

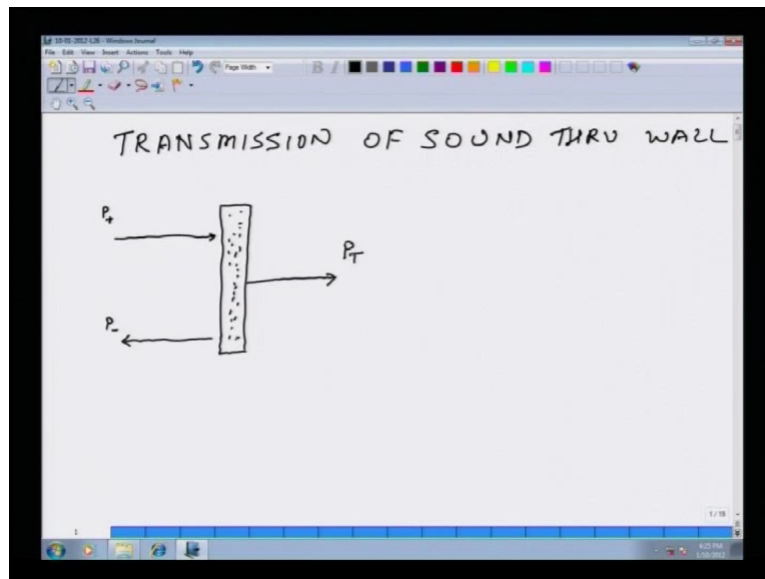
Acoustics
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Lecture 01
Module 3
Sound Transmission through Walls

Hello again. In today's lecture we will be using some of the concepts which we have developed in previous lectures specifically the transmission line theory and use this approach to figure out what happens when sound as it propagates through medium it hits a wall, how does sound get transmitted across a wall? And to solve this problem we will use the transmission line theory. So what we will analyze is first transmission of sound through a wall when the incident angle of the sound as it hits the wall is 90 degrees.

That is the first problem we will solve and then subsequently what happens if it is hitting at all sorts of random angles and then using this approach we will figure out how sound gets transmitted across a wall. So that is what we are going to do today. So I will make a very simple picture. Let us say I have a wall and the sound is hitting the wall at an incident angle which is 90 degrees so it is normal incidence.

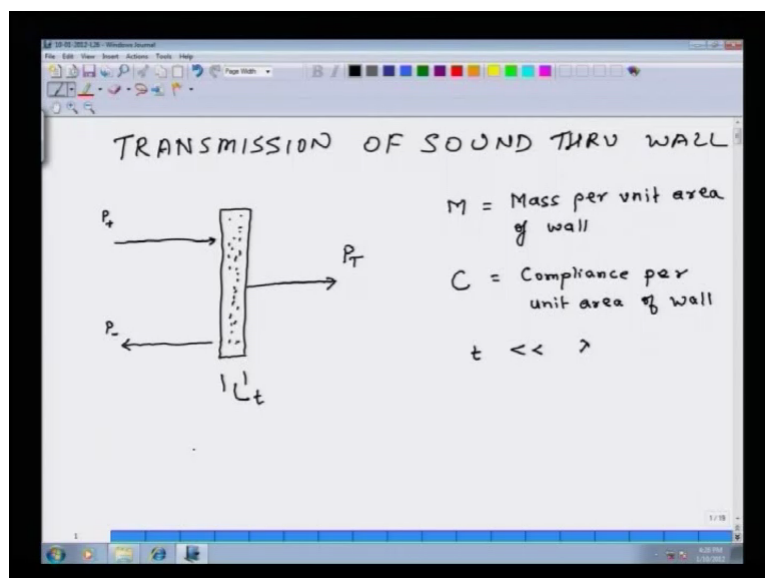
So this is my incident wave and that is my reflected wave. So the complex magnitude of incident wave is P_{plus} , of reflected wave is P_{minus} and then this is the wall in question. And a part of this sound gets transmitted to the other side and let us say the complex amplitude of this wave is P_T .

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Let us also assume that M is equal to mass per unit area of wall. So, 1 square metre of this is going to be M kilograms. And this wall could also have some compliance because when something hits a wall these walls may bend. They are not perfectly rigid so they may have some compliance. And C is the compliance. But again it is per unit area and this thickness is t and we assume that the thickness of the wall is fairly small compared to the wavelength or wavelength of the sound which is hitting the wall. So it is extremely small compared to λ .

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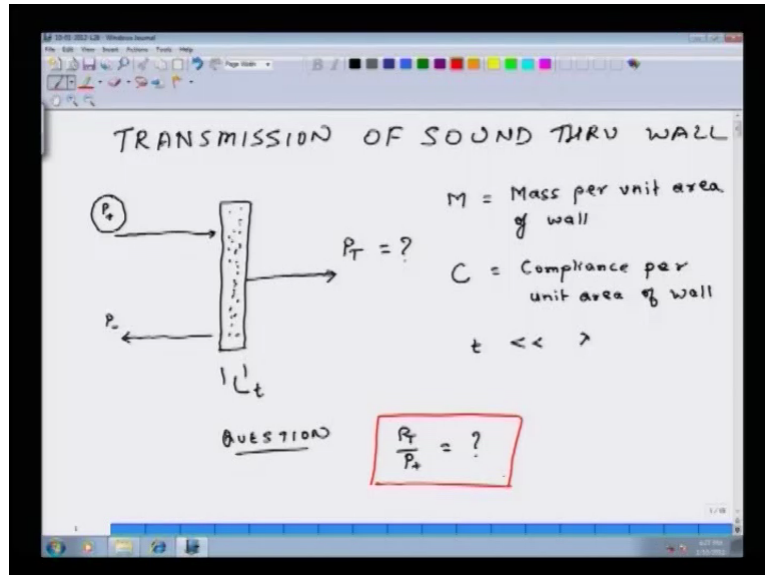


So this is the problem formulation and what we are interested in knowing is, so question, if the question is that if I know P_i plus then what is the value of P_T ?

Because P_i is the incident energy going into the system and P_T is something which is coming out by

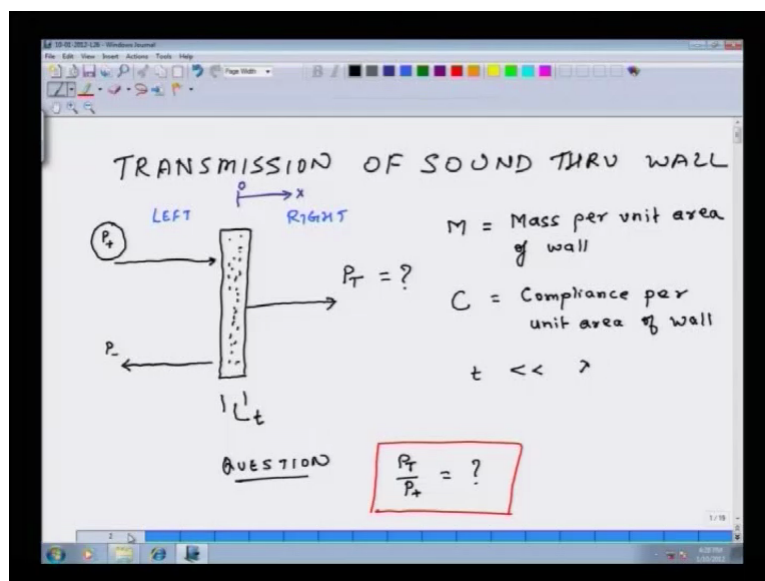
on the wall. So I want to figure out the value of this transfer function P_T over P_i and this is what we are interested in finding out, okay.

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So once again we will start with the transmission line equations. So for the transmission line equations we will write two sets of transmission line equations. So this is the left side of the wall and this is the right side of the wall. So I will have one set of transmission line equations for the left side, another set of transmission line equations for the right side. Also what I am going to do is I am going to establish my coordinate system. So this is 0. So wall stands at the location x equals 0. So with this now I am going to write my transmission line equations.

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So for left side, pressure and velocity and they are functions of space and time and this is equal to P plus P minus P plus over Z_0 minus P minus over Z_0 . So this matrix is going to be multiplied by this vector $e^{-sx/c}$ and $e^{+sx/c}$ times e^{st} and we know that $s = j\omega$. So this is my first question. And then I have likewise equations for the right side.

So on the right side let us say I call pressure as P_2 and velocity as U_2 . So P_2 now when we see this problem here is no reflected waves because I am assuming that there is no reflecting surface on the right side of the wall. So there is no reflected wave on the right side of the wall. So my P plus will be same as P_T . And since there is no reflected component this element of the matrix is 0 so again I have a 0. This is my second equation. So I have now two sets of equations, one for the left side and one for the right side.

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The image shows two equations written on a whiteboard. The first equation is labeled 'LEFT SIDE' and shows a vector of pressure $P_1(x, t)$ and velocity $U_1(x, t)$ equal to a matrix of P_+ , P_- , P_+/Z_0 , and $-P_-/Z_0$ multiplied by a vector of $e^{-sx/c}$ and $e^{+sx/c}$, all multiplied by e^{st} with $s = j\omega$. The second equation is labeled 'RIGHT SIDE' and shows a vector of pressure $P_2(x, t)$ and velocity $U_2(x, t)$ equal to a matrix of P_T , 0, P_T/Z_0 , and 0 multiplied by a vector of $e^{-sx/c}$ and $e^{+sx/c}$, all multiplied by e^{st} .

Now at this point of time I start imposing the boundary conditions, okay. So my first boundary condition is that whatever is the velocity on this side at $x=0$ that velocity is same on just the right side of the wall again at location x is equal to 0. So boundary condition is that U_1 at 0 equals U_2 at 0 and what that gives me if I substitute in equations 1 and 2 the relations for velocity and I put $x=0$.

So from first set of equations I get $U_1 = 0 = P_+ - P_- / Z_0$ and this is equal to $U_2 = 0 = P_T / Z_0$ and that is equal to P_T / Z_0 times e^{st} because s is identically 0. So these terms sx/c and $minus sx/c$ they vanish and they become 1. So now what I do is I equate these two terms and what I get finally is $P_+ - P_- = P_T$. So this is let us call a consequence of this boundary condition that at $x=0$ the velocity on right side of the wall is same as velocity on the left side of the wall.

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LEFT SIDE

$$-\begin{Bmatrix} P_1(x,t) \\ v_1(x,t) \end{Bmatrix} = \begin{bmatrix} P_+ & P_- \\ \frac{P_+}{Z_0} & -\frac{P_-}{Z_0} \end{bmatrix} \begin{Bmatrix} e^{-sx/c} \\ e^{+sx/c} \end{Bmatrix} \cdot e^{st} \quad s = j\omega \quad (1)$$

RIGHT SIDE

$$-\begin{Bmatrix} P_2(x,t) \\ v_2(x,t) \end{Bmatrix} = \begin{bmatrix} P_T & 0 \\ \frac{P_T}{Z_0} & 0 \end{bmatrix} \begin{Bmatrix} e^{-sx/c} \\ e^{-sx/c} \end{Bmatrix} \cdot e^{st} \quad (2)$$

BC $v_1(0,t) = v_2(0,t)$

$$v_1(0,t) = \frac{(P_+ - P_-)}{Z_0} e^{st} = v_2(0,t) = \frac{P_T}{Z_0} e^{st}$$

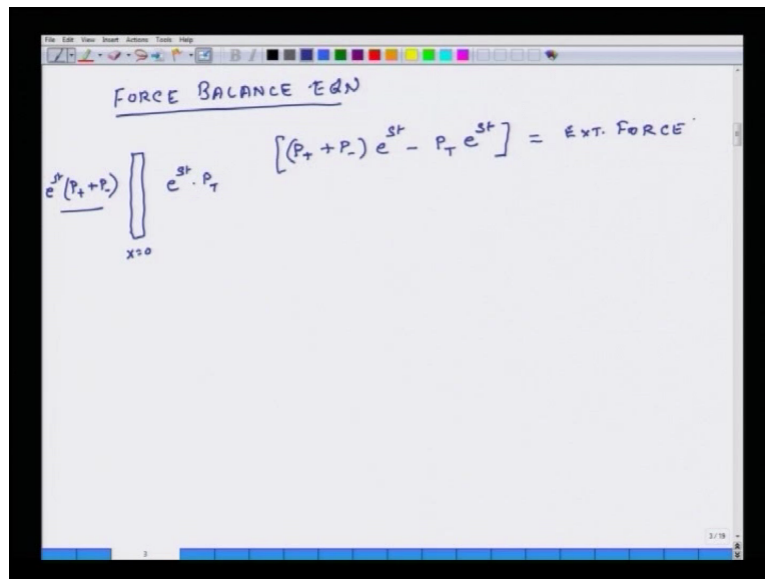
$$(P_+ - P_-) = P_T \quad (3)$$

The other condition at this $x=0$ location is that the wall is experiencing a force. It is experiencing a force and this external force is essentially the difference of pressures on left side and right side. So this is the overall external force which the wall is experiencing and this force will be equal to the acceleration of the wall times mass plus stiffness of the system times the displacement. So now I am going to develop an equation for force balance.

So this is my wall and on the left side my total pressure is P_+ plus P_- times e^{st} of course at $x=0$ and how I get this?

Essentially what I am doing is I am in equation 1 putting $x=0$ and I am finding the value of pressure. So on the left side the pressure is this and then on the right side pressure is set to the power of st times P_T . So my force balance equation is P_+ plus P_- times the power of st , this is the force on left side minus P_T times the power of st . So this is the overall external force.

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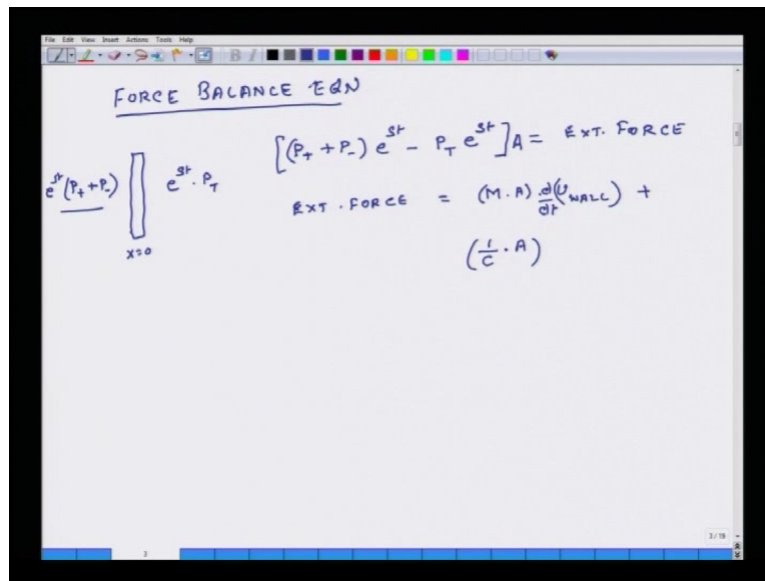


And then this external force we know if we draw a free body diagram of this system is equal to mass times acceleration. So what is the mass of the overall mass?

So excuse me this is a difference of pressures and I have to multiply this by the area of the wall which is A . So this is the external force and this is equal to the mass times acceleration of the wall plus stiffness times displacement of the wall.

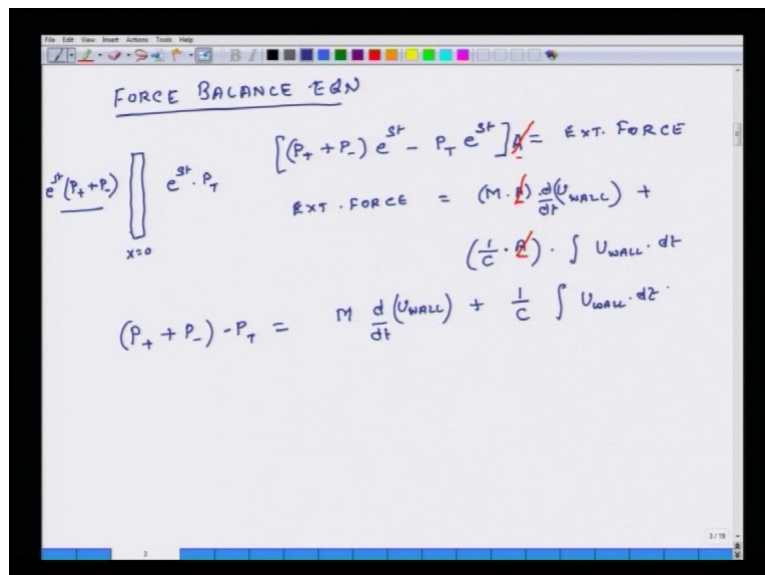
So mass is M times area. This is mass times acceleration and if I know the velocity of the wall which is let us say U_{wall} then if I take a differential of this then that is the acceleration of the wall. So this is mass times acceleration plus stiffness. And stiffness of the wall is essentially 1 over compliance times area. So C is specific compliance and then I am going to multiply this by area because it is compliance per unit area.

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And this time again if I know the velocity of the wall and if I integrate that velocity then that is what I get a displacement. So I am going to integrate over $dt U_{wall}$. and I see that area is common on left side and a right side so I can eliminate it. So my overall equation becomes so I have to make a correction here. This should have been integral of U_{wall} with respect to time. So I will make that correction here as well.

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Now in this equation I am also going to put a negative sign and the reason I am going to put this negative sign is because if I have a positive pressure then the pressure is actually moving in the negative direction. It always acts in reverse. A positive pressure acts in reverse. So to account for that reality I have to put a negative sign here. So this is my equation of motion, okay.

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FORCE BALANCE EDN

$$\int_{x=0}^{st} (P_+ + P_-) e^{st} \cdot P_T$$

$$[(P_+ + P_-) e^{st} - P_T e^{st}] = \text{EXT. FORCE}$$

$$\text{EXT. FORCE} = (M \cdot A) \cdot \frac{d(U_{WALL})}{dt} + (\frac{1}{C} \cdot A) \cdot \int U_{WALL} \cdot dt$$

$$(P_+ + P_-) - P_T = - \left[M \frac{d(U_{WALL})}{dt} + \frac{1}{C} \int U_{WALL} \cdot dt \right]$$

EDN OF MOTION FOR WALL.

Now what we are going to do is on the right side of this equation I have U_{wall} . So I will find a relationship for U_{wall} plug into this and then do some more mathematical manipulation. So we know that U_{wall} is equal to U_2 at x is equal to 0. And if I see this relation for U_2 then I know that U_2 is nothing but U_2 equals P_T over Z_0 times e^{st} to the power of m minus s over C times e^{st} .

And if I put x equals 0 then I get U_2 as, and because s is $j\omega$ what I get is this relation because s equals $j\omega$. So what I am going to do is replace this term and this term by this term because that is the value of U_{wall} .

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FORCE BALANCE EDN

$$\left[(P_+ + P_-) e^{st} - P_T e^{st} \right] A = \text{EXT. FORCE}$$

$$\text{EXT. FORCE} = (M \cdot A) \cdot \frac{d(U_{WALL})}{dt} + \left(\frac{1}{C} \cdot A \right) \cdot \int U_{WALL} \cdot dz$$

$$(P_+ + P_-) - P_T = - \left[M \frac{d(U_{WALL})}{dt} + \frac{1}{C} \int U_{WALL} dz \right]$$

EDN OF MOTION FOR WALL.

$$U_{WALL} = U_2(x, t) |_{x=0} = \frac{P_T}{Z_0} e^{st} = \frac{P_T}{Z_0} e^{j\omega t} \because s = j\omega$$

So what I get finally is plus the compliance term. So in this relation P_T and Z_0 they are constants. P_T can be a complex entity but it is still a constant. So then I can very easily differentiate this term and I can very easily integrate this term. And that is what I do in the next step.

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FORCE BALANCE EDN

$$\left[(P_+ + P_-) e^{st} - P_T e^{st} \right] A = \text{EXT. FORCE}$$

$$\text{EXT. FORCE} = (M \cdot A) \cdot \frac{d(U_{WALL})}{dt} + \left(\frac{1}{C} \cdot A \right) \cdot \int U_{WALL} \cdot dz$$

$$(P_+ + P_-) - P_T = - \left[M \frac{d(U_{WALL})}{dt} + \frac{1}{C} \int U_{WALL} dz \right]$$

EDN OF MOTION FOR WALL.

$$U_{WALL} = U_2(x, t) |_{x=0} = \frac{P_T}{Z_0} e^{st} = \frac{P_T}{Z_0} e^{j\omega t} \because s = j\omega$$

$$(P_+ + P_-) - P_T = - \left\{ M \frac{d}{dt} \left[\left(\frac{P_T}{Z_0} \right) e^{j\omega t} \right] + \frac{1}{C} \int \left(\frac{P_T}{Z_0} e^{j\omega t} \right) \cdot dz \right\}$$

So after integrating and differentiating these terms what I ultimately end up getting is. So I omitted one thing here that I had an e there. So I should have e there and I will replace this e in this relation by $j\omega e$.

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FORCE BALANCE EDN

$$e^{st} (P_+ + P_-) - P_T = \text{EXT. FORCE}$$

$$\text{EXT. FORCE} = (M \cdot \frac{d}{dt} U_{\text{WALL}}) + (\frac{1}{C} \cdot \int U_{\text{WALL}} \cdot dz)$$

$$e^{st} (P_+ + P_-) - P_T = - \left[M \frac{d}{dt} (U_{\text{WALL}}) + \frac{1}{C} \int U_{\text{WALL}} \cdot dz \right]$$

EQN OF MOTION FOR WALL.

$$U_{\text{WALL}} = U_2(x, t)|_{x=0} = \frac{P_T}{Z_0} e^{st} = \frac{P_T}{Z_0} e^{j\omega t} \quad \because s = j\omega$$

$$e^{st} (P_+ + P_-) - P_T = - \left\{ M \frac{d}{dt} \left(\frac{P_T}{Z_0} e^{j\omega t} \right) + \frac{1}{C} \int \left(\frac{P_T}{Z_0} e^{j\omega t} \right) \cdot dz \right\}$$

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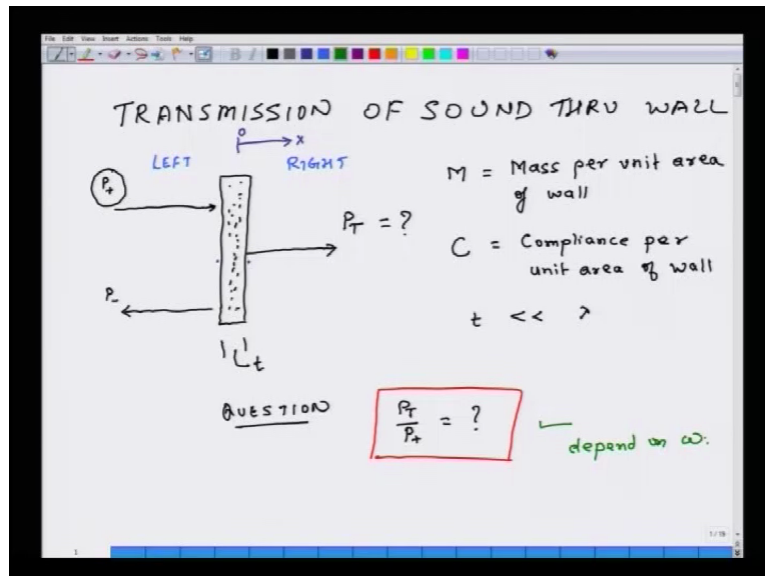
$$\left[(P_+ + P_-) - P_T \right] e^{j\omega t} = - \left[\frac{M P_T}{Z_0} j\omega e^{j\omega t} + \frac{1}{C Z_0} P_T e^{j\omega t} \right]$$

$$(P_+ + P_- - P_T) = - \frac{P_T}{Z_0} \left[jM\omega + \frac{1}{j\omega C} \right] \quad (4)$$

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So between equation 3 and equation 4 I have three unknowns, one is P_+ , the other one is P_- and the third one is P_T . These are constants but they are unknowns. I know what is M , I know what is ω and I know what is C which is the specific compliance. So then using these two equations, this equation and this equation, I will like to solve. I get my transfer function which is this. And please bear in mind that this transfer function will depend on ω .

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So with that intention what I do is I reframe this equation in such a way that I can rewrite this equation as P_- minus equals, so I take P_- minus on the right side same as P_+ minus P_T and I call this equation 3A.

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LEFT SIDE

$$-\begin{Bmatrix} P_1(x,t) \\ V_1(x,t) \end{Bmatrix} = \begin{bmatrix} P_+ & P_- \\ \frac{P_+}{Z_0} & -\frac{P_-}{Z_0} \end{bmatrix} \begin{Bmatrix} e^{-sx/c} \\ e^{+sx/c} \end{Bmatrix} \cdot e^{st} \quad s = j\omega \quad (1)$$

RIGHT SIDE

$$-\begin{Bmatrix} P_2(x,t) \\ V_2(x,t) \end{Bmatrix} = \begin{bmatrix} P_T & 0 \\ \frac{P_T}{Z_0} & 0 \end{bmatrix} \begin{Bmatrix} e^{-sx/c} \\ e^{+sx/c} \end{Bmatrix} \cdot e^{st} \quad (2)$$

BC $V_1(0,t) = V_2(0,t)$

$$V_1(0,t) = \frac{(P_+ - P_-)}{Z_0} e^{st} = V_2(0,t) = \frac{P_T}{Z_0} e^{st}$$

$(P_+ - P_-) = P_T$ (3)

$\rightarrow P_- = P_+ - P_T \rightarrow (3A)$

Now I put this equation 3A in equation 4. So I replace here P minus by P plus minus P T and let us see what we get. So, P plus plus P plus minus P T. This is what P minus equals minus P T equals minus P T over Z 0 j omega plus 1 over j omega C. And let us call this function for actually let us call this function capital D. So with this what we get is this is equal to minus P T over Z 0 times D where D is this whole term in brackets, okay.

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$$\left[(P_+ + P_-) - P_T \right] e^{j\omega t} = - \left[\frac{P_T}{Z_0} j\omega e^{j\omega t} + \frac{1}{C j\omega} \left(\frac{P_T}{Z_0} \right) e^{j\omega t} \right]$$

$(P_+ + P_- - P_T) = - \frac{P_T}{Z_0} \left[jM\omega + \frac{1}{j\omega C} \right] \quad (4)$

$$P_+ + (P_+ - P_T) - P_T = - \frac{P_T}{Z_0} \underbrace{\left[jM\omega + \frac{1}{j\omega C} \right]}_D = - \frac{P_T}{Z_0} \cdot D$$

So now I simplify this so I get on the left side 2 P plus minus 2 P T is equal to minus P T over Z 0 times D or if I move this on this side I get 2 P plus equals 2 P T minus P T over Z 0 and that is same as P T 2 minus, so I missed the D here, D over Z 0. So with this I can write P T over P plus is nothing but 2 over 2 minus D over Z 0. This is

my relation for this question where D equals $jM\omega + 1/j\omega C$ where C is specific compliance, okay. So let us call this equation 5.

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$$\left[(P_+ + P_-) - P_T \right] e^{j\omega t} = - \left[M \frac{P_T}{Z_0} j\omega e^{j\omega t} + \frac{1}{Cj\omega} \left(\frac{P_T}{Z_0} \right) e^{j\omega t} \right]$$

$$(P_+ + P_- - P_T) = - \frac{P_T}{Z_0} \left[jM\omega + \frac{1}{j\omega C} \right] \quad (4)$$

$$P_+ + (P_+ - P_T) - P_T = - \frac{P_T}{Z_0} \left[jM\omega + \frac{1}{j\omega C} \right] = - \frac{P_T}{Z_0} \cdot D$$

$$2P_+ - 2P_T = - \frac{P_T}{Z_0} \cdot D$$

$$2P_+ = 2P_T - \frac{P_T}{Z_0} \cdot D = P_T \left[2 - \frac{D}{Z_0} \right]$$

$$\frac{P_T}{P_+} = \frac{2}{2 - \frac{D}{Z_0}} \quad (5) \quad \text{where } D = jM\omega + \frac{1}{j\omega C}$$

So now I am going to pan this further. So I get P_T over P_+ plus equal 2 minus, and I am going to replace D by his whole relation, so what I am going to get is, so this is equation 6. So this is my transfer function and this transfer function it depends on ω . Its value changes with ω or the angle of frequency of the sound wave which is striking the wall.

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$$\frac{P_T}{P_+} = \frac{2}{2 - \left[\frac{jM\omega + 1/j\omega C}{Z_0} \right]} \quad (6)$$

So using relation 6 I can calculate what will be the value of P_T if an incident wave of strength P_+ is hitting it?

So now what I am going to do is now I am going to do some further processing on this relation and based on what frequencies we are talking about. So what we see from this relation is that this term $Mj\omega + 1/Cj\omega$. So this I can approximate as $Mj\omega$ for all ω or just to make it simpler, for ω which is large compared to $1/CM$.

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$$\frac{P_T}{P_s} = \frac{2}{2 - \left[\frac{Mj\omega + 1/Cj\omega}{z_0} \right]} \quad (6)$$

$$Mj\omega + \frac{1}{Cj\omega} \approx Mj\omega \quad \text{for} \quad \omega \gg \frac{1}{CM}$$

So if ω is extremely large and by large I mean it is extremely large compared to the natural frequencies of the system then this term approximates to $Mj\omega$. This range is called mass controlled region. Similarly $Mj\omega + 1/Cj\omega$, it approximates to $1/j\omega C$ for ω which is extremely small compared to natural frequency of the system that is $1/\sqrt{CM}$. And this range of frequencies is called stiffness controlled region.

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The image shows a whiteboard with the following content:

$$\frac{P_T}{P_r} = \frac{2}{2 - \left[\frac{Mj\omega + 1/cj\omega}{z_0} \right]} \quad (6)$$

$(Mj\omega + \frac{1}{cj\omega}) \approx Mj\omega$ for $\omega \gg \frac{1}{\sqrt{GM}}$
 MASS CONTROLLED REGION

$(Mj\omega + \frac{1}{cj\omega}) \approx \frac{1}{j\omega c}$ for $\omega \ll \frac{1}{\sqrt{GM}}$
 STIFFNESS CONTROLLED REGION

So we will try to understand how this function works?

This function works, this is equation 6, in stiffness controlled region and also in mass controlled region. Now once again to recap, if frequency is extremely small compared to the natural frequency of the system which is $1/\sqrt{GM}$ then that range of frequencies where it is extremely small to the natural frequency is called stiffness controlled region.

If the frequency we are (ta) considering is extremely large compared to natural frequency of the system then that range of frequencies is supposed to lie in mass controlled region because the mass term dominates the response of the system. So we will look at stiffness controlled. So again I will write down the relation P_T/P_r plus equals $2/2 -$. And we know that in the stiffness controlled region I can omit $Mj\omega$ and I have to just include $1/j\omega c$.

So what I get is $1/2Z_0 c j\omega$. So I can simplify this. So there is j in the denominator of this term so I can simplify this by moving j upwards but also eliminating the negative sign. What I am doing is that in this term I am multiplying this and also dividing this term by j . So what I am getting is $2Z_0 c \omega$.

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The image shows a whiteboard with the title "STIFFNESS CONTROLLED REGION". Below the title, the following equation is written:

$$\frac{P_T}{P_4} = \frac{2}{2 - \frac{1}{2Z_0 c j \omega}} = \frac{2}{2 + \frac{j}{2Z_0 c \omega}}$$

And now I am further simplifying this and rationalising this by taking the j in the numerator. So what I am going to do is I am going to multiply this whole function and also divide this whole function by the complex conjugate of the denominator. So I multiply numerator by $2 - j$ over $2Z_0 c \omega$ and I divide the numerator by the same term.

So what I get is, so this 2 should not be there, and here what I will do is I will again divide the numerator and the denominator by 2 . So I get this plus j over $2Z_0 c \omega$. And now I am going to rationalize it. So what I end up getting is this relation.

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The image shows a whiteboard with the title "STIFFNESS CONTROLLED REGION". Below the title, the following equations are written:

$$\frac{P_T}{P_4} = \frac{2}{2 - \frac{1}{2Z_0 c j \omega}} = \frac{2}{2 + \frac{j}{2Z_0 c \omega}} = \frac{1}{1 + \frac{j}{2Z_0 c \omega}}$$
$$\frac{P_T}{P_4} = \frac{1 - \left(\frac{j}{2Z_0 c \omega}\right)}{1 + \left(\frac{j}{2Z_0 c \omega}\right)^2}$$

Now we know that if I have a wall, if this is my incident wave, this is reflected wave and this is transmitted wave then the incident energy is directly proportional to magnitude of P_+ plus whole squared and transmitted energy is directly proportional to magnitude of P_T . So the attenuation that is the loss of sound as sound travels across the wall is equal to intensity of the transmitted wave divided by intensity of incident wave and that is nothing but this ratio.

So this is my attenuation and I can also call this as this. So now I have this equation let us call this equation A. From equation A I am going to find what is the level of attenuation?

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STIFFNESS CONTROLLED REGION

$$\frac{P_T}{P_+} = \frac{2}{2 - \frac{1}{Z_0 c j \omega}} = \frac{2}{2 + \frac{j}{Z_0 c \omega}} = \frac{1}{1 + \frac{j}{2Z_0 c \omega}}$$

$$\left| \frac{P_T}{P_+} \right| = \frac{1 - \left(\frac{1}{2Z_0 c \omega}\right)^2}{1 + \left(\frac{1}{2Z_0 c \omega}\right)^2}$$

$\begin{array}{c} \rightarrow P_+ \\ \left| \text{Wall} \right. \\ \leftarrow P_- \end{array} \quad \begin{array}{l} \text{Incident energy} \propto |P_+|^2 \\ \text{Transmitted energy} \propto |P_T|^2 \end{array}$

$$\text{Attenuation} = \frac{I_{TR}}{I_{IN}} = \frac{|P_T|^2}{|P_+|^2}$$

Attenuation I am writing it as $\frac{1 - \frac{1}{4Z_0^2 c^2 \omega^2}}{1 + \frac{1}{4Z_0^2 c^2 \omega^2}}$, the whole thing squared. And what I do is I take the magnitude of numerator which is $1 - \frac{1}{4Z_0^2 c^2 \omega^2}$. This is the magnitude of numerator. Magnitude of denominator is same as the denominator because it is a real number and then I square the whole thing. So my attenuation comes out to be $\frac{1 - \frac{1}{4Z_0^2 c^2 \omega^2}}{1 + \frac{1}{4Z_0^2 c^2 \omega^2}}$. So now that I have developed a relation for attenuation of sound as it gets transmitted across a wall.

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A screenshot of a digital whiteboard showing a handwritten derivation. The top equation is $a_{tm} = \left| \frac{1 - \frac{j}{2Z_0 c \omega}}{1 + \left(\frac{j}{2Z_0 c \omega}\right)^2} \right|^2 = \left[\frac{1 + \left(\frac{1}{2Z_0 c \omega}\right)^2}{1 + \left(\frac{1}{2Z_0 c \omega}\right)^2} \right]^2$. Below it, a boxed equation shows $a_{tm} = \frac{1}{1 + \left(\frac{1}{2Z_0 c \omega}\right)^2}$.

Now what I will try to find is the transmission loss in decibels. So I call it TL and that is defined as $10 \log_{10}$ of 1 over 1 over attenuation. And that is essentially $10 \log_{10}$ of this whole thing. And because it is 1 over attenuation so this (deno) denominator comes in the numerator. So I get 1 over.

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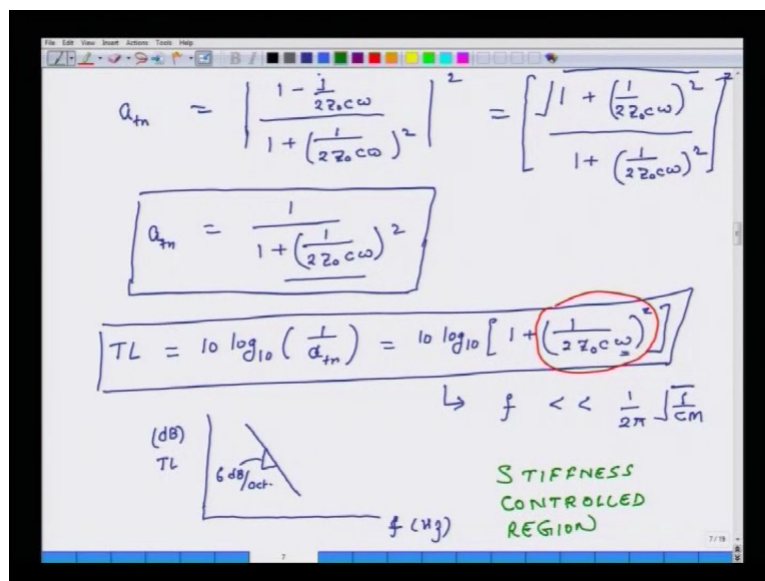
A screenshot of a digital whiteboard showing a handwritten derivation. The top equation is $a_{tm} = \left| \frac{1 - \frac{j}{2Z_0 c \omega}}{1 + \left(\frac{j}{2Z_0 c \omega}\right)^2} \right|^2 = \left[\frac{1 + \left(\frac{1}{2Z_0 c \omega}\right)^2}{1 + \left(\frac{1}{2Z_0 c \omega}\right)^2} \right]^2$. Below it, a boxed equation shows $a_{tm} = \frac{1}{1 + \left(\frac{1}{2Z_0 c \omega}\right)^2}$. At the bottom, the equation $TL = 10 \log_{10} \left(\frac{1}{a_{tm}} \right) = 10 \log_{10} \left[1 + \left(\frac{1}{2Z_0 c \omega}\right)^2 \right]$ is written.

And please bear in mind that this relation is good if the frequency of the incident sound is extremely small compared to $1/2\pi cM$, extremely small compared to the natural frequency of the system. The other thing we see from this is that if ω is below the natural frequency of the system then as I keep on reducing ω , my transmission loss keeps on increasing.

So as I get closer and closer to 0 hertz I get an improved transmission loss. So if I plot in on a log scale so this is frequency and this is in decibels I am plotting transmission loss. And frequency I am plotting in hertz. And because this is a log scale my bode plot will look something like this.

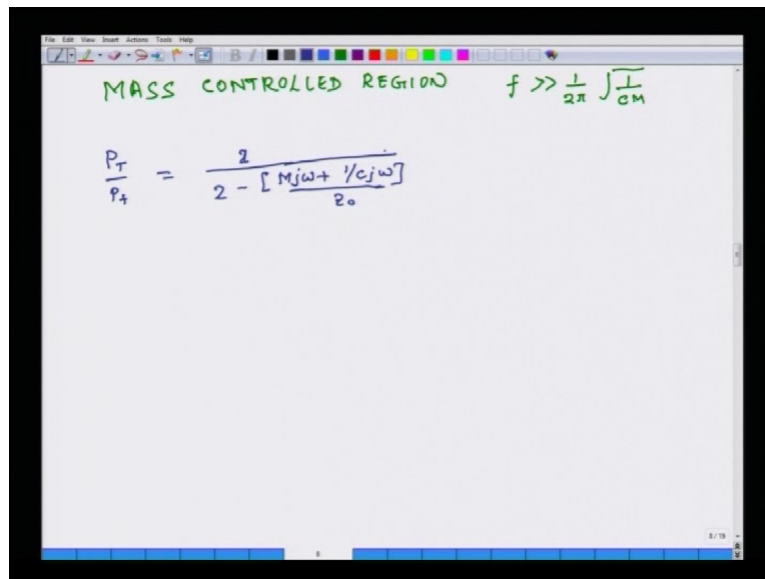
It will be a straight line because it is an asymptotic response and this slope will be 6 decibels per octave because as omega goes down I get this 6 decibels slope because as omega is extremely small the term in the parenthesis, this term is extremely large compared to 1 and when I take its log I get a 6 decibels per octave slope because there is a square term there, okay. So this is the response of the system for stiffness controlled region.

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So now we move on and now we start looking at mass controlled region, okay. And the definition of mass controlled region is that my frequency should be large compared to 1 over 2 pi times 1 over CM square root which is essentially the natural frequency of the system. So once again my original relation for P over P plus was this thing.

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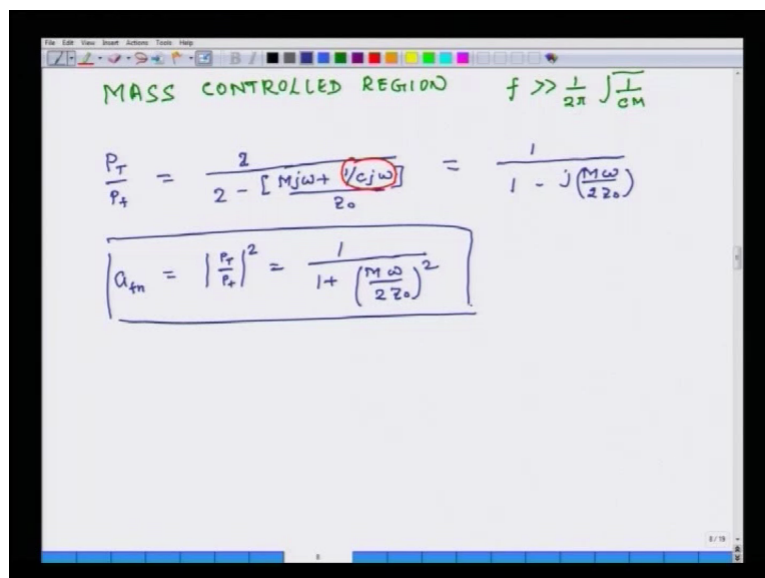


MASS CONTROLLED REGION $f \gg \frac{1}{2\pi} \sqrt{\frac{L}{C}}$

$$\frac{P_T}{P_4} = \frac{2}{2 - \frac{[Mj\omega + 1/cj\omega]}{Z_0}}$$

And in the mass controlled region I ignore this term because the product of M and omega is extremely large compared to the number 1 over C times omega because omega is extreme. So if that is the case then I can simplify this as, and the mathematics is very similar so I am not going to repeat that mathematics, I can simplify this as 1 minus j M omega over 2 Z_0. And as we had calculated earlier attenuation in this case is on ce again the square of this term and this comes to be like this.

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MASS CONTROLLED REGION $f \gg \frac{1}{2\pi} \sqrt{\frac{L}{C}}$

$$\frac{P_T}{P_4} = \frac{2}{2 - \frac{[Mj\omega + 1/cj\omega]}{Z_0}} = \frac{1}{1 - j \left(\frac{M\omega}{2Z_0} \right)}$$

$$A_{fm} = \left| \frac{P_T}{P_4} \right|^2 = \frac{1}{1 + \left(\frac{M\omega}{2Z_0} \right)^2}$$

And finally we will calculate the relation for transmission loss T L and that is essentially 10 times log 10 of 1 over attenuation. So what that is?

So here in this relation we see that like in stiffness controlled region if I reduce this stiffness my attenuati

on would go up and so would my transmission loss. In case of a mass controlled region I have to increase the frequency to ensure higher transmission losses.

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MASS CONTROLLED REGION $f \gg \frac{1}{2\pi} \sqrt{\frac{k}{cm}}$

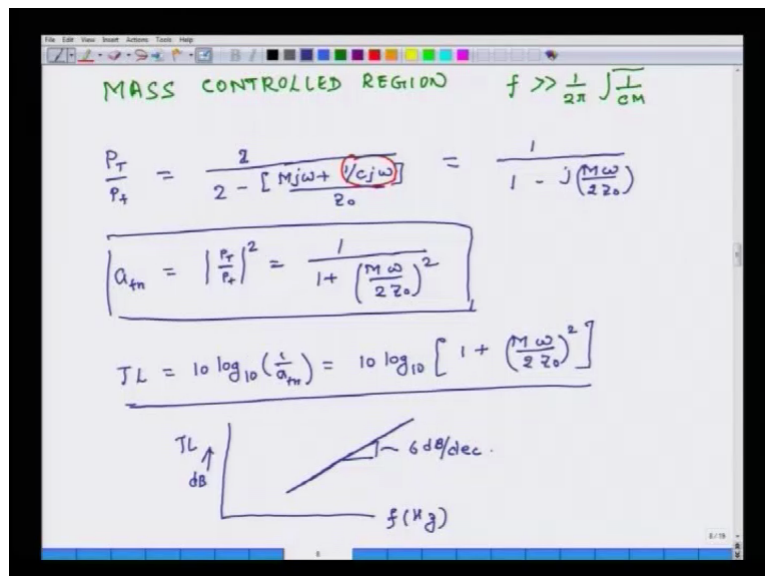
$$\frac{P_T}{P_4} = \frac{2}{2 - [Mj\omega + \frac{1}{c}j\omega]} = \frac{1}{1 - j\left(\frac{M\omega}{2z_0}\right)}$$

$$\left| a_{fm} \right| = \left| \frac{P_T}{P_4} \right|^2 = \frac{1}{1 + \left(\frac{M\omega}{2z_0}\right)^2}$$

$$TL = 10 \log_{10} \left(\frac{1}{|a_{fm}|} \right) = 10 \log_{10} \left[1 + \left(\frac{M\omega}{2z_0}\right)^2 \right]$$

So if I again plot this in decibels and if I construct the bode plot then it will be something like a straight line. The asymptotic response as omega becomes very large will be a straight line and this slope will be 6 decibels per decade. So this shows the system is going to respond as omega goes up.

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So what that means is that if I have a wall and if I am striking it normally with frequencies which are large compared to natural frequency of the system then as I keep on increasing my frequencies less and less so

and passes through that barrier because my transmission loss goes up by 6 decibels every octave. Every octave it goes up by factor of 2 that is 6 decibels. Now the question is what happens at the resonance point?

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MASS CONTROLLED REGION $f \gg \frac{1}{2\pi} \sqrt{\frac{1}{cm}}$

$$\frac{P_T}{P_+} = \frac{2}{2 - \left[\frac{Mj\omega + 1/Cj\omega}{z_0} \right]} = \frac{1}{1 - j \left(\frac{M\omega}{2z_0} \right)}$$

$$\left| A_{fm} \right|^2 = \left| \frac{P_r}{P_+} \right|^2 = \frac{1}{1 + \left(\frac{M\omega}{2z_0} \right)^2}$$

$$TL = 10 \log_{10} \left(\frac{1}{|A_{fm}|^2} \right) = 10 \log_{10} \left[1 + \left(\frac{M\omega}{2z_0} \right)^2 \right]$$

TL ↑ dB

f (Hz)

6 dB/dec.

WHAT HAPPENS AT RESONANCE?

So, when I have a condition for resonance then this term essentially $Mj\omega + 1/Cj\omega$ comes to 0. So the influence of mass counteracts and it cancels the influence of stiffness exactly at the resonance frequency. So when this term becomes 0 then my P_T over P_+ plus is essentially exactly equal to 1. So P_T over P_+ plus equals 1.

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MASS CONTROLLED REGION $f \gg \frac{1}{2\pi} \sqrt{\frac{1}{cm}}$

$$\frac{P_T}{P_+} = \frac{2}{2 - \left[\frac{Mj\omega + 1/Cj\omega}{z_0} \right]} = \frac{1}{1 - j \left(\frac{M\omega}{2z_0} \right)}$$

$$\left| A_{fm} \right|^2 = \left| \frac{P_r}{P_+} \right|^2 = \frac{1}{1 + \left(\frac{M\omega}{2z_0} \right)^2}$$

$$TL = 10 \log_{10} \left(\frac{1}{|A_{fm}|^2} \right) = 10 \log_{10} \left[1 + \left(\frac{M\omega}{2z_0} \right)^2 \right]$$

TL ↑ dB

f (Hz)

6 dB/dec.

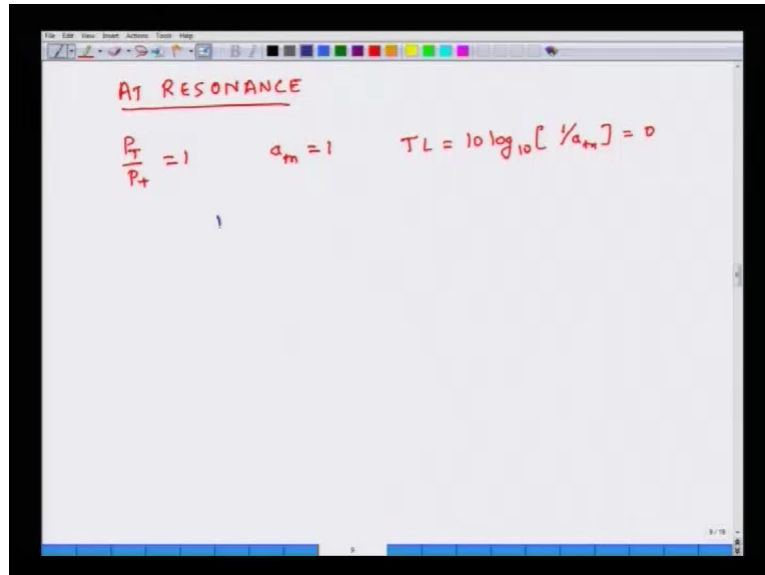
WHAT HAPPENS AT RESONANCE?

$P_T/P_+ = 1$

And thus at resonance what mathematics tells us is that P_T over P_+ plus equals 1, attenuation equals 1 based on this relation and transmission loss is 0. So I don't have any transmission loss across the wall.

So if I am hitting a wall normally with a frequency which is equal to the resonance of the system of the wall then most of the sound will just go across the wall without any damping out. But in reality what happens is that at resonance frequency the damping of the system starts playing a role.

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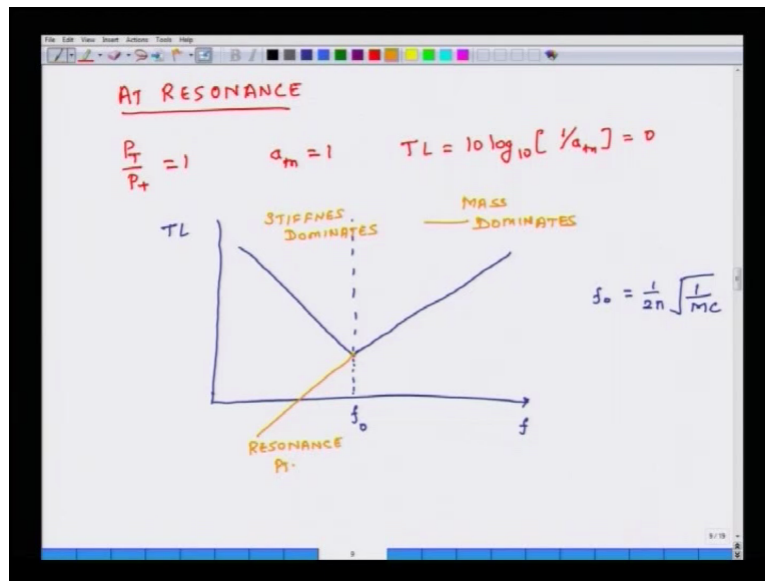


AT RESONANCE

$$\frac{P_r}{P_t} = 1 \quad a_m = 1 \quad TL = 10 \log_{10} [1/a_m] = 0$$

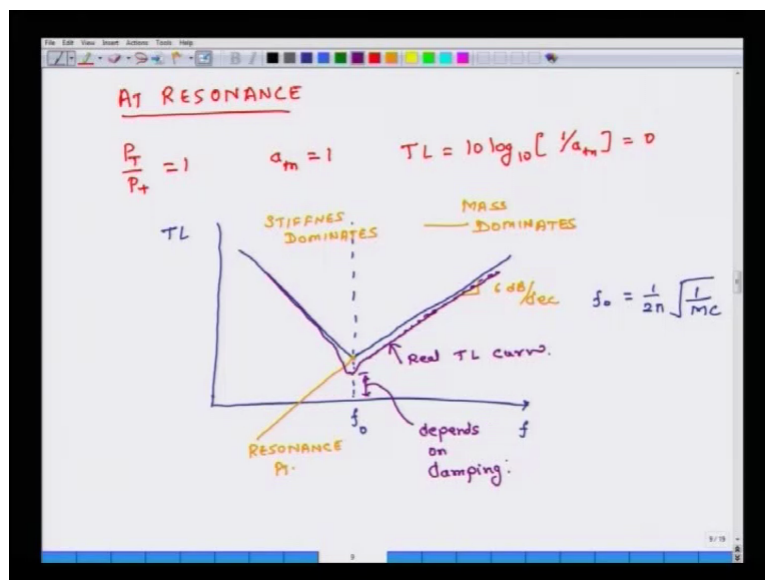
So the overall transmission loss curve it looks something like this. So let us say this is my resonance point where f_0 equals $1/2\pi$. Then in the mass controlled region the (as) asymptotic response, the bode plot will look something like this and this is how the bode plot will look in the stiffness controlled region. So this is my stiffness dominates and in this region mass dominates and this is my resonance point.

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Now these straight lines they have a slope and same slope on this side in the stiffness controlled region but it is a negative slope. So this is my ideal curve but in reality we have damping and also we have this approximation, at lower frequencies not exactly true. So the real response, the real transmission loss curve looks something like this. So asymptotically it goes and merges to. So this is my real response curve, real TL curve. And this height depends on damping.

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Thank you very much for your patience and we will meet you once again in our next lecture. Thank you.