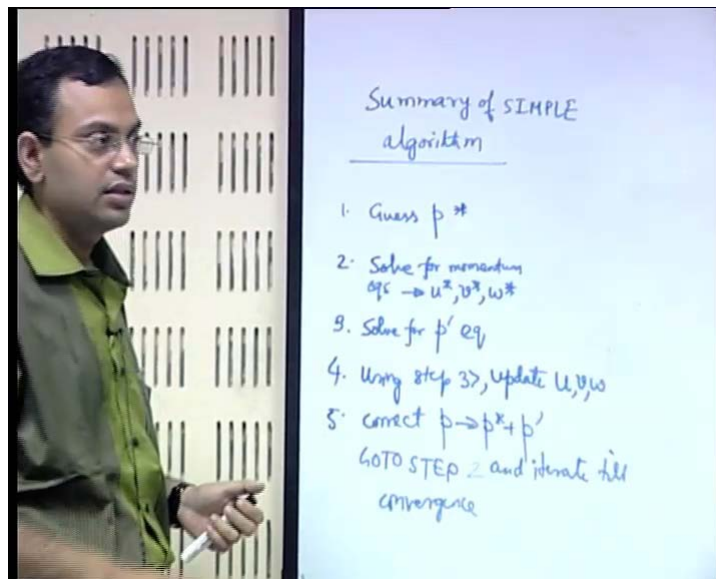


Computation Fluid Dynamics
Prof. Dr. Suman Chakraborty
Department of Mechanical Engineering
Indian Institute of Technology, Kharagpur

Lecture No. # 37
Discretization of Navier Stokes Equations (Contd.)

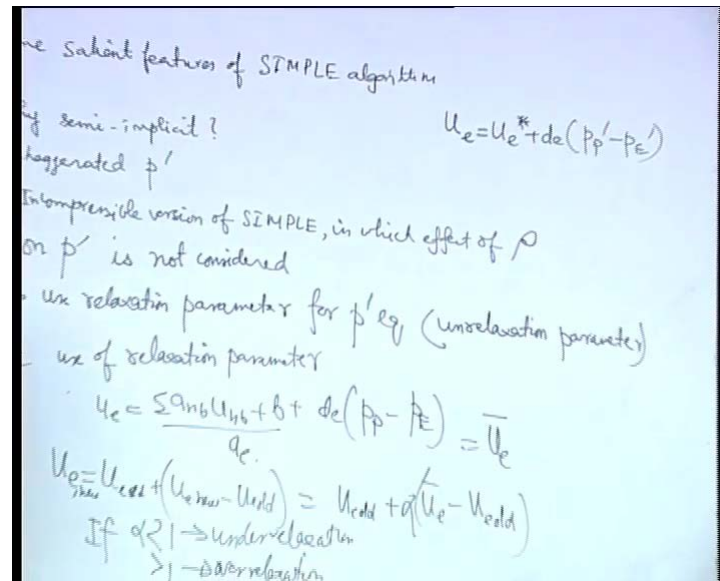
In our previous lecture, we were discussing about the simple algorithm for solution of fluid flow equations. We derived various important equations in the algorithm and we can summarize the algorithm again which we did in the previous lecture as well just for recapitulation.

(Refer Slide Time: 00:33)



So, in the simple algorithm, what you do? You guess the value of the pressure. From that you solve for the momentum equation. Then, you solve for a pressure correction equation which you derive from the continuity equation and then, using the pressure correction equation, you update the velocity and the pressure and go to the step one. Go to the step, basically go to step two it should be because your pressure is already guessed, so go to step two and iterate till convergence.

(Refer Slide Time: 01:26)



Now, let us discuss some salient features of the simple algorithm. Some features we have already discussed that why it is semi-implicit. So, remember that the key formula in the simple algorithm is the velocity correction and the pressure correction formula. So, for example, the velocity correction is $u_v = u_v^* + d_e(p_p' - p_e)$.

So, the velocity correction is a function of the pressure correction at the neighbouring grid points, but not the explicit function of the velocity correction at the neighbouring grid points. So, in that way the pressure correction carries the sole burden of correcting the velocity. So, the velocity correction could in principle be a combination of velocity correction due to neighbouring grid points plus pressure correction due to neighbouring grid points. Since, the velocity correction due to neighbouring grid points is not considered, that is omitted, so pressure correction at the neighbouring grid points is taking the sole responsibility of correcting the velocity. In doing so, it is exaggerating the pressure correction. So, that is one important consideration.

Then, the third important characteristic is that point to note is that pressure correction at a point or velocity correction at a point could also be a function of density if it were a compressible flow. Now, here in the simple algorithm which we have described, this we have described basically for incompressible flows, so that we have not used any

relationship between the pressure correction and the density. So, this is incompressible version of simple algorithm.

On pressure correction is not considered. So, this we have to keep in mind that the simple algorithm that we have described, that needs to be suitably extended for compressible flows. It is not otherwise fit for compressible flows because of the non-consideration of the density dependence on pressure correction. Now, when we have an exaggerated pressure correction, what it does is something as follows. So, when it has an exaggerated pressure correction, the new value of pressure which is predicted on the basis of pressure correction is always exaggerated from the value that you would have expected. Whatever value of pressure that would have expected, the correction is more severe to take it away from that.

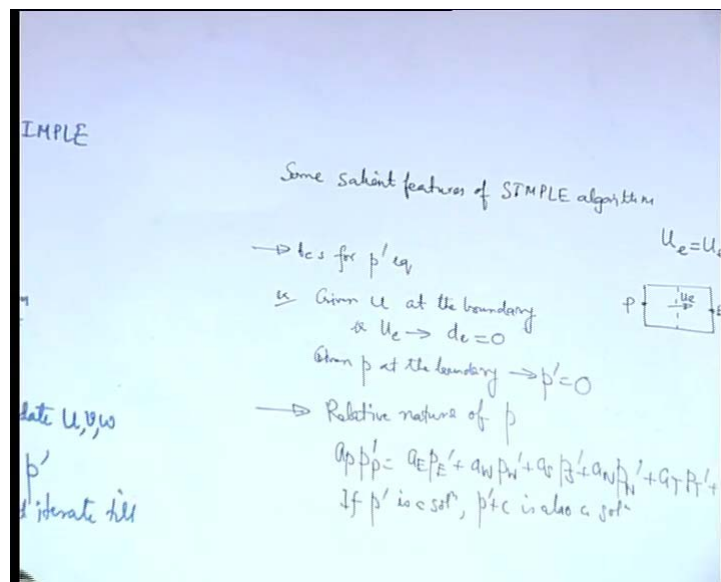
So, how would you bring the pressure back to a non-exaggerated corrected value? So, you can do that in certain ways. One is use relaxation parameter for pressure correction equation. So, what is a relaxation parameter? For example, if you wanted to use a relaxation parameter for momentum equation, how you would have done it. So, just as an example use of relaxation parameter, so u_e is equal to $\sigma \frac{a_n b_n}{a_e} + b_e$ plus b_e into $p_p - p_e$. So, u_e is equal to $\sigma \frac{a_n b_n}{a_e} + b_e$ by a_e , this into d_e . So, let us call this as u_e^{bar} . So, we could write u_e is equal to $u_e^{\text{old}} + u_e^{\text{new}} - u_e^{\text{old}}$. So, this is something that we can write irrespective of any constraint, that is u_e . This u_e^{new} is equal to $u_e^{\text{old}} + \text{new} - \text{old}$, right.

So, now in place of u_e^{new} which should be u_e^{bar} , we can write this $u_e^{\text{old}} + u_e^{\text{bar}} - u_e^{\text{old}}$, just different name. So, this is the same equation. Just we in place of u_e^{new} , we have put u_e^{bar} to explicitly mention the expression. Next, what we do is, we multiply this by a relaxation factor alpha. This type of policy we have adopted in the relaxation techniques for system of solving systems of algebraic equations. So, the same thing that we are doing here just in the context of solution of these discretized equations is that, when we have this relaxation parameter alpha by this, you control the change. So, u_e^{new} is equal to $u_e^{\text{old}} + \text{the change}$. So, if this alpha is less than 1 that means you are slowing down the change. So, in this way, you can if alpha is less than 1, it is called as under relaxation parameter. If alpha is greater than 1, it is over relaxation.

So, in case of pressure correction equation, what type of relaxation you want to use, under relaxation or over relaxation? Under relaxation. So, when you say use relaxation parameter for pressure correction equation, we may amplify a bit more and say that it is under relaxation parameter, ok.

Now, there are few other facts that remain about the simple algorithm which are what we discussing and one of the key issues is the boundary conditions for pressure correction equation. See pressure correction equation has evolved as one of the artefacts of this algorithm. So, we need to discuss more specifically on the pressure correction equation, its various criticalities. So, one of the criticalities is how to apply the boundary conditions. So, boundary conditions for pressure correction equation.

(Refer Slide Time: 11:01)



Now, there are several types of boundary conditions possible. We can discuss two important boundary conditions. One is given value of pressure at the boundary and there is given value of velocity, normal component of velocity at the boundary. So, if you have given velocity at the boundary, then how do you reflect that in in your implementation of the algorithm? How do you reflect that? See when you have a given velocity at the boundary or where ever, then add that particular location. You do not require any velocity correction, right. Since, you do not require any velocity correction, but you you may require pressure correction. So, this term may be there, but you want u v equal to u v star.

As an example, if you have specified velocity at e and that means, that you must have d_e equal to 0. Example, u_v , then d_e equal to 0 which is equivalent to a_e equal to 0 or it is better to say, d_e equal to 0 because it directly covers the case without going through the original coefficients. If you have given pressure at the boundary, then obviously pressure correction equal to 0.

The other very important characteristic of the pressure correction equation is the relative nature of pressure. So, if you recall the pressure correction equation is $a_p p_p' = a_e p_e' + a_w p_w' + a_s p_s' + a_n p_n' + a_t p_t' + a_b p_b' + b$, where the convergence criteria is that b is the mass source term from continuity equation. So, b equal to 0 is the convergence criteria that when b equal to 0, that means you have come up with a continuity satisfying velocity field. So, when b equal to 0, 0 on convergence, then we can see that if p^* is a solution of the equation, then $p^* + c$ is also a solution and that follows from $a_p p_p' = \sigma a_n b$.

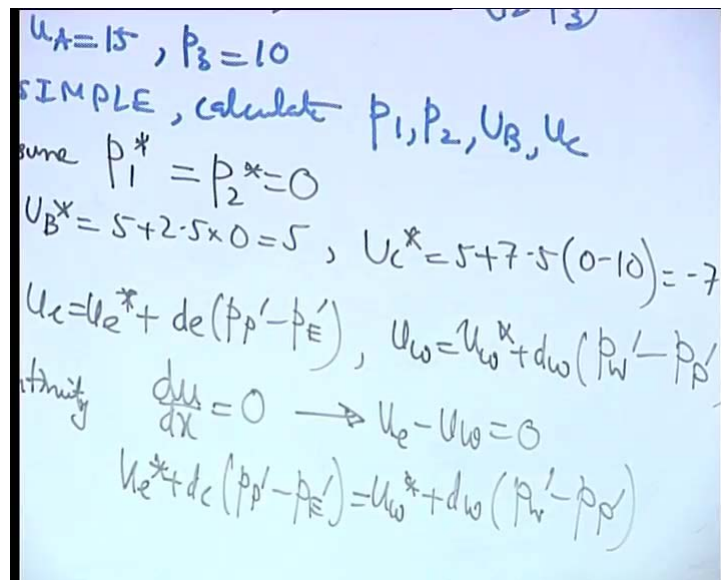
So, you can get non-ambiguous solution of pressure correction. Of course, you can get a unique solution if you set pressure correction at a particular point equal to a reference value and you can calculate the pressure corrections at other points based on that particular reference value, but otherwise, there is no (()) about the value of the pressure correction. The reason is that in an incompressible flow when you are not considering a density dependence of pressure correction, it is the difference in pressure that is important for driving the flow and that difference in pressure is reflected in terms of the difference in pressure correction and the difference in pressure correction does not matter. Its value does not matter irrespective of the value of c . It will come out to be the same because for example, if you have $p_P' - p_E'$, it is same as $p_P' + c - p_E' + c$.

So, that $+c$ will not matter. It is difference in pressure or difference in pressure correction. They are equivalent. So, that is what is mattering. In fact, $p^* = 0$ is a trivial solution of this equation and that is quite physically intuitive because 0 pressure correction means, as if you have come up or you have arrived at converge pressure where there is no further correction of pressure necessary. When there is 0 pressure correction, the source term, the mass source term in this equation becomes 0, ok.

So, it is very important to keep in mind that this pressure correction equation has these very important specific characteristics. The other thing is that it does not have any one way type of coordinate behaviour. So, it is essentially an electric type of equation, where the effect of pressure variation at a point is felt at all neighbouring points, but if you consider flow which has a strong unidirectional property, like a case where you are having boundary layer type of approximation that, you do not have any pressure gradient in the wide direction within the boundary layer.

So, in that case, you have a one way type of behaviour and also, when you have a high velocity compressible flow in a particular direction, so in that case also you are adding directionality to the equation in terms of making it a one way system. That depends on the mach number of flow. So, it all depends on what is the mach number of flow for compressible flows. For incompressible flow, until and unless you have a special situation like the boundary layer where you have gradient of pressure at one particular direction equal to 0, you do not have such situation. In the normal case, you have the pressure correction at a point is affected by pressure correction at all other neighbouring points, ok.

(Refer Slide Time: 19:38)



$u_A = 15, P_3 = 10$
 SIMPLE, calculate P_1, P_2, U_B, U_C
 assume $P_1^* = P_2^* = 0$
 $U_B^* = 5 + 2.5 \times 0 = 5, U_C^* = 5 + 7.5 \times (0 - 10) = -7$
 $U_C = U_C^* + d_C(P_P' - P_E'), U_W = U_W^* + d_W(P_W' - P_P')$
 continuity $\frac{dU}{dx} = 0 \rightarrow U_C - U_W = 0$
 $U_C^* + d_C(P_P' - P_E') = U_W^* + d_W(P_W' - P_P')$

Now, with this background, let us try to work out 1 or 2 examples on the simple algorithm. It is a one-dimensional problem and you have given the momentum equations for the grid points B and C. U_B is equal to 5 plus 2.5 into P_1 minus P_2 , U_C is equal to

$5 + 7.5 \Delta x$ into $P_2 - P_3$. The boundary conditions are $U_A = 15$, $P_3 = 10$. Using simple calculation procedure, calculate P_1 , P_2 , U_B and U_C . So, let us mark the given values in the figure just for convenience. $U_A = 15$ with some arbitrary units, $P_3 = 10$ and the grid points are equidistant. So, what would be the first step? Guess P^* , right. So, your first step is to guess what the value of the pressure at each point is. So, how will you guess the value of P^* ? You can make some intelligent choice and even if you do not make any intelligent choice, any arbitrary choice will also do. So, let us just make any arbitrary choice just to see that how it functions.

So, let us say that $P_1^* = P_2^* = 0$. Really, it is a wrong, very wrong choice if you can see. If you have a flow here like this with a pressure gradient driven, then you do not expect that these two pressures will be equal, but just let us see that how the algorithm behaves with this. So, when you have this one, then next step will be to solve for momentum equations to get u^* , v^* and w^* . So, the step 2, if you solve for the momentum equation, then what is U_B^* ? $5 + 2.5 \Delta x \cdot 0$ that is 5. U_C^* is equal to $5 + 7.5 \Delta x \cdot 0 - 10$, so that is minus 70.

Next will be to solve for the pressure correction equation. So, in this simplified case, let us derive the pressure correction equation from the continuity equation. So, you have, if you consider grid point e , where you have the velocity u_e , so you have $u_e = u_e^* + d_e (p_p - p_e)$ and $u_w = u_w^* + d_w (p_w - p_p)$. So, continuity equation is, you assume one-dimensional and $\rho = \text{constant}$. So, continuity equation $\frac{du}{dx} = 0$. If you integrate it with respect to x , what you get? $U_v - U_w = 0$. So, you have $u_v^* + d_e (p_p - p_e) = u_w^* + d_w (p_w - p_p)$.

(Refer Slide Time: 26:47)

$$(d_e + d_w) p'_p = d_e p'_E + d_w p'_W + (U_w^* - U_e^*)$$

pt 1

$$\left(\frac{d_B + d_A}{2.5}\right) p'_1 = d_B p'_2 + d_A p'_W + (U_A^* - U_B^*)$$

$$2.5 p'_1 = 2.5 p'_2 + 10$$

$$\Rightarrow p'_1 = p'_2 + 4$$

pt 2

$$\left(\frac{d_C + d_B}{7.5}\right) p'_2 = d_C p'_3 + d_B p'_1 + (U_B^* - U_C^*)$$

$$10 p'_2 = 2.5 p'_1 + 7.5$$

$$\Rightarrow 4 p'_2 = p'_1 + 30$$

Given to
 $U_B = 5$
BCs
 Using s
 step 1) Assu
 step 2) U
 step 3) U
 Cont

So, you have $d_e + d_w p'_p$ is equal to $d_e p'_E$, sorry $d_e p'_E$ plus $d_w p'_W$ plus $U_w^* - U_e^*$. So, in place of d_e and d_w , what are the values you will be putting? It depends on what are the grid points for which you are solving. So, what are the points for which you will solve? One is for 1, another is for 2. So, you have one control volume for pressure correction as this, another control volume for pressure correction as this. So, if one is the point p , then what is e and small e and small w ? Capital A is small w and capital B is small e . So, you can write for point 1, $d_B + d_A$ into p'_p is equal to $d_B p'_B$ plus $d_A p'_A$ plus $U_A^* - U_B^*$.

What is d_B ? What is the value of d_B ? What is the momentum equation given? U_B equal to it is of the form $U_B = U_B^* + d_B (p_1 - p_2)$. So, d_B is 2.5. What is d_A ? d_A is 0 because U_A is given. So, $2.5 p'_p$ is equal to 2.5. In place of p , we will put 1, p'_1 , sorry this instead of B and A , these will be the numbers. So, this will be d_B . Instead of p'_e , what will be that? 2, p'_2 ? Remember, this d refers to the face of the control volume and this number refers to the corresponding main grid point. So, it is not the same. Just mistakenly I have written it to be the same, it is not the same.

So, what will be the w prime? W prime will be, so it does not matter because you have d_A equal to 0. There is no such point and clearly reflected by $d_A = 0$. So, $2.5 p'_1$

prime equal to $2.5 p_2$ prime. What is u_A star minus u_B star? So, u_A star is 15, u_B star is 5 plus 10. So, that means you have p_1 prime is equal to p_2 prime plus 4. This is one equation.

Then, consider point 2. Let us write it straight away. So, for point 2, it will be d_C and d_B . So, what is d_C ? So, let us write d_C plus d_B into p_2 prime is equal to $d_C p_3$ prime plus $d_B p_1$ prime plus U_B star minus U_C star. So, let us substitute the values. d_C is 7.5, d_B is 2.5. So, 7.5. This is 2.5, but even if it is 7.5, it does not matter because p_3 is given. So, p_3 prime is 0. Then, U_B star minus U_C star. U_B star is 5 and U_C star is minus 70. So, you have $10 p_2$ prime is equal to $2.5 p_1$ prime plus 75. That means $4 p_2$ prime is equal to p_1 prime plus 30. Now, you can calculate. Let us do it at the top. Now, you can calculate p_1 prime and p_2 prime.

(Refer Slide Time: 33:50)

Handwritten mathematical derivations on a blue background. The equations show the calculation of pressure corrections p_1' and p_2' using velocity differences and density ratios. A note "Ex 1" is written in the top right.

$$3p_2' = 34$$

$$p_2' = \frac{34}{3}$$

$$p_1' = p_2' + 4 = \frac{34}{3} + 4 = \frac{46}{3}$$

$$U_B = U_B^* + d_B(p_1' - p_2')$$

$$= 5 + 2.5\left(\frac{46}{3} - \frac{34}{3}\right)$$

$$= 15$$

$$U_C = U_C^* + d_C(p_2' - p_3')$$

$$= -70 + 7.5\left(\frac{34}{3} - 0\right)$$

$$= -70 + \frac{7.5 \times 34}{3} = 15$$

$$p_1 = p_1^* + p_1' = \frac{46}{3}$$

$$p_2 = p_2^* + p_2' = \frac{34}{3}$$

So, you can write $4 p_2$ prime. You can just solve these equations. In place of p_1 prime, you can write $4 p_2$ prime plus 30 equal to p_2 prime plus 4 minus 30. So, $3 p_2$ prime is equal to 4. That means, p_2 prime is 34 by 3 and p_1 prime is p_2 prime plus 4. So, 34 plus 4 by 3 , so 46 by 3 . So, once you obtain the pressure corrections, next step will be.

What will be the next step? So, you have to update the velocity based on the pressure correction. Now, you have U_B equal to U_B star plus d_B into p_1 prime minus p_2 prime. What is U_B star? 5 plus d_B 2.5 into 46 by 3 minus 34 by 3 . So, this is equal to 12 by 3 , that is 4 into 2.5 is 10 plus 5 is 15 and you need to calculate U_C also. U_C equal

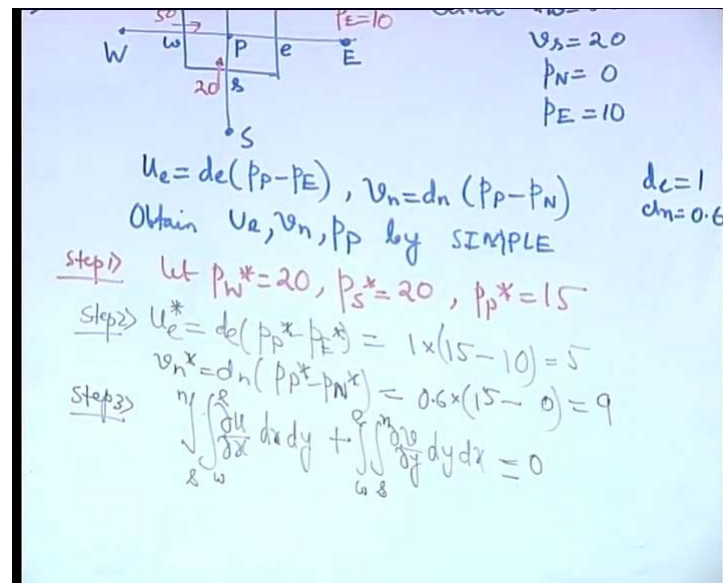
to U_C star plus dC into p_2 prime minus p_3 prime. U_C star is minus 70 plus dC 7.5 into p_2 prime minus p_3 prime. So, let us just simplify it a bit. 75 by 10 into 34 by 3. 5, 5, 17, 15.

So, once you calculate this, next you should check for convergence. That is if the mass source term is 0, then you need not calculate anything else and you can simply write what are the pressures as the old pressures plus the pressure correction and stop your calculation there. So, anyway, first let us write the pressures, p_1 is equal to p_1 star plus p_1 dash. So, that is equal to 46 by 3, p_2 equal to p_2 star plus p_2 dash. That is equal to 34 by 3. What is B ? B in the momentum equation was u_w star minus u_e star. So, for control volume 1, there are two control volumes.

For control volume 1, B is equal to U_A star minus U_B star which is equal to 0. For control volume 2, B equal to U_B star minus U_C star. This is equal to 0. That means it has converged. So, it is a very interesting thing to note that irrespective of your initial choice, your initial guess in the pressure value, the simple algorithm in a one-dimensional problem has converged just in one step of the calculations. One of the important insights towards that is that the continuing continuity satisfying velocity field in that case ensures the same velocity at all points, which is readily arrived at. So, there is no mass source term that remains.

The other important thing to observe is that, it is p_1 prime minus p_2 prime. That is important. So, p_1 prime minus p_2 prime equal to 4. That was the sole important thing for dictating what U_B is. So, even if p_1 prime was p_1 prime plus c and p_2 prime was p_2 prime plus c that would have not changed or created any difference. Similarly, even if p_2 prime was p_2 prime plus c and p_3 prime was p_3 prime plus c that would not created any difference. From where that plus c could have come? It would have come from different initial guess of p_1 prime and p_1 star and p_2 star. So, if would have guessed something different, what you would have expected is that the final value due to difference in pressure. The final value of pressure may be the final value, so pressure corrections may be different, but the differences in pressure corrections will still remain the same. The differences in pressure correction will not change. The velocities will remain the same; just the values may change depending on how you start with your initial guess, ok.

(Refer Slide Time: 41:34)



Let us work out another problem. This is a two-dimensional problem with uniform grid spacing along x and y, that is delta x equal to delta y. It is given that u w equal to 50, v s equal to 20, p N equal to 0, p E equal to 10 and the momentum equations are given as follows. U e is equal to d e into p p minus p E, v is equal to d n into p p minus p N, where d e equal to 1 and d n equal to 0.6. Obtain u e, v n, p p by simple algorithm.

So, let us just mark in the figure, what are the parameters given. U w equal to 50, p s equal to 20, p n equal to 0 and p e equal to 10. So, what will be your step 1? Guess pressure value at the points where pressures are not given, that is capital P, capital W and capital S. So, let us just for example, let p w star equal to 20, p s star equal to 20 and p p star equal to 15 based on some arbitrary guess values. Based on these guess values, you can next calculate what is u v star, sorry u e star? What will be u e star? This is step 2. It will be d e into p p star minus p e star.

So, 1 into 15 minus. What is p e star? P e star is same as p e, which is given equal to 10, this is equal to 5. Then, v n star is equal to d n into p p star minus p n star. So, 0.6 into p p star is 15 minus p w star is 20, sorry p n star is 0. So, that is equal to 9. This is N star c. So, you have calculated the guess values corresponding to the momentum equation for velocity. What will be the next step? Next step is to derive the pressure correction equation. So, it is a two-dimensional problem incompressible flow.

(Refer Slide Time: 47:59)

$$+ (u_w^* - u_e^*) + (v_s^* - v_n^*)$$

$$1.6 p_p' = p_E' + 0.6 p_N' + (50 - 5) + (20 - 9)$$

$$1.6 p_p' = 56 \rightarrow p_p' = 35$$

step 4)

$$u_e = u_e^* + d_e (p_p' - p_E')$$

$$= 5 + 1 \times (35 - 0) = 40$$

$$v_n = v_n^* + d_n (p_p' - p_N')$$

$$= 9 + 0.6 \times (35 - 0) = 30$$

So, we have integrated the continuity equation. So, it will be u_v minus u_w into Δy plus v_n minus v_s into Δx equal to 0. Δy and Δx are the same. In place of u_e , you can write $u_e^* + d_e$ into $p_p^* - p_E^*$. In place of u_w , $u_w^* + d_w$ into $p_p^* - p_W^*$. Similarly, in place of v_n , $v_n^* + d_n$ into $p_p^* - p_N^*$. In place of v_s , $v_s^* + d_s$ into $p_p^* - p_S^*$ equal to 0. So, if you assemble it, it will be d_e plus d_w plus d_s plus d_n , p_p^* is equal to $d_e p_E^* + d_w p_W^* + d_n p_N^* + d_s p_S^* + u_w - u_e + v_s - v_n$ is the mass source term.

So, let us substitute these values now. What is d_e ? d_e is equal to 1. What is d_w ? U_w is given, so d_w is 0. What is d_s ? V_s is given, so d_s is 0. What is d_n ? D_n is 0.6. So, this is 1, d_w is 0, d_n is 0.6 and d_s is 0. These are stars, right, $u_w^* - u_e^* + v_s^* - v_n^*$. So, $1.6 p_p'$ is equal to p_E' plus $0.6 p_N'$ plus $u_w^* - u_e^* + v_s^* - v_n^*$. What is u_w^* ? U_w^* is given. What? That is u_w that is 15 minus. What is u_e^* ? U_e^* is 5 plus $v_s^* - v_n^*$. v_n^* is 9 and since, at E and N, p values are given, so p_E' equal to 0 and p_N' equal to 0 because p_E and p_N are given. So, there corrections are 0. So, you have $1.6 p_p'$ equal to $50 - 5$, that is 40, $50 + 20$ is 70 minus 14, that is 56. So, if you solve for p_p' , p_p' will be equal to 35. So, once you have calculated p_p' , what will be the next step?

So, step 4. U_v is equal to u_v^* plus d_e into p_P' minus p_E' . So, 5 plus 1 into p_P' minus p_E' . 35 minus p_E' is 0. So, this equal to 40. Then, v_n equal to v_n^* plus d_n into p_P' minus p_N' . So, what is v_n^* ? 9 plus d_n 0.6 into 35 minus 0. So, what will be this? 30. So, the unknown velocity is we have obtained as the new u_E equal to 40 and new v_N equal to 30. So, what is the new pressure? So, p_P .

(Refer Slide Time: 55:46)

The whiteboard contains the following content:

- Diagram:** A central node 'P' is surrounded by four nodes: 'W' (west), 'E' (east), 'N' (north), and 'S' (south). Distances are marked: $\Delta x = \Delta y$. Velocities are shown: $u_w = 50$ (westward), $v_s = 20$ (southward), $u_e = 40$ (eastward), and $v_n = 30$ (northward). Pressures are marked: $p_N = 0$, $p_E = 10$, and $p_P = 15$.
- Equations:**

$$u_e = d_e(p_P - p_E), \quad v_n = d_n(p_P - p_N)$$
- Text:** "Obtain u_e, v_n, p_P by SIMPLE" and "Given $u_w = 50, v_s = 20, p_N = 0, p_E = 10$ ".
- Steps:**

$$p_P = p_P^* + p_P' = 15 + 35 = 50$$
- Convergence check:**

$$b = u_w^* - u_e^* + v_s^* - v_n^* = 50 - 40 + 20 - 30 = 0 \text{ (converged)}$$

Step 5, p_P equal to p_P^* plus p_P' . So, 15 plus 35, that is 50. Next convergence check what was b here? $U_w^* - u_e^* + v_s^* - v_n^*$. U_w^* is 50 that is given. Minus u_e^* is and this is new u_e^* , this is new v_n^* . So, u_e^* is 40, v_s^* is 20 minus v_n^* is 30. So, this is equal to 0. That means it has converged. So, you can see that the total rate of inflow is same as total rate of outflow about this control volume. So, that means the calculations in this iteration whatever have been obtained, these are the converged values for u_e, v_n and p_P . So, we will stop here today and in the next class, we will consider a slightly improved version of this algorithm known as revised simple or simpler algorithm. That we will see in the next class.

Thank you