

Finite Element Method

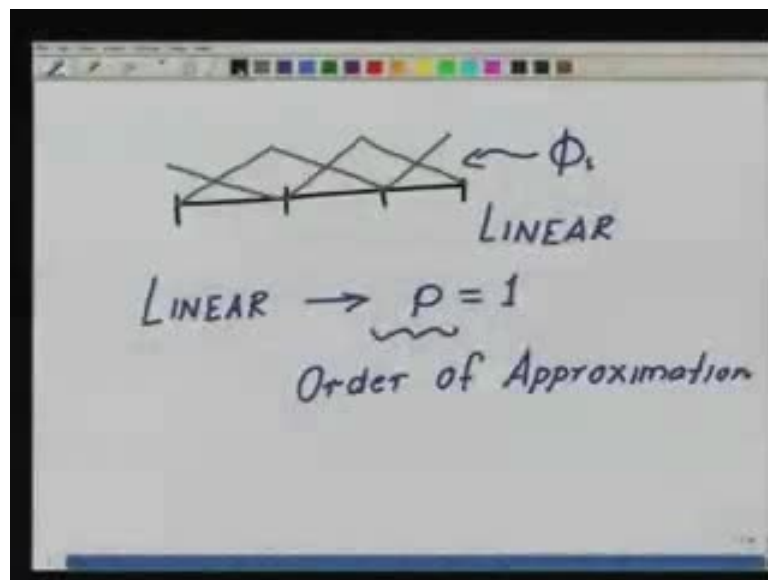
Prof. C. S. Upadhyay

Indian Institute of Technology, Kanpur

Module No. # 03

Lecture No. # 01

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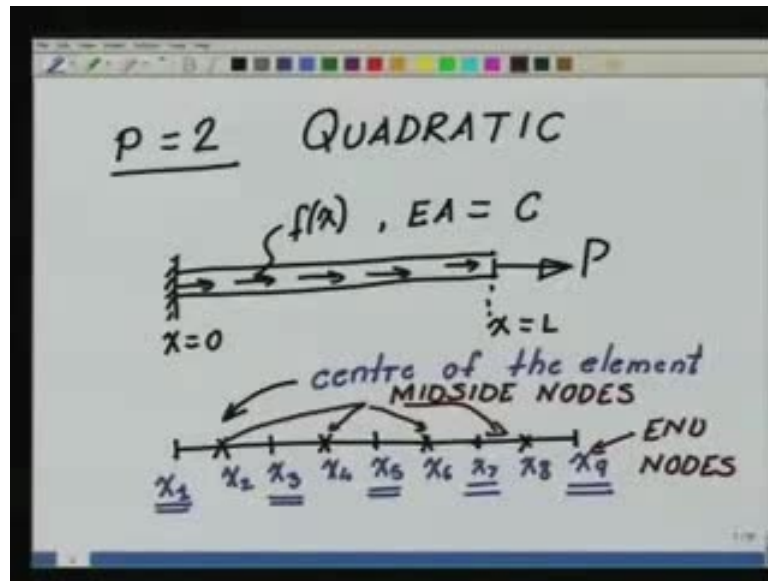


Till now, we have looked at the one-dimensional finite element problem using linear basis function. So, if you had this domain, what we have done is, we had partitioned the domain into elements, we had corresponding nodes and then called the element, we went ahead and constructed approximation using these functions ϕ_i , which are linear. Also the question - is that all we can do or can we do more than checking such linear approximation? The answer is yes. So, what today we are going to look at, is higher order approximation for the finite element solution.

So, what is the notation? Let us first introduce when it is a linear approximation, then we will represent it by $P = 1$, where P we call has the order of approximation. Now,

what we have implicitly assumed, I will assume it throughout this course, unless it is specified, specifically, that this order of approximation is the same in all the elements, that throughout the domain, we are going to use the same order of approximation; one can always use different order of approximation, in different regions of **auto mode**, that case we will not handle now.

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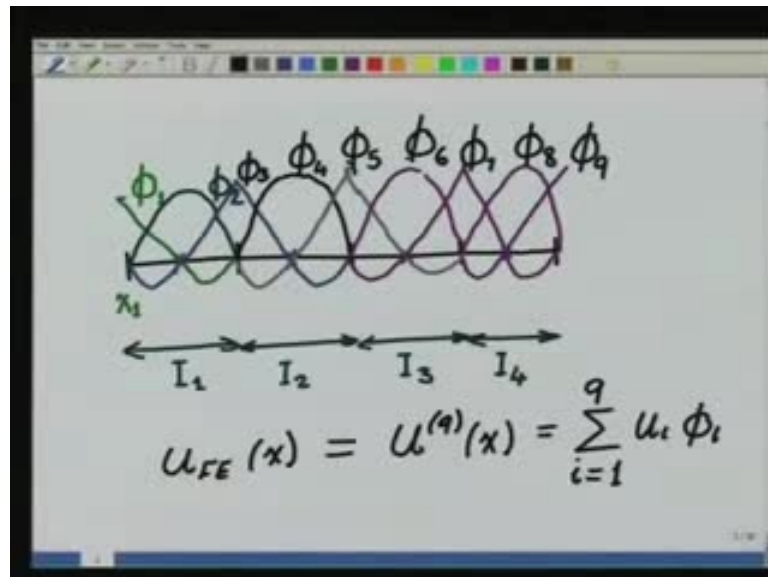
So, let us now see, how this order of approximation can be increased. So, the next example that would we have to do is, P equal 2; that is the order of approximation is quadratic. For this, let us see, what is it that we have to do, as far as the approximation is concerned. So, for this, you take the same domain that we had taken earlier, we send a load p , this is x equal to 1, this is x equal to 0 and some distributed forces $f(x)$. For $f(x)$, let us also take EA is equal to constant in the domain, that need not be true. So, using this, given this data for the problem, let us now go ahead and do the approximation. So, how are we going to do this? What we need to do now, is to first break the domain into elements as we have done till now.

Maybe I will take 4 elements here. So, these partitions that I have drawn, using these end vertical lines, these are our elements. So, this is element 1, this is element 2, this is element 3 and this element 4. So, in this element, in each of these elements, what I am

going to do is add an extra point. So, in each of the element, I am going to add an extra point. This point is located at the center of the element. So, now we are going to do this, the locations of this point. So, now, instead of having 1, 2, 3, 4, 5 points for the 4 elements that we have drawn, now we have 9 points. So, we will give them name. So, this is point x 1, this is x 2, this is point x 3, x 4, x 5, x 6, x 7, x 8, x 9.

What you should note, is that these extremities of the element are given by the point x 1, x 3; so, these are the extremities of element 1; extremities of the element 2 are the point x 3 and x 5; extremities of the elements 3 are the points x 5 and x 7; extremities of the element 4 are the point x 7 and x 9. These points x 2, x 4, x 6, x 8 are generally called mid time nodes or mid edge nodes. So, we will give a name to them; these are mid side nodes and the points x 1, x 3, x 5, x 7, x 9 are called these n vertices or simply the extremities of the elements. So, this point becomes end nodes or elements nodes or extremities of the elements. Now, what do we do next?

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So, what will do is - over this point checked that we have created, we are going to use it somehow to create our basic function, which are quadratic in nature. So, I have this point set, I am going to construct the basis function, which now should be quadratic in the elements. So, first, I am going to draw; then, we will talk about how to construct

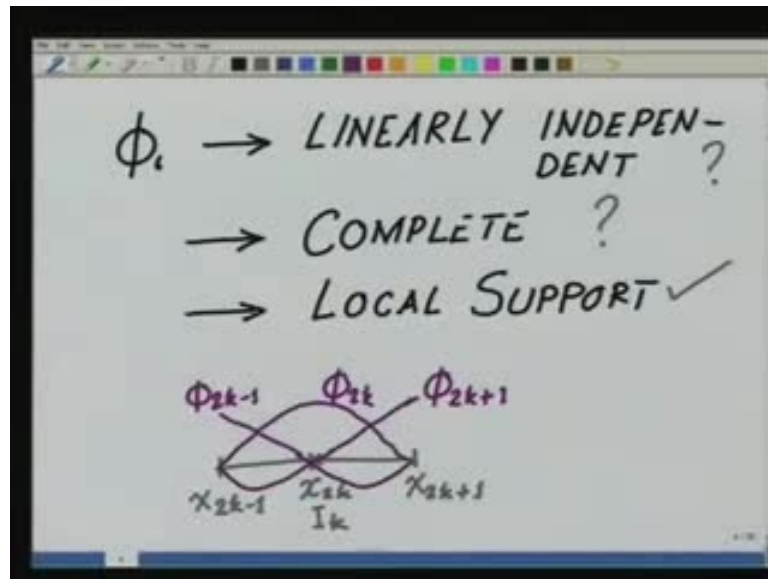
mathematically.

So, while drawing, what had we said about the linear function, what we wanted these functions to do, what should have a value 1 at one of the nodes and 0 at all other nodes; the same principle we are going to use as far as construction of the quadratic functions. So, let us say the function ϕ_1 that is corresponding to the nodes x_1 or the point x_1 . The ϕ_1 will be 1 at the point x_1 and 0 at all other points; so, if I want to make that ϕ_1 as this function. Similarly, I would like to make ϕ_2 ; ϕ_2 will be a function, which is 1 at this point and the point x_2 , and 0 at all other points. So, what we see is that we have defined it in a local region; that is, ϕ_2 is only defined in the first element.

So, if I can draw that element here, this is element I 1, this is element I 2, this is element I 3 and this is element I 4, then I can draw ϕ_3 . According, ϕ_3 should be 1 at this point and 0 everywhere else. So, by the same token that I have done ϕ_3 like this, then ϕ_4 . ϕ_4 should be 1 here, 0 at all other points ϕ_4 . Similarly, $\phi_{\phi\phi\phi}$ will be 1 here; 0 will be where are... Similarly, if I want to use, ϕ_6 will be this, ϕ_7 will be this, ϕ_8 will be this and ϕ_9 will be this.

So, what we got is ϕ_2 is here, so naming wise, this is ϕ_3 , this is my ϕ_4 , this my ϕ_5 ϕ ; sorry, I made a mistake here. So, I have to go back and change my naming convention. So, before ϕ_2 , this is going to be ϕ_3 , this column is going to be ϕ_4 , this one is ϕ_5 , this one is ϕ_6 , ϕ_7 , ϕ_8 and then ϕ_9 .

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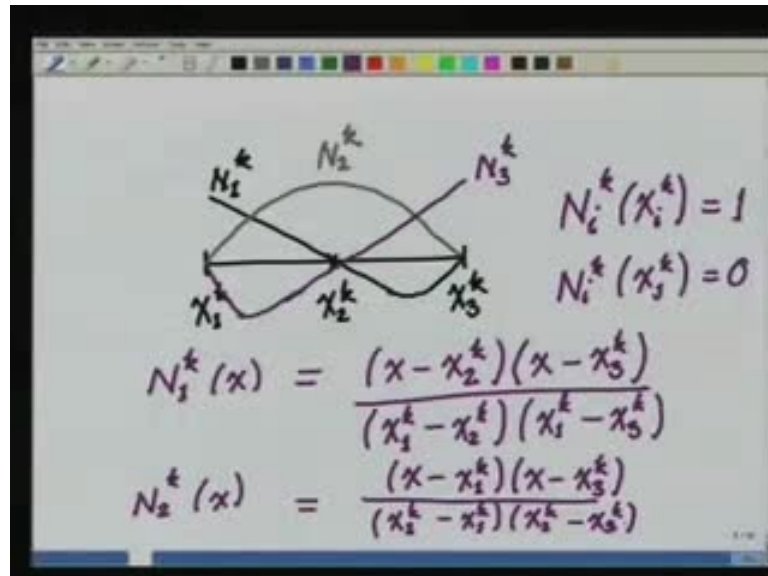
So, here, I have the 9 phi, which I have constructed; they look quadratic, we have to also give an expression to them mathematically; why are they quadratic? Because they have a value 1 at one point, and 0 at two other points, and then we extend it as 0 everywhere. So, they should be quadratic; that means they look like that. So, in some will this function, how am I going to write my 500 ml solution. So, u F E of x, we will use our earlier notation, is it is going to be, u is the 9-term solution u 9 of x. This is equal to sigma i is equal to 1 to 9 u i phi i.

So, this is a pixel optical. So, now, what is this, that the function has to satisfy in order to be admissible basis function? The first thing that we have done till now is that, this function phi i should be, it should be linearly independent; second thing that they have to satisfy is that they should be complete; and third thing that we have done by construction is they should local support, that is, they are only defined in one or two elements and in the rest of the element there, 0.

So, by construction, we see that this property has satisfied linear independence; we do not know this, we do not know. So, let us first make this function in such a way that they are quadratic, linearly independent and complete. So, how are we going to do that? So to do that, let us now consult this function element by element. So, if I look at element - a

generic element I k - if you look at the generic elements I k, what are the nodes that this elements has or the point it will be? x_1^k, x_2^k, x_3^k . Similarly, which is the phi, which is non-zero here? So, phi which are non-zero, here are phi 2 k minus 1 phi 2 k plus 1.

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So, let us now go and transform this to our element notation that we had introduced earlier. So, from the element notation point of view, in the element, I will call the first node as x_1 of an element k ; the second one, x_2 of an element k ; and the third one is x_3 of element k .

Similarly, the phi 2 k minus 1, in this element could become, would be called N_1 of element k and phi 2 k will be called N_2 of k . Similarly, phi 2 k plus 1 will be called N_3 of k . And like in the case of linear approximation, in this we want this function N_1 of k to be to have a value 1 at the point x_1 of k and 0 at all other points. N_2 of k should have a value 1 at the point x_2 of k ; at all other points, N_3 of k should have a value 1 at the point x_3 of k and 0 at all other points. So, what we can write in short is, N_i^k as the point x_i^k is equal to 1 and at all other points j it is equal to 0. Set property is what we want to have for this function. So, if we want to construct N_1^k with this property such that N_1^k is 0 at the point x_2^k and x_3^k .

So, how will I form the function N_1^k ? This should vanish at the point x_2^k , certainly, this representation should have this form, **something into is** there, then at x_2^k this expression goes to 0, it should also vanish at the point x_3^k . So, it should also have this part sitting there. You see that this expression vanishes at the point 2 and the point 3 of the element; now what else is required at the point 1? This expression should have a value 1. So, what I will do is simply divide by, what I have done in the bottom part, I have replaced x with x_1^k ; you see what has happened, this is a quadratic expression, it vanishes at the point where you wanted to vanish and it has the value 1 at the point where we want it to have a value 1.

So, by the same token, can we define N_2^k . We are defining this thing only in the element ϕ_k . This will be equal to what? Very simple; it will be x minus, it should vanish at the point 1, and 2 is going to be x minus x_1^k x minus not 1 and 2, but 1 and 3 x_3^k , and it should have a value 1 at the point x_2^k . So, it will be x_2^k minus x_1^k x_2^k minus x_3^k .

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$$N_3^k(x) = \frac{(x - x_1^k)(x - x_2^k)}{(x_3^k - x_1^k)(x_3^k - x_2^k)}$$

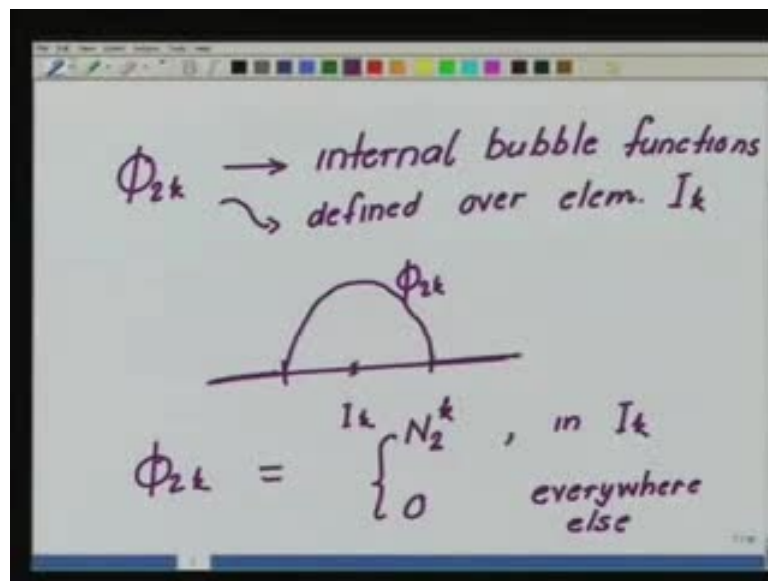
$$\phi_{2k-1}(x) = \begin{cases} N_3^{k-1}(x), & \text{in elem. } I_{k-1} \\ N_1^k(x), & \text{in } I_k \\ 0, & \text{everywhere else} \end{cases}$$

Similarly, N_3^k by the same token, can be written as x minus x_1^k into x minus x_2^k divided by x_3^k minus x_1^k into x_3^k minus x_2^k . So, we have constructed the three functions at the element level; this satisfy the three requirements we have imposed as far

as the values are concerned. Now, what do we note? That if I look at the function ϕ_{2k-1} of x , where is this function, and this **is for we** have to differentiate between the two things, this function ϕ_{2k-1} corresponds to an edge vertex, that is a node which is shared by two elements; that is, this corresponds to if k is 1, it is 1. So, it is 1, 3, 5, 7, 9 this function has to be non-zero in the two elements sharing that node. So, this will be equal to N_3 in the element $k-1$ **for** it will be N_1 in element k ; hence, it will be 0 everywhere else.

So, what you said is this function, if I talk of this node $2k-1$; this is element $k-1$; this is element k . So this, the function is given as N_3 of $k-1$, which we now know how to construct and here N_1 in k .

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So, **this** we can construct, all the global of basis function, odd ones using these $N_{I_k}(s)$ defining the element; what about the ϕ_{2k} that is the even one? So, the even one which you see are defined only in the element. So, the even one - the ϕ_{2k} is equal to 1, the number of elements, these are sometimes called internal bubble functions and they are only defined over element I_k , that is, this is my element I_k . So, this is **by** the $2k$ node and ϕ_{2k} is non-zero in this element and 0 everywhere else. So, what we know now that ϕ_{2k} is equal to by definition N_2 of element k in element I_k and 0

everywhere else.

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$$u^{(q)}(x) = \sum_{i=1}^q \underline{u_i} \underline{\phi_i(x)} \equiv 0$$
$$u^{(q)}(x_i) = 0 = u_i$$

$\phi_i(x)$ \rightarrow piecewise quadratic and linearly independent

So, **these**, now you see that when we went, we came from the linear to the quadratic. The construction has been become a little involved; nevertheless, the steps that we are going to follow will be the same, irrespective whether it is linear, quadratic, and as we will see cubic forth order or fifth order, any order that we would like to have. Now, the question is that - are these functions linearly independent? So, once I have defined these functions ϕ_i , then if you remember, we had written $u^{(q)}(x)$ is equal to $\sum_{i=1}^q u_i \phi_i(x)$. How do we check linear independence? If you remember, linear independence means that if this function is identically equal to 0, then the coefficient u_i should come out to be equal to 0, how do I show that the coefficient u_i is 0? So, **forgot**, let us see a very important property of this function; what are these ϕ_i ? If you remember this ϕ_i has a value 1 at the node with respect to all the point, **with respect to** they have been defined, and at all other points that we have put in the domain, these functions are 0.

So, if this function $u^{(q)}(x)$ has to be 0 everywhere, it has to be 0 at the point x_i also, is also equal to 0, which is equal to **from the summation**, what do we get? All other $\phi_i(s)$ will vanish, only the u_i will remain. This will be equal to u_i . So, if I do this for all the 9

nodes, we are having the domain, what do I get **that** from this condition? That u_9 is equal to 0 everywhere, we get that all the coefficient u_i are 0, which means, that the ϕ_i , **are...** this will be called piecewise quadratic; that is, in every element they are quadratic and linearly independent.

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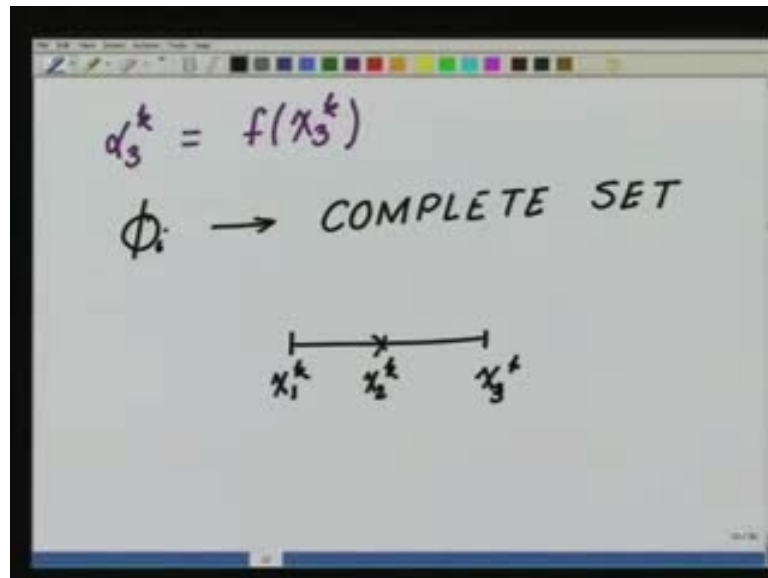
$$\begin{aligned}
 f(x) &= a_0 + a_1 x + a_2 x^2 \\
 &= \sum_{i=1}^3 \alpha_i \phi_i \\
 f(x) &= \alpha_1^k N_1^k + \alpha_2^k N_2^k + \alpha_3^k N_3^k \\
 &= \beta_0 + \beta_1 x + \beta_2 x^2 \\
 \alpha_1^k &= f(x_1^k); \quad \alpha_2^k = f(x_2^k)
 \end{aligned}$$

What about completeness? So, for the completeness - if we go, and what do we like, want to do? We would like to see, whether a function of this type, if the function f of x , this function is given as the generic quadratic a_0 plus $a_1 x$ plus $a_2 x^2$; if I have this function, then I should be able to represent it as the linear combination of a ϕ_i ; that is, I will call it as $\alpha_i \phi_i$. Now, what is this? Because, we are saying these approximating functions are piecewise quadratic for completeness, we want the series represented by these functions to exactly represent at least a quadratic polynomial, not more than that; so, either I have, if you see, this is, these are arbitrary coefficient.

So, this series has to exactly represent the constant represented by a 0 or a linear a_0 plus $a_1 x$ or a quadratic, which is a_0 plus $a_1 x$ plus $a_2 x^2$. So, if it has to do it in the whole domain, then it should also be able to represent a quadratic in an element, so in the element if **I write...** So, instead of doing **it** in the whole domain, let us do it in the element. So, in the element, if I want to write $f(x)$ it is equal to, I will call it $\alpha_1^k N_1^k$

1 of k plus α_2 of k N 2 of k plus α_3 of k N 3 of k , and this, let say that the quadratic polynomial that we have taken in the element, it is of this form β_0 plus $\beta_1 x$ plus $\beta_2 x^2$.

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Now, by the various functions have been defined, what will be the α_1 of k be? α_1 of k , where the equal to f evaluated at the point x_1 of k ; α_2 of k will be equal to f evaluated at the point x_2 of k ; α_3 of an element k will be equal to f , evaluated at the point x_3 of k . So, with this representation for the α , one should go **and** check that indeed, what we have done in the previous stage is really... I do not know, whether this is going to be like this. So, the equalities is question mark and what we can now check is that is not a question mark, but indeed this is an equality.

This is a simple algebraic exercise, and one can show that, yes, indeed just linear combination of these three functions is able to exactly use a quadratic polynomial defined in the elements and thus in the whole domain, which means that this function ϕ_i , the set of function ϕ_i **represented** in the complete set. So, this in the construction of this ϕ_i is... one has to be very careful, one cannot arbitrarily define this function ϕ_i as we wish.

Now, if you see this point x , another point we have to note is that the point x_2 of k that we have taken, x_2 of k , we have said it is at the mid side, it is not been, it could be anywhere; but as the convention, it is taken at the middle of the element always, but one should remember it need not be the case, specially when we have solve element, which we will be dealing with later on.

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Weak Form :

$$\int_{x=0}^L EA \frac{du}{dx} \frac{d\phi}{dx} dx = \int_{x=0}^L f v dx + P \sigma / L$$

$B(u, v)$ $F(v)$

ith eqn.
 $B(u^{(q)}, \phi_i) = F(\phi_i)$

Now, that we have defined the ϕ_i , what next? So, once we have defined the ϕ_i , the next thing that we have to do is to go ahead and find the coefficient u_i , in order to form the solution to the problem. So, to form the coefficient where do we start from? We start from the weak formulation, and for the problem that we have taken, the weak form is very easy, it is x is equal to 0 to L , it will be $EA \frac{du}{dx} \frac{d\phi}{dx} dx$ plus p into v evaluated at L .

Now, in weak form what do we do? We go and substitute, instead of u . So, this will be replaced by u and to form the i th equation, what we do? We replace v with ϕ_i . So, to make the notations a little bit compact, this part as we have done a few lectures ago, they are going to represent as the bi-linear form, as I said it is linear in u and v . So, it will be called as the bi-linear form given by this compact notation $b(u, v)$; and this side, this we are going to call by F of u , which is the linear function and given by the name F of u ,

because here as the number of functions increase, the algebra get tedious. So, we would like to be compact only for that reason, we are introducing these things. So, the i th equation is given as B of u ϕ_i is equal to F of ϕ_i .

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The image shows a whiteboard with the following handwritten equations:

$$B\left(\sum_{j=1}^9 u_j \phi_j, \phi_i\right) = F(\phi_i)$$

$$\Rightarrow \sum_{j=1}^9 \underbrace{B(\phi_j, \phi_i)}_{K_{ij}} u_j = F(\phi_i)$$

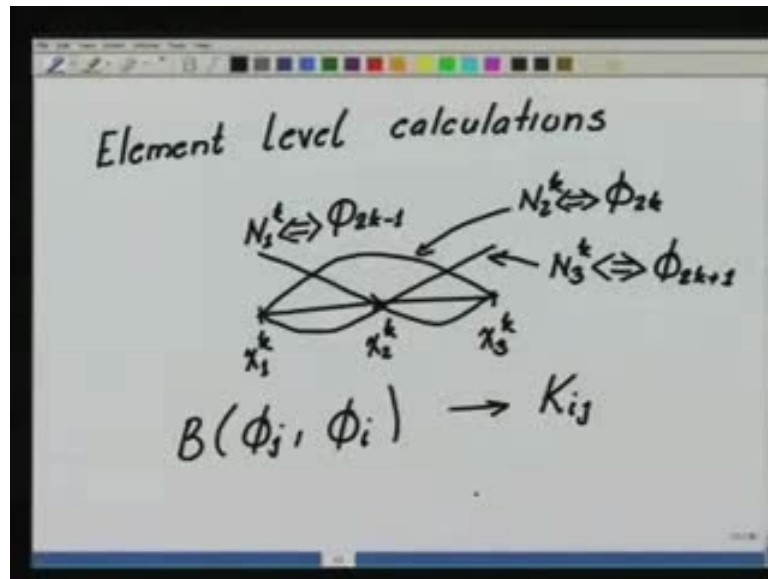
$$[K]_{9 \times 9} \{u\} = \{F\}$$

The matrix $[K]$ is underlined in red, and the vector $\{F\}$ is circled in red.

So, now if I have this, now I can expand the u 9. So, what will that be equal to? I can write it as B of sigma i is equal to 1 to 9 u_i ϕ_i - we will call it j - u_j , ϕ_i is equal to F of ϕ_i . Now, since this is bi-linear, by the definition of bi-linear functions this summation over this coefficient I can take out. So, this is equivalent to writing form of j equal to 1 to 9 b of $\phi_j \phi_i$ whole thing multiplied by u_j is equal to F of ϕ_i .

If you see for the i th equation, this becomes, this term becomes the coefficient of the j th unknown. So, what is it called? If you want to go back to what we have to done earlier, this term will be equal to k for the i th equation j th call. So, this is k_{ij} . Now, our job is... So, if this is k_{ij} , then we can write the whole problem in the form of the global stiffness matrix k into the unknown displacement vector u , where now this is k is 9 by 9, u is the vector of ϕ 9 this is equal to the vector F .

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So, our job is to find the entries of this phase and of this vector. So, if we can find anything, then we **have assemble**d to make this problem and all that we have to do is invert this matrix; first, we have to apply one-way condition, invert the matrix and solution is there. So, to do this, what do we do? We have to again go back to the element calculation; so, this is element level calculation.

Now, let me redraw the whole figures again for the element; this is x_1 of an element k , x_2 of an element k , x_3 of an element k and if you remember, so this was N_1 , N_2 , N_3 ; so, this was N_1 of an element k , which is equivalent to ϕ_{2k-1} . This is N_2 of element k , which is equivalent to ϕ_{2k} , and this one is N_3 of element k , which is equivalent to ϕ_{2k+1} in the element k . Just like we have done for the linear problem for the ϕ equal to 1 approximation, here what do we know, that the ϕ is which are non-zero in the element are these three ϕ (s), ϕ_{2k-1} , ϕ_{2k} and ϕ_{2k+1} equal to 1, 2, 3, 4 that is a number of up to the number of element.

So, what element is going to contribute to, is the $2k-1$ th equation, $2k$ th equation, and $2k+1$ th equation, and which rows of these equation are going to be non-zero, which column of these rows are going to be non-zero? The columns which are going to be non-zero for each of these rows are the $2k-1$, $2k$ and $2k+1$. So, these

columns only, the element is going to contribute, and none of the other column it is going to contribute. So, if I take that **b b**, that I had written $\phi_j \phi_i$, which is nothing but as we have said $k_i j$.

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The image shows a handwritten derivation of the element stiffness matrix. It starts with the definition of the 3×3 matrix $[K^k]$ as a block of three integrals over the element length x_1^k to x_3^k . Each integral involves the axial stiffness EA and the derivatives of the shape functions N_1^k, N_2^k, N_3^k . Below this, the general entry K_{ij}^k is defined as the integral of EA multiplied by the product of the derivatives of the shape functions N_j^k and N_i^k .

$$[K^k]_{3 \times 3} = \begin{bmatrix} \int_{x_1^k}^{x_3^k} EA \frac{dN_1^k}{dx} \frac{dN_1^k}{dx} dx & \dots & \dots \\ \int_{x_1^k}^{x_3^k} EA \frac{dN_2^k}{dx} \frac{dN_1^k}{dx} dx & \dots & \dots \\ \int_{x_1^k}^{x_3^k} EA \frac{dN_3^k}{dx} \frac{dN_1^k}{dx} dx & \dots & \dots \end{bmatrix}$$

$$K_{ij}^k = \int_{x_1^k}^{x_3^k} EA \frac{dN_j^k}{dx} \frac{dN_i^k}{dx} dx$$

Which of the i and which of the j will get contribution from the element? As we have said, i equal to $2k - 1$, i equal to $2k$ and i equal to $2k + 1$. Similarly, j is equal to $2k - 1$, j equal to $2k$ and j is equal to $2k + 1$. So, let us find **the** contribution, how we had found these contributions earlier.

So, what we are going to define now, it is for this element k . The element stiffness matrix - now what will be the size of this element stiffness matrix? Because there are now 3 $n(s)$ or 3 $\phi(s)$, which are non-zero in the element. So, it will be a 3 by 3 matrix. So, what will the entries be? I will write only of few entries of this and then it will be integral form x_1^k to x_3^k $EA \frac{dN_1^k}{dx} \frac{dN_1^k}{dx} dx$; this I will check. So, for the first row of this, **I will** $EA \frac{dN_1^k}{dx} \frac{dN_1^k}{dx} dx$ into $\frac{dN_1^k}{dx}$ will be the first column entry $EA \frac{dN_1^k}{dx} \frac{dN_1^k}{dx} dx$ into $\frac{dN_2^k}{dx}$ is the second column entry and the third will be $\frac{dN_1^k}{dx}$ into $\frac{dN_3^k}{dx}$ is the third column entry.

And similarly, if I come here to the second row, so it will be x_3^k $EA \frac{dN_2^k}{dx} \frac{dN_1^k}{dx}$

dx and so on; and the third will have integer x_1^k to x_3^k ; you see that limits of the integration are from one **extremate** of the element to next extremate of the element. So, that is should be kept in mind $\int_{x_1^k}^{x_3^k} f N_i^k dx$. Can I write the k in the element k ? This will be equal to $\int_{x_1^k}^{x_3^k} EA d N_j^k dx$.

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$$F_i^k = \int_{x_1^k}^{x_3^k} f N_i^k dx$$

Element

load vector

$$K_{ij}^k \xrightarrow{?} K_{mn}$$

$$F_i^k \xrightarrow{?} F_m$$

Similarly, F_i in the element k will be equal to nothing but $\int_{x_1^k}^{x_3^k} f N_i^k dx$; remember, that here we are not going to add the part due to the p that is going to be added, when we are applying the **(())** or the force found the condition; this is all that the F_i^k from the element will have. So, once we have this, then we have obtained the element level stiffness matrix and the element level load vector. So, this will go to the element load vector.

So, once I have these, now what we do? We have to find the correspondence between these element level entries and the global entries; that is, where in the global stiffness matrix should be this k i j go **globally? It is which m n it should go to, that is where I have to assemble these things.** Similarly, where will be the F_i at **the element go to globally, which F this equation has this information, we have to help.**

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The image shows a whiteboard with the following text:

Local to Global Numbering
or
Connectivity Information

<u>Global</u>		<u>Local (1_k)</u>
$2(k-1) + 1$	\longleftrightarrow	1
$2(k-1) + 2$	\longleftrightarrow	2
$2(k-1) + 3$	\longleftrightarrow	3

So, what has been done earlier, as far as this information is concerned, we had created a local to global numbering or 90 times it is called the connectivity information. So, this connectivity information has to be constructed. So, let us now do it for the elements. So, what I will do is, here I write the global number, and here, I will write the corresponding local number for the element k . So, this is the local number K in the element; I have how many? 1, 2, 3; this global number, does it correspond to 1? Corresponds to which global basis function? N_{1k} corresponds to ϕ_{2k-1} . So, it should correspond to globally. I will re-write it in another form, $2k - 1 + 1$ which is nothing but $2k - 1$.

This one will be N_{2k} corresponds to ϕ_{2k} globally; so, it will be **as...** rewrite as this plus 2; similarly, N_{3k} will corresponds to ϕ_{2k+1} . So, remember what we have done. So, before we go and do the element calculation, we will stretch the entries of the global stiffness matrix and the global load vector equal to 0.

The process of the assembly that we had talked about in great detail, in the previous lecture, essentially is adding the elemental contributions to this global stiffness matrix and the global load vector, in order to complete the global equation, because what we have said, is integration over the full domain can be partitioned into the integration over

the elements, and when we add these elemental integrals together, we get the global representation.

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$$K_{2(k-1)+i, 2(k-1)+j} = K_{2(k-1)+i, 2(k-1)+j} + K_{ij}^k$$

$i, j = 1, 2, 3$

$$F_{2(k-1)+i} = F_{2(k-1)+i} + F_i^k$$

ASSEMBLY

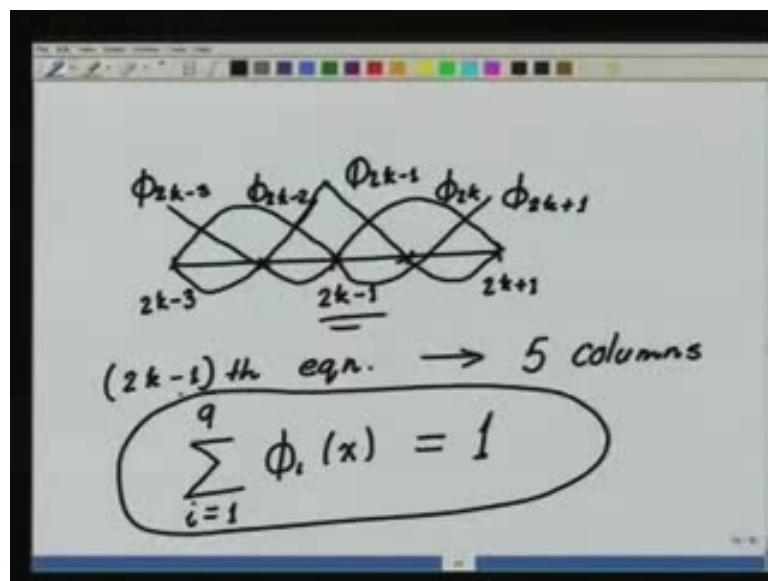
So, the global entry which is going to get contribution from element are going to be: $2k - 1 + i$, $2k - 1 + j$ is equal to... what we are going to do? It is to the original number, which was sitting there, I am going to add k i j . So, what has happened to the global stiffness entry $2k - 1 + i$, $2k - 1 + j$? I am going to add the elemental i j th. So, this is the part, as the assembly part, as far as the stiffness is concerned and this for i, j is equal to 1, 2, 3. Similarly, the $F_{2k - 1 + i}$ will be equal to $F_{2k - 1 + i}$, to this I am going to add F_i^k . So, this is the assembly procedure.

So, we have obtained the element calculation, using the function which we have defined the elemental level, and assemble them to get the global **equation, in terms** of the basis function that we are after, the coefficient for the global basis function. One should remember, that in any finite element approximation, we are really looking for the coefficients of the global basis function, and the element calculation, is a simple way of doing the integration, **relevant that have to be done**, to obtain the entries of the global stiffness matrix and **the global load vector by doing at the element level**, adding it up to

get the global equation.

One question that should come to mind now is - earlier, we have seen for P equal to 1, that the i th equation had only non-zero entries corresponding to the i minus 1 column, the i th column and the i plus 1 th column; in this case, what are the non-zero entries for the i th row?

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So, let us check; now take the i th row; I will take this one as the $2k$ minus 1 th point. So, this is $2k$ minus 3. Here we have to differentiate between this nodal function and the internal bubble function. So, let us take the nodal function that we have. So, if you see that I am talking on the equation corresponding to this one. So, I am corresponding to the equation corresponding to this function which is ϕ_{2k-1} .

This is the phi that we are going to contribute to the equation corresponding to this. Certainly, it is going to be this phi, it is going to be this phi and this phi. So, this is going to be ϕ_{2k-3} , this is ϕ_{2k-2} , this is ϕ_{2k} and this is ϕ_{2k+1} . What can you see? That for the $2k$ minus 1 th equation will have non-zero entries corresponding to the $2k$ minus 3 column $2k$ minus 2 column $2k$ minus 1 column $2k$ column and $2k$ plus 1 column. So, how many columns will be non-zero? 1, 2, 3, 4, 5; so

five columns will have at least, not at least, at most five columns will have non-zero entries; for all other ϕ_i the column entries are going to be 0, and because all other ϕ_i are going to disappear or become 0 in the region, where this ϕ_{2k-1} is defined to be.

You see that if **right** global stiffness matrix, the number of non-zero entries has increased in a row. This is the another property of these approximation that we have going to see and how they reflect in terms of the **part city** of the global stiffness matrix and that also this **part city**, we are talking about, we have talk about solver. So, this we will tackle at a later date. See, there is the very curious thing about this function ϕ_k ; this function ϕ_k , if you add them up anywhere, you see their value is equal to 1; why is it so?

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The image shows a whiteboard with the following handwritten content:

$$f(x) \equiv 1 = \sum_{i=1}^9 u_i \phi_i$$

$$f(x_i) = 1 = u_i$$

$$\sum_{i=1}^3 N_i^k = 1 \Rightarrow \sum_{i=1}^3 \frac{dN_i^k}{dx} = 0$$

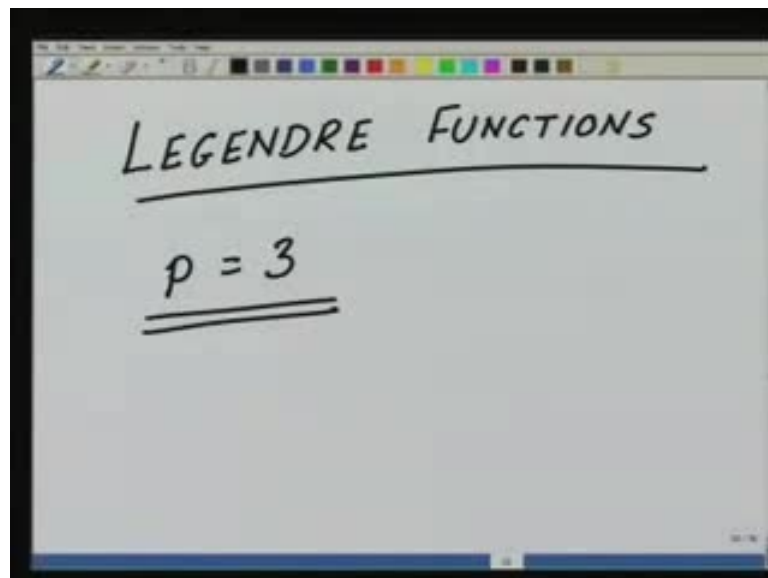
Below the equations, there are handwritten labels: "element shape functions" and "Lagrangian shape/basis functions".

Remember, we had said that these functions ϕ_k should be able to exactly represent any polynomial up to a quadratic. So, a constant is also global polynomial, which should be represented exactly, and in constant I will take my function $f(x)$, which I want to represent to be 1. This will be equal to $\sum u_i \phi_i$. Now, is this function is equal to 1 everywhere in the domain? It has to be 1 at the points x_1, x_2, x_3, x_9 . So, if I go to the point x_i , this is still equal to 1, but then this will be equal to u_i , which tells me that the u_i here on the right hand side are all equal to 1 is the u_i are all **1**, then what we get is some

of the ϕ_i is equal to 1 and this is also true in the element; same thing applies in the element. So, in the element, some of the shape function will be ϕ_i is equal to 1 to 3 is equal to 1; this is a property is that we should keep in mind, and what it also tells us that it implies, that if I do this summation, this has to be equal to 0, because this sum is equal to constant that delivered the constant is 0; these are certain things, which we should have in mind. So that when we go and write the computer program to do the finite element analysis, we can check all function, these basis functions of the element shape functions that we have called, which have N_i is are nothing but the element shape function, we can check whether they have been correctly program or not.

The definition of this element shape function that we have used, this definition is called Lagrangian shape or basis function; we will see how to generalize these, to go for a **keys** order approximation in future.

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So, this Lagrangian basis functions that we have constructed, are note, the only one that we can have. So, those who are interested, there is also a very popular family of shape functions **that are** basis function, that can be used is Legendre function, but we are not going to discuss it, here in this analysis.

In the next class, what we are going to do is, we are going to look at the cubic approximation, the P equal to 3 approximation, also construct basis function, how to do the elemental calculation, how to go for the load vector and from there we will generalize to the P for the approximation. And once you have done the P for the approximation, then we can do a finite element computation using any order of approximation in the domain.

After that, we will see how they are going to benefit us; just doing them is not enough, why we should do them, how they are going to benefit us is going to be in the future lecture.

Thank you.