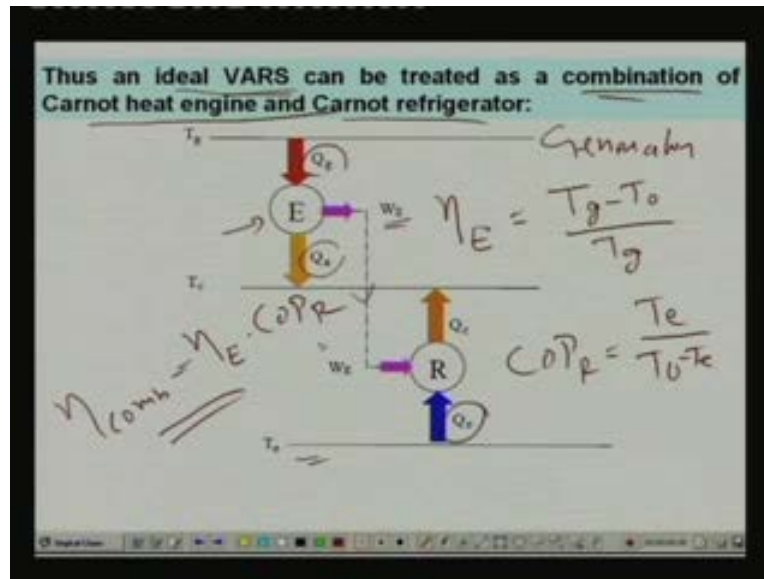
$$\text{COP}_{\text{ideal VARS}} = \frac{Q_c}{Q_g} = \left(\frac{T_c}{T_o - T_c} \right) \left(\frac{T_g - T_o}{T_g} \right) = \text{COP}_{\text{Carnot}} \cdot \eta_{\text{Carnot}}$$

Now for a totally because we started this discussion with a view to find out the maximum COP okay. So as I said maximum COP takes place when the system is ideal okay. And for an ideal system entropy change is zero okay entropy change of system is zero for both ideal as well as real system because it is a cyclic process so for an ideal system in addition to this also should be zero okay. That means delta S surroundings for a cut completely reversible system is equal to zero so if you are equating this from the earlier expression you will get this expression okay.

From this expression you get the COP for an ideal system this is the maximum possible COP of okay, of any vapour absorption refrigeration system operating between three temperatures T e T naught and T g okay.

Now if you look at this expression you will notice an interesting thing. For example you take a look at this quantity okay. And look at this quantity this quantity for example looks like the Carnot COP of a vapour compression system okay. Because if you remember Carnot COP is simply given by T e divided by T c minus T e where T c is equal to T naught in this case. So this particular quantity is nothing but the COP of the Carnot system and what is this quantity this quantity is nothing but the efficiency of Carnot heat engine okay. So the ultimately the COP of an ideal vapour absorption system is shown to be a product of Carnot COP into Carnot heat engine okay.

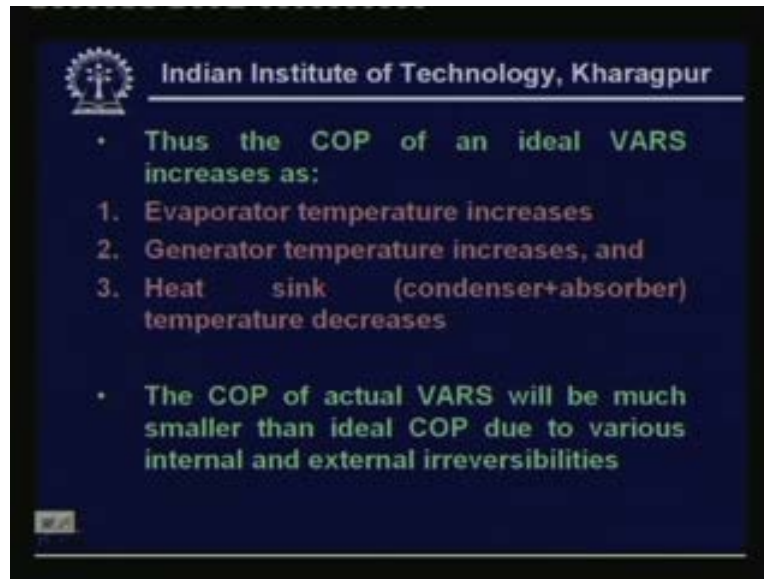
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That means you can show an ideal vapour absorption system as a combination of Carnot heat engine and Carnot refrigerator okay. So what you are doing is this is the generator okay. You supply Q_g from the generator to a Carnot heat engine and produce work and reject some heat to the surroundings. And this work is used to run a Carnot refrigerator okay. So the same work is supply to run a Carnot refrigerator and this refrigerator takes heat from the low temperature surroundings Q_e and again it rejects the heat to the heat sink T_{naught} . And the efficiency of this heat engine is nothing but T_g minus $T_{T\ naught}$ by T_g and COP of this Carnot cycle is, if you remember T_e divided by T_{naught} minus T_e .

So the combined efficiency of this n combined is nothing but the efficiency of this multiplied by the efficiency of this that is η_E into COP_R okay. So that is how you can split a three temperature refrigeration system as a combination of two temperature systems.

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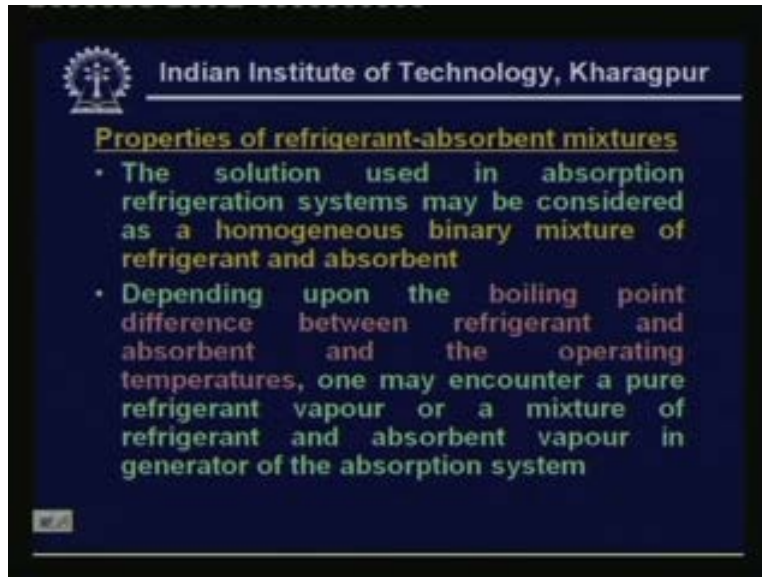
So you can see that, so from this you can easily infer that the COP of an ideal vapour absorption system increases as the evaporator temperature increases as the generator temperature increases and the heat sink temperature decreases. When generated temperature increases and heat sink temperature decreases the heat engine efficiency increases okay. And similarly when the evaporator temperature increases and the condenser temperature reduces the COP of the Carnot refrigerant cycle increases.

As a result of it the combined efficiency improves okay. So if you want to have a very high COP of a vapour absorption refrigeration system an ideal system you have to operate the system at as higher generated temperature is possible as high an evaporator temperature is possible and as low the heat sink temperature as possible okay. However you will find that the COP of actual system will be much smaller than the ideal COP due to various internal and external irreversibilities. So as usual you will find that all real systems will gives you COPs which are much smaller than the ideal system COP okay.

This is mainly because of the irreversibilities. So remember that an ideal difference between ideal and real cycle is lies in the irreversibilities okay. So in the real cycle you have irreversibilities both internal as well as external okay. For example what are the internal irreversibilities internal irreversibilities could be pressure drop due to friction it could be in this case irreversibilities due to mixing right. And the external irreversibilities are irreversibilities due to temperature difference between the working fluid and the external heat sink or source okay.

So mainly there are temperature differences so these are the different reversibilities which are a must in a real system okay. So as a result the real system COP will be much less than the ideal vapour absorption refrigeration system COP okay.

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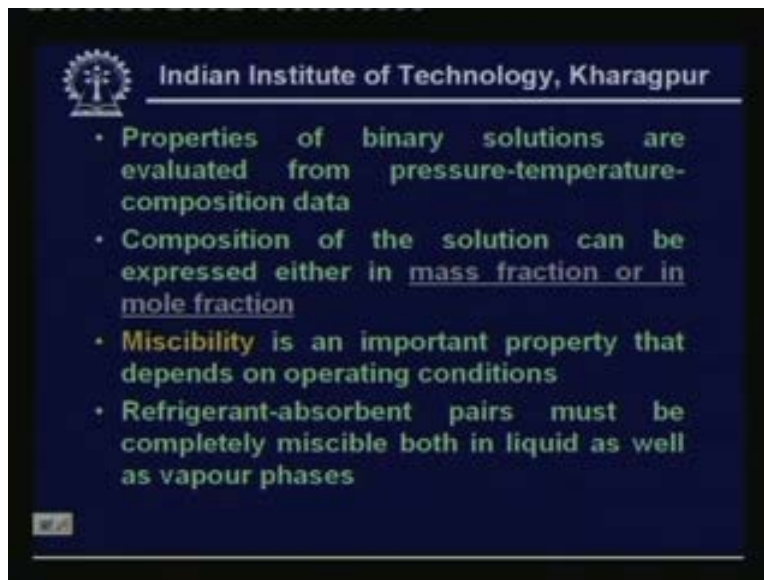


Now let us look at properties of refrigerant absorption mixtures the solution used in absorption refrigeration systems may be considered as a homogeneous binary mixture of refrigerant and absorbent okay. Because you have, so noticed that in the thermal compression part of the vapour absorption system we have a solution okay. Solutions circulates to the components and this what is the solution. The solution is nothing but a mixture of refrigerant and absorbent and for simplicity we assume that it is a binary mixture. And it is a homogeneous mixture okay. Now depending upon the boiling point difference between the refrigerant and absorbent and the operating temperatures one may encounter a pure refrigerant vapour or a mixture of refrigerant and absorbent vapour in generator of the absorption system okay.

That means while discussing the, or describing the simple vapour absorption refrigeration system. I mention that in the generator you supply heat at high temperature and refrigerant vapour is generated okay. And that refrigerant vapour goes to the condenser and gets condensed and all that but in actual systems depending upon the boiling point temperature difference between the refrigerant and absorbent in addition to the refrigerant vapour you may also have some vapour of the absorbent in the generator okay.

That means when you are supplying heat to the generator both refrigerant as well as absorbent may boil okay. That means what goes to the condenser may not be pure refrigerant but a mixture of refrigerant and absorbent vapors okay. Whether you have a mixture or a pure refrigerant purely depends upon the boiling point temperature difference between the refrigerant and absorbent. If you have a very high boiling point temperature difference that means when the absorbent is non volatile then you will find that whatever is generated in the generator is pure refrigerant okay. On the other hand if the temperature difference is not too high that means absorbent is also volatile then both will be generated in the generator okay. An example of the first case where you have non volatile absorbent is when you use water and lithium bromide okay so where lithium bromide is absorbent it is non volatile. So pure water vapour is generated where as if you use ammonia water systems where water is absorbent and ammonia is refrigerant both water and ammonia may be generated in the generator okay. So this is the difference between different refrigerant absorbent pairs okay.

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Now properties of binary solutions are evaluated from pressure temperature composition data. So if you want to find the properties you have to specify pressure temperature and composition of the solution can be expressed either in mass fraction or in mole fraction okay. So what is the mass fraction mole fraction?

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Composition in terms of mass fraction (concentration):

$$\xi_1 = \frac{m_1}{m_1 + m_2}; \quad \xi_2 = \frac{m_2}{m_1 + m_2}$$

Where m_1 and m_2 are mass of components 1 and 2

$$\xi_1 + \xi_2 = 1 \Rightarrow \xi_2 = 1 - \xi_1$$

Composition in terms of mole fraction:

$$x_1 = \frac{n_1}{n_1 + n_2}; \quad x_2 = \frac{n_2}{n_1 + n_2}$$

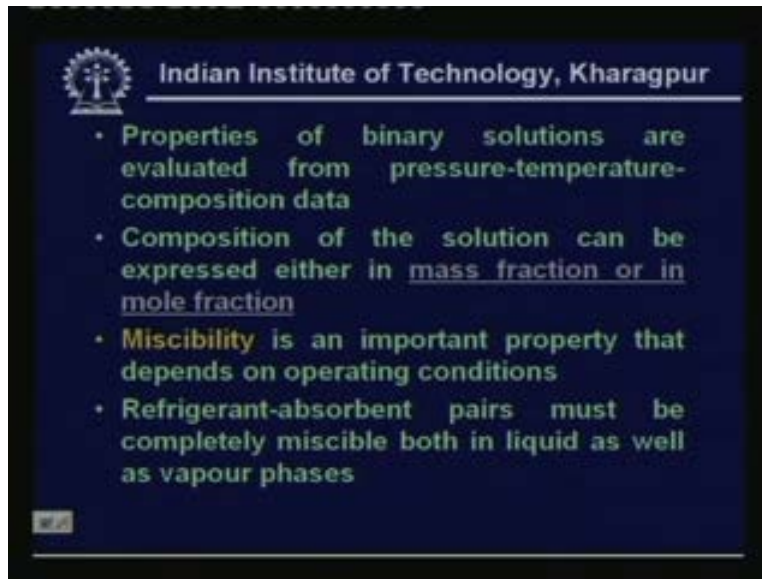
Where n_1 and n_2 are no. of moles of components 1 and 2

$$x_1 + x_2 = 1 \Rightarrow x_2 = 1 - x_1$$

So mass fraction is defined as okay mass fraction is also sometimes called as concentration of component one ξ_1 is simply defined as the mass of that particular component divided by the total mass of the solution okay. That means m_1 divided by $m_1 + m_2$ similarly mass fraction or concentration of component two is nothing but mass of that component in the solution m_2 divided by the total mass of the solution okay. m_1 and m_2 are mass of component one and two so for a binary system you can very easily show that $\xi_1 + \xi_2$ is equal to one from the above expression that means ξ_2 is equal to one minus ξ_1 okay. So if you know the composition of one component the composition of the other component can be easily obtained okay.

Now the composition in terms of mole fraction, so instead of talking about masses we talk about the number of moles so mole fraction of component one is nothing but the ratio of number of moles of component one divided by the total number of moles of component one and two in the solution okay. Similarly mole fraction of two x_2 is given by n_2 by $n_1 + n_2$ where n_1 and n_2 are number of moles of components one and two okay. Just like the mass fraction it can be very easily show shown that $x_1 + x_2$ is equal to one or x_2 is equal to one minus x_1 .

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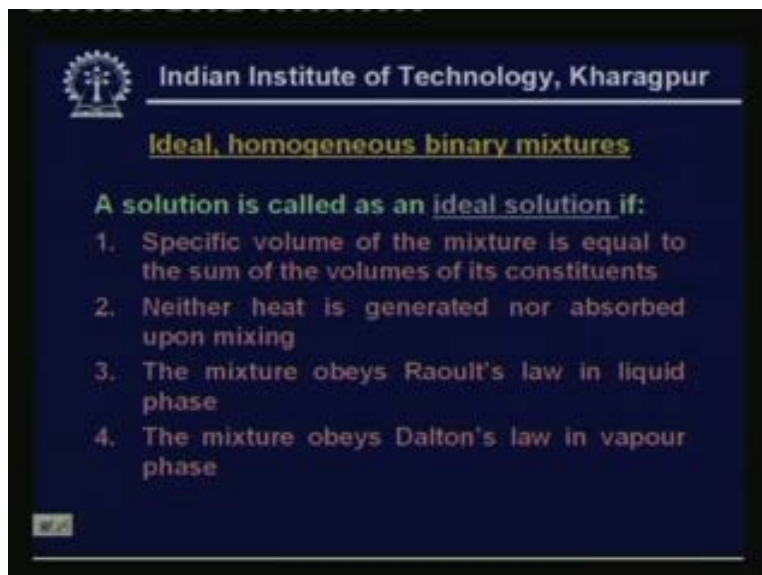


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- Properties of binary solutions are evaluated from pressure-temperature-composition data
- Composition of the solution can be expressed either in mass fraction or in mole fraction
- **Miscibility** is an important property that depends on operating conditions
- Refrigerant-absorbent pairs must be completely miscible both in liquid as well as vapour phases

And very another, very important property as far as refrigerant absorbent pairs are concerned is what is known as miscibility okay. And miscibility is an important property and it depends upon the operating conditions. That means under certain operating conditions a refrigerant absorbent pairs may not be very highly miscible where as at other condition there may be highly miscible okay. So it depends upon the operating conditions and generally refrigerant absorbent pairs must be completely miscible both in liquid as well as vapour phases. So that is how you choose the pairs. So that they get mixed completely and you get a homogeneous mixture.

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Ideal, homogeneous binary mixtures

A solution is called as an ideal solution if:

1. Specific volume of the mixture is equal to the sum of the volumes of its constituents
2. Neither heat is generated nor absorbed upon mixing
3. The mixture obeys Raoult's law in liquid phase
4. The mixture obeys Dalton's law in vapour phase

Now let us define what is known as an ideal homogeneous binary mixtures okay. A solution is called as an ideal solution if specific volume of the mixture is equal to the sum of the volumes of its constituents. That means, let us take a binary mixture i take a component one and component two component one has a specific volume of v_1 and component two has specific volume v_2 and I mix certain masses of these two components. You will find that the specific volume of the mixture is simply equal to the volume of its constituents okay. Some of the volume of its constituents okay.

Then during this mixing process neither heat is generated nor absorbed okay. So this is another characteristic of ideal solution and the mixture obeys Raoult's law in liquid phase and the mixture also obeys Dalton's law in vapour phase. So these are the four conditions they are not totally unrelated actually these conditions are related. But these are based on these four points you can say whether the solution these has an ideal solution or not okay. So let us look at mathematically what do we mean by this?

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Ideal solution $\Delta V = 0$

Condition 1:

$$v = \xi_1 \cdot v_1 + \xi_2 \cdot v_2$$

Condition 2:

$$h = \xi_1 \cdot h_1 + \xi_2 \cdot h_2 = \xi_1 \cdot h_1 + (1 - \xi_1) \cdot h_2$$

Condition 3 (Raoult's law):

$$P_{v,1} = x_1 \cdot P_{1,sat}$$

$$P_{v,2} = x_2 \cdot P_{2,sat}$$
 $x_i = \text{Liquid phase mole fraction}$

$$P_1(T)$$

Condition 4 (Dalton's law):

$$P_{v,1} = y_1 \cdot P_{total}$$

$$P_{v,2} = y_2 \cdot P_{total}$$

So condition one condition one as I mentioned the solution of the specific volume of the solution should be simply equal to sum total of the specific volumes of the components okay. So this is the mass fraction of component one and this is specific volume of component one this is the mass fraction of component two this is specific volume of component two okay. So the specific

volume of the mixture is simply equal to this means the solution neither expands nor contracts that means there will be not be any volume change upon mixing okay.

So this is of a condition one and condition two the specific enthalpy okay. Since no heat is released or absorbed it can be very easily shown that the specific enthalpy of the solution is simply equal to the weighted average enthalpies of component one and component two okay.

x_1 and x_2 as I said are mass fractions h_1 and h_2 are the specific enthalpies of component one and two at that particular temperature and pressure okay. So the same thing can be written in this form. Because x_1 and x_2 is equal to one minus x_1 this is the condition second condition.

And what is Raoult's law? Raoult's law says that for an ideal solution the vapour pressure exerted by component one is simply equal to the product of its liquid phase mole fraction x_1 x_1 is equal to liquid phase mole fraction okay. So it is a vapour pressure exerted by the component one is equal to a product of liquid phase mole fraction x_1 into P_1^{sat} what is P_1^{sat} P_1^{sat} is nothing but the saturated pressure of this component one at that particular temperature T okay. So P_1^{sat} is this so the vapour pressure is given for component one is given by this for component two is given by this okay, where x_2 is liquid phase mole fraction of component two.

So this is what is known as Raoult's law okay. So if you know the composition and if you also know the saturation properties you can find out what is the vapour pressure in solution okay.

What is Dalton's law, if you remember Dalton's law is for the vapour phase and it is says that vapour pressure in vapour phase is equal to the mole fraction of component one in vapour phase into the total pressure P_{total} . Similarly the vapour pressure for component two is equal to the product of mole fraction y_2 into the total pressure okay. This is the Dalton's law okay.

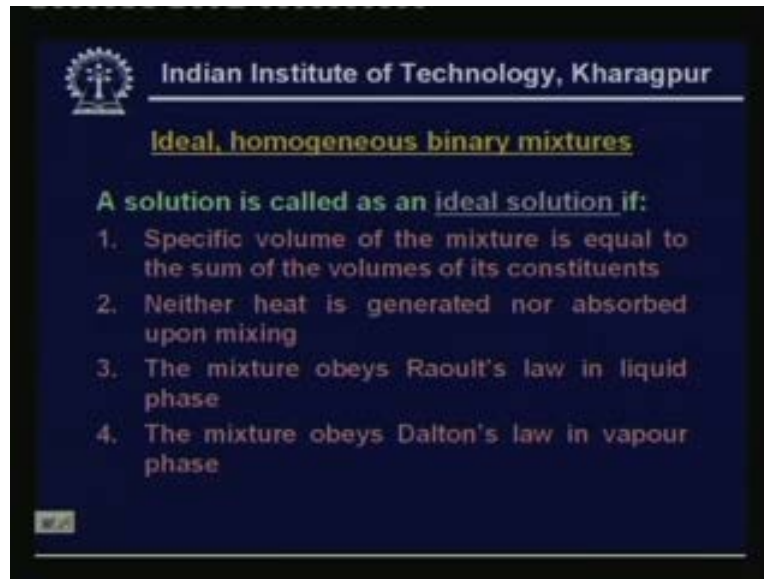
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- The vapour phase mole fractions y_1 and y_2 are related by:
$$y_1 + y_2 = 1 \Rightarrow y_2 = 1 - y_1$$
- The total pressure, P_{total} is given by:
$$P_{\text{total}} = P_{v,1} + P_{v,2}$$
- If one of the component (say 2) is non-volatile, then, $y_2 \approx 0$, hence: $y < 1$
$$P_{\text{total}} \approx P_{v,1} = x_1 \cdot P_{1,\text{sat}}$$

So you can easily show that the vapour phase mole fractions y_1 and y_2 are related by this expression $y_1 + y_2 = 1$ just like your liquid phase mole fraction so $y_2 = 1 - y_1$ and the total pressure total pressure is nothing but the sum total of the pressure exerted by component one plus component two okay $P_{v,1} + P_{v,2}$ suppose if you have a component which is non volatile let us say the component two is non volatile then y_2 is equal to almost y_2 is equal to zero that means what you have is only pure vapour only volatile component of and y_2 is equal to zero that means y_1 is equal to one

So in the such case when you are clubbing Raoult's law and Dalton's law you can very easily show that total pressure exerted is simply equal to vapour pressure exerted by component one which is equal to $x_1 \cdot P_{1,\text{sat}}$ okay. That means again if you know the saturated properties for the volatile component. And if you also know the composition then you can easily calculate what is the total pressure exerted okay.

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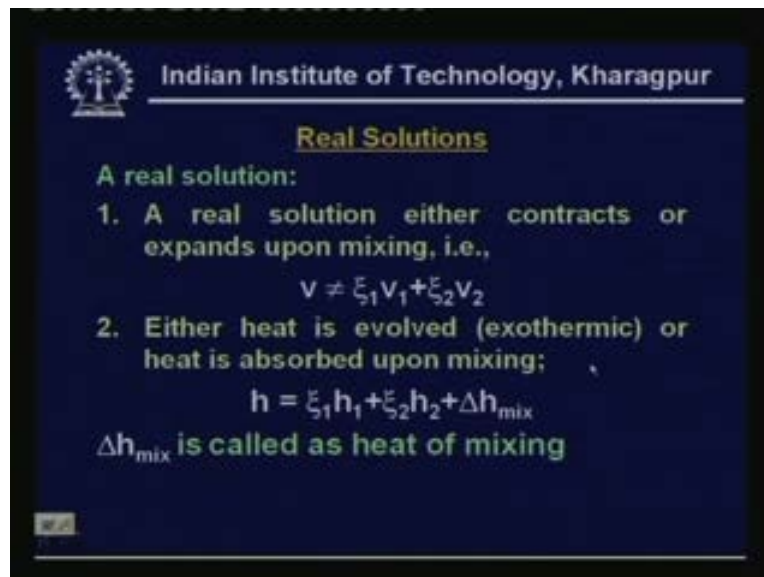
Ideal, homogeneous binary mixtures

A solution is called as an **ideal solution** if:

1. Specific volume of the mixture is equal to the sum of the volumes of its constituents
2. Neither heat is generated nor absorbed upon mixing
3. The mixture obeys Raoult's law in liquid phase
4. The mixture obeys Dalton's law in vapour phase

So these are the ideal solutions.

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Real Solutions

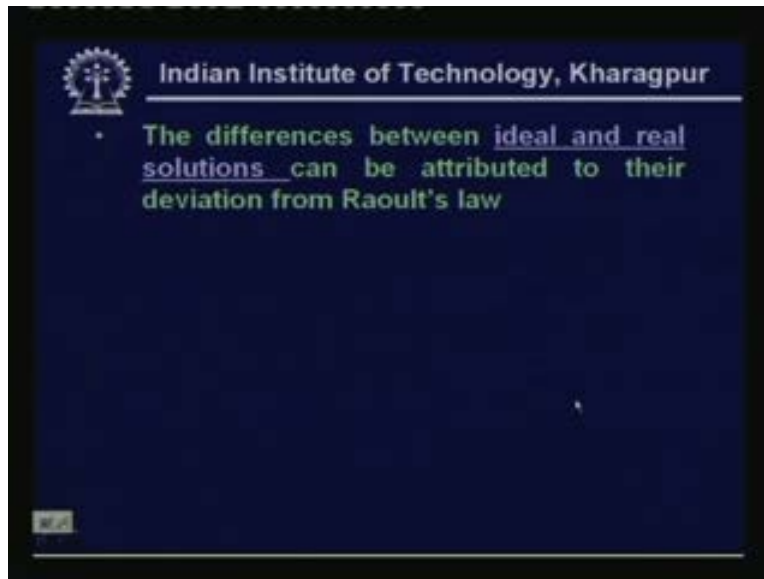
A real solution:

1. A real solution either contracts or expands upon mixing, i.e.,
$$V \neq \xi_1 V_1 + \xi_2 V_2$$
2. Either heat is evolved (exothermic) or heat is absorbed upon mixing;
$$h = \xi_1 h_1 + \xi_2 h_2 + \Delta h_{\text{mix}}$$

 Δh_{mix} is called as heat of mixing

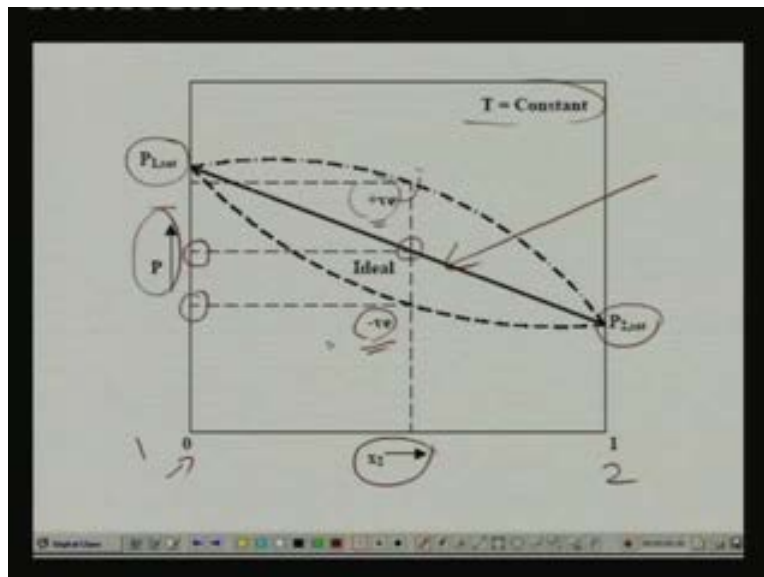
Obviously the real solutions are not ideal solutions real solution either contracts or expands upon mixing. That means the specific volume V is not equal to $\xi_1 V_1 + \xi_2 V_2$ and either heat is evolved or heat is absorbed upon mixing. That means the mixing process is exothermic either exothermic or endothermic. That means h is not equal to $\xi_1 h_1 + \xi_2 h_2$ but it is equal to $\xi_1 h_1 + \xi_2 h_2 + \Delta h_{\text{mix}}$ where Δh_{mix} is called as heat of mixing which could be positive or negative.

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So the difference between ideal and real solutions can be attributed to their deviation from Raoult's law okay. So let me show that.

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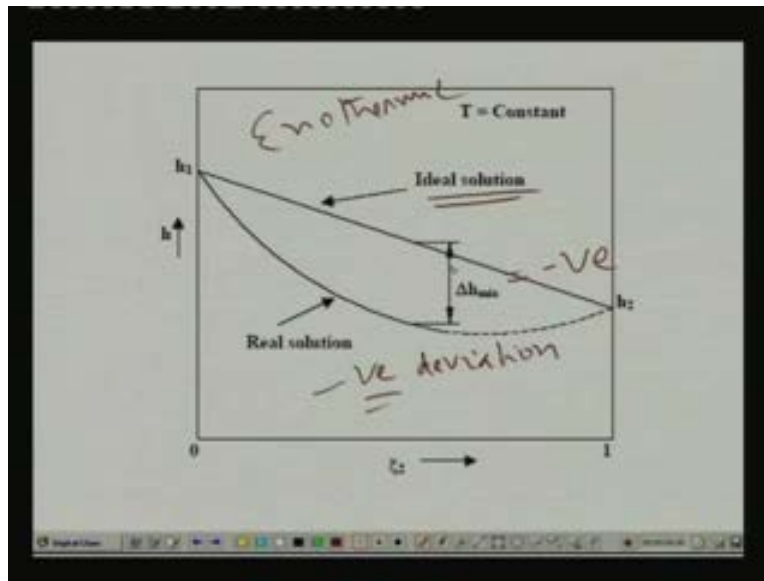


So what I have shown here is the mole fraction of component two versus pressure when the mole fraction is one zero here. That means you have pure component one and here you have component two okay. That is why the pressure here is nothing but the saturation pressure of component one and the pressure here is the saturated pressure of component two. Remember that the temperature is constant here and if the solution behaves an ideal solution you have this

line. Because at any point pressure is simply equal to $p_1 + x_2 p_2$ okay, that is from your Raoult's law.

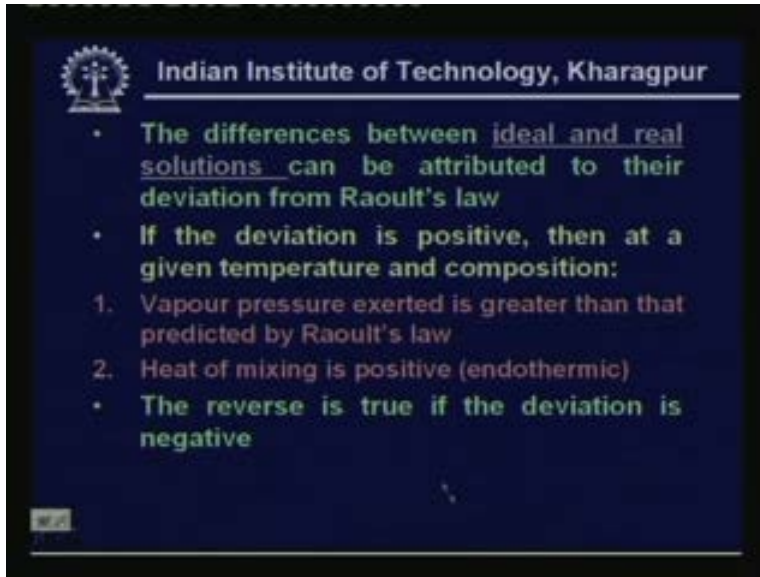
But the real solution will deviate either in the positive manner or in a negative manner if the deviate from the positive, in a positive manner the actual vapour pressure will be larger than the vapour pressure predicted by Raoult's law okay. This is what you call as positive deviation and if the deviate in a negative manner you find that the actual pressure is less than the pressure predicted by the ideal solution okay. That is from the Raoult's law okay this you call it as negative deviation from Raoult's law okay. The same thing you can also shown.

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Enthalpy chart what I have shown here is only for the negative deviation okay. So real solution with negative deviation because this, what you encounter in vapour absorption refrigeration systems. So for real solution with negative deviation you will find that Δh_{mix} is negative okay. That means heat is evolved during the mixing process that means this process is exothermic okay. And this straight line gives a enthalpy of an ideal solution and the enthalpy of real solution with negative deviation will be less than this because the Δh_{mix} is negative okay.

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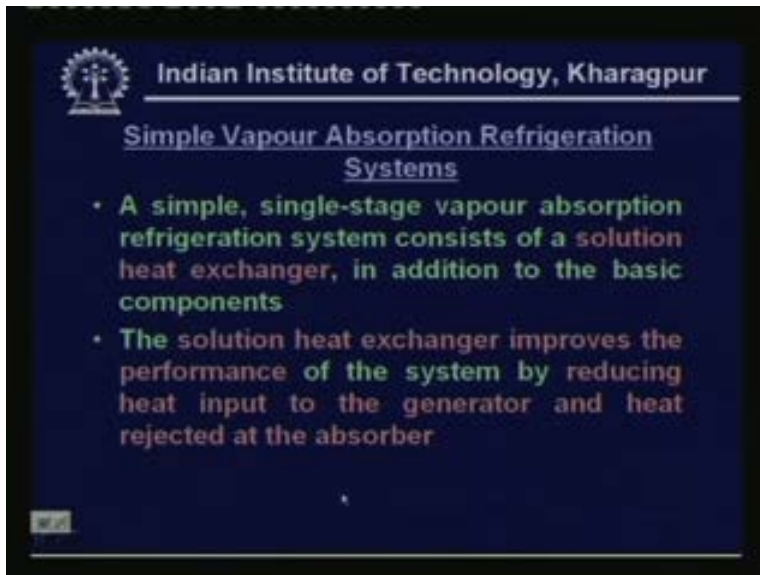


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- The differences between ideal and real solutions can be attributed to their deviation from Raoult's law
- If the deviation is positive, then at a given temperature and composition:
 1. Vapour pressure exerted is greater than that predicted by Raoult's law
 2. Heat of mixing is positive (endothermic)
- The reverse is true if the deviation is negative

So as I said if the deviation is positive then at a given temperature and composition vapour pressure exerted is greater than that predicted by Raoult's law and heat of mixing is positive. That means endothermic for positive deviation is endothermic for negative deviation it is exothermic. So the reverse is true if the deviation is negative.

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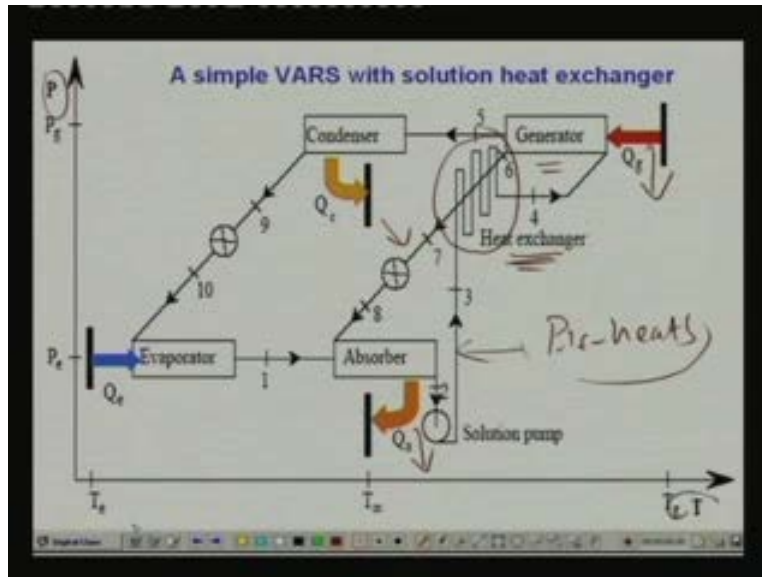
Simple Vapour Absorption Refrigeration Systems

- A simple, single-stage vapour absorption refrigeration system consists of a solution heat exchanger, in addition to the basic components
- The solution heat exchanger improves the performance of the system by reducing heat input to the generator and heat rejected at the absorber

Now let us look at simple vapour absorption refrigeration systems. A simple single stage vapour absorption refrigeration system consists of a solution heat exchanger in addition to the basic components. The solution heat exchanger improves the performance of the system by reducing

the heat input to the generator and heat rejected at the absorber. That means only difference between the earlier basic system and this simple practical system is in addition of one component.

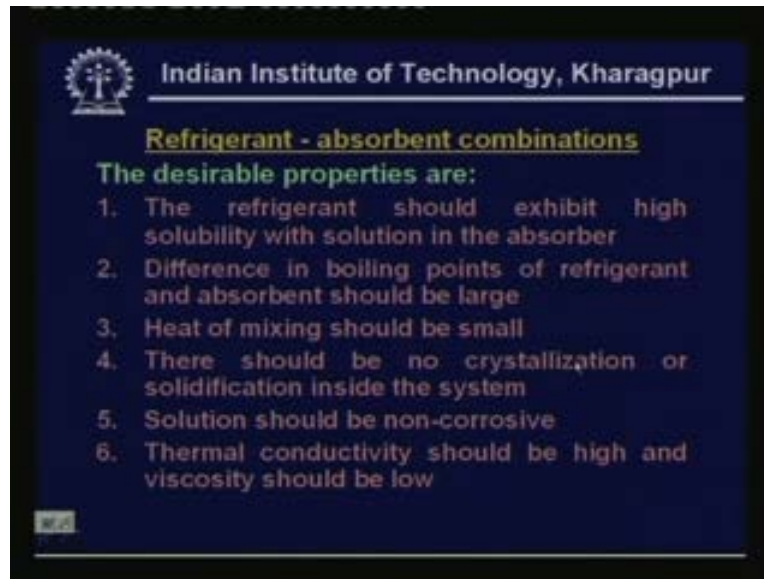
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That is called as solution heat exchanger. So what we have done in this system is an extra component is added is called a solution heat exchanger what is the function of this solution heat exchanger. This solution heat exchanger pre heats okay, pre heats the solution that is going to the generator by using the heat of the solution that is coming from the generator. So you can see that there is heat exchange between the hot solution coming from the generator and the cold solution that is going to the generator. So there is a heat exchange as a result Q_g reduces this also reduces okay.

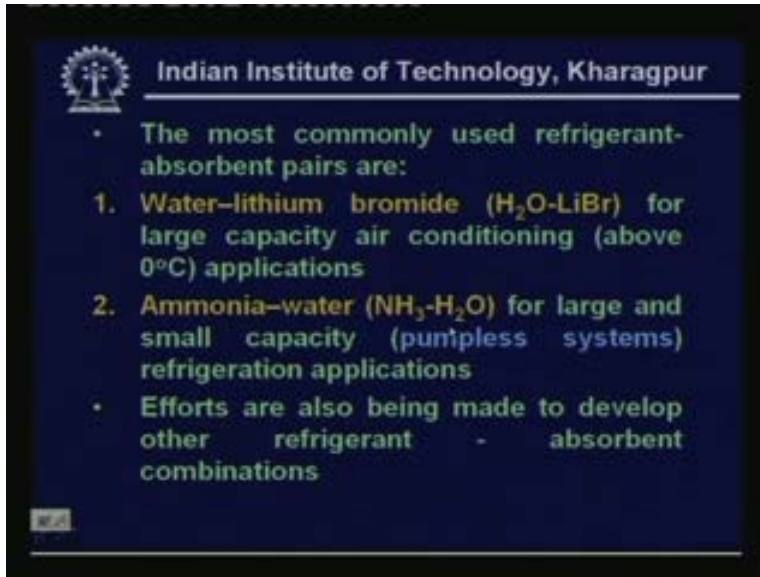
So that is the function of the solution heat exchanger here rest of the components are same okay. In fact this figure is shown as pressure versus temperature okay. The, so the you can also see the respective pressures and temperatures on this diagram okay. This I will explain in detail when we discuss the actual systems.

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Now let me quickly look at the refrigerant absorbent combinations the desirable properties are the refrigerant should exhibit high solubility with solution in the absorber it should be highly soluble in the absorber. And the difference in boiling points should be large. So that only refrigerant boils in the generator okay. This is another desirable point and heat of mixing should be small okay of course point one and three are contradictor you cannot have both okay. Then there should be no crystallization or solidification inside the system we will see what is crystallization or solidification in the next class okay. Then the solution should be non corrosive and it should exhibit good transport properties. That means thermal conductivity should be high and viscosity should be low. So these are the desirable properties.

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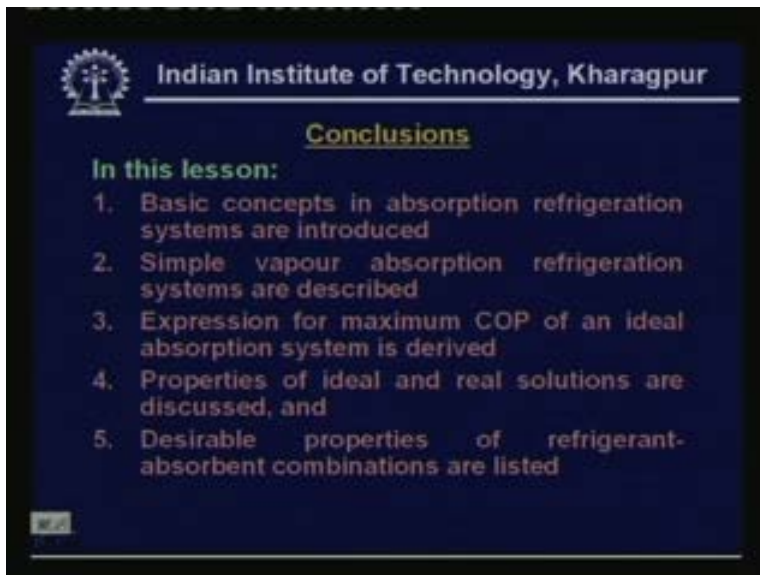


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- The most commonly used refrigerant-absorbent pairs are:
 1. Water–lithium bromide ($\text{H}_2\text{O}-\text{LiBr}$) for large capacity air conditioning (above 0°C) applications
 2. Ammonia–water ($\text{NH}_3-\text{H}_2\text{O}$) for large and small capacity (pumpless systems) refrigeration applications
- Efforts are also being made to develop other refrigerant - absorbent combinations

And based on these desirable properties there are two most commonly used refrigerant absorbent pairs they are water lithium bromide for large capacity air conditioning applications and ammonia water for large and small capacity refrigeration applications. So we will be discussing these systems in details in next class one or two lectures okay. And there are also other refrigerant absorbent pairs which are in at research level they are not yet commercialized okay. So basically the most important pairs as far as the commercialized systems are concerned are water lithium bromide and ammonia water pairs okay.

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Conclusions

In this lesson:

1. Basic concepts in absorption refrigeration systems are introduced
2. Simple vapour absorption refrigeration systems are described
3. Expression for maximum COP of an ideal absorption system is derived
4. Properties of ideal and real solutions are discussed, and
5. Desirable properties of refrigerant-absorbent combinations are listed

So let me quickly summarize what we have learned in this lesson. In this lesson basic concepts in absorption refrigeration systems are introduced and simple vapour absorption refrigeration systems are described and expressions for maximum COP of an ideal absorption system is derived. And properties of ideal and real solutions are discussed and finally we have listed desirable properties of refrigerant absorbent combinations okay. In the next lecture I shall discuss lithium bromide water systems okay after that i shall discuss ammonia water systems okay.

Thank you.