

Basics of Finite Element Analysis – Part II
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Lecture - 34
Stiffness and Force matrices for Rectangular element

Hello. Welcome to Basics of Finite Element Analysis Part II. This is the 6 week of this course, today is the 4th day of the week in the last week we had calculated elements of K and F matrices, and these calculation for specific for a 3 noded triangular element, that is a linear triangular element. What we will do is something very much similar to what we did in the last class, but with the difference that we will be using all that knowledge to 4 noded rectangular elements.

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CALCULATE $[k]$ and $\{F\}$ FOR 4-NODED RECTANGULAR ELEMENT

TRANSFORMATIONS

$x = \bar{x} + x_1^e$
 $y = \bar{y} + y_1^e$
 $dx = d\bar{x}$
 $dy = d\bar{y}$

$(x_1^e, y_1^e) = \text{coords of N1 in global coord system.}$

$S_{ij}^{00} = \int_{x_1^e}^{x_1^e+a} \int_{y_1^e}^{y_1^e+b} \psi_i^e(x,y) \psi_j^e(x,y) dx dy = \int_0^a \int_0^b \psi_i^e(\bar{x},\bar{y}) \psi_j^e(\bar{x},\bar{y}) d\bar{x} d\bar{y}$
 $S_{ij}^{01} = \int_0^a \int_0^b \psi_i \frac{\partial \psi_j}{\partial \bar{x}} d\bar{x} d\bar{y}$
 $S_{ij}^{11} = \int_0^a \int_0^b \frac{\partial \psi_i}{\partial \bar{x}} \frac{\partial \psi_j}{\partial \bar{x}} d\bar{x} d\bar{y}$
 $S_{ij}^{10} = \int_0^a \int_0^b \frac{\partial \psi_i}{\partial \bar{x}} \psi_j d\bar{x} d\bar{y}$
 $S_{ij}^{12} = \int_0^a \int_0^b \frac{\partial \psi_i}{\partial \bar{x}} \frac{\partial \psi_j}{\partial \bar{y}} d\bar{x} d\bar{y}$

So, what we plan to do today is calculate elements of elements of K matrix and F vector for a 4 noded rectangular element. So, these are my coordinates x and y and we know that my rectangle was such that it is coordinates are aligned to the axis x and y axis and then I had developed approximation function for this 4 noded element in local coordinate system $\bar{x}$ and $\bar{y}$ and the 4 coordinates are 1,2,3,4. So these are the 4 nodes and the length of 1 side of the rectangle is a the other side is b. So, these nodes are 0,0 a,0 a, b and 0,b.

So, now first let us look at the transformations. So, this is a point x in the global coordinate system, that can be written as. So, the x coordinates of any point in a global coordinate system is equal to $\bar{x}$ plus x_1 . What is x_1 ? So, x_1 is this distance, it is the x coordinate of the first node in the global coordinate system. So, any point in local coordinate system can be mapped to that in the global coordinate system for the x direction using x this relation, x is equal to $\bar{x}$ plus x_1 . Similarly y is equal to $\bar{y}$ plus y_1 . What is y_1 ? y_1 is this in.

So, in the global coordinate system the coordinates are x_1 and y_1 . x_1 , y_1 are coordinates of node 1 in which system global coordinate system. And in the local coordinate system the coordinates of first node are 0, 0. So the other thing is dx if I differentiate first equation is same as $d\bar{x}$ and dy is same as $d\bar{y}$. So, these are the transformations and using these transformations I can calculate values of S metric and different S matrices for instance. We have developed that S_{00ij} is equal to ψ_i . This is the original definition for elements of S_{00} .

Now, here we note that ψ_i is expressed as function of $\bar{x}$ ψ_j is for expressed as function of x and y and same is ψ_i ψ_i also right, but I have safe function or interpolation functions in the local coordinate system which we had developed earlier.

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$$\begin{aligned}
 u^e(x, y) &= u_1 \left[1 - \frac{\bar{x}}{a} - \frac{\bar{y}}{b} + \frac{\bar{x}\bar{y}}{ab} \right] + u_2 \left[\frac{\bar{x}}{a} - \frac{\bar{x}\bar{y}}{ab} \right] + \\
 &\quad u_3 \left[\frac{\bar{x}\bar{y}}{ab} \right] + u_4 \left[\frac{\bar{y}}{b} - \frac{\bar{x}\bar{y}}{ab} \right] \\
 &= u_1 \underbrace{\left(1 - \frac{\bar{x}}{a} \right)}_{\psi_1} \underbrace{\left(1 - \frac{\bar{y}}{b} \right)}_{\psi_2} + u_2 \underbrace{\frac{\bar{x}}{a}}_{\psi_2} \underbrace{\left(1 - \frac{\bar{y}}{b} \right)}_{\psi_2} + u_3 \underbrace{\frac{\bar{x}\bar{y}}{ab}}_{\psi_3} + u_4 \underbrace{\frac{\bar{y}}{b}}_{\psi_4} \underbrace{\left(1 - \frac{\bar{x}}{a} \right)}_{\psi_4}
 \end{aligned}$$

$$\boxed{
 \begin{aligned}
 \psi_1(\bar{x}, \bar{y}) &= \left(1 - \frac{\bar{x}}{a} \right) \left(1 - \frac{\bar{y}}{b} \right) & \psi_2 &= \frac{\bar{x}}{a} \left(1 - \frac{\bar{y}}{b} \right) & \psi_3 &= \frac{\bar{x}\bar{y}}{ab} & \psi_4 &= \frac{\bar{y}}{b} \left(1 - \frac{\bar{x}}{a} \right)
 \end{aligned}
 }$$

$$\text{OR} \quad \psi_i^e(\bar{x}, \bar{y}) = (-1)^{i+1} \left[1 - \left(\frac{\bar{x} + x_i}{a} \right) \right] \left[1 - \left(\frac{\bar{y} + y_i}{b} \right) \right] \leftarrow$$

EVALUATE ELEMENTS OF $[K]$ & $\{F\}$

- $[K]$ and $\{F\}$ — usually evaluated using numerical integration scheme. $\leftarrow$
- If $a_{11}, a_{12}, \dots, a_{nn}$ are constant, then exact integration is

See these are the interpolation functions. We had developed our interpolation functions using the local coordinate system, but my expression for S is in the global coordinate

system. So if I have to use these expressions for these approximation functions using the local coordinate system, then I have to transform dx into dx bar and I also have to change the limit is right. So this I can re write in the local coordinate system as ψ_i, x bar, y bar ψ_j, x bar, y bar, dx bar, dy bar. Why can I write straight away $d x, dy$ bar because I know the dx is equal to d bar and dy is equal to dy bar. My limit is in the local coordinates system what? So, my initial limit is so for a rectangular element if I have to integrate I have to integrate it 2 times.

So, the integration were would have happened from x_1 to x_1 plus a and y_1 to y_1 plus b and because this is the eth element I have to put superscript e everywhere. Now in the local coordinate system this limit is change. So, x_1 becomes 0 and x_1 plus a becomes a , y_1 becomes 0 and y_1 plus b becomes b . Similarly $S_{ij}^{(e)}$ I can write it as a double integral 0 to a , 0 to b .

So, now I am directly writing, the expression in local coordinates system it is ψ_i, ψ_j divided by Δx bar dx bar, dy bar, I can directly write that. Similarly $S_{ij}^{(e)}$ equals double integrals 0 to a 0 to b Δx bar Δy bar $\psi_i \psi_j dx$ bar dy bar and then $S_{11}^{(e)}$ equals Δx bar Δy bar $\psi_i \psi_j$ over Δx bar Δy bar dx bar dy bar. So, what is $S_{12}^{(e)}$ it is the first derivative ψ_i derivative of ψ_j with respect to x bar and derivative of ψ_j with respect to y bar dx bar dy .

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$$S_{ij}^{(e)} = \int_0^a \int_0^b \frac{\partial \psi_i}{\partial \bar{x}} \frac{\partial \psi_j}{\partial \bar{y}} d\bar{x} d\bar{y}$$

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$$S_{11}^{(e)} = \int_0^a \int_0^b \left(1 - \frac{\bar{x}}{a}\right)^2 d\bar{x} d\bar{y} = \frac{a}{3}$$

$$S_{12}^{(e)} = \int_0^a \int_0^b \frac{\bar{x}}{a} \left(1 - \frac{\bar{x}}{a}\right) d\bar{x} d\bar{y} = \frac{a}{6}$$

NOTE

$$\int_0^a \left(1 - \frac{\bar{x}}{a}\right) d\bar{x} = \frac{a}{2}$$

$$\int_0^a \frac{\bar{x}}{a} d\bar{x} = \frac{a}{2}$$

And I have 2 more expressions S_{21} that equals 0 to a, 0 to b and finally, S_{22} that equals partial of ψ_i with respect to y bar, partial of ψ_j with respect to y bar dx bar y bar. So, these are the formulas and my ψ_i and ψ_j the expression for those ψ are already given here ψ_1 , ψ_2 , ψ_4 . So for different ψ s i can compute all the individual terms of the S matrix. So, while we are doing this computations, we must just note some facts that when I integrate from 0 to a $1 - x$ by a square dx bar.

What i get is a by 3, an also if I integrate x bar by a into $1 - x$ bar by a dx bar I get a divided by 6, so because we will encounter these integrals. So, I can directly replace them and similarly $1 - x$ bar by a integral from 0 to a dx bar equals half of a an integral from 0 to a, x bar over a dx bar equals a over 2. So, we can use these standard mathematical facts when we are computing integral for S_{11} , S_{12} so on so forth.

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Handwritten mathematical derivations for the stiffness matrix S of a rectangular element:

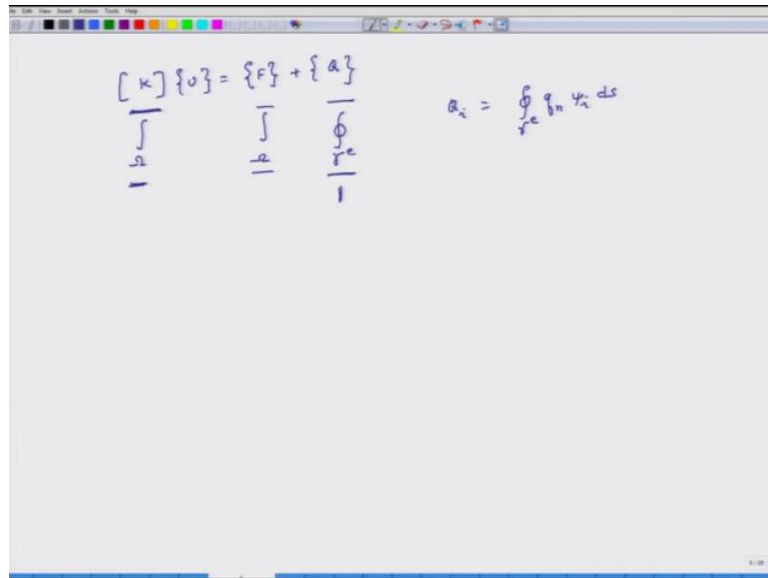
- $S^{00} = \frac{ab}{36} \begin{bmatrix} 4 & 2 & 1 & 2 \\ 2 & 4 & 2 & 1 \\ 1 & 2 & 4 & 2 \\ 2 & 1 & 2 & 4 \end{bmatrix}$
- $S^{12} = \frac{1}{4} \begin{bmatrix} 1 & 1 & -1 & -1 \\ -1 & -1 & 1 & 1 \\ -1 & -1 & 1 & 1 \\ 1 & 1 & -1 & -1 \end{bmatrix} = [S^{21}]^T$
- $S^{11} = \frac{b}{6a} \begin{bmatrix} 2 & -2 & -1 & 1 \\ -2 & 2 & 1 & 1 \\ -1 & 1 & 2 & 2 \\ 1 & -1 & -2 & 2 \end{bmatrix}$
- $S^{22} = \frac{a}{6b} \begin{bmatrix} 2 & 1 & -1 & -2 \\ 1 & 2 & -2 & -1 \\ -1 & -2 & 2 & 1 \\ -2 & -1 & 1 & 2 \end{bmatrix}$
- Force vector: $\{F\} = \frac{5ab}{4} \begin{Bmatrix} 1 \\ 1 \\ 1 \\ 1 \end{Bmatrix}$

A diagram of a rectangle with width a and height b is also shown.

So, what I will do is, I will write down expressions for S_{00} . So, S_{00} ab is ab over 36 this is S_{00} . $4 \ 2 \ 1 \ 2, 2 \ 4 \ 2 \ 1, 1 \ 2 \ 4 \ 2, 2 \ 1 \ 2 \ 4$, then S_{12} equals 1 over 4 , $1 \ 1$ minus 1 minus 1 , minus 1 minus $1 \ 1 \ 1$, minus 1 minus $1 \ 1 \ 1$, $1 \ 1$ minus 1 minus 1 , this is also equal to S_{21} transpose of S_{21} and then S_{11} equals b over $6a$ and that is 2 minus 2 minus $1 \ 1$, minus $2 \ 2 \ 1 \ 1$, minus $1 \ 1 \ 2 \ 2$, 1 minus 1 minus $2 \ 2$ and then finally, S_{22} is equal to a over $6b$, $2 \ 1$ minus 1 minus 2 , $1 \ 2$ minus 2 minus 1 , minus 1 minus $2 \ 2 \ 1$, minus 2 , minus $1 \ 1 \ 2$ and finally, the force vector.

So, here is a question, if there is an element a times b wide and force per unit area is F , then what will be these 4 values? What by $4 F$ times and what is a a b . So, it will be F $a b$ divided by 4 and these values will be 1, 1, 1, 1. So, this completes are coverage for linear 4 noded rectangle elements also. So, what we have done. So, far in these 4 lectures is that we have computed elements of K and F matrices for a triangular element and for a 4 noded rectangular element.

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$$[K]_e \{u\}_e = \{F\}_e + \{A\}_e$$

$$Q_i = \oint_{\Gamma_e} q n_i \psi_i ds$$

Now, in our finite element equation, which that is the equation at the element level the overall equation, is what? K times u equals and F vector plus there is another vector which is q vector. Elements of this matrix are calculated by a surface integral. Elements of this vector are calculated by a surface integral. So, we learned how to compute surface integrals. What we have not done what are elements of this matrix? They are computed through what through a boundary integral right because Q_i equals $Q_n \psi_i ds$, we have developed this expression earlier. So, we have learnt how to calculate learn surface integrals for in context of stiffness matrices and force vector, but we have not figured out or I am not discussed it till so far, how we calculate this term.

So, in the next 2 lectures, we will cover this term the boundary integral and that will complete our coverage of 2 dimensional finite element analyses at the element level. So, once we are comfortable at the element level then we will learn how to do assembly of

element level equations. So, that is what I look forward to talking about tomorrow and we will meet tomorrow.

Thank you.