

Computational Fluid Dynamics for Incompressible Flows
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Module 1: Introduction to Computational Fluid Dynamics
Lecture 2: Basic equations of fluid dynamics and heat transfer

Hello everyone, in today's class we will discuss about the basic equations of fluid mechanics and heat transfer in basic fluid dynamics course and basic heat transfer course you might have derived these equations. So we will not derive in this class these equations only will write down the governing equations of fluid flow and heat transfer. First will write down the fluid flow equations for incompressible and Newtonian fluid flow.

(Refer Slide Time: 1:02)

Incompressible Flow equation in Cartesian Coordinate

Assumptions:

- i) incompressible flow
- ii) Newtonian fluid flow
- iii) constant properties

$\vec{u} = u\hat{i} + v\hat{j} + w\hat{k}$

Continuity equation (Conservation of mass)

$$\nabla \cdot \vec{u} = 0$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

2D $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$

Momentum equations (Conservation of momentum)

Navier-Stokes equations

$$\frac{\partial (\rho \vec{u})}{\partial t} + \nabla \cdot (\rho \vec{u} \vec{u}) = -\nabla \bar{P} + \nabla \cdot (\mu \nabla \vec{u}) + \rho \vec{b}$$

ρ - density μ = dynamic viscosity
 \bar{P} - pressure \vec{b} = body force

$\frac{\partial \vec{u}}{\partial t} + \nabla \cdot (\vec{u} \vec{u}) = -\frac{1}{\rho} \nabla \bar{P} + \nu \nabla^2 \vec{u}$ - constant properties
 - negligible body force

2D

x-mom eqn: $\frac{\partial u}{\partial t} + \frac{\partial (u^2)}{\partial x} + \frac{\partial (uv)}{\partial y} = -\frac{1}{\rho} \frac{\partial \bar{P}}{\partial x} + \nu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$

y-mom eqn: $\frac{\partial v}{\partial t} + \frac{\partial (uv)}{\partial x} + \frac{\partial (v^2)}{\partial y} = -\frac{1}{\rho} \frac{\partial \bar{P}}{\partial y} + \nu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right)$

} conservative form

So incompressible flow equations in Cartesian coordinate, okay so if we consider a Cartesian coordinate, let us say this is your x, this is your y and this is your z, so respectively will define the velocities in x direction u, in y direction v and in z direction w. So, if you consider a velocity vector u then this is we can write u is the velocity in the x direction then the unit vector in that direction i, v, j, v is the velocity in the y direction and w.

So will have some assumptions to write the governing equations, so one assumption already we have told that it is incompressible flows that means density is constant or you can tell that mac number is less than 0.3 Will also consider Newtonian fluid flow and will consider

constant properties, so with those assumptions if you write down the governing equations. So the assumptions we have taken one is obviously incompressible flow, second is Newtonian fluid flow and we can write with constant properties.

So in fluid flow equations, so will first write the continuity equation which you can derive from the conservation of mass, right. So will write the continuity equation first, continuity equation okay, so you can derive it from conservation of mass, so it will conserve the mass, right, so it is conservation of mass. So, as it is incompressible flow so it will be we just in vector form divergence of, so we can write this continuity equation for incompressible flow in vector form as divergence of u is equal to 0.

So we can write $\text{Del } u \text{ by Del } x \text{ plus Del } v \text{ by Del } y \text{ plus Del } w \text{ by Del } z$ is equal to 0. So, if you write this equation for 2 dimensional then it will be just $\text{Del } u \text{ by Del } x \text{ plus Del } v \text{ by Del } y$ is equal to 0. So if you write this equation for 2 dimensional case then it will be $\text{Del } u \text{ by Del } x \text{ plus Del } v \text{ by Del } y$ is equal to 0. So, this is the continuity equation.

Now, will write the momentum equations, so in momentum equation we conserve the momentum. So, momentum equations, conservation of momentum, so as we are using incompressible flow and for Stokesian fluid, we can write the Navier-stokes equations. So, this is also known as Navier-Stokes equations, Navier-stokes equations okay will write in vector form, first will write in general so $\text{del by del } t \text{ rho } u \text{ plus divergence of the rho } u, u$ is equal to $\text{minus grad } p \text{ plus divergence of } \mu \text{ grad } u \text{ plus rho } b$, okay.

So where ρ is your density of the fluid okay and μ is the viscosity of the fluid, it is dynamic viscosity okay. So it is dynamic viscosity. So you can write μ is equal to dynamic viscosity of the fluid. And p , p is your pressure. Okay so p is your pressure and b is the body force, body force. So you can have gravity as body force okay or if you have a multi-physics problem, then electromagnetic force or magnetic force you can have as source term or body force term.

So, this equation now for the constant properties if you write down this equation, it will be $\text{Del } u \text{ by Del } t$. So, ρ you can take it outside and divide both sides then divergence of u is equal to $\text{minus } 1 \text{ by } \rho \text{ grad } p \text{ plus}$. So, if μ is constant you can take it outside and μ by ρ will be μ . So, $\text{grad square } u$, okay this equation what we are writing constant properties and no body force or negligible body force, okay negligible body force.

So, for a 2 dimensional situations you can write down these equations u momentum equation and v momentum equation or x momentum equation and y momentum equation. So, for 2D, 2 dimensional situation you can write x momentum equation as $\text{Del } u \text{ by Del } t \text{ plus Del } u \cdot u \text{ by Del } x \text{ plus Del } u \cdot v \text{ by Del } y$ is equal to minus 1 by rho, so obviously in the x direction. So, pressure gradient will be $\text{Del } p \text{ by Del } x \text{ plus Nu Del }^2 u \text{ by Del } x \text{ square plus Del }^2 u \text{ by Del } y \text{ square}$.

Okay similarly, y momentum equation you can write as $\text{del } v \text{ by del } t \text{ plus del } u \cdot v \text{ by del } x \text{ plus del } v \cdot v \text{ by del } y$ is equal to minus 1 by rho $\text{del } p \text{ by dal } y$ is the pressure gradient in the y direction plus $\text{Nu del }^2 v \text{ by del } x \text{ square plus del }^2 v \text{ by del } y \text{ square}$ okay. So, you can see the second term and third term we have written the velocities inside the derivative. So, these form are known as conservative form of the governing equations, conservative form, okay.

So, now let us write these equations for steady 2 dimensional flow in non-conservative form. So, if you do so, then if it is steady then this term and this term you can drop down and these you can see how you can write.

(Refer Slide Time: 9:52)

2-D steady flow non-conservative form
 $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$

$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + \frac{\partial u}{\partial t} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$

$v \frac{\partial v}{\partial x} + u \frac{\partial v}{\partial y} + \frac{\partial v}{\partial t} = -\frac{1}{\rho} \frac{\partial p}{\partial y} + \nu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right)$

1-D Navier-Stokes equation without pressure term

Burger's equation
 For a given $u(x,t)$ and kinematic viscosity, ν

Viscous Burger's equation
 $\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = \nu \frac{\partial^2 u}{\partial x^2}$

Inviscid Burger's equation
 $\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = 0$
 - non linear model eqn

So, if you consider to 2D steady flow okay and in non-conservative form we are writing, in non-conservative form we want to write, conservative form. So, if you write in this form, so, you will actually invoke the continuity equation and you know this for 2 dimensional situation $\text{del } u \text{ by del } x \text{ plus del } v \text{ by del } y$ is equal to 0 is continuity equation and you will get $\text{del } u \text{ by del } x$ (okay) plus $u \text{ del } u \text{ by del } x$ then you will get $u \text{ del } u \text{ by del } y$ plus, 1 minute.

So $u \frac{\partial v}{\partial y} + v \frac{\partial u}{\partial y}$ is equal to $-\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}$ okay. So, if you do that, so, you can see these 2 terms okay if you take u common then it will be $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}$. So, now you can see that it is a continuity equation. So, for incompressible flows obviously, this will become 0, okay. So, this will become 0.

So, these 2 terms will become 0 combinedly, because it is actually continuity equation. So, you can write the equation as $u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y}$ is equal to $-\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}$. So, this is the x momentum equation in non-conservative form for 2 dimensional steady flow.

Similarly, you can write the y momentum equation. Similarly, you can write y momentum equation as $u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y}$ is equal to $-\frac{1}{\rho} \frac{\partial p}{\partial y} + \nu \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2}$ okay. So, these equations are written in non-conservative form. Now let us write the 1 dimensional okay 1D may be a stoke equation without pressure term. Okay because this is a very simple equation and we consider it as model equation in our CFD course. So that we can discretize this equation using different scheme.

So, it is a model equation 1 dimensional unsteady Navier-stokes equation without pressure term. So, obviously you can write it as, so it is actually known as Burgers equation. So, it is a fundamental partial differential equation from fluid mechanics and it relates to the 1 dimensional Navier-Stokes equation for incompressible flow with the pressure term removed.

So, for a given u which is function of one space coordinate x and time and kinematic viscosity, kinematic viscosity ν you can write this equation viscous burgers equation, viscous burgers equation as $\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x}$ is equal to $\nu \frac{\partial^2 u}{\partial x^2}$ okay. So, you can see here you have the temporal term $\frac{\partial u}{\partial t}$ okay you have the convective term as well as you have the diffusion term okay.

So, it represents a model equation, where you have all the terms involved and it is simple equation where pressure term is removed. And similarly, you can write in burgers equation just dropping the conductive term sorry you can write the inviscid burger equation dropping the diffusion term. So, this is your convective term and this is your diffusive term.

Now, you can write inviscid burgers equation dropping a diffusive term, so, you can write simple $\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x}$ is equal to 0 okay. So, this is kind of a wave

equation 1 dimensional wave equation with a varying speed u . So, this u is actually wave speed which is varying, so obviously this is known as nonlinear model equation, nonlinear model equation.

(Refer Slide Time: 16:51)

Handwritten mathematical derivations:

$$\frac{\partial u}{\partial t} + c \frac{\partial u}{\partial x} = 0$$

c - const wave speed
 ↳ first order wave equation

$$\frac{\partial u}{\partial t} = -c \frac{\partial u}{\partial x}$$

$$\frac{\partial^2 u}{\partial t^2} = -c \frac{\partial}{\partial x} \left(\frac{\partial u}{\partial t} \right) = -c \frac{\partial}{\partial x} \left(-c \frac{\partial u}{\partial x} \right) = c^2 \frac{\partial^2 u}{\partial x^2}$$

↳ 2nd order wave equation

Stoke's equation
 Reynolds number, $Re = \frac{\rho U L}{\mu}$ $Re < 1$
 Inertia terms may be dropped from Navier-Stokes eqs
 creeping flow approximations

$$\nabla \cdot \vec{u} = 0$$

$$\frac{\partial(\rho \vec{u})}{\partial t} = -\nabla p + \nabla \cdot (\mu \nabla \vec{u}) + \rho \vec{b}$$

Now, if you consider u as a constant speed some way speed c then the equation you can write as $\text{Del } u \text{ by Del } t \text{ plus } c \text{ Del } u \text{ by del } x$ is equal to 0, if c is constant okay, wave speed then this equation is known as first order wave equation okay and you can see this is linear because c is constant, so it is a linear equation.

And now, we can write $\text{Del } u \text{ by Del } t$ is equal to minus $c \text{ Del } u \text{ by Del } x$. If you take the time derivative, in both sides, then you can write $\text{Del }^2 u \text{ by Del } t \text{ square}$ is equal to minus c , c is constant. So you can take it outside, you change the variable so you can write $\text{Del of del } x \text{ of Del } u \text{ by Del } t$ because we are taking the time derivative.

Now, you can substitute $\text{Del } u \text{ by Del } t$ with this equation, so you can write $c \text{ Del of del } x$ minus $c \text{ Del } u \text{ by Del } x$. So, you can see now it will be minus-minus plus and c square $\text{Del }^2 u \text{ by Del } x \text{ square}$. So, you got this equation $\text{del }^2 u \text{ by del } t \text{ square}$ is equal to c is the speed c square $\text{del }^2 u \text{ by del } x \text{ square}$ and this is known as second order wave equation, second order wave equation.

So, now, if you consider the full Navier-Stokes equations and if it is very low Reynolds number flow, Reynolds number, what is the Reynolds number? Reynolds number is the ratio of inertia force by viscous force. If the Reynolds number is very low, then your inertia force is very low, so viscous force is dominant.

In that case, you can drop the convective term from the Navier-Stokes equation and flow is known as creeping flow. So, this equation is known as Stokes equations, Stokes equation. So Stokes equation, so here Reynolds number, okay Reynolds number is very small, okay Re is equal to ρ some characteristic velocity u , characteristic length L divided by viscosity μ and ρ is the density.

So if Reynolds number is less than 1 then inertia term you can drop because viscous force will dominate. Okay so inertia, inertia terms may be dropped from Navier-Stokes equation, from Navier-Stokes equation. So, this is a creeping flow approximation, Reynolds number less than 1, so this is your creeping flow approximation. So, in that case you can write the governing equations as obviously the continuity equation will be as it is and momentum equation will be just $\nabla \cdot \vec{u} = 0$.

So, inertia term may not be there, you just write the pressure gradient term plus the viscous term and obviously you can have the body force term. So, now if you have a high Reynolds number flow, okay so in high Reynolds number flow inertia force will be dominating. So, in that case you can drop the viscous term and that equation is known as Euler equation.

(Refer Slide Time: 21:06)

Euler equation
 very high Reynolds number flow
 the viscous terms may be dropped from the Navier-Stokes equations

$$\nabla \cdot \vec{u} = 0$$

$$\frac{\partial(\rho \vec{u})}{\partial t} + \nabla \cdot (\rho \vec{u} \vec{u}) = -\nabla p + \rho \vec{b}$$

Boundary Layer approx
 2-D steady incompressible flow

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = U_\infty \frac{dU_\infty}{dx} + \nu \frac{\partial^2 u}{\partial y^2}$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = \nu \frac{\partial^2 v}{\partial y^2}$$

$$\frac{\partial p}{\partial y} = 0$$

U_∞ = c for flow over flat plate

Diagram: A schematic showing a flat plate with a boundary layer. The free stream velocity is U_∞ . The boundary layer thickness is δ . The region near the plate is labeled as the "viscous region" and the region further away as the "inviscid region". The "edge of BL" is indicated. The boundary layer thickness is also labeled as δ -BL thickness. The conditions $\frac{\delta}{L} \ll 1$ and $Re \gg 100$ are noted.

So, will write now Euler equation where you have a high Reynolds number flow, so Reynolds number is very high okay. So, in that case the viscous terms can be or so, Euler equation we can write for high Reynolds number flow, very high Reynolds number flow, Reynolds number flow. So, in that case you can drop the viscous term, so the viscous term

may be dropped from the Navier-Stokes equation. So we can write the continuity equation will be as it is, only the momentum equation you can drop the viscous term.

So, you can write as $\frac{d\rho u}{dt}$ plus divergence of ρu is equal to minus $\text{grad } p$. So, there will be no viscous term just ρb . Now, if you consider a fluid flow, over a flat plate then you can have the boundary layer flow. So, already you have started the boundary layer equations, so will write down the boundary layer equation.

So, obviously boundary layer flow you can see that due to the no slip condition because velocities of those fluid particles sitting on the solid wall will be 0. So, from 0 to the free stream velocity there will be velocity gradient and you can distinct two different regions, one is viscous region okay where velocity variation will be there and you can have the inviscid region outside these boundary layer, edge of the boundary layer that is known as inviscid region.

So, with these certain assumptions, you can write the Navier stokes equation in a droppings you can write the Navier stokes equation dropping some term. So, that is known as boundary layer equations and the assumptions for writing this boundary layer equation is that there is no flow separation and the boundary layer thickness is much-much smaller than the characteristic length and if it is a high Reynolds number flow.

So, for that you can write the boundary layer equation and you can write for 2D steady incompressible flow. So, if you consider a flat plate you have free stream velocity at u infinity. So, when it will flow over this flat plate there will be one region which is known. So, there will be a distinct region where you will have viscous region and another is inviscid region.

So, in inviscid region your velocity will be at free stream velocity. So, whatever free stream velocity you have that will be your free stream velocity and inside this viscous region there will be change in the velocity from 0 to free stream velocity okay.

So, this is known as the edge of boundary layer and the distant at any location x , if it is x the distance of this edge of boundary layer is known as δ which is your boundary layer thickness, boundary layer thickness. So with δ and L is the length of the plate then $\frac{\delta}{L}$ is much-much smaller than 1 and it is valid when you have a Reynolds number greater than 100 okay.

So for that you can write the equation, continuity equation $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}$ is equal to 0 and you can have the boundary layer equation $\frac{\partial^2 u}{\partial x^2} + v \frac{\partial u}{\partial y}$ is equal to free stream velocity $u_\infty \frac{du_\infty}{dx}$ that you can write the pressure gradient in terms of the free stream velocity plus $\frac{1}{2} \frac{d}{dx} (u_\infty^2)$, so here from the viscous term $\frac{\partial^2 u}{\partial x^2}$ is dot because that is much-much smaller than the $\frac{\partial^2 u}{\partial y^2}$.

So, you can have this $\frac{\partial^2 u}{\partial y^2}$ and for flow over flat plate as u_∞ is constant. So, this will be 0 for flow over flat plate. Okay so, you can have the equation as $\frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \frac{\nu}{l} \frac{\partial^2 u}{\partial y^2}$ and you have $\frac{\partial p}{\partial y} = 0$. These are the equations of fluid flow. So, now, another transport equation will derive from the Navier stokes equation.

(Refer Slide Time: 27:12)

Vorticity transport equation
two-dimensional flow

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \quad \text{- x momentum eqn}$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial y} + \nu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) \quad \text{- y momentum eqn}$$

$$\frac{\partial}{\partial t} (\text{x mom eqn}) - \frac{\partial}{\partial x} (\text{y mom eqn})$$

vorticity $\omega = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$

$$\frac{\partial \omega}{\partial t} + u \frac{\partial \omega}{\partial x} + v \frac{\partial \omega}{\partial y} = \nu \left(\frac{\partial^2 \omega}{\partial x^2} + \frac{\partial^2 \omega}{\partial y^2} \right) \quad \omega$$

- vorticity transport eqn

Stream-function equation

$$u = \frac{\partial \psi}{\partial y} \quad v = -\frac{\partial \psi}{\partial x}$$

$$\omega = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = -\frac{\partial^2 \psi}{\partial x^2} - \frac{\partial^2 \psi}{\partial y^2}$$

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = -\omega$$

So, if you have 2 dimensional unsteady Navier stokes equation, then we can write the, derive the vorticity transport equation, vorticity transport equation okay. So, in vorticity transport equation, how can you derive? So, you have the momentum equations, so you have momentum equations $\frac{\partial u}{\partial t}$, so 2 dimensional flow okay.

So, we are writing $\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u}{\partial x^2} + \nu \frac{\partial^2 u}{\partial y^2}$. So, this is the x momentum equation. Now, if you write the y momentum equation you will get $\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = \frac{1}{\rho} \frac{\partial p}{\partial y} + \nu \frac{\partial^2 v}{\partial x^2} + \nu \frac{\partial^2 v}{\partial y^2}$

equal to $-\frac{1}{\rho} \frac{\partial p}{\partial y} + \nu \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2}$.

So you can see that this is your x momentum equation and this is your y momentum equation okay. So, now, if you do this mathematical algebra $\frac{\partial}{\partial y}$ of x momentum equation minus $\frac{\partial}{\partial x}$ of y momentum equation then you can write down this equation as $\frac{\partial}{\partial t} \omega$ sorry. So, you can write this equation with the vorticity if you define ω as $\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$. So, vorticity we are defining ω sometime in book you will get this as a angular velocity, but in this case we are defining ω as the vorticity.

Okay so, vorticity is equal to 2 into angular velocity. So, vorticity is $\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$, if you do this mathematical algebra, you can write this equation as $\frac{\partial \omega}{\partial t} + u \frac{\partial \omega}{\partial x} + v \frac{\partial \omega}{\partial y} = \mu \nabla^2 \omega$ and what you are doing actually, you are actually canceling this pressure term. So, doing this mathematical algebra you can see $\frac{\partial}{\partial y} \frac{\partial p}{\partial x}$ so it will be $\frac{\partial^2 p}{\partial x \partial y}$ and this term will be $\frac{\partial}{\partial x} \frac{\partial p}{\partial y}$, so it will be canceled.

So, you are actually canceling this pressure term and you will have $\mu \nabla^2 \omega$ okay and this equation is known as Vorticity transport equation. So, this equation along with the stream function equation if you solve then you can have the, you can solve the fluid flow equation.

So stream function equation now you define the stream function. So, u is defined as $\frac{\partial \psi}{\partial y}$ and v as $-\frac{\partial \psi}{\partial x}$. So, you have the ω which is your $\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$. So, you can see that if you do the $\frac{\partial v}{\partial x}$ it will be $-\frac{\partial^2 \psi}{\partial x^2}$ and $-\frac{\partial u}{\partial y}$ it will be $-\frac{\partial^2 \psi}{\partial y^2}$, then you can solve $\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = -\omega$. So, this is your stream function equation.

So, if you solve this equation you can get the value of ψ and if you solve the ψ you can find the velocity u and v. Once you solve the u for the u v, you can solve this vorticity transport equation because u v are known. So, in that way you can also solve the fluid flow equations.

Now, let us consider the energy equation, will now have the conservation of energy and will write down the energy equation in terms of temperature.

(Refer Slide Time: 32:07)

Energy equation (conservation of energy)

$$\frac{\partial}{\partial t} (\rho c_p T) + \nabla \cdot (\rho c_p \vec{u} T) = \nabla \cdot (k \nabla T) + q''' + \frac{\mu \Phi}{\rho c_p}$$

\uparrow thermal conductivity \uparrow heat generation per unit volume
 \uparrow viscous dissipation term

- constant properties
 - neglecting viscous dissipation term

$$\frac{\partial T}{\partial t} + \nabla \cdot (\vec{u} T) = \alpha \nabla^2 T + \frac{q'''}{\rho c_p}$$

$\alpha = \frac{k}{\rho c_p}$ thermal diffusivity

2-D

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) + \frac{q'''}{\rho c_p}$$

So, now we are writing energy equation, conservation of energy and we are going to write this equation in terms of temperature. So, it will be $\frac{\partial}{\partial t} (\rho c_p T) + \nabla \cdot (\rho c_p \vec{u} T) = \nabla \cdot (k \nabla T) + q''' + \frac{\mu \Phi}{\rho c_p}$ okay.

So, here k is the thermal conductivity of the fluid thermal conductivity and q''' is the heat generation per unit volume, heat generation per unit volume and this is the viscous dissipation term, viscous dissipation term okay due to the shear there will be convection of mechanical energy to intermolecular energy which in turn will rise the temperature and $\frac{\mu \Phi}{\rho c_p}$ is the viscous dissipation function, so, that I am not going to write.

So, if you can neglect this viscous dissipation term and write this equation for a constant properties, then you can write constant properties, constant properties and neglecting viscous dissipation term. We can write this equation as $\frac{\partial T}{\partial t} + \nabla \cdot (\vec{u} T) = \alpha \nabla^2 T + \frac{q'''}{\rho c_p}$ so ρc_p you can take it outside. So, $\frac{\partial T}{\partial t} + \nabla \cdot (\vec{u} T) = \alpha \nabla^2 T + \frac{q'''}{\rho c_p}$ is equal to α is, α is the thermal diffusivity $\text{grad}^2 T + \frac{q'''}{\rho c_p}$ okay.

So, you see α is nothing but k by ρc_p which is known as thermal diffusivity. So it is constant properties we have considered, so ρc_p you have taken outside and we have divided. So, α is equal to k by ρc_p thermal diffusivities. So, in 2 dimensional situation you can write this equation as $\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) + \frac{q'''}{\rho c_p}$.

Okay so this is the energy equation in 2 dimensions neglecting the viscous dissipation term. So, now if you consider that velocity is 0, so if you consider this heat conduction in solid,

then you can make this velocity as 0 and you can write this energy equation as heat conduction equation in a solid.

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Heat conduction Equation in Solid
 $\vec{u} = 0$
 $\frac{\partial}{\partial t} (\rho c_p T) = \nabla \cdot (k \nabla T) + \dot{q}'''$
 $\frac{\partial T}{\partial t} = \alpha \nabla^2 T + \frac{\dot{q}'''}{\rho c_p}$ ←
 Fourier Biot equation
 Neglecting heat generation,
 $\frac{\partial T}{\partial t} = \alpha \nabla^2 T$ - Diffusion equation
 Steady with heat generation
 $\alpha \nabla^2 T + \frac{\dot{q}'''}{\rho c_p} = 0$
 $\Rightarrow \nabla^2 T + \frac{\dot{q}'''}{k} = 0$ - Poisson equation
 Steady without heat generation,
 $\nabla^2 T = 0$ - Laplace equation
 2D $\frac{\partial T}{\partial t} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right)$
 1D $\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial x^2}$

So now will write this equation as now will write heat conduction equation, heat conduction equation in solid okay, so we are considering solid, so obviously velocity you can make 0, okay you can make 0. So your convective term will become 0 and you will have the equation as del of del t rho c p T. So, this your convective is 0 because u is 0 is equal to divergence of K grad T plus q triple prime okay.

So now, if you write for constant properties then you can write del t by del t is equal to alpha grad square T plus q triple prime by rho c p. So, alpha is your thermal diffusivity and this equation is known as Fourier biot number, a biot equation, Fourier biot equation okay. So, q triple prime is the heat generation per unit volume in the solid okay.

Now, if you neglect this heat generation term then you can write this equation as, so neglecting heat generation okay you can write this equation as del T by del t is equal to alpha grad square t and this equation is known as diffusion equation, heat diffusion equation okay. Now if you consider steady heat conduction equation then you can drop the temporal term, then you can write this equation steady with heat generation, steady with heat generation.

So, this equation you consider, so if it is a steady then the first term you can make 0 then you will get alpha grad square T plus q triple prime by rho c p is equal to 0 or you can write grad square t plus q triple prime by K is equal to 0 and this equation is known as Poisson equation.

Now, if you have steady and negligible heat generation, so steady and without heat generation, so this is a simple one because you have no heat regeneration and you have steady state so $\frac{\partial T}{\partial t}$ is equal to 0. So, you will have $\text{grad}^2 T$ is equal to 0 which is known as Laplace equation okay.

And in 2 dimension if you want to write these equations, then you can write $\frac{\partial T}{\partial t}$ is equal to $\alpha \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$ neglecting the heat generation term and obviously in 1D you can write $\frac{\partial T}{\partial t}$ is equal to $\alpha \frac{\partial^2 T}{\partial x^2}$. Similarly, if you have species transport in the with the fluid flow then you can write the species transport equation okay and we can write in terms of the mass fraction of the species.

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Species transport equation

Y_i - mass fraction of species i
 ρ - density of the mixture
 ω_i - reaction rate of species i (formation rate) } \rightarrow known from chemical kinetics

$$\frac{\partial(\rho Y_i)}{\partial t} = \nabla \cdot (\rho \vec{u} Y_i) = \nabla \cdot (\rho D_{i,n} \nabla Y_i) + \omega_i$$

\leftarrow diffusivity

So, will write species transport equation, species transport equation, so now will write in terms of mass fraction which will denote with y_i , i is the n species i , so that is your mass fraction of species i and ρ is the density of the mixture, density of the mixture. And will consider W_i which is your reaction rate or formation rate of species i okay or formation rate. So, this is known from the chemical kinetics, known from chemical kinetics.

So, if you write the governing equation then you can write it as $\frac{\partial(\rho y_i)}{\partial t}$ is equal to divergence of ρu , y_i is equal to the diffusion term divergence of $\rho D_{i,n}$ is the diffusion coefficient $D_{i,n}$ so i to n species and $\text{grad} y_i$ plus ω_i . So, this is your diffusivity, okay. So, you we can see that all these equations Navier-Stokes equations, the

energy equation, the vorticity transport equation and the species transport equation you can write this equation in a general form, okay convective diffusive equation.

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General transport equation
 ϕ - any variable
 All these transport equation can be written in the following form for any general variable ϕ

$$\frac{\partial(\rho\phi)}{\partial t} + \nabla \cdot (\rho \vec{u} \phi) = \nabla \cdot (\Gamma \nabla \phi) + S_\phi$$

Diffusion coefficient

ϕ	Γ	S_ϕ	Equation
1	0	0	$\nabla \cdot \vec{u} = 0$ continuity equation
u	μ	$-\frac{\partial P}{\partial x}$	x-momentum equation
v	μ	$-\frac{\partial P}{\partial y}$	y-momentum equation
w	μ	$-\frac{\partial P}{\partial z}$	z-momentum equation
ω	μ	0	vorticity transport equation
T	$\frac{k}{c_p}$	$\frac{\dot{q}}{c_p}$	Energy equation
Y_i	$\rho D_{i,m}$	ω_i	species transport equation

So will write the general transport equation, general transport equation okay, so will write for any variable phi, phi is any variable okay it may be u, it may be v or it may be t okay. So, all these transport equations can be written in the following form for any general variable phi. So, this you can write as del rho phi by del t which you have the temporal term plus you have convective term, divergence of rho u phi.

Okay so phi is convected by the velocity u is equal to divergence of gamma grad phi where gamma is your diffusion coefficient, so this is your diffusion terms, so gamma is your diffusion coefficient, diffusion coefficient and plus some source term S phi. Okay it may be pressure gradient term for the Navier-Stokes equations okay or heat generation term for the energy equations.

So, these all these equations whatever we have written in today's class okay we can write in this form. So here you can see you have a temporal term, convective term and diffusive term and with some source term is phi okay. So, you can see that if you write phi is equal to 1 okay and gamma and this is your S phi, then what your equation you are going to get? Okay so you see, so if you put phi is equal to 1, it is incompressible force over density obviously, is constant. So, this term will become 0.

And if you put these terms, so phi is equal to 1 and density is constant, so gamma dot rho u is equal to now, if you gamma if you put 0 then this diffusion term will become 0 and S phi if

you put 0 then you are going to get the equation divergence of u is equal to 0, so that means it is your continuity equation okay.

So, from this general transport equation you can see if you put ϕ is equal to 1, γ is equal to 0 and S_ϕ is equal to 0 you are going to get continuity equation. Similarly, if you put ϕ is equal to u and γ is equal to μ and S_ϕ as $\frac{\partial p}{\partial x}$, S_ϕ as $-\frac{\partial p}{\partial x}$, then you are going to get x momentum equation okay without the body force term or if you write body force term then you can add it here.

Or for velocity v if you put γ as μ , S_ϕ as $-\frac{\partial p}{\partial y}$, you are going to get y momentum equation. Similarly, if you write for w and γ as μ and S_ϕ as $-\frac{\partial p}{\partial z}$ then you are going to get z momentum equation and similarly for vorticity transport equation you can see.

So, if you write ω_ϕ is equal to ω and γ is equal to ν , okay γ is equal to ν sorry γ is equal to μ because ρ is there in the left hand side and if it is source term is 0 then you will get vorticity transport equation, vorticity transport equation. And for energy equation if you put ϕ is equal to t and γ as $\frac{k}{c_p}$ and S_ϕ as q''' then you will get energy equation.

And if you put mass fraction ϕ is equal to mass fraction y_i and γ as ρD_i and this is as ω_i then you will get mass fraction equation or species transport equation, species transport equation. So, why I have written this equation? Because it is a general transport equation which represent any of these equations okay putting the values of ϕ or diffusion coefficient γ or the source term S_ϕ you can write any equations from this general transport equation.

So, when we discretize these equations, okay first will discretize in general transport equation, so that you have a convective term, temporal term and the diffusion term and if you can discretize this equation using some discretization method may be finite difference method or finite volume method then you can innovate discretize the other equations like Navier-Stokes equations or the energy transport equation. Only thing is that separately you have to discretize the pressure term.

So, for that reason we have written this equation and when we will use finite volume method specifically that time will consider this general transport equation and will discretize. So, in today's class we have started with writing the basic fluid flow equations, conserving the mass,

conserving the momentum, we have written the continuity equation and the Navier stokes equations and from this general Navier-Stokes equation we have written the burgers equation which is your 1 dimensional Navier-Stokes equation without the pressure term.

So, we have written for viscous burgers equation and inviscid burger equation dropping the viscous term and from there we have written the first order wave equation and second order wave equation for a constant speed c , constant wave speed c . Then, we have also written the vorticity transport equation and from there we have written stream function equation, so that these vorticity transport equation and the stream function equation combinedly if you solve you will be able to solve a fluid flow problem.

Then we consider the energy equation, so we from this energy equation in general we have written for a, with the fluid flow, then putting the velocity as 0 we have written the heat conduction equation in a solid and after that we have written the species transport equation in terms of the mass fraction y_i .

And at last we have written all these equations, transport equations in a general transport equation for any variable, general variable ϕ and where you have the temporal term, convective term then diffusive term as well as you have a source term $S \phi$. Thank you.