

Finite Element modeling of Welding processes
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Module – 02
Fundamentals of finite element (FE) method
Lecture – 11
Weighted residue technique

Good afternoon everybody. Today we will discuss the different aspect of the Finite Element Method, last class what we discussed that we develop the stress analysis model the relation of the stiffness matrix the formation of the stiffness matrix for a particular element. And we can see all that stress analysis part we normally use the constitutive relation between the stress versus strain and the stress strain versus displacement.

So, we use some relation and by following the potential energy minimization we finally, develop the formulation of that we bring the stiffness matrix and we solve for displacement field. So, that was the general approach in case of the stress analysis model, but in any kind of the physical process or maybe that can govern some kind of the physical law also.

For example it is a heat transfer problem, in any kind of the manufacturing process that it may associate with some kind of the heat transfer. So, once we looking into the heat transfer or we are interested to know what is the temperature distribution, then we should know what are the governing laws or what are the governing equation basically drives this kind of the physical mechanism.

Or maybe that is why when any particular we try to solve in general the heat transfer problem. So, associated with the boundary interaction or boundary condition, then governing equation along with the boundary condition there is a need to look into the some techniques so; that means, we normally use the weighted residue technique to find the finite element based formulation.

So, today we will discuss that part, how we can using the weighted residue technique we can do finite element based formulation in the cases where there is a governing equation is there,

as well as the mathematical interpretation of the boundary condition is also there. So, in that case we look into that how the finite element formulation can be done.

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Weighted residual method

Suppose the governing equation and boundary conditions are given as

Governing Eq: $A(T) = 0$ (1)

Boundary condition: $B(T) = 0$

If an arbitrary temperature distribution is assumed in the domain and it is substituted in Eq. 1, these equations will not be satisfied. The obtained results will be as follows:

$$\begin{cases} A(T') = R_1 \neq 0 \\ B(T') = R_2 \neq 0 \end{cases} \quad (2)$$

These obtained quantities are referred to as residues.

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But before that what is the weighted residual method or weighted residue technique we normally use in any kind of the finite element formulation?

Suppose the governing equation and boundary condition represented by these two different form of the equation. So, equation 1 we can see that A the equation the functional form of a governing equation in general and B that is the functional form of a boundary condition. And both as a function of the T is the basically the solution variable we can say for example, heat transfer problem it is a it is equivalent to the temperature.

So, once we get these two equations what is the governing equation, what is the boundary condition for this particular problem? Then we assume that some arbitrary temperature distribution in for example, in this case we assume some arbitrary temperature distribution in the domain. And that arbitrary temperature distribution we consider as a solution of this particular equation.

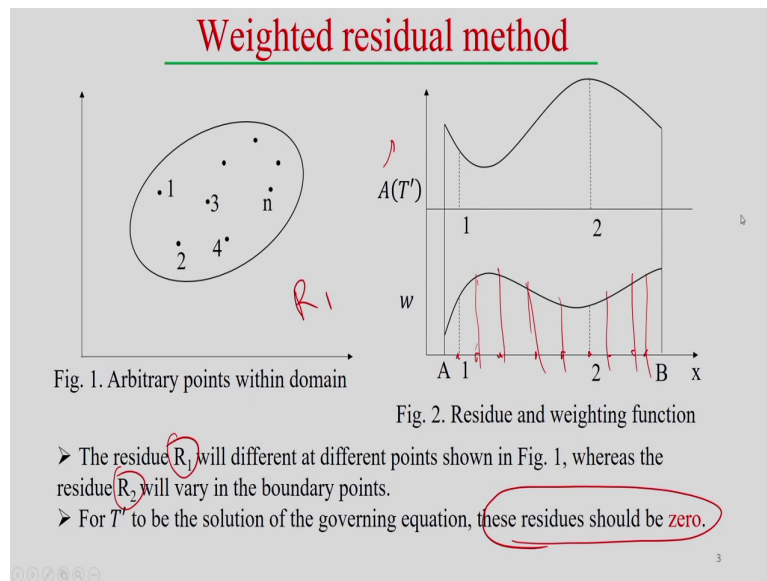
By assuming that if it is substituted in this equation this particular equation in this case is it is equation 1, then this equation will not be satisfied may not be satisfied also. Because, in this case we do not know the exact solution, but assuming some arbitrary solution and then that arbitrary solution we are fitting to the equation we are just try to fitting this arbitrary solution equation it is not necessary it will satisfy this particular equation.

So, therefore, in the mathematical form we can write the obtained results once we put we assume this particular solution of this equation. Then put this mathematical form of the equation we can see that $A \cdot T$; T we assuming this is the solution of this particular equation. So, it should satisfy, then or B is the this is a boundary condition and it is a the solution is the T .

So, then both should satisfy if it is the exact solution, but we do not know the beforehand we assuming some solution that is why it may not satisfy. So, once we put this thing this there exist an some sort of the residuals. So, that is the quantities called R_1 and R_2 residuals and in the mathematical form it is not equal to 0; that means, residuals some residuals are there; that means, definitely it is not equal to 0.

If it is equal to 0, then our assumption was correct and we are getting the solution of this equation by assuming this particular solution, but it is not possible to get this solution in general. So; that means, we arbitrarily by assuming some arbitrary solution if we want to satisfy this particular equation there must be some amount of the residuals must be there and that residuals can be represented this way R_1 , R_2 . So, then this equation two is represented like that.

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Other way also if you look into this figure 1 that arbitrary points within the domain. So, that so many arbitrary points are there 1 2 3 4 up to dot dot n.

So, this residue R_1 will different so; that means, that this different at the different points R_1 value can be different at the different points shown in the figure. Whereas, the residue R_2 will vary on the boundary points actually, the R_1 residue R_1 the residual residue is defined within the domain, but R_2 is thus the residue existence of because on the boundary. So, therefore, R_2 will vary on the boundary points.

So, but it is not necessary R_1 can be fixed value, so R_1 can vary the residue can vary at the different points. So, in even we are looking in the from the point of the finite element base method, because in finite element what we do we just discretize the domain; discretize the domain means we create the elements small small elements within this particular solution

domain. And we are trying to look into what is happening the this looking into the residual in the particular node points.

So, that is why different different point 1 2 3 is the domain that we assume that we can it indicates the kind of the node point in this domain. And we are trying to satisfy this equation with the particular defining we are defining the equation in the node points. And based on that we can say that when you try to satisfying some arbitrary solution of this particular equation, then we feed the value looking into what are the values what looking into what are the residuals is exactly on the different node points.

Now, this T dot, for T dot for we are assuming T dot is a arbitrary solution for this particular equation governing equation and boundary condition as well. So, T dot to be the solution so; that means, T dot to be the solution of this governing equation. So, then if it is not T dot it is exactly the solution of this governing equation then definitely there may not be any kind of the residuals, so residue should be 0; so then in that cases residue should be 0.

If T dot is exactly satisfying this equation and if each and each and every node point then that is the exact that, when solution it is possible to that we consider this T dot is the solution of this particular equation, otherwise there exist an some sort of the residuals. So, from that concept we can finally, analyse these things.

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Weighted residual method

- Considering a 1-D domain extending from point A to B as shown in Fig. 2.
- If the distribution of the residue for some arbitrary temperature distribution T' is given by $A(T')$, then we consider another function w .
- The function w is chosen such that when $A(T')$ and w is multiplied at every point and added, we obtain the quantity, $\rightarrow \downarrow$

$$\int_A^B w \cdot A(T') dx = 0 \quad \rightarrow \mathcal{L}$$

where, w is an arbitrary function. It is also called weighting function.

- $A(T')$ will not be zero at all the points for a distribution of T' which is not the solution of the problem.
- Therefore, the possibility of the above integral being zero is minimal. $A(T') =$

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So, now to understand these things how this residual weighted residual technique works on that we assume some one dimensional domain. Extending from point A to and point B we can see that one dimensional domain and this is a x direction one dimensional domain and A T dot is the this functional form T dot is the solution this particular case.

And w is the weighted residue again weighting function and this we discretize this domain in the different thing or maybe that small elements. So, it is a one dimensional element such that we consider, what is the this discrete point as basically node point we are looking into the solution or we are looking into the residuals for this particular equation.

Now, if the distribution of the residue then we just distribution of the residue means in the discrete point, what are the value of the residue? And this distribution we consider for the for some arbitrary temperature distribution T' dot is given by $A(T')$ dot; that means, this functional

form $A \cdot T$ the particular distribution of the T dot or a functional form of this $A \cdot T$ dot we are assuming this is the solution of this equation.

Then we consider the another function. So, in that case we introduce the another function w which is called the weighting function. Now, this function w is chosen in such a way that when $A \cdot T$ dot; that means, this is the T dot is the solution for the particular equation and w is that the another function if we consider and w is multiplied at every point and added we obtain the quantity.

So, integration of this thing A to B , but in this case this is the weighting function and this is the actual assuming the T dot is the solution arbitrary solution of this governing equation and this is the functional form of the $A \cdot T$ dot. So, this weighting function and multiply this $A \cdot T$ dot this is one dimensional problem, so one only the variation along x axis.

So, therefore, $\int dx$ integrand of this we can edit this quantity we can represent this thing. So, this where w is the also arbitrary function that weighting arbitrary function it is called the weighting function. So, w is called the weighting function. So, to satisfy this the solution or to bring some kind of the solution of a particular equation we just multiply with another arbitrary function that is called the weighting function. And in the form of a integral this thing, but definitely this where integration, but this integral part is defined or maybe we can look into the numerical integration of this thing.

So, in that integral form we can represent this multiplying weighting function and the actual governing equation for that governing equation we assuming some solution arbitrary solution. Then $A \cdot T$ dot will not be 0 at all the points, definitely that this functional form $A \cdot T$ dot the $A \cdot T$ dot is basically it is in if you look into the analytical solution it follows some kind of the distribution or some functional form it follow.

So, therefore, $A \cdot T$ dot will not be 0 at all the points for a distribution of T dot which is not solution of the problem. So, if $A \cdot T$ dot is 0 each and every point; that means, each and every we looking into the for one dimensional problem each and every node point if it is equal to 0

then this is the solution, but if it is not equal to 0 then this is not the solution of this particular equation.

So, therefore, the possibility of the integral being 0 is minimal. So, the chance's is very that being the 0 of being the 0 is a minimal. So, that is why we multiply this thing the weighting function in the form of an integral.

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Weighted residual method

➤ If we consider several arbitrary distributions of w (e.g. w_1, w_2, \dots) and obtain a distribution of T which makes this integral zero for all values of w , then the only possibility in which this can happen is when T is the desired solution of the problem.

➤ Thus the condition for a temperature distribution T to be the solution of a problem stated in the form of expression (1) is given by,

$$\int_V w_1 A(T) dv + \int_S w_2 B(T) dS = 0 \rightarrow T = ? \quad (3)$$

where, w_1 and w_2 comprise many sets of arbitrary weighting functions.

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Now, if we consider several arbitrary distribution of the weighting function w . So, different form of the w several arbitrary different types of the different functional form of the weighting function and w_1, w_2 or maybe different weighting function at the different discrete points.

If you consider and obtain a distribution of the T which makes this integral 0 for all values of w then only the possibility we see in which this can happen when the T is the desired solution of the problem. It means that in other way we can see that define and if it is equal to 0, then it indicates that it means that the by putting the weighting function we choose the weighting function in such way that it becomes 0 then we can say that T dot is the solution of this particular problem.

So, we looking into this thing desired solution T dot, T is the desired solution of this particular problem and we assume that T is the desired solution of the particular problem the other way also. So, whatever functional form we can see that solution of this particular equation and this we can obtain with the multiplying of the different weighting function. So, therefore, thus the condition for temperature distribution.

So, basically we are looking for the temperature distribution T the that distribution to be the solution stated in the form of the expression of one expression of the equation one we can look back to the equation one also that this is the expression of the.

So, this $A T$ equal to 0 means, T will be the solution of this particular temperature distribution if get the T solution if this is the this multiply by the weighting function w_1 , but this equation one means both are ah when you are talking this kind of problem both it is important to consider the governing equation in the domain of the solution domain as well as the what are the boundary condition is important and combined together we can define the in a particular problem.

So, that means we have giving some weightage weighting function introduce some weighting function which is multiplied by the governing equation and this since the governing equation is valid over the volume over the domain then whole domain; that means, over the volume. So, that is why we put the $d v$ plus integration we put the another weighted function w_2 it is not necessary weighting function can be same also can be different also, but that different weighting function if we consider w_2 and $B T$ represents the boundary condition.

So; that means, it is a boundary interaction. So, which is defined over the surface because boundary is represented with three dimensional problem, boundary is represented over the surface. So, then this weighting function into this boundary condition mathematical form of the boundary condition assuming that T is the solution and what satisfying this should equal to 0.

It means once this satisfying a condition this particular condition equal to 0 then we can say that T from this expression we can get the T is the solution; that means, temperature distribution in this case is the solution for this particular problem. So, that other way we just in this case. So, w_1 and w_2 comprise of the many sets of arbitrary weighting functions. So, there are so many possibilities of defining the what is the w_1 and w_2 or both can be the same also.

But, finally in the mathematical form when you are multiplying the governing equation boundary condition with some weighting function do doing the integration which is integrated over the volume for the governing equation, and integrated over the surface area for the boundary interaction. Then the whole system equal to 0 then we can assume the by solution of this equation is the from here what is the temperature distribution that is the solution of this particular problem.

So, in the other way by introducing the weighting function we can form the mathematical form of a any particular problem. And which is basically looking into that particular problem and then we can formulate the by using the finite element method any kind of the problem, which is governed by the one particular governing equation and along with the boundary interaction or boundary condition.

Now, we can see w_1 and w_2 may be have different sets or different weighting function there are so many possibility are there for w_1 and w_2 . How looking into that the so many possibilities of w_1 w_2 . And I think that is not discussing what are the mathematical aspect the what are the different forms of the weighting function and then what are the limitation and all these things.

And how we can form this weighting function that is not beyond the scope of this particular course rather we can focus on the very simplified way to understand the concept of the weighted residue technique in this particular case and then how this what way we can put the weighting and more in the we can define the heat transfer problem associated with the welding process that is the focus of this particular course.

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Weighted residual method

Based on the selection of weight function the weighted residual method can be divided into five categories:

- Collocation method – *Weighting function is chosen from the family of Dirac δ functions in the domain.*
- Sub-domain method – *A modification of the collocation method.*
- Least Squares method – *Summation of all the squared residuals is minimized.*
- Galerkin method – *It will be discussed further in the course.*
- Method of moments – *The weight function are chosen from the family of polynomials.*

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So, therefore, based on the selection of the weighting function and there may be different techniques weighted residual method can be divided into 4 5 categories. You can see there are in general there are 5 categories problem can be divine defined based on the different nature of the weighting function.

So, one is the collocation method, collocation method the weighting function is chosen from the family of the direct delta function in the domain. So, it is a basically simply in general

sense we can say that this is the this method is basically the particular weighting function we can choose and accordingly this method has been developed or this method is normally used to get the desired finite element base equation or may be the to defining the problem using some governing equation boundary condition.

Similarly, sub domain method it is a simply some modification of the collocation method is required in this particular cases. Even least square methods also in this case the summation of the all the square residuals.

So, we estimate the residuals so summation of the all the residuals; that means, we putting the weighting function for a particular node point and this governing equation though we can assume some solution. Then multiply this thing summation of this thing all the residuals and square root may be summation of all the residuals and square of them can be minimized to get the finite element formulation for this using this least square method.

So, that is the methodology is beyond our scope of analysis in this particular course. Then Galerkin method, so Galerkin method basically we will be discussing and we will be for this particular courses and based on this Galerkin method what we can develop the different finite element formulation of the associated the welding process. And that is the main focus of this course we will discuss later on this thing.

Then method of movements in this cases the weight function are chosen from the family of the polynomial. So, from the family of the polynomials the weighting function can be chosen and based on that the method movements ah techniques has been developed.

So, we can see that all this methodology and with weighted residue technique in general sense we can say that how we can choose the this thing, how we can choose the weighting function and what way we can minimize the residuals and based on that the different methodology different techniques of the finite element formulation has been developed.

Now, let us look into what is the Galerkin method which we are supposed to use in this particular course.

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Weighted residual method

Condition of a function to be used as a weighting function:

- i. All functions should be totally independent.
- ii. The functions should be simple in order to avoid computational difficulties.

Fig. 3 Variation of nodal shape function

Fig. 3 shows a 1-D element with n nodes within, 1-2, 2-3, 3-4... are each separate elements.

N_1, N_2, \dots, N_n are nodal shape functions.

Now, condition weighted residual method condition of a function to be used as a weighting function, two things are there two conditions are there that what are the as a, which functional form can be used as a weighting function? One is the, first point is the all function should be totally independent; we have to chosen the weighting function in such a way that all the functions should be totally independent.

And second thing is that the function should be very simple. So, in order to avoid any kind of the computational difficulty; so, it is a definitely there are lots of possibilities to choose the

different form of the functional form, but it is as simple as possible other such that we can avoid some kind of the computational difficulties.

So, this case you can see the figure before going into the details of this analysis we understand we should understand these things in a particular 1 D element and suppose there are n nodes and there are so many elements n . I think if there are n nodes I think there are N minus 1 elements will be there are each separated it is separate elements. So; that means, this is the node number 1 2 1 and 3 node number 4 5 6 7 8 9 like that 10 like that these are the different node numbers and this is the node number n particular n number.

Now, 1 2 this indicates the one element in a one dimensional problem. Similarly 2 3 is the another element 3 4 is another element like that. So, this way we can define the different elements nodes also in a one dimensional problem. But, we can show the variation on shape function we have seen we have already discussed that shape function value even if we look into the expression of the shape function in the that we can see that where from shape function from one particular associated with node 1. So, we can use the several shape function N_1, N_2 something like that for a particular element we use the different shape function.

So, if one element they are having the tetrahedron element in that cases there are 4 nodes so we can find out that there are 4 shape function N_1, N_2, N_3 and N_4 that we have already discussed in the last class also. Now, in this case we can assume there is a 2 1 element and there is a node 1 element have associated with the 2 nodes N_1 and N_2 . But on the particular case this if it is a N_3 that node N_3 value of the shape function will be 1 for this particular node, but its 0 corresponds to the other surrounding zone 0.

So, therefore, N_1, N_2, N_n are the nodal shape functions. So, that is why this shape function we can say the nodal shape function because we are N_1 which basically one is the node number so accordingly we can define the shape function also. So, N_1, N_2, N_3 this all represents the these are the nodal shape function. Now, we will see how it works in this case.

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Weighted residual method

- Nodal shape function has relevance at a particular node and adjoining elements.
- The value of nodal shape function is 1 at a particular node and its value is zero at every other node. This feature can be seen in Fig. 3.
- If these shape functions are used as the weighting function then this approach is called the Galerkin approach. →
- e.g., $w_1 = N_i$ and $w_2 = -N_i$ where $(i = 1, 2, 3, \dots, n)$. Thus, the weighted residual statement given in Eq. 3 becomes,

$$\int_V N_i A(T) dv - \int_S N_i B(T) dS = 0 \quad (4)$$

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Now, nodal shape function has the relevance at the particular node definitely nodal shape function is a particular node and the adjoining elements. So, one particular node and the element.

For example in this case this is the particular node N 3 equal to 1, but adjacent elements for these cases are the adjacent node 2 3 and adjacent element 3 4. The at the node, at the node value at 4 basically node point 4 equal to 0 for this particular case, shape function will be 0. So, the value of the nodal shape function is 1 at a particular node and its value is 0 at every other node.

So, we can see that for the particular N 3 value N 3 equal to 1 for this particular node, but it is 0 the shape function the nodal shape function value equal to 0 for other nodes that is very obvious also ah. Now, if this shape function can be used as a weighting function then this

approach is called the Galerkin method that is to if this shape function are used as a weighting function.

For example we have seen that that when you try to establish the weight weighted residue technique we have to choose some weighting function. So, particularly the Galerkin weighted residue technique; that means, in Galerkin method we normally use the weighting function as a shape function. Same shape function if you use then this approach is normally called the Galerkin approach.

So, is the same the weighting function is the same as the shape function. For example, in this case if we consider the one weighting function associated with the governing equation as a N_i . So, N_i is the weighting function is the N_i , i indicates the 1 to n its basically indicates the node ah ; basically indicates the node point. Now, w_2 that means, another weighting function it can be used the also minus N_i .

So, if we consider the governing equation in such a way that it is a plus N_i ; that means, shape function similarly weighting function w_2 can be considered as a minus N_i . So, N_i corresponds to the basically the nodal shape function for each and every node point particular node point.

Thus the weighted residual statement is given equation becomes that, if you see that this is the weighting function and this is also weighting function. So, this weighting function w_2 we considered the minus N_i . So, we simply put the N_i here and this is the governing equation this is the boundary condition and because it is defined over the surface and this is over defined over the volume.

So, multiply by the shape function and this equal to 0 in this case once we establish this equation and the in the integral form. It means that once we get the solution if we find out what is the temperature distribution from here then that indicates the solution of this particular problem or we can say this is the solution of this particular problem by just putting

in the weighting function. So, that is the importance of the putting some kind of the weighting function in a finite element analysis.

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Heat conduction analysis

The steady state heat conduction equation is given by:

$$k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \dot{Q} = 0$$

where, \dot{Q} is the rate of heat generation in unit volume.

The boundary conditions specified at the surface is expressed as:

$$k \frac{\partial T}{\partial n} + \alpha T + q = 0 \text{ at } S_1$$

where, S_1 represent the portions of the boundary on which boundary conditions are specified.

Now, look into this particular problem the heat conduction analysis. So, we assume the steady state heat conduction equation we know the steady state heat conduction equation and k thing k into del T by del x this thing Q dot and the, I think I equal to rho C p del T by t.

So, basically this term equal to 0. So, then there is no time component here in this particular governing equation. So, we can say this is a steady state equation just simply neglecting or maybe make it equal to 0 because temperature variation is not independent of the time component. So, that is why it becomes the steady state heat conduction equation.

So, this is the steady state equation and it is also the x, y, z ; that means, we can say the it is a three dimensional steady state heat conduction equation where \dot{Q} is the rate of internal heat generation a per unit volume.

So, this equation what way we can see that how this is we assume this is the governing equation any kind of the heat transfer problem, it can be associated with the welding any manufacturing process or it can be associated with the some other problem also. But in general this is there is a heat transfer problem we consider the Fourier heat conduction equation or three dimensional heat conduction equation in the steady state condition.

But the boundary condition specified at the surface so; that means, in a welding problem we can see the boundary condition. So, suppose this is the domain and we have seen the boundary condition in a welding problem also it is as in general the heat is conducted a on the surface that indicates the k into $\frac{\partial T}{\partial n}$ that normal to, n equal to n vector represents the normal to the surface. So, it is defined on the exactly the heat conduction, but that is defined exactly on the surface.

αT is basically maybe heat loss by convection and radiation from here, and maybe other surfaces and the q is the basically heat flux, the impose there may be some in particular problem there may be the heat is applied heat flux is applied to the surface and that is the q in general. So, q is the heat input to the surface and in general I am talking about and αT is the heat loss though h equal to h sorry the heat loss by convection per unit area T minus T ambient temperature. So, basically $h T$ in general αT we can say in the generalized form that αT is the variable in this case.

So, therefore, it is a general form of the boundary interaction normally associated with the heat conduction problem if you assume that and that is defined only on the surface S_1 . So, let us see let us look into this all this defined over the surface S_1 and this boundary interaction. Now, S_1 represent the portion of the boundary on which boundary conditions are specified. So, it is not necessary the whole boundary is subjected to some sort of the boundary interaction.

So, it is a particular boundary interaction may be possible even some other boundary condition can be imposed in the other part of the boundary. So, we assume that maybe we assuming that it is a small part of the boundary the this boundary condition in general form of the boundary condition is there.

So, therefore, we can see this is the governing equation this is the boundary condition. So, from here what we can develop the using the application of the Galerkin residue technique and we can formulate the heat transfer problem.

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Heat conduction analysis

Considering $A(T)$ as the governing equation and $B(T)$ as the boundary equation in Eq. 4, and applying the concept of weighted residual method to the 3-D steady state heat transfer problem, we have:

$$\int_V N_i \left[k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \dot{Q} \right] dV - \int_S N_i \left[k \frac{\partial T}{\partial n} + \alpha T + q \right] dS = 0 \quad (5)$$

or,

$$\int_V k N_i \nabla^2 T dV + \int_V N_i \dot{Q} dV - \int_S k N_i \frac{\partial T}{\partial n} dS - \int_S N_i \alpha T dS - \int_S N_i q dS = 0 \quad (6)$$

First form of Green's theorem,

$$\iiint_V (u \nabla^2 \phi - \nabla u \cdot \nabla \phi) dV = \iint_S (u \nabla \phi) \cdot d\vec{S}$$

Now, considering A T if you look remember equation 1 A T is the governing equation and B T we consider the boundary condition (the T is the is the functional form T is the as a function of T we can say like that. As a function of T means as a function of temperature this is the functional form. As the boundary equation in equation 4 and applying the concept of the

weighted residual method to the three dimensional steady state heat transfer problem, so three dimensional heat transfer problem.

So, this is the if you see that $A T$ this weighting function N_i , other is the $B T$ and weighting function N_i and this is the plus and this is our volume over surface and this is $d v$ it is $d s$. The same way we have considered, so this is the governing equation up to $Q \cdot$ this third bracket within the third bracket N_i is the weighting function as the same as shape function over the volume integrand over the volume and this is the integration over this volume the volume integral.

So, now similarly for boundary interaction this is the $B T$ in this case and this was $A T$ this case and this is the $B T$ and this is the shape function surface. Because boundary interaction over the surface and minus shape function we have defined. If it is a plus for the governing equation the minus for the boundary interaction. So, this becomes 0.

Now, this is the formulation this thing in that cases the what are the temperature distribution we will be getting, then this is the solution of this particular equation. And of course, in this case we are using the we following the weighted residue technique. Now, this look into the individual elements for this particular equation.

So, this can be represented also this equation can be represent also $\nabla^2 T$ the differences are $\text{del to } T$ gradient in if you look into the gradient divergence color in the vector form we can represents this second $\text{del }^2 T$ by $\text{del } x$ square plus $\text{del }^2 T$ by $\text{del } y$ square they are simply represented by this equation can be written the in general sorry $\nabla^2 T$.

So, that is T is the governing equation here. Now, k we just keep it outside k . So, we assuming this in k the thing N_i is the variable and $d V$ is the volume over the volume. Second term this $Q \cdot$ term $Q N_i Q \cdot d V$ over the volume, this without expanding this different elements of this particular integral.

Then $\nabla \cdot \mathbf{k}$, \mathbf{k} is the this is the from boundary interaction $\nabla \cdot \mathbf{T}$ by $\nabla \cdot \mathbf{n}$ into dS . Second term is coming like this $\nabla \cdot \mathbf{T} dS$ over the surface, third term it comes like that it is also $\nabla \cdot \mathbf{q} dS$ this is also over the surface.

So, from here now we apply first form of the Green's theorem. So, Green's theorem is simply we can use the relation from the volume integral to the surface integral in that formula. From here you can see that we apply the Green's theorem here because in this case from this term we can use the Green's theorem.

So, this term is equivalent to this term and then from here we can see that this Green's theorem over the volume thus volume integral to conversion from volume integral to the surface integral. So, if we apply the greens theorem here, then this part will come to this side, but it is will be negative sign. And the another surface components will be there another this if you see over the volume. So, this is volumetric component will be there on the surface components will be there if we apply the Green's theorem for this particular part.

Now, see from here we can expand by Green's theorem that two terms will be there. So, this will come other side; that means, this term will be there as well as this surface term and this volume term will be there. Now, looking into this equation how this can form. Then this term terminology the first term from here we can converted to this term.

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Heat conduction analysis

Using the first form of Green's theorem to rewrite Eq. 6, we have,

$$\int_S k N_i \frac{\partial T}{\partial n} dS + \int_V N_i \dot{Q} dV - \int_S k N_i \frac{\partial T}{\partial n} dS - \int_S N_i \alpha T dS - \int_S N_i q dS = 0 \quad (7)$$

or,

$$\int_V k \left(\frac{\partial N_i}{\partial x} \frac{\partial T}{\partial x} + \frac{\partial N_i}{\partial y} \frac{\partial T}{\partial y} + \frac{\partial N_i}{\partial z} \frac{\partial T}{\partial z} \right) dV - \int_V N_i \dot{Q} dV + \int_S N_i \alpha T dS + \int_S N_i q dS = 0 \quad (8)$$

On discretizing the domain into four-noded tetrahedron elements, the temperature within the element can be expressed in terms of nodal temperature as,

$$T = \sum_{i=1}^4 N_i T_i = [N] \{T^e\} \quad (9)$$

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So, this term; so this term represent that here you can see minus k del N i by del x del T by del x, del N i by del y del t by del y, this terms will be coming into the picture d V. And another application of the Green's theorem also we can find out this is other surface term will be also be there.

So, u is equivalent to here we can see the shape function u is equivalent to here shape function and phi is basically u is basically equivalent to the shape function N i and phi is equivalent to basically temperature T here. So, N i N T in terms of that, we can find out k del N i by del x. So, this is in the gradient basically del this indicates the sorry; this is the u it indicates the gradient of u or we can in this case the gradient of u means here N i.

So, gradient of N_i and gradient we can see the gradient is basically $\frac{\partial}{\partial x_i}$ this is a vector quantity $\frac{\partial}{\partial y_j}$ plus $\frac{\partial}{\partial z_k}$. So, from here the gradient of that it represents the this indicates that 2 gradient is there and gradient of ϕ .

So, in this case gradient ϕ means it is the it will be simply the ϕ is represented by T basically the yeah T and then dot product of that indicates that $\frac{\partial N_i}{\partial x}$ the first term $\frac{\partial T}{\partial x}$ $\frac{\partial N_i}{\partial y}$ $\frac{\partial T}{\partial y}$ $\frac{\partial N_i}{\partial z}$ $\frac{\partial T}{\partial z}$. So, this is the term first term is coming into this picture over the dV .

And second another surface terminology will be coming that plus this is the $k N_i \frac{\partial T}{\partial n}$ we assume it is a constant this thing. So, $\frac{\partial N_i}{\partial n}$ or other parameters are variable $\frac{\partial T}{\partial n}$ dS . So, then it is coming from the from here this term the this term will be coming the surface term surface integral term will be come into the picture u is equivalent to the T here, u is equivalent to sorry shape function N_i and ϕ is equivalent to T .

So, $\frac{\partial \phi}{\partial n}$ the gradient of ϕ means gradient of T in this case ϕ equivalent to T . So, therefore, we will be getting this expression $k N_i \frac{\partial T}{\partial n}$ into dS . So, this why $\frac{\partial T}{\partial n}$ because we define the surface means, but we defining $\frac{\partial T}{\partial n}$; that means, this temperature gradient which is defined normal to the surface. So, $\frac{\partial T}{\partial n}$ into dS this term is coming after the composition from the volume integral to the surface integral.

Now, look into the other term this is already was there and this is from the surface term and already from the boundary condition there. Now, next line this term from; the this comes from the governing equation and this term from the governing equation by applying the Green's theorem, but this comes from the boundary condition though. So, that will balance if we look into this thing. So, finally, we the expression is like that $\int dV N_i$ this one N_i equal to 0.

So, therefore, on discretizing the domain the domain into the 4 noded, so these are the different terminology we can use and this kind of expression we reach after the application of the Galerkin weighted residue technique. So, on discretizing the now it is necessary to

discretize the domain 4 noded. Now, this is the general form of the equation now depending upon the N_i , what should be the value of i ? It depends on the what kind of the element how many nodes are there in the particular element that has to be.

For example if it is the 4 noded tetrahedron elements; 4 noded tetrahedron elements i can vary from 1 to 4, but if it is a brick element then i can vary from 1 to 8. So, depending upon the what kind of the element we consider or you have discretized the domain accordingly i can vary. So, therefore, if we assuming that on discretizing the domain into 4 noded tetrahedron elements, then the temperature within particular element can be written like that. So, temperature variable here T .

Expression in the temperature T itself within the in the form of a nodal temperature as well as the shape function form. So, that $N_i T_i$ summation of i equal to 1 to 4 which is also equal to the shape function into T that we have already seen. That even we have shown in case of the displacement field also if you remember correctly in the stress analysis part there we have developed that we have seen that displacement field can be represented in the form of a nodal value. So, T in this cases also temperature can also be represent in the form of this is the shape function and this is the in the form of a nodal temperature value so T_i ; so that form we can represent.

So, but in this case assuming that N is the variable quantity so whatever variable quantity means we can do the derivative first derivative it can be if it is a linear shape function if you do the first derivative it becomes constant also. The T is the nodal temperature we can assume this is a nodal value.

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Heat conduction analysis

- The volume integrals and the surface integrals in Eq. 8 are expressed as the sum over all the elements.
- If there exists n nodes within the volume there will be n unknown temperatures T_i in Eq. 8.
- To obtain the T_i values, n number of equations are required that can be solved simultaneously. i=1 to n
- The equations can be obtained by considering n separate values of weight functions, N_i , each n value giving a separate equation. N₁, N₂, N₃, ... N_n
- Thus, if the number of nodes is n , then the number of N_i values is also n . → N₁, N₂, N₃, ... N_n

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So, therefore, the volume integrals and the surface integrals of the last equation 8 are expressed as the sum of the over all the elements. So, once we do all this term this in this particular expression here we can discretize we can do in integrand, but integration we can perform over the numerical integration, then we can perform for a particular element, then once we get the particular value of the sorry particular element where you can distribute the value in each in node point.

But once we assemble for the contribution for the all elements then accordingly we can put the their nodal value which point the node point is common 1, 2 or 4 different element.

So, which keep on adding the contribution basically we calculate all this thing one particular element. Then we call one by one element and accordingly we can put the position the

position of the particular node point. Because a one particular node point may be the common node point more than one or more than one elements in that particular cases.

So, once we call the particular element what are the contribution for the node point and the when you consider other element and both the element having some common node point, then we just keep on adding for this particular common node point and. In that way we can form the contribution for the each and every node point and we form the linear system of equation or we can say the form of the matrix that size is normally that number of depends on the number of nodes.

If there is n number of nodes the size of the matrix A X equal to size of the matrix we can see that, $A X$ equal to B that is the final form of the equation. So, A matrix if there is n nodes the a can be n into n node, but this calculation we can do for particular element. And then we call all the element and in a form that we met we make the assemble one big matrix A which is dimension of this matrix is the n by n it depends on the number of nodes in this particular domain, then we solve for the equation.

Therefore if there exist n nodes within the volume. So, there will be n unknown temperature definitely each and every nodes are there. So, each and every node point the temperature can be considered as a unknown quantity and that is temperature can be considered as the T_i . So, where i can vary from one to n in that particular equation 8.

Then to obtain the T_i values; that means, T_i equal to 1 to n ; n is the number of nodes. So, in that cases n by n matrix has to be solved equation so we can get the n number of equations and n number of variables. So, in that case we can solve this equation and then solve simultaneously solve for the values. So, in that cases we will be able to find out what is the value of the temperature for each and every node point.

So, therefore, the equations can be obtained by considering the n separate values of the weighting function N_i each n value giving a separate equation. So, that is also possible the equation can be obtained considering the n separate values of the weighting function that is also possible. In this case the weighting function is equal to N_i the each n value giving the

one separate equation. So, if the number of nodes is n then the number of N_i values will be the n .

So, N_i also value it can be also $n-1$ to n , so N_1, N_2, N_3 that up to N_n . So, that are the different different shape function will be able to feed in this particular case and then we will be able to solve this particular problem.

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Heat conduction analysis

➤ Therefore Eq. 8 can be expressed as:

$$\sum_{e=1}^m \int_{V^e} k \left(\frac{\partial N_i}{\partial x} \frac{\partial T}{\partial x} + \frac{\partial N_i}{\partial y} \frac{\partial T}{\partial y} + \frac{\partial N_i}{\partial z} \frac{\partial T}{\partial z} \right) dV - \sum_{e=1}^m \int_{V^e} N_i \dot{Q} dV + \sum_{e=1}^r N_i \alpha T dS + \sum_{e=1}^r \int_{S^e} N_i q dS = 0 \quad (10)$$

where, we have m elements, of which r elements have boundary of domain as their face.

Considering a tetrahedron mesh that has only 4 nodes, only 4 non-zero values of N_i will exist for an element.

Thus an element will contribute terms only in four equation of a set of n equations expressed as Eq. 10.

$$T = \sum_{i=1}^4 N_i T_i = [N] \{T^e\}$$

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Therefore equation 8 can be expressed like that contributing from all the elements then we can find out the v^e element for this we expressed is first we estimate for a one element and we assuming the one element having the 4 nodes.

So, contribution from the 4 nodes or in general one element we can form this matrix first and then we assemble for the all the elements so the summation of the all the elements. So, same

way it can be done for other cases also volume in this the surface over the surface and all this thing the different contribution. So, therefore, we have the m elements of which r elements have boundary domain as their face.

So, if you look into have to be look into that that whether this that one particular component of this particular expression of finite element formulation this part; that whether it is defined over the volume or it is defined over the surface. So, contribution from the surface boundary condition that is over the surface.

So, in that cases this particular heat interaction with the boundary the, which part of the boundary is basically or how many number of elements are is associated with this particular that has to be taken care. For example, in this case r number of elements exactly on the boundary which is may be interaction through the boundary.

So, therefore, r can be different as compared to the m ; m is defined for the whole domain total number of elements. So, then N_i over the domain so that is how we consider the m in this cases the whole number of elements the whole domain having total m number of elements. So, accordingly the contribution can be considered summation can be considered from vehicle to 1 to m .

Here contribution from 1 to r contribution from r , because r is the number of boundary elements which is boundary interaction is basically happening in this particular case. Now, considering a tetrahedron mesh that has only 4 nodes so therefore, only 4 nonzero values of N_i will exist for an a particular element definitely, in a tetrahedron elements mesh that are only 4 nodes. So, therefore, four non zero values of N_i will exist for an element.

So, basically one particular element one is from this the interaction from the each and every node to other node within the element will be 4 because there are 4 number of nodes one particular element and particular in case of tetrahedron mesh. Therefore, element will contribute terms only in 4 equations of a set and of a n equation expressed in equation 10.

So, therefore, element will compute terms only the 4 equations. So, therefore, we count one of the m of although we are doing the summation for e equal to 1 to m . So, total m number of elements, but nodes number are different is node number this is not equal to the element number. So, node numbers can be different as compared to the node number.

So, once we assemble this thing, so accordingly the node tracking of the node numbering is also there in their particular domain such that finally, we will be able to find out what is the temperature of each and every node point, so that is the node point.

So, that is a dimension of the equation in such a way that it depends on the what is the total number of nodes not total number of elements in this particular case. Now, this expression you have already seen the temperature variable can be expressed as a function into T the nodal temperature or summation of i equal to 1 is to for N i T i depend i equal to; i equal to 4 up to 4 because it is a tetrahedron element, if it is weak element then 4 can be replaced by the 8, number 8.

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Heat conduction analysis

If four nodes associated with an element 'e' are designated as 1, 2, 3, 4 for simplicity, the corresponding term-wise contribution from this element towards Eq. 10 will be:

(i) For first term:

$$\int_{V^e} k \left(\frac{\partial N_1}{\partial x} \frac{\partial [N]}{\partial x} \{T^e\} + \frac{\partial N_1}{\partial y} \frac{\partial [N]}{\partial y} \{T^e\} + \frac{\partial N_1}{\partial z} \frac{\partial [N]}{\partial z} \{T^e\} \right) dV$$
$$\int_{V^e} k \left(\frac{\partial N_2}{\partial x} \frac{\partial [N]}{\partial x} \{T^e\} + \frac{\partial N_2}{\partial y} \frac{\partial [N]}{\partial y} \{T^e\} + \frac{\partial N_2}{\partial z} \frac{\partial [N]}{\partial z} \{T^e\} \right) dV$$
$$\int_{V^e} k \left(\frac{\partial N_3}{\partial x} \frac{\partial [N]}{\partial x} \{T^e\} + \frac{\partial N_3}{\partial y} \frac{\partial [N]}{\partial y} \{T^e\} + \frac{\partial N_3}{\partial z} \frac{\partial [N]}{\partial z} \{T^e\} \right) dV$$
$$\int_{V^e} k \left(\frac{\partial N_4}{\partial x} \frac{\partial [N]}{\partial x} \{T^e\} + \frac{\partial N_4}{\partial y} \frac{\partial [N]}{\partial y} \{T^e\} + \frac{\partial N_4}{\partial z} \frac{\partial [N]}{\partial z} \{T^e\} \right) dV \quad (11)$$

$\frac{\partial T}{\partial x} = \sum [N] \frac{\partial T}{\partial x}$
 $\frac{\partial T}{\partial x} = \sum \left(\frac{\partial [N]}{\partial x} T \right)$

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So, now look into this thing if four nodes associated with the particular element e and they start designated as 1, 2, 3, 4 for the simplicity, the corresponding term wise contribution for this element contribution from this element for the in more explore this particular part how thus formulation can be done.

So, if you look into there are 4 node and a particular element. So, term can be represented like that $\frac{\partial T}{\partial x} = \sum [N] \frac{\partial T}{\partial x}$ this N is the shape function because this if you see d to the del T by del x that was the term actually. So, T we represent T equal to the shape function into nodal temperature.

So, then we can say the del T by del x can be write that del N, because N is the variable in terms of N we remember that when we express the shape function N can be represented in the form of a x y z if it is three dimensional two depending upon three dimensional two

dimensional problem, N can be expressed in terms of the coordinates and the as a variable x y and z .

So, therefore, it can be derivation can be possible here and in this case equal to T^e . So, in from that sense it is coming $\frac{\partial T}{\partial x}$ is replaced by this value. Similarly, for this thing N 1 and this is the x , this is for the $\frac{\partial N}{\partial z}$. All these cases we can see, but in same way that is the node 1, so if it that is change in the node 2, then N 2 will come node 3 N 3 will be coming node 4 N 4 will be coming. If it is a 8 node then N 5, N 6, N 7 up to N 8 will be there. So, that needs to be accounting look into this thing.

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Heat conduction analysis

- The terms of $\{T^e\}$ are nodal temperatures that do not vary within the element,
- Therefore, this vector is taken out of the integral sign and on re-arranging the remaining terms we obtain the elemental contribution in matrix form as:

$$\begin{bmatrix} h_{11}^e & h_{12}^e & h_{13}^e & h_{14}^e \\ h_{21}^e & h_{22}^e & h_{23}^e & h_{24}^e \\ h_{31}^e & h_{32}^e & h_{33}^e & h_{34}^e \\ h_{41}^e & h_{42}^e & h_{43}^e & h_{44}^e \end{bmatrix} \begin{Bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{Bmatrix} = [h^e] \{T^e\} \quad (12)$$

where,

$$h_{ij}^e = \int_{V^e} k \frac{\partial N_i}{\partial x_m} \frac{\partial N_j}{\partial x_m} dV$$

$i = 1, 2, 3, 4$
 $j = 1, 2, 3, 4$
 $m = 1, 2, 3$

So, all terminology first term we can explore further looking into all these components. Therefore, the terms T^e are nodal temperature that we have already explained this thing that do not vary within the element. So, nodal temperature does not vary within the element.

So, that is why we consider this as a constant, but n shape function we are assuming it is a variable. So, therefore, this vector is taken out of a integral sign that is true sign and rearranging the remaining terms we obtain the elemental contribution for elemental contribution in the matrix form like that.

So, therefore, rearranging all these things we can see that looking into this thing h_{11}, h_{12} term will be there, h_{13} and contribution these things $14, 21, 22, 23, 24$. So, basically the arrangement so it is interaction between the node 1 to node 4. So, different way you can see the interaction between node within the one element the interaction between $11, 12, 13$ like that 14 .

Similarly, $21, 22, 23, 24$ and the $41, 42, 43, 44$; like that there is interaction and each term can be like that, h_{11}, h_{12} this way. And all this contribution from the e indicates the elemental form and finally, this T_1 is the basically that tetrahedron element that is the having the 4 node.

So, therefore, the nodal temperature and 4 node is T_1, T_2, T_3 and T_4 . And in general we can say that h_e and the T is the nodal temperature in that form, but the general expression for h_{ij} equal to the integration over the $v_e k \frac{\partial N_i}{\partial N_j} \frac{\partial x_m}{\partial x_n}$, but in this cases m equal to 123 ; that means, and i equal to 1234 in this particular case.

So; that means, h_{11} , I can say that h_{11e} can be like that v_e and then $k \frac{\partial N_1}{\partial N_1} \frac{\partial x_m}{\partial x_n}$ or x_1 means x_1 means x_2 means y direction x_3 means z direction. So, that is why this formulation can be form also it is a j equal to 1 in this case 11 . Similarly, $12, 13$ like that, it can be represent in this way also in general. So, I think we can see this part also here.

So, $11, 12, 13, 14$ like that 11 . So, that is way we can represent in general way, but remember the bottom side is either a combination of the $11, 12, 13$. So, this is the general expression, but this one find out this thing there is a need to do the integration. So, over the

volume integration, but the numerical integration is actually required in this particular problem.

We will may be next time we will show how we can do the numerical integration or one particular form of the element how we can form this how we can form one particular element of this matrix in any kind of the problem. Specifically I try to explain in the heat transfer problem how this one element is formed.

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Heat conduction analysis

(ii) For 2nd term
 The element contribution towards the second term is made of four terms given as:

$$f_{Q_i}^e = - \int_{V^e} \dot{Q} N_i dV \text{ or vector } \{f_Q^e\} \quad i=1, 2, 3, 4$$

(iii) For 3rd and 4th terms
 The contribution towards the 3rd and the 4th terms can similarly be obtained as:

$$[\bar{h}^e] \{T^e\} \text{ and } \{f_q^e\}$$

where,

$$\bar{h}_{ij}^e = \int_{S^e} \alpha N_i N_j dS \quad f_{q_i}^e = \int_{S^e} q N_i dS \quad \text{and } i, j = 1, 2, 3, 4$$

The total contribution from an element 'e' is thus obtained as:

$$[h^e] \{T^e\} + [\bar{h}^e] \{T^e\} + \{f_Q^e\} + \{f_q^e\}$$

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Now, for the 2nd term also we can see that the f_{Q_i} similarly this expression can be represented like that the 3rd and 4th term also can be represented in generally $h^e T^e$ or you can see that f_{Q_i} ; that means, it is a expression see this is the this is all these cases is basically required to do some kind of the either integration over the surface or integration over the

volume, but all these cases we can do the numerical integration this thing, but how we can do the numerical integration we can show in the other lectures also.

So, therefore, total contribution in the matrix form can be write that h e this part, this is also part and this is the load part. So, that in the by with the application of the Galerkin weighted residue technique and in this cases we using this weighting function same as the shape function and from that shape function we can form the matrix form of a particular equation.

So, definitely with the weighting function all this application all this thing is required once you try to do the analysis the any kind of the problem which is defined in some governing equation which is driven by some governing equation or at the same time some boundary interaction is there.

So, that kind of problem we can put the weighted residue technique and the different matrix form we can form. Now, in more details one particular element what are the different elements; that means, this matrix can be formed that will show in the next class.

So, thank you very much for your kind attention