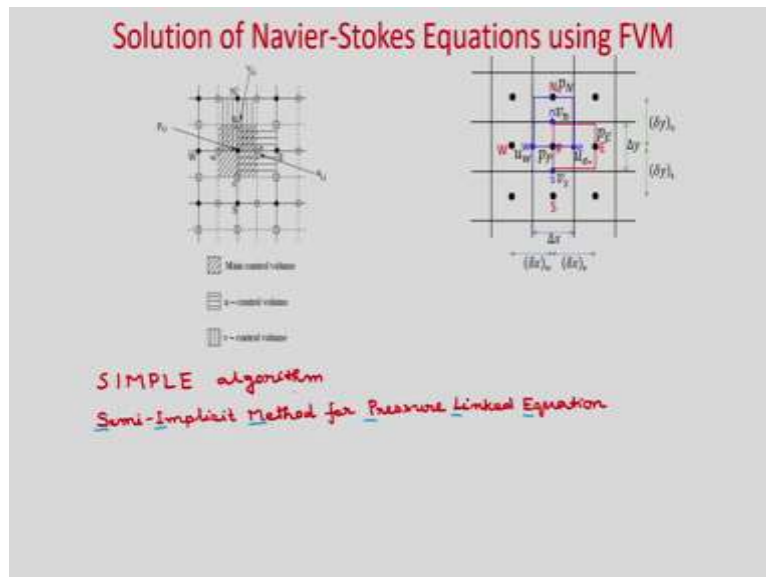


**Computational Fluid Dynamics for Incompressible Flows**  
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**Lecture 02**  
**Solution of Navier-Stokes Equations using FVM-2**

Hello everyone, so in last class, we integrated the pressure term or pressure gradient term appears in the Navier-Stokes equation using finite volume method and also we have integrated the continuity equation using finite volume method and we have shown why there is a need to go for staggered grid. So, today we will integrate the full Navier-Stokes equation using finite volume method in staggered grid.

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So, you can see that in staggered grid, the pressure is solved in the main control volume. So, you can see this is the main control volume and at cell centre capital P, this  $P_p$  is solved. Now, at the face centre of this control volume, small e, now, we have another this red colour cell. So, in that cell we solve for the u velocity for the face centre small e  $U_e$ .

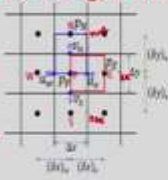
Similarly, the V velocity we solve in this blue colour control volume and at the face centre small n for the velocity  $V_n$  and similarly we solve  $V_s$  at this face centre, small s and  $U_w$ , this face centre w. So, we can see that, for this u velocity when you are solving in this control volume, the pressure difference  $P_e$  minus  $P_p$  is the natural driving force.

Similarly, for velocity  $V_n$ , pressure difference between  $P_n$  and  $P_p$  is the driving force for this velocity  $V_n$ . And for the main control volume  $p$ , you can see that we can satisfy the continuity equation,  $U_v$  minus  $U_w$  plus  $V_n$  minus  $V_s$  in that way. So, that is the advantage of using staggered grid. So, we will learn today simple algorithm due to Patankar and the main idea behind this simple algorithm is to create a discrete equation for pressure or related quantity called as pressure correction from the discrete continuity equation.

So, what is the full form of SIMPLE? So, we will learn today, SIMPLE algorithm. The full form is Semi Implicit Method for Pressure Link Equation. So, you can see this is the S I M P L E so this is called as simple algorithm and it was proposed by Professor SB Patankar. Now let us write the discretized momentum equation for U velocity in the control volume  $U_e$ .

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**Solution of Navier-Stokes Equations using FVM**



$$a_e U_e = \sum a_{nb} U_{nb} - \Delta x (P_e - P_w) + b_u \quad \dots (1)$$

$$a_n V_n = \sum a_{nb} V_{nb} - \Delta x (P_n - P_s) + b_v \quad \dots (2)$$

Let  $p^*$  represents the discrete pressure field which is used in the solution of the momentum equations.

$$a_e U_e^* = \sum a_{nb} U_{nb}^* - \Delta x (P_e^* - P_w^*) + b_u \quad \dots (3)$$

$$a_n V_n^* = \sum a_{nb} V_{nb}^* - \Delta x (P_n^* - P_s^*) + b_v \quad \dots (4)$$

Similar expressions may be written for  $U_w^*$  and  $V_s^*$ .

Subtract Eq(3) from Eq(1)

$$a_e (U_e - U_e^*) = \sum a_{nb} (U_{nb} - U_{nb}^*) - \Delta x \{ (P_e - P_e^*) - (P_w - P_w^*) \} \quad \dots (5)$$

$$a_n (V_n - V_n^*) = \sum a_{nb} (V_{nb} - V_{nb}^*) - \Delta x \{ (P_n - P_n^*) - (P_s - P_s^*) \}$$

We propose a correction to obtained velocity field such that the corrected values satisfy the continuity equation.

$$U_e = U_e^* + U_e'$$

$$V_n = V_n^* + V_n'$$

$$P = P^* + P'$$

$$U_e - U_e^* = U_e'$$

$$V_n - V_n^* = V_n' \quad \dots (6)$$

$$P - P^* = P'$$

Okay so, if you write that then already we have learned for the convection diffusion equation, similarly, you can write this equation as  $A_e U_e$ , now, we are not writing  $A_p U_p$  because we are solving this  $u$  velocity at small  $e$ . This is the face centre of the main control volume. So, we are writing  $U_e$  is equal to summation of  $A_{nb} U_{nb}$ , then the pressure gradient term, we have derived  $\Delta y (P_e - P_w)$  and some source term  $b_u$ .

And similarly, for the velocity  $V_n$  you can write  $a_n V_n$  is equal to summation of  $A_{nb} V_{nb}$  minus  $\Delta x (P_n - P_s)$  plus source term for the  $V$  momentum equation. So, you can see, so this when you are solving  $A_e U_e$ , so, this is the diagonal coefficient  $A_e$  and  $U_e$  is the velocity  $e$  in the face centred small  $e$ . So, now the summation of  $A_{nb} U_{nb}$ . So, this  $U_{nb}$

now it will contain the neighbours of  $U_e$ . So,  $U_e$  will be at this point, these are the neighbours and similarly at this point, then you have this point and also you have this point.

So, you can see that these are if you represent, so, it will be small  $e$  double  $E$ , then this will be  $u_e$ . Then this will be  $w$ , it is anyway  $w$  and this point, it will be  $u_w$ . So, in this neighbours you have to get the summation of  $A_{nb} U_{nb}$ . Similarly for summation of  $A_{nb} V_{nb}$  and when you are solving this equation, so initially pressure is unknown.

So now, let us assume some pressure for the initialization. So that will start with the assumed pressure field  $P^*$ . So let  $P^*$  represents the discrete pressure field which is used in the solution of the momentum equations. So,  $P^*$  is the pressure field then it will satisfy these discrete equations. So if you put it there, then we will get some velocity, which will be the provisional velocity. So,  $U_e^*$  and  $V_n^*$ .

So, we can write  $A_e U_e^*$  is equal to summation of  $A_{nb} U_{nb}^*$  minus  $\Delta y P_e^*$  minus  $P_p^*$  plus  $b_u$ . As we are assuming the pressure field,  $p^*$ , so obviously, after solving the momentum equation, we will get some provisional velocity. That is your  $u^*$ . So, we have written this equation as  $A_e V_e^*$  is equal to summation of  $A_{nb} U_{nb}^*$  minus  $\Delta y p^*$  minus  $P_p^*$  plus  $B_u$  where  $P^*$   $P_p^*$  are the assumed pressure field.

Similarly, for the  $y$  momentum equation you can write  $A_n V_n^*$  is equal to summation of  $A_{nb} V_{nb}^*$  minus  $\Delta x P_n^*$  minus  $P_p^*$  plus  $V_p$ . So, similar expression you can write for the West face  $U_w$  and the South face  $V_s$ . So similar expressions maybe written for  $U_w^*$  and  $V_s^*$ .

So, now this equation if you tell that equation number 1 and this is your 2. Now subtract 2, equation 2, subtract equation 2 from equation 1. So, what you will get? So, you can see, so if you subtract these equations from the equations 1, so you will get  $A_e U_e$  minus  $U_e^*$  is equal to summation of  $A_{nb} U_{nb}$  minus  $U_{nb}^*$  minus  $\Delta y P_e$  minus  $P_e^*$  minus  $P_p$  minus  $P_p^*$  and this will get cancelled the source term.

Similarly, you can write  $A_n V_n$  minus  $V_n^*$  is equal to summation of  $A_{nb} V_{nb}$  minus  $V_{nb}^*$  in  $V$  minus  $\Delta x$ , then  $P_n$  minus  $P_n^*$  minus  $P_p$  minus  $P_p^*$ . So now, let us introduce the velocity correction. So, what is velocity correction? So, this  $U_e$  minus  $U_e^*$  will tell us velocity correction. So, you can see, this  $u$  velocity will satisfy the continuity equation, but this  $U_e$  we have got the solution from the assumed pressure field which may not satisfy the continuity equation.

The difference between these two velocities we are calling as velocity correction. So, we propose a correction to star velocity field such that the corrected values satisfy the continuity equation. So, we will propose  $U_e$  star so, this way I will write. So, we are proposing a correction in the star velocity, so,  $U_e$  is equal to  $U_e$  star plus some correction we are making so that it will satisfy the continuity equation.

Similarly, you can write  $V_n$  is equal to  $V_n$  star plus  $V_n$  prime and similarly the pressure, so  $P$  will be  $p$  star plus  $p$  prime, okay. So, now you can see the difference  $U_v$  minus  $U_v$  star, you can write in terms of the velocity correction.

So,  $U_v$  star you can write the velocity correction and  $V_n$  minus  $V_n$  star you can write as  $V_n$  prime and  $P$  minus  $P$  star will be your  $P$  prime. So, these are the pressure correction and velocity corrections, okay so now these we can represent, these terms we can represent with the correction. So now, if this is equation 3 and this is 4.

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**Solution of Navier-Stokes Equations using FVM**

Equation (3) can be written as

$$a_e u_e' = \sum a_{nb} u_{nb}' - \Delta y (P_e' - P_p') - a_n v_n' = \sum a_{nb} v_{nb}' - \Delta x (P_n' - P_p') - \Delta y \Delta x \mu \nabla^2 u_e' = -\Delta y (P_e' - P_p')$$

$$a_n v_n' = -\Delta x (P_n' - P_p')$$

$$u_e' = -\frac{\Delta y}{a_e} (P_e' - P_p') = -d_e (P_e' - P_p') \quad \text{where } d_e = \frac{\Delta y}{a_e}$$

$$v_n' = -\frac{\Delta x}{a_n} (P_n' - P_p') = -d_n (P_n' - P_p') \quad d_n = \frac{\Delta x}{a_n}$$

$$u_w' = -\frac{\Delta y}{a_w} (P_p' - P_w') = -d_w (P_p' - P_w') \quad d_w = \frac{\Delta y}{a_w}$$

$$v_s' = -\frac{\Delta x}{a_s} (P_p' - P_s') = -d_s (P_p' - P_s')$$

The diagram shows a control volume with dimensions  $\Delta x$  and  $\Delta y$ . It is surrounded by neighboring cells. The central cell is labeled with  $P_p'$ . The east, west, north, and south faces are labeled  $P_e'$ ,  $P_w'$ ,  $P_n'$ , and  $P_s'$  respectively. Velocity corrections  $u_e'$ ,  $u_w'$ ,  $v_n'$ , and  $v_s'$  are shown as arrows pointing outwards from the control volume faces.

Now equation 3 can be written as. So, now we are introducing the pressure correction and velocity correction. So, it will be  $A_e U_e$  prime is equal to summation up  $A_{nb} U_{nb}$  prime minus  $\Delta y P_e$  prime minus  $P_p$  prime. And  $A_n V_n$  prime is equal to summation of  $a_{nb} V_{nb}$  prime minus  $\Delta x P_n$  prime minus  $P_p$  prime. And similar expression may be written for  $U_w$  prime and  $V_s$  prime.

So, here now we will make one important assumption. So here now we will make the important simplification, you can see this term summation of  $A_{nb} U_{nb}$  prime. So, if you are solving for the (pressure), if you are solving for the velocity correction,  $U_e$  prime at this small

face centre, at the face centre small  $e$ , then you need to know the velocity correction from the neighbour points as well, so this  $U_{nb}'$ .

So obviously, these neighbour points again it will involve the other neighbour points so it will be very cumbersome to calculate this  $U_e'$ . So now we will make this important simplification that will drop these terms. So these terms will make as 0, so now these two terms will drop. So, this is the important simplification and this is known as simple algorithm.

So, why it is semi-implicit, now let us understand, you see this is the implicit equation, it is fully implicit equation because  $U_e'$  it depends on the neighbor velocity  $U_{nb}'$ . But now we are dropping these terms so now some semi-implicitness is coming because it is not full-implicit. Okay as we are dropping this term, that is why this is known as semi implicit method for pressure linked equation.

So now, if you drop this term, so you can write the velocities in terms of only pressure correction. So, if you drop these terms, then you can write the velocities only in terms of the pressure correction. So, you can write  $A_e U_e'$  is equal to minus  $\Delta y$   $P_e'$  minus  $P_p'$  and  $A_n V_n'$  you can write as minus  $\Delta x$   $P_n'$  minus  $P_p'$ . So, now we can write  $U_e'$  as minus  $\Delta y$  by  $A_e$   $P_e'$  minus  $P_p'$  and this we will write as  $d_e$  into  $P_e'$  minus  $P_p'$  where  $d_e$  is equal to  $\Delta y$  by  $a$ . So, this is your face area and this is your diagonal coefficient  $A_e$ .

Similarly for  $V_n'$  what you can write? It will be minus  $\Delta x$  by  $n$   $V_n'$  minus  $P_p'$  is equal to  $d_n$  sorry here minus sign will be there equal to minus  $d_n$  into  $P_n'$  minus  $P_p'$  and  $d_n$  is equal to  $\Delta x$  by  $A_n$ . Now this velocity correction let us write for the west face and south face as well.

So, you can write  $U_w'$  so, at this  $W$  face we are writing for the velocity correction  $U_w'$ . So, this will be in terms of the pressure correction so, it will be just  $P_p'$  minus  $P_w'$ ,  $P_p'$  minus  $P_w'$ . So, this will be  $\Delta y$  by  $A_w$  so,  $W$   $P_p'$  minus  $P_w'$  and we will write as minus  $d_w$   $P_p'$  minus  $P_w'$  where  $d_w$  is  $\Delta y$  by  $A_w$ .

And similarly  $V_s'$  so, at this face centre we will solve for  $V_s$  and this will be  $V_s'$  is equal to minus  $\Delta x$  by  $A_s$ . And what is the pressure correction difference? It will be  $P_p'$  minus  $P_s'$ , so it will be  $p'$  minus  $P_s'$  is equal to minus  $d_s$   $P_p'$  minus  $P_s'$ .

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### Solution of Navier-Stokes Equations using FVM

$$\nabla \cdot (\rho \vec{u}) = 0$$

$$\int_V \nabla \cdot (\rho \vec{u}) dV = 0$$

$$\int_A \rho \vec{u} \cdot d\vec{S} = 0$$

$$\Rightarrow F_e - F_w + F_n - F_s = 0$$

$$F_e = \rho u_e \Delta y$$

$$F_w = \rho u_w \Delta y$$

$$F_n = \rho v_n \Delta x$$

$$F_s = \rho v_s \Delta x$$

We may write the face flow rates.

$$F_e^* = \rho u_e^* \Delta y$$

$$F_w^* = \rho u_w^* \Delta y$$

$$F_n^* = \rho v_n^* \Delta x$$

$$F_s^* = \rho v_s^* \Delta x$$

The corrected face flow rates

$$F_e = F_e^* + F_e'$$

$$F_w = F_w^* + F_w'$$

$$F_n = F_n^* + F_n'$$

$$F_s = F_s^* + F_s'$$

Now, let us write the discrete continuity equation. So, if you see that continuity equation, so it will be divergence of Rho U is equal to 0, so we integrate over the control volume, then you can write divergence of Rho U is equal to 0, dV is equal to 0 and if you convert to the surface integral, then it will be Rho u dot d s is equal to 0.

Now you can write in terms of mass flow rate Fe minus Fw plus Fn minus Fs is equal to 0. So this is the mass flow rate Fe, okay so F is your mass flow rate. So you can see Fe will be your Rho, if it is constant then you can write only Rho Ue delta y, Fw is Rho Uw delta y Fn is your Rho Un Vn delta x, we are writing for the uniform grid, so delta x is same and delta y is same.

So, it will be Rho Vs delta x and this minus sign you know, because U dot ds when you are doing so, obviously, you can see that the face normal is outward direction, so it is a negative x direction that is why it is minus and here also you are getting minus so, this is the continuity equation.

So now, you see that, obviously your velocities Ue, Uw, Vn and Vs will satisfy the continuity equation, but when we assume the pressure field P star and whatever provisional velocity we got, U star and V star those will not satisfy the continuity equation. So, now, this equation let us write in terms of the star quantity.

Now, we may write the face flow rates from the U star quantity, so, it will be Fe star is equal to Rho Ue star delta y. Fw star will be your Rho Uw star delta y and Fn star will be Rho Vn

star into delta x and F<sub>s</sub> star will be Rho V star into delta x. And now the corrected face flow rates will be now Fe is equal to Fe star plus Fe prime.

So, F<sub>n</sub> is equal to F<sub>n</sub> star plus F<sub>n</sub> prime, F<sub>w</sub> is equal to F<sub>w</sub> star plus F<sub>w</sub> prime and F<sub>s</sub> is equal to F<sub>s</sub> star plus F<sub>s</sub> prime. So, now, you can see from this equation Ue prime, Vn prime, Uw prime and Vs prime. So, this we have written in terms of the pressure correction only.

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**Solution of Navier-Stokes Equations using FVM**

$$F_e' = \rho u_e' \Delta y = -\rho d_e (P_e' - P_p') \Delta y = \rho d_e (P_p' - P_e') \Delta y$$

$$F_w' = \rho d_w (P_w' - P_p') \Delta y$$

$$F_n' = \rho d_n (P_p' - P_n') \Delta x$$

$$F_s' = \rho d_s (P_s' - P_p') \Delta x$$

$$F_e - F_w + F_n - F_s = 0$$

$$F_e^* + F_e' - F_w^* - F_w' + F_n^* + F_n' - F_s^* - F_s' = 0$$

$$\Rightarrow F_e' - F_w' + F_n' - F_s' + F_e^* - F_w^* + F_n^* - F_s^* = 0$$

$$\Rightarrow \rho d_e (P_p' - P_e') \Delta y - \rho d_w (P_w' - P_p') \Delta y + \rho d_n (P_p' - P_n') \Delta x - \rho d_s (P_s' - P_p') \Delta x + \Sigma F_j^* = 0$$

$$\Rightarrow (\rho d_e \Delta y + \rho d_w \Delta y + \rho d_n \Delta x + \rho d_s \Delta x) P_p' = \rho d_e \Delta y P_e' + \rho d_w \Delta y P_w' + \rho d_n \Delta x P_n' + \rho d_s \Delta x P_s' - \Sigma F_j^*$$

$$\Rightarrow a_p P_p' = a_e P_e' + a_w P_w' + a_n P_n' + a_s P_s' + (F_w^* - F_e^* + F_s^* - F_n^*)$$

$$\Rightarrow a_p P_p' = \Sigma a_{nb} P_{nb} + b$$

- Pressure correction equation

$$a_p = \Sigma a_{nb} \quad a_e = \rho d_e \Delta y \quad a_w = \rho d_w \Delta y \quad a_n = \rho d_n \Delta x \quad a_s = \rho d_s \Delta x \quad b = F_w^* - F_e^* + F_s^* - F_n^*$$

So, now, we will write the corrected mass flow rate Fe prime as Rho e Rho Ue prime delta y. So, now Ue prime you just write in terms of the pressure correction so, it will be minus Rho de Pe prime minus Pp prime into delta y. Or you can write negative sign if you take inside, then it will be Rho into de Pp prime minus Pe prime into delta y.

Similarly, Fw prime you can write Rho dw. So, it will be Pw prime minus Pp prime into delta y, Fn prime will be Rho dn Pp prime minus Pn prime delta x and Fs prime will be your Rho into ds into Ps prime minus Pp prime into delta x. So now, we have written the corrected mass flux, we have also written the star quantity mass flux F star, now let us put these into the main continuity equation.

So, what is the discrete main continuity equation? That is your Fe minus Fw plus Fn minus Fs is equal to 0. So if you put it, so what you are going to get? So Fe is Fe star plus Fe prime minus Fw star minus Fw prime, then Fn star plus Fn prime and minus Fs star minus Fs prime is equal to 0.

So now you can write  $F_e' - F_w' + F_n' - F_s'$ , so this we will write in terms of pressure correction and you have  $+F_e^* - F_w^* + F_n^* - F_s^*$  is equal to 0. Now, let us substitute the corrected mass flux in terms of the pressure correction. So, if you write that, so  $F_e'$  what is that? So, you can write  $\rho \int_{de} P_p' - P_e'$ .

And  $F_w'$  is  $-\rho \int_{dw} P_w' - P_p'$  here  $\Delta y$  will be there and here  $\Delta y$ , then  $F_n'$  is  $\rho \int_{dn} P_p' - P_n'$  into  $\Delta x$  and  $-\rho \int_{ds} P_s' - P_p'$  into  $\Delta x$ . Now, you can see this is your, you can write  $\sum F_f^*$ , all the faces it is the star velocities when it satisfied the continuity equation. So, you have written summation of  $F_s^*$ .

So, initially this will not be 0 summation of  $F_s^*$ , but when at convergence your velocity correction will be 0 that time your  $U_e$  will become  $U_e^*$  and hence this will become 0. So now, you write the equation for pressure correction. So, now all the  $P_p$  term you just take together, so you can see, so this is your  $P_p$  term, this is your  $P_p$  term,  $P_p$  and  $P_p$ .

So, this you take in the left hand side and all other terms you in the right hand side, so that you can write in terms of  $A_p \phi_p$ . So, you can see these so, you can see the coefficient is  $\rho \int_{de} \Delta y$  for this it is minus-minus plus so, it will be plus  $\rho \int_{dw} \Delta y$  for this it is plus  $\rho \int_{dn} \Delta x$  and for this it is plus, minus-minus plus  $\rho \int_{ds} \Delta x$ . So, this is the coefficient for the  $P_p'$ .

Now you, all other times you take in the right hand side, so for  $P_e$ , so it is minus so it will be plus, so  $\rho \int_{de} \Delta y$  and it is for  $P_e'$  This is your minus, so this will be plus so it will be  $\rho \int_{dw} \Delta y P_w'$ . Then you have north so, it is minus so this side will become plus  $\rho \int_{dn} \Delta x P_n'$ . And similarly for south face  $\rho \int_{ds} \Delta x P_s'$ .

So, we have taken all the terms right hand side and these also you have taken the right hand side, so it will be minus summation of  $F_f^*$ . So, now you just write in terms of coefficient, diagonal coefficient  $A_p$  in the left hand side, so it will be  $A_p P_p'$  is equal to  $A_e P_e' + A_w P_w' + A_n P_n' + A_s P_s' - \sum F_f^*$  or you can write plus  $A_w^* - F_e^* + F_s^* - F_w^*$ .

At minus  $F_f^*$  we have written so, it will be  $F_w^* - F_e^*$ . So, now you can write it as  $A_p P_p'$  is equal to summation of  $A_{nb} \phi_{nb}$  plus source term B, sorry not phi, summation of  $A_{nb} P_{nb}'$  plus source term B.



So, now you can see that we have written this equation for pressure correction. So, this equation is known as pressure correction equation, where  $A_p$  is equal to summation of  $A_{nb}$ , you can see your  $A_e$  is your  $\rho d_e \Delta y$   $A_w$  is  $\rho d_w \Delta y$ ,  $A_n$  is  $\rho d_n \Delta x$  and  $A_s$  is  $\rho d_s \Delta x$ . So, you can see in left hand side you have  $A_e u_e^* + A_w u_w^* + A_n u_n^* + A_s u_s^*$  so,  $F_e$  is equal to summation of  $A_{nb} u_n^*$  and  $b$  is your  $F_e$ , so  $b$  is equal to  $F_w^* - F_e^* + F_s^* - F_n^*$ . So, this is sorry this will be north, so plus  $F_s^* - F_n^*$ .

So, now you can see that you can solve this equation. Once you solve this equation, you will get the pressure correction. Now, if pressure corrections are known now you can find the velocity correction and that velocity correction now, you can actually use to correct the velocity with the  $U^*$  star, because we assume the pressure  $P^*$  star, we solved for the velocities  $U^*$  star and  $V^*$  star and now, once we know the correction, then we can add  $U^*$  star plus  $U'$  prime and  $V^*$  star plus  $V'$  prime so, that we get the correct velocity field  $U$  and  $V$ .

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**Solution of Navier-Stokes Equations using FVM**

**SIMPLE algorithm**

1. Guess the pressure field  $P^*$
2. Solve for  $u^*, v^*$   
 $a_e u_e^* = \sum a_{nb} u_{nb}^* - a_p (P_e^* - P_p^*) + b_u$   
 $a_n u_n^* = \sum a_{nb} u_{nb}^* - a_p (P_n^* - P_p^*) + b_u$
3. Calculate  $\sum F_j'$
4. Solve the pressure correction equation to obtain  $P'$   
 $a_p P_p' = \sum a_{nb} P_{nb}' + b$       $b = -\sum F_j'$
5. Correct  $u, v, P$       $P = P^* + P'$       $u = u^* + u'$       $v = v^* + v'$
6. Check the convergence.  
 If not converged, go to step 1 with  $P^* = P$   
 otherwise exit.

$P = P^* + \alpha P'$   
 $\alpha = 0.6 - 0.2$

So now, let us write the algorithm whatever we have derived today for the simple algorithm. So first is guess the pressure field  $P^*$ . Then you solve for  $U^*$  star and  $V^*$  star. So what  $U^*$  star  $V^*$  star so you can write  $A_e u_e^*$  is equal to summation of  $A_{nb} u_n^*$  minus  $\Delta y (P_e^* - P_p^*)$  with sum source term  $B_u$ .

Similarly,  $A_n v_n^*$  is equal to summation of  $A_{nb} v_n^*$  is equal minus  $\Delta x (P_n^* - P_p^*)$  plus  $b_v$ . So, once you solve the equation for  $U^*$  star  $V^*$  star obviously, you can calculate the summation of  $F_f^*$  which appears in the pressure correction equation, right.

So, once these are calculated, you can calculate summation of  $F_f^*$ . So now, solve for pressure correction equation to obtain  $P'$ .

So what is that equation we have written?  $A_p P_p'$  is equal to summation of  $A_{nb} P_{nb}'$  plus source term summation of  $F_f^*$  so that is your  $b$ , where  $b$  is your minus of summation of  $F_f^*$ . So now, once you know the pressure correction now you correct the velocities, so correct  $U$ ,  $V$  and  $P$  so, you can write  $P$  is equal to  $P^*$  plus  $P'$ . So, now this is the guess pressure for the next iteration and  $U$  is equal to  $U^*$  plus  $U'$  and  $V$  is equal to  $V^*$  plus  $V'$ .

Now, you see whether, now you check whether your continuity equation is satisfied or not whether summation  $F_f^*$  is equal to 0 or not. If not, then you take this pressure field as the guess pressure field for the next iteration and repeat the algorithm. So 6, check the convergence, if not converged go to step 1 with, now you make  $P^*$  is equal to  $P$ .

So, whatever  $p$  you have calculated with  $P^*$  plus  $P'$  so these will be used as a  $P^*$  for the next iteration otherwise exit. So, today we have learned the simple algorithm due to Patankar. So, main idea of this simple algorithm is to create one equation for pressure or pressure like equation like pressure correction from the continuity equation.

So, today we started with the staggered grid, we solved the velocities  $U_e$ ,  $U_w$ ,  $V_n$  and  $V_s$  with the guess pressure field  $P^*$ . So, you got some provisional velocity  $U^*$  and  $V^*$ , obviously, this will not satisfy that continuity equation. So, we subtracted  $U_e$  minus  $U_w$  and wrote the equation for the velocity correction.

So, but in the velocity correction when we wrote in the right hand side, you have the summation of  $A_{nb} U_{nb}'$  and summation of  $A_{nb} V_{nb}'$  in the  $V$  momentum equation. So, as we have dropped these terms so, now it has become semi implicit, it is no longer full implicit. Now, we have retained the velocity correction in terms of the pressure correction only.

We substituted these velocity correction in the terms of corrected mass flow rate to satisfy the continuity equation and we have derived the pressure correction equation. And that pressure correction equation once you solve, you will get the  $P'$  and once you know that  $P'$  you can calculate the velocity correction  $U'$  and  $V'$ .

And with those velocity corrections under pressure correction, you can update the velocity  $U$  and  $V$  and  $P$ . So, if you check for the convergence, if it is not converged, then this  $P$  you take a  $P^*$  for the next iteration. So, as we have dropped that term summation of  $A_{nb} U_{nb}^*$   $A_{nb}$ , so pressure may diverge during the solution of the pressure correction equation.

So, pressure correction equation may diverge for that you can use some under relaxation factor while correcting the pressure. So, where you have written this  $P$  is equal to  $P^*$  plus  $P'$ , you can use actually  $P$  is equal to  $P^*$ . And you would use some under relaxation factor  $\alpha$  into  $p'$  and these under relaxation you can take in the range of 0.6 to 0.8 as you have dropped the summation of  $A_{nb} U_{nb}^*$ , for that reason, it tends to diverge. So if you use some under relaxation then it will not diverge. Thank you.