

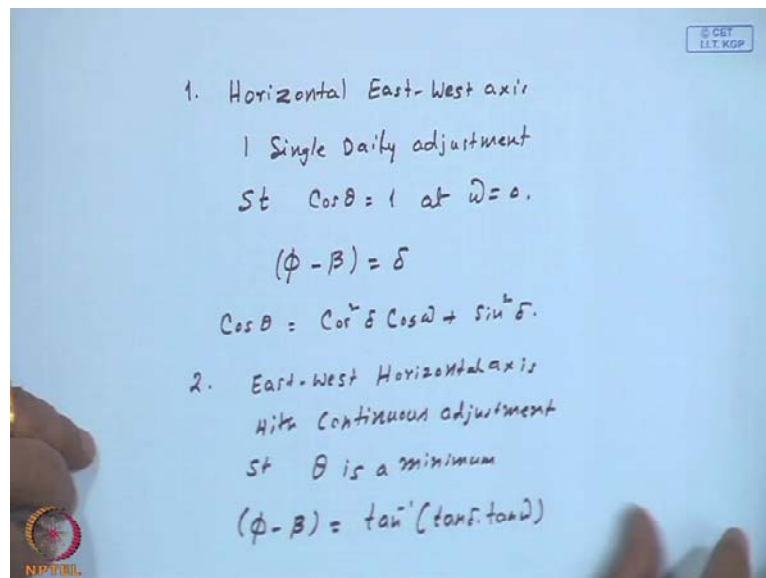
Solar Energy Technology
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Lecture - 20
Concentrating Collectors (Contd.)

Last time, we were considering concentrating collectors, and we found that in order that concentration is achieved, the solar radiation received over a larger aperture area either through reflection or refraction has to be focused on to a smaller receiver area. This requires tracking. So, quite often tracking collectors, concentrating collectors, focusing collectors these names are synonymously used though even a flat plate conductor can be tracked.

So, in order that concentration is achieved, focusing is as necessary which calls for tracking; that is the way I remember the distinction, when to call a concentrating collector, focusing collector and or tracking is necessary thing to achieve focus and concentration.

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In that, we consider two of the simpler tracking modes; with one, a horizontal east west axis with one single daily adjustment, such that $\cos \theta$ is 1 at the noon time equal to 0.

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such that the solar beam is normal to the collector aperture plane at solar noon

In this mode of tracking, the aperture plane is an imaginary plane with $\gamma=0$. Thus the slope of the aperture plane at solar noon, i.e., at $\omega=0$ can be found by setting $\theta=0$ [or $\cos \theta = 1$,] in the equation for $\cos \theta$, as,



So, this gives us the condition to be satisfied $\phi - \beta = \delta$.

(Refer Slide Time: 02:03)

$$1 = \cos(\phi - \beta)\cos \delta + \sin(\phi - \beta)\sin \delta$$

The above equation is satisfied when

$$(\phi - \beta) = \delta$$

Thus for this mode of tracking,



So, that cosine theta is given by $\cos^2 \delta \cos \omega + \sin^2 \delta$.

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$$\cos \theta = \cos^2 \delta \cos \omega + \sin^2 \delta \quad (\text{Tr. 1})$$

2. A plane (aperture) is rotated about a horizontal east-west axis with continuous adjustment to minimize the angle of incidence. Since the aperture plane is facing south ,

Eq. (a)



Then the second mode, again a east west horizontal axis with continuous adjustment such that theta is a minimum.

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$$\cos \theta = \cos(\phi - \beta) \cos \delta \cos \omega + \sin(\phi - \beta) \sin \delta$$

In order to find the condition to be satisfied for θ to be a minimum, RHS of the above equation is differentiated with respect to β and on equating to zero, it follows,

$$(\phi - \beta) = \tan^{-1}(\tan \delta / \cos \omega) \quad (\text{b})$$



So, we consider the equation for the cosine theta for a south facing surface, because it is a east west axis, then differentiate it with respect to beta and obtained that phi minus beta at any hour angle should satisfy tan inverse tan delta tan omega, which gives you the same condition as phi minus beta is equal to delta, at the time omega equal to 0.

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Using Eq.(b) in Eq.(a) , $\cos\theta$ is now given by,

$$\cos\theta = (1 - \cos^2\delta \sin^2\omega)^{1/2} \quad (\text{Tr. 2})$$

3. *A plane rotated about a horizontal north-south axis with continuous adjustment to minimize the angle of incidence:*



And for this the angle of incidence at any instance is given by 1 minus cos square delta sin squared omega to the power 1 half.

(Refer Slide Time: 03:46)

Handwritten notes on a blue background. At the top right, there is a small rectangular box containing the text '© IIT KGP'. The main text includes the equation $\cos\theta = (1 - \cos^2\delta \sin^2\omega)^{1/2}$, followed by a numbered list item '3. Plane rotated about a horizontal N-S axis. with continuous adjustment to minimize the angle of incidence'. Below this, there are two lines of text: ' $\omega < 0, \gamma = -90^\circ$ ' and ' $\omega > 0, \gamma = 90^\circ$ '. At the bottom, there is a larger equation: $\cos\theta = (\sin\phi \sin\Gamma + \cos\phi \cos\delta \cos\omega) \cos\beta - \cos\delta \sin\omega \sin\beta$. The NPTEL logo is visible in the bottom left corner of the slide.

Now, tracking mode three is what we are going to consider in detail now in this class. It is a plane rotated about a horizontal north south axis with continuous adjustment to minimize the angle of incidence. So, in order to distinguish between the two modes we described earlier and the third mode that we are talking about now. Let us say this is the horizontal north south axis and I turn towards east right in the morning, so that the Sun's rays are near normal to the aperture plane and I keep rotating, becomes horizontal around noon time and turns towards west as the Sun goes to set in the west.

So, the horizontal south, north south axis about which we will be rotating the collector if this is a parabolic collector facing east to my left and then turns like this faces west around the sunset time which is to my right.


(Refer Slide Time: 06:17)

In this case, the surface azimuthal angle (γ), is -90° before noon and $+90^\circ$ after noon. Thus, the general equation for $\cos\theta$ before noon becomes,

Eq. (a)

$$\cos\theta = (\sin\phi\sin\delta + \cos\phi\cos\delta\cos\omega)\cos\beta - \cos\delta\sin\omega\sin\beta$$

To find the condition to be satisfied such that the angle of incidence is a minimum,



So, this is such that we should choose the cosine theta for this. What we realize is for omega less than 0 gamma will be minus 90 degrees, for omega greater than 0 gamma will be plus 90 degrees. There are only two states if you consider this is the plane, this is the horizontal at noon time then there is no azimuthal angle because the projection of the outer normal will be a point only and towards the east or any time before solar noon, you have the outer normal of the surface facing towards east which indicates gamma minus 90 as per our notation.

Similarly, in the afternoon it will be gamma is equal to plus 90. So, for this either you choose minus 90, so cosine theta gets simplified from our general equation that cos theta

is equal to $a + b \cos \omega + c \sin \omega$ that simplifies to whatever I am writing down over here times $\cos \beta - \cos \delta \sin \omega \sin \beta$.

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RHS of Eq.(a) is differentiated with respect to β and equated to zero, which yields,


Eq.(b)

$$\beta = \tan^{-1} \left[\frac{-\cos \delta \sin \omega}{\sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega} \right]$$

Using Eq.(b) in Eq.(a),

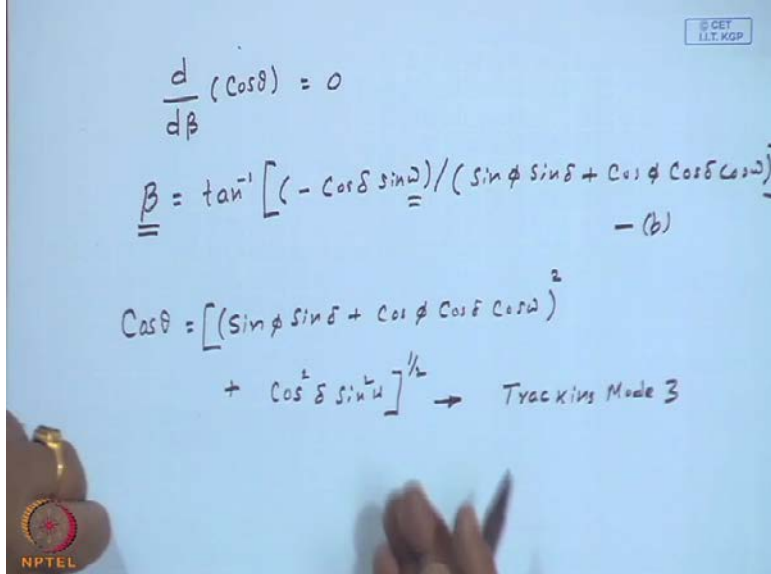
$$\cos \theta = \left[(\sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega)^2 + \cos^2 \delta \sin^2 \omega \right]^{1/2} \quad (\text{Tr. 3})$$

Exercise: Obtain the expression for $\gamma = 90$



To find this we differentiate this with respect to beta and equate it to 0.


(Refer Slide Time: 08:05)



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$$\frac{d}{d\beta} (\cos \theta) = 0$$

$$\beta = \tan^{-1} \left[\frac{-\cos \delta \sin \omega}{\sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega} \right] \quad \text{--- (b)}$$

$$\cos \theta = \left[(\sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega)^2 + \cos^2 \delta \sin^2 \omega \right]^{1/2} \rightarrow \text{Traxxins Mode 3}$$


And you will get the condition that beta should be tan inverse of minus cos delta sin omega upon sin phi sin delta plus cos phi cos delta cos omega bracket closed bracket closed. So, if we use, call this b. In the previous equation for cos theta we get cos theta longer expression sin phi sin delta plus cos phi cos delta cos omega whole square plus

$\cos^2 \delta \sin^2 \omega$ whole to the power one half. So, this is the equals angle of incidence for tracking mode three.

Tracking mode three recall it is a horizontal north south axis turned from east to west to minimize the angle of incidence for which we get the condition that beta at any instance as given by omega is governed by this and then you can have a similar exercise put in gamma equal to 0 and you will get a cosine theta angle similar.

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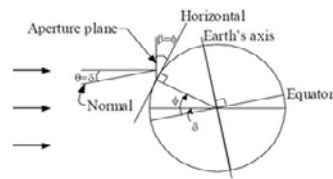
4. A plane rotated about a north-south axis parallel to the earth's axis with continuous adjustment, (polar mount)

- The focal axis is north-south and when inclined at an angle equal to the latitude, the axis is parallel to the earth's axis (see Figure).



Now, fourth mode of tracking, it is called a polar mount or a plane rotated about a north south axis parallel to Earth's axis with continuous adjustment. So, we have got a north south axis, but tilted parallel to the earth surface and rotate the plane under consideration in the direction opposite to that of the rotation of the earth at the same speed as the rotation of the earth.

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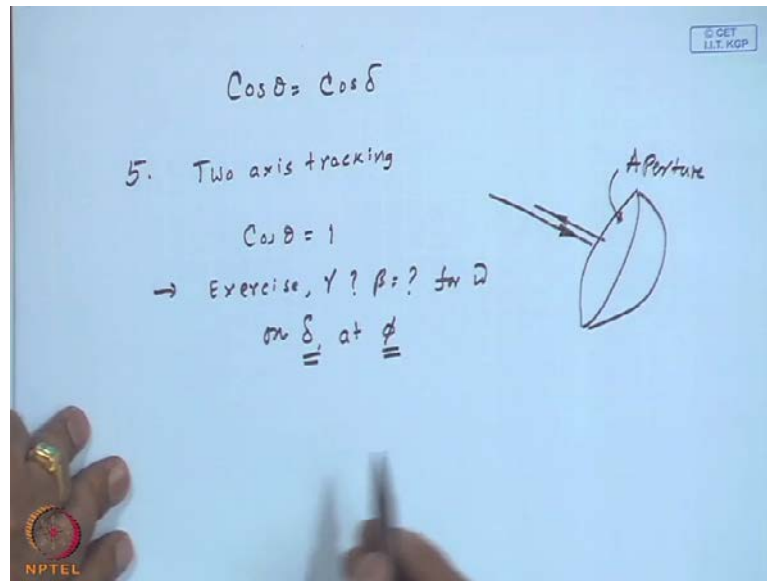
- The collector is rotated about this axis at an angular velocity equal and opposite to the earth's rate of rotation.



So, you can see the picture over here. Equatorial plane is the mid line to which the inclination, this is the equator and this is your Earth's axis and this will be your delta, the tilt or the declination and if I am having at any location of latitude phi and you have got a horizontal and this is your aperture plane with a slope beta being continuously adjusted then if this is the Sun's ray and this is the outer normal you have got the angle of theta should be equal to delta.

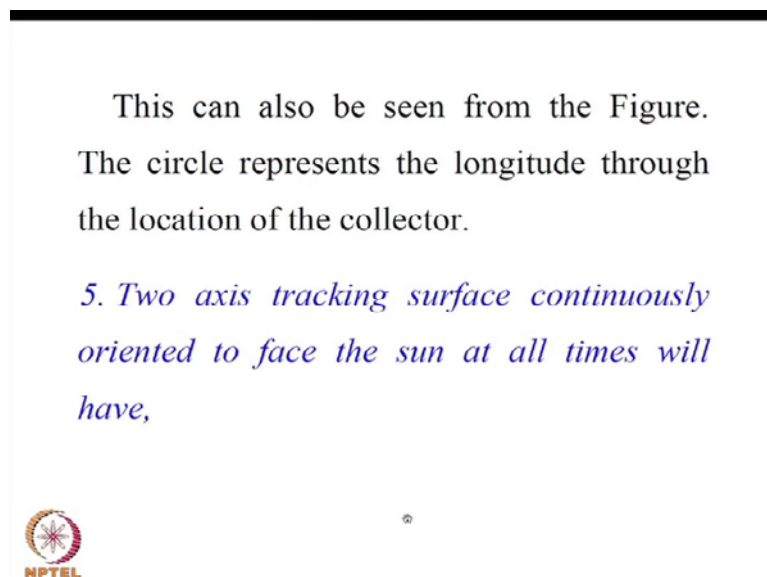
This is your Earth's axis, this is horizontal or you can focus this figure a little longer. This is the x axis which is shown over here and if you look at carefully the angles will be clear and consequently your cosine theta will simply be equal to cos delta.

(Refer Slide Time: 13:12)



So, this is also a single axis tracking a north south axis parallel to the Earth's axis, the collector being rotated in the direction opposite to that of Earth's rotation, at the same speed as Earth. So, it feels like the location with the tilt delta on that particular day consequently the angle of incidence will be cos theta is given by cos delta. So, this is also single axis tracking.

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Then last is two axis tracking. So, you do whatever you are doing in the case of tracking four. In addition you further see that the Sun's ray is normal to the outer surface under

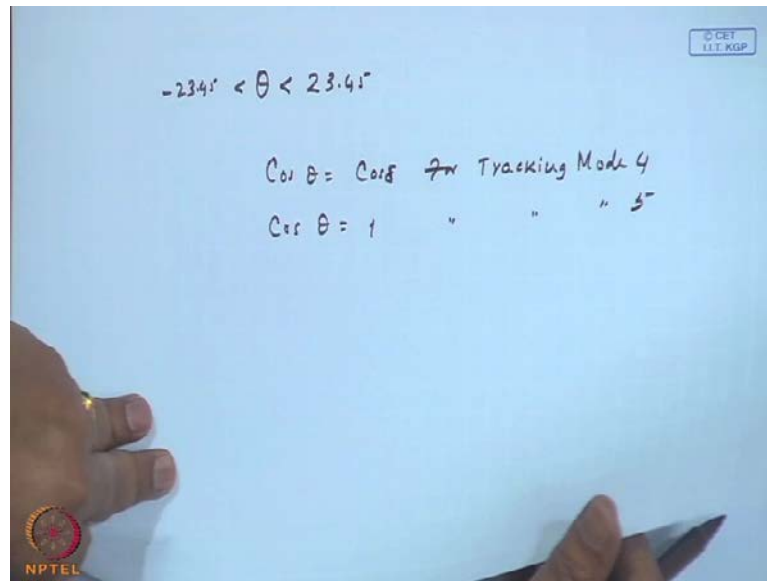
consideration. So, that $\cos \theta$ will be equal to your 1 all the time, that means θ is equal to 0 degrees which means coincides Sun's rays will coincide with the outer normal to the surface. So, you can have a little exercise that means you need a γ how much? β how much? For a given ω on a delta day at a location of ϕ .

So, if you can find out what should be the azimuthal angle and the slope at a given instance of time given by the hour angle for a particular day characterized by the declination δ at a location of latitude ϕ you can find out $\cos \theta$ is equal to 1. In other words if you are having let us say a paraboloidal dish, it will be moving from east to west in so doing the north south axis will be at different tilts. Always, the Sun's rays are parallel to the outer normal to the aperture plane which may be called this is the aperture. So, $\cos \theta$ is equal to 1. So, let us recapitulate five modes of tracking we have considered.

One is a east west axis tracking horizontal with one single daily adjustment which gives the condition $\phi - \beta = \delta$. The second one is again a east west horizontal axis with continuous adjustment so that angle of incidence is a minimum, that gave a condition from which we found $\phi - \beta$ should be something which will be obviously better than the first mode of tracking. The third mode is a horizontal north south axis. The aperture plane being rotated facing east in the morning to facing west in the afternoon for which the condition will be, your azimuthal angle should be minus 90 in the forenoon and should be equal to plus 90 as per notation in the afternoon.

And if you set the general equation for cosine θ or the angle of incidence and differentiate with respect to β that is the slope you will find, what should be the slope at different instance and it gives the long expression for the cosine angle of incidence for the surface tracked along a horizontal north south axis. The last one, fourth one is a polar mount. It is as if the surface is rotating parallel to the Earth's axis. So, consequently cosine θ should be equal to $\cos \delta$ or θ is equal to δ .

(Refer Slide Time: 17:35)



So, a word about this is theta will change from plus 23.45 to minus 23.45. In other words plus or minus it really does not matter because it is a cosine theta equal to cos delta. So, your theta will have the largest value of 23.45 magnitude, cosine theta will be almost 0.92 or 0.95, not much different from cos theta is equal to 1 though it is a single axis tracking compared to double axis tracking where cos theta compare cos theta is equal to cos delta for tracking mode four and cos theta is equal to 1 for tracking mode five.

Two axis tracking, so whereas this is a single axis tracking. So, this does not differ by more than 10 percent compared to cos theta being equal to 1. Now, we obviously, this will result in a similar change in the R b factor for the tracking surfaces.

(Refer Slide Time: 19:01)

the apparent sunrise and sunset angles are equal in magnitude. i.e.,


$$|\omega_{sr}| = |\omega_{ss}| = \omega_{str}''$$

It is safe to assume $\omega_{sr} < 0$ and $\omega_{ss} > 0$

Further, ω_{str}'' is to be limited to ω_s where

$$\omega_s = \cos^{-1}(-\tan \phi \tan \delta)$$

Thus,




Now, apparent sunrise or sunset hour angles for tracked surfaces.

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Apparent Sunrise or Sunset hour angles for tracked surfaces.

1) Tracking Makes Symmetric Sunrise - Sunset (Apparent) hour angles.

$$|\omega_{sr}| = |\omega_{ss}| = \omega_{str}''$$
$$\omega_s = \cos^{-1}(-\tan \phi \tan \delta)$$


First thing, we realize is tracking makes symmetric sunrise and sunset apparent hour angles. So, if I designate it with our conventional notation of ω_{SR} modulus should be equal to modulus of ω_{SS} which I shall call it simply ω_{str}'' because we are considering ω_{SD} from the south facing fixed surface. So, this tr indicates that it is tracking and we have used ω_{SD} as the hour angle as seen by the tracking surfaces without or before emitting it to the physical

sunrise or sunset hour angle. So, physical sunrise sunset is given by $\omega_s \cos^{-1}(-\tan \phi \tan \delta)$, you can recall one of our very early equations.

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$$\omega'_{str} = \min [\cos^{-1}(-\tan \phi \tan \delta), \omega''_{str}]$$

ω''_{str} for different tracking modes.

Tracking Mode 1
 $\theta = \pi/2$ at $\omega = \omega''_{str}$

$$0 = \cos^2 \delta \cos \omega''_{str} + \sin^2 \delta$$

$$\omega''_{str} = \cos^{-1}(-\tan^2 \delta)$$

So, in our standard notation ω_s dashed, but for a tracking surface it will be the minimum of $\cos^{-1}(-\tan \phi \tan \delta)$ and this number ω_s t r double prime. Now, we need to find out ω_s t r double prime for different tracking modes. So, tracking mode one, how do we do? θ should be equal to $\pi/2$ at ω equal to ω_s t r double prime giving rise to 0 should be equal to $\cos^2 \delta \cos \omega_s$ t r double prime plus $\sin^2 \delta$.

This I am, we have done it, I have written it elaborately by setting $\cos \theta$ the simple equation for the tracking mode 1 equal to 0 because θ is equal to $\pi/2$ the hour angle at which that occurs is the apparent sunrise sunset hour angle for the plane rotated about a horizontal east west axis with one single daily adjustment. ω_s t r double prime thus will be equal to $\cos^{-1}(-\tan^2 \delta)$. This coincides with our south facing surface because $\phi - \beta$ is equal to δ , $\cos^{-1}(-\tan \phi \tan \delta)$ now becomes $\cos^{-1}(-\tan^2 \delta)$.

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$$\omega_{str}' = \min \{ \cos^{-1}(-\tan \phi \tan \delta), \omega_{str}'' \}$$

Tracking Mode 2

$$\omega_{str} = \min \{ \cos^{-1}(-\tan \phi \tan \delta), 90^\circ \}$$
$$\cos \theta = (1 - \cos^2 \delta \sin^2 \omega)^{1/2}$$
$$\theta = \pi/2, \cos \theta = 0$$
$$\rightarrow \omega_{str}'' \rightarrow \sin^{-1} \left(\frac{1}{\cos^2 \delta} \right)$$

> 1 & ω_{str}'' Limited to 90° .

So, you have got finally, ω_{str}' should be equal to minimum of $\cos^{-1}(-\tan \phi \tan \delta)$ and ω_{str}'' . So, if you do the same thing for tracking mode two set θ is equal to $\pi/2$ ω_{str}' will be again minimum of physical sunset hour angle which is $\cos^{-1}(-\tan \phi \tan \delta)$ and 90 degrees. Now, you will find that this 90 degrees come from, if you look at your tracking mode two, this is the one, $\cos \theta$ is $(1 - \cos^2 \delta \sin^2 \omega)^{1/2}$.

So, if you put θ is equal to $\pi/2$ and $\cos \theta$ hence equal to 0 solve for ω_{str}'' , this will be something like $\sin^{-1} \left(\frac{1}{\cos^2 \delta} \right)$, is it right? If I, this is 0 so I can square it up, $\sin^2 \omega$ will be equal to $\frac{1}{\cos^2 \delta}$. So, $\sin^{-1} \left(\frac{1}{\cos^2 \delta} \right)$. So, this is going to be greater than 1. So, θ should be sorry ω_{str}'' be limited to 90 degrees. The logic being it will pass through 90 and beyond that there is no solar radiation received by the tracking mode two.

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Yielding

$$\omega_{str}'' = \cos^{-1}(-\tan^2 \delta)$$
$$\omega_{str}' = \min[\cos^{-1}(-\tan \phi \tan \delta), \omega_{str}'']$$

Tr. Mode 2

$$\omega_{str}' = \min[\cos^{-1}(-\tan \phi \tan \delta), 90^\circ]$$

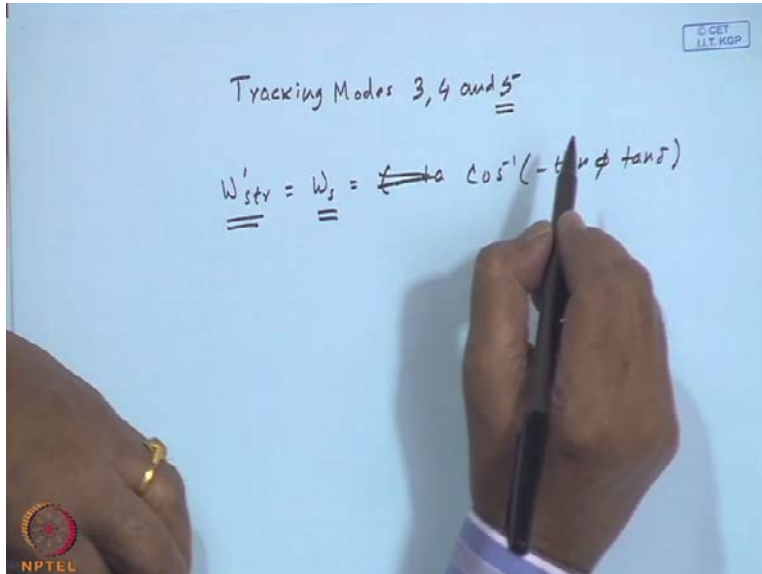
Tr. Mode 3, 4,5

$$\omega_{str}' = \omega_s = \cos^{-1}(-\tan \phi \tan \delta)$$



Let us get back to our other things, tracking mode two is over.

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Tracking Modes 3, 4 and 5

$$\omega_{str}' = \omega_s = \cos^{-1}(-\tan \phi \tan \delta)$$


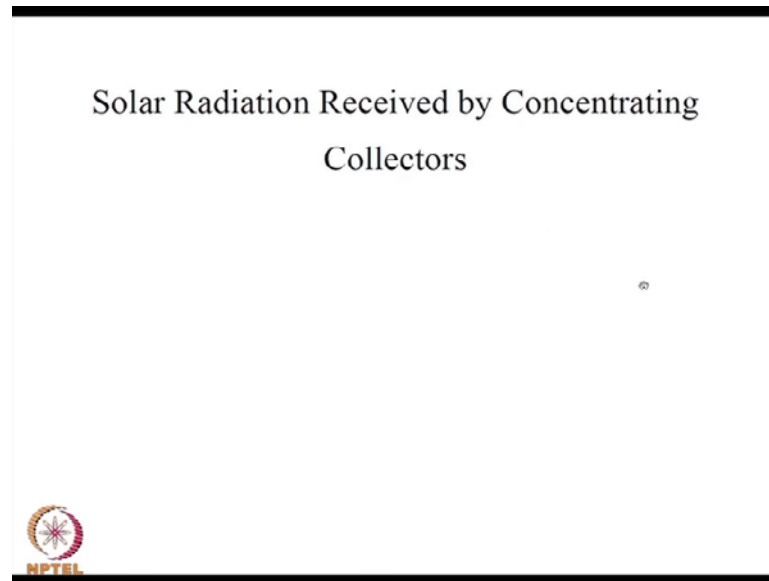
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For tracking modes three, four and five, three is a horizontal north south axis facing east in the sunrise time and facing west in the sunset time consequently my ω_{str} single dashed should be the same as ω_s should be equal to minus cos inverse minus tan phi tan delta. Similarly, this is for tracking mode four. It is a polar mode again a north south axis tilted parallel to the Earth's axis. So, it will see this on all the time the sun is above the horizon.

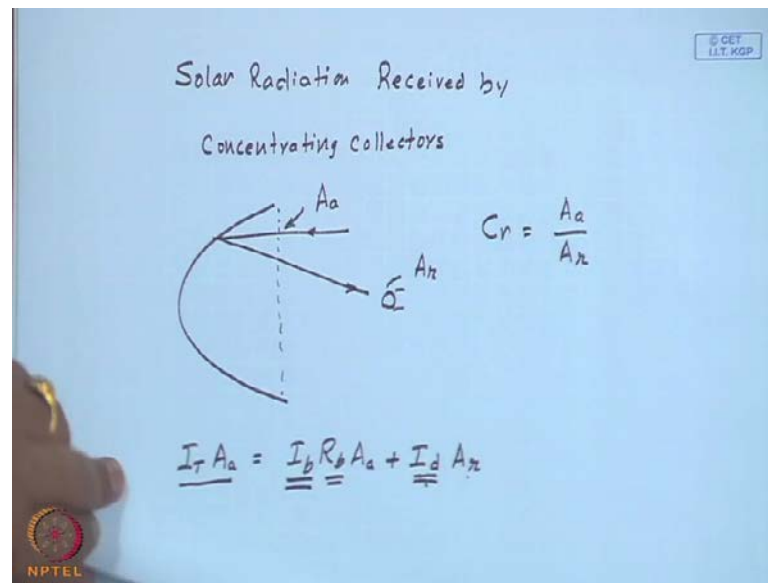
Consequently, again ω_{str} will be the physical sunrise or sunset hour angle given by $\cos^{-1}(\tan \phi \tan \delta)$. Of course, there is no ambiguity as far as the mode of tracking is considered that is because it is a double axis at every instant the Sun's ray is normal to the aperture plane so it will see the sun all the time, the sun is above the horizon.

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Now, why we are doing it is, parallel to the fixed surfaces we will try to estimate solar radiation received by concentrating collectors. So, now we know the time duration over which the rotating or tracking plane receives the solar radiation.

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So, if to get back this is a parabolic reflector of aperture area A_a reflected on to the receiver of receiver area A_r . So, per unit area of the aperture if I_T is the solar radiation received per meter square multiplied by A_a is the total radiation received by the aperture should be equal to $I_b R_b$, whatever is the radiation of the horizontal plane multiplied by the R_b factor for the aperture which is been tracked times A_a plus I_d times A_r .

So, this is the total amount of solar radiation received by the aperture which gets reflected according to some optical efficiency, that should be equal to whatever is the beam radiation received plus whatever is the diffused radiation directly received over the projected area of the receiver, because the diffused radiation that passes through the aperture will not be reflected according to the loss of optics and it may not be captured by A_r .

Nevertheless, whatever is the diffused radiation that is directly captured by the receiver will be I_d into A_r . This is all the difference between the flat plate collector and the tracking collector. And we deliberately write it in terms of the area of the aperture because that is what is going to indicate how large the collector is and depending upon the area of the A_r the ratio is going to give us what is called the geometric concentration ratio C_r is A_a upon A_r .

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$$I_T = I_b R_b + I_d (A_r/A_a)$$
$$= I_b R_b + \frac{I_d}{C_r}$$
$$C_r = \frac{A_a}{A_r}$$
$$R_b \rightarrow \text{Evaluated at } \omega = \frac{\omega_1 + \omega_2}{2}$$
$$I \rightarrow \text{J/m}^2\text{-hr}$$
$$\text{m}^2 \rightarrow \text{Aperture area}$$

So, now you will find I_t equal to $I_b R_b$ plus I_d times A_r by A_a which is $I_b R_b$ plus I_d by the geometric concentration ratio C_r . So, if C_r is very large this will be a pretty small a component where C_r once again is defined as A_a upon A_r . So, this is for any instance which we normally use it for a period of one hour and R_b being evaluated as we have done for flat plate collectors at the midpoint of the hour characterized by the two hour angles ω_1 and ω_2 by 2.

And I_b is the solar direct radiation on a horizontal surface and I_d is the diffused radiation on a horizontal surface. So, this I_t we should say is so many joules per meter square hour let us say and this m^2 is pertains to aperture. In other words this is a radiation received per unit area of the aperture.

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$$I_T A_a = I_b R_b A_a + I_d A_r$$

$$I_T = I_b R_b + I_d (A_r / A_a)$$

$$I_T = I_b R_b + \frac{I_d}{C_r}$$

where C_r the 'concentration ratio' is defined by,
 $C_r = A_a / A_r$,

Similarly, for a day, the solar radiation received per unit aperture area is given by,




Similarly, for a day you can sum up and you will get...

(Refer Slide Time: 34:32)

$$H_T = H_b \bar{R}_b + \frac{H_d}{C_r}$$

\bar{R}_b is the tilt factor, evaluated under extra-terrestrial conditions.

$\bar{R}_{bt} \rightarrow$ terrestrial conditions

$$R_b = \frac{\cos \theta}{\cos \theta_z}; \quad \bar{R}_b = \frac{\int_0^{\omega_s} \cos \theta \, d\omega}{\int_0^{\omega_s} \cos \theta_z \, d\omega}$$


According to our notation H_T will be H_b times \bar{R}_b plus a fraction due to the diffused radiation caught by the receiver. Now, \bar{R}_b is the tilt factor for the day evaluated under extra terrestrial conditions according to our notation because if you recall \bar{R}_{bt} is evaluated under terrestrial conditions. Mind you, your R_b at any instance is $\cos \theta$ by $\cos \theta_z$ and \bar{R}_b is under extra terrestrial conditions $\int_0^{\omega_s} \cos \theta \, d\omega$ upon $\int_0^{\omega_s} \cos \theta_z \, d\omega$

d omega... Where cos theta z is given by cos phi cos delta cos omega plus sin phi sin delta where this is nothing but the theta z the zenith angle or the angle of incidence further horizontal surface.

(Refer Slide Time: 36:27)

$$\cos \theta_z = \cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta$$

$\theta_z = \text{Zenith angle}$
OR angle of incidence for the horizontal surface

$$\cos \theta = \cos^2 \delta \cos \delta \cos \omega + \sin^2 \delta \quad (\text{Tr. 1})$$

$$\cos \theta = (1 - \cos^2 \delta \sin^2 \omega)^{1/2}$$

So, this is a equation that we already knew and used a large number of times. Now, cos theta for the purpose of calculating R b or R b bar for focusing collectors is given by let me repeat, so that it will be with you, you remember that the appropriate cos theta expression needs to be used for the tracking collectors. So, this is tracking mode one and for mode two, to the power one half.

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$$\cos \theta = \left[(\sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega)^2 + \cos^2 \delta \sin^2 \omega \right]^{1/2} \quad \text{--- Tr. 3}$$
$$\cos \theta = \cancel{\cos \delta} \cos \delta \quad \rightarrow \text{Tr. 4}$$
$$\cos \theta = 1 \quad \rightarrow \text{Tr. 5.}$$
$$R_b = \frac{\cos \theta}{\cos \theta_z}$$

For tracking mode three, $\sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega$ whole squared plus $\cos^2 \delta \sin^2 \omega$ whole to the power one half. So, you use this expression in calculating R_b for tracking mode three or R_b for tracking mode three. And of course, $\cos \theta$ is simply, this is for tracking mode three is simply $\cos \delta$ sorry for tracking mode four and $\cos \theta$ is 1 for tracking mode five. So, I can now evaluate R_b as in general $\cos \theta$ by $\cos \theta_z$ depending upon the tracking mode.

(Refer Slide Time: 39:53)

$$\bar{R}_b = \frac{\int_0^{\omega_s} w_s t r \cos \theta d\omega}{\int_0^{\omega_s} \cos \theta d\omega}$$

$\bar{R}_{bt} \rightarrow$ can be evaluated as has been done for non-tracking surfaces.

And $\bar{R}_b = \frac{\int_0^{\omega_s} w_s t r \cos \theta d\omega}{\int_0^{\omega_s} \cos \theta d\omega}$. We already know the expressions for $w_s t r$ and θ is the zenith angle which we already know.

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\bar{R}_b can also be evaluated under terrestrial conditions. Let the terrestrial value be designated by \bar{R}_{bt} . As has been done for tilted surfaces (non-tracking), \bar{R}_{bt} can be obtained from,

Now, we have done this calculation under terrestrial conditions for fixed orientation surfaces which we called it \bar{R}_{bt} . We can do, similar can be evaluated as has been done for non tracking surfaces. You should realize that the definition in terms of the


radiation components remains the same. What differs is the R_b factor or specifically cosine theta expression that needs to be used depending upon the tracking mode.

(Refer Slide Time: 41:32)

$$\bar{R}_{bt} = \frac{\int_0^{\omega_{sr}} (a + b \cos \omega - D_f) \cos \theta d\omega}{\cos \phi \cos \delta \int_0^{\omega_s} (a + b \cos \omega - D_f) (\cos \omega - \cos \omega_s) d\omega}$$

$\cos \theta$ is one of the expressions obtained depending on the tracking mode.

Expressions for \bar{R}_b



So, I can start with a slightly second or third step as we have already done this in the case of fixed surfaces $a + b \cos \omega - D_f$ times cosine theta $d\omega$ upon $\cos \phi \cos \delta$ integral 0 to ω_s $a + b \cos \omega - D_f$ times $\cos \omega - \cos \omega_s$ $d\omega$. Let me quickly recapitulate, what we did in the case of fixed collectors or non tracking surfaces. We expressed I_b as $I_{in} - I_{d}$ as $I_{in} (1 - \dots$