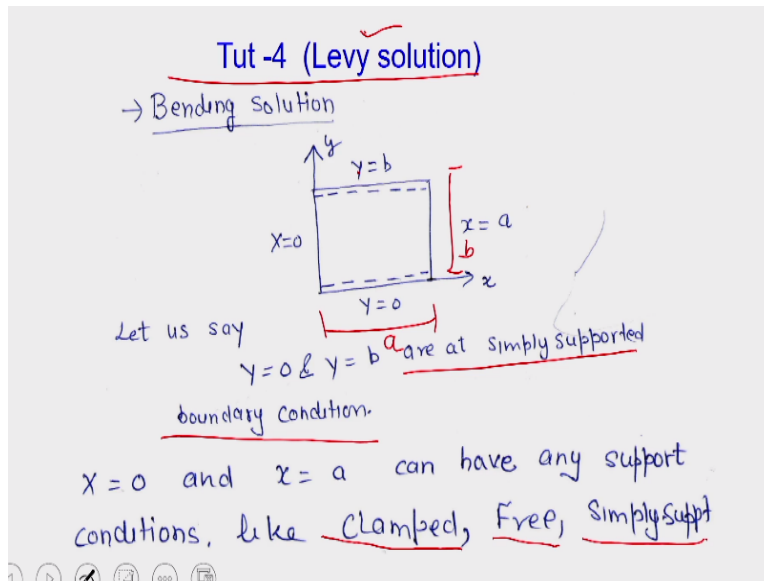


Theory of Rectangular Plates - Part 1
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Lecture – 14
Tutorial: Levy Solutions

So welcome to tutorial 4. Here I would like to solve some problems based on Levy solutions.

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First of all, I would like to define a geometry let us say a rectangular plate whose length is a along x axis, width is b along y axis and $y = 0$ as $y = b$ are at simply supported. What is the necessary condition for a Levy plate that 2 opposite axis must be simply supported like this to opposite axis? Sometimes in some books you may find that $x=0$ and $x=a$ are simply supported and the next that $x=0$ and $x=a$ can have any support conditions.

What do you mean by telling any support condition? It means it may be clamped, free, or simply supported. $x=0$ may be clamped, $x=a$ may be free and so on.

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Tut-4 (Levy solution)

Step 1

Governing Equation.

orthotropic

$$D_{11} W_{n,xxxx} - (2\bar{n}^3 D_{12}) W_{n,xx} + (\bar{n}^4 D_{22}) W_n = q_n$$

$$W = \sum_{n=1}^{\infty} W_n(x) \frac{\sinh n y}{b}, \quad q_n = \frac{2}{b} \int_0^b q(x) \frac{\sinh n y}{b} dy$$

1/2 y-ss

For a isotropic plate

$$W_{n,xxxx} - 2\bar{n}^2 W_{n,xx} + \bar{n}^4 W_n = \frac{q_n}{D}$$

So very first step to analyze this problem is that suitable governing equation fourth order in x, see second order in x and w_n and this is your q_n . I am first giving you an equation for an orthotropic plate. So if somebody asks you that what will be deflection of a clamped free plate, Levy type and axis clamped and f is free and it is made of some orthotropic material. So, we will first come to this equation, substitute the value of D_{12} , D_{22} and let us say that the loading is UDL or side loading.

Then accordingly find out this value $\bar{n}$ and $\bar{n}^4$. So, basically this W is expressed like W_n which is a function of x and $\sinh n * y / b$ because along y axis is it simply supported and what is q_n ? q_n is nothing but $2/b * q(x, y) \sinh n * y / b * dy$. Now reduces to its reverse I am here going to explain you for an orthotropic plate similarly one can go for an orthotropic plate. So for an isotropic plate this d becomes D only. So D may common out going there. Now this equation we are going to solve.

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Tut -4 (Levy solution)

Let $n=1$, 'Square plate $a=1\text{m}$, $b=1\text{m}$
made of steel, $E=210\text{GPa}$, $\nu=0.3$
 $\bar{h} = n\pi = \pi$

$$W_{n,xxxx} - (2\pi^2)W_{n,xx} + (\pi^4)W_n = \frac{q_n}{D}$$

Homogeneous part

$$W_n = W_n^h + W_n^p$$

$$W_n^h = C e^{\lambda x}$$

So very first case is that we say that let us say we are making some assumptions where n is 1, and a square plate a is 1, b is 1 and it is made of steel. E and these things are given. So n bar becomes only $n * \pi$ where n is 1 so it becomes 1. So this constant becomes $2 * \pi^2$ and these constants becomes π^4 and q_n/D . So this equation reduces to like this. Then again if you want to put the value of D now this is a differential equation fourth order.

So it will have a 2 solution, homogenous solutions and particular solution for the homogenous case this part will be $= 0$ and the homogenous solution is assumed like this. C is an arbitrary constant e raise to the power of λx . λ is unknown are the roots of the equation I would like to say that.

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Tut -4 (Levy solution)

$$C \lambda^4 e^{\lambda x} - 2\pi^2 C \lambda^2 e^{\lambda x} + \pi^4 C e^{\lambda x} = 0$$

$$(\lambda^4 - 2\pi^2 \lambda^2 + \pi^4) e^{\lambda x} = 0$$

$$\lambda^4 - 2\pi^2 \lambda^2 + \pi^4 = 0$$

Put $\lambda^2 = \gamma$

$$\gamma^2 - 2\pi^2 \gamma + \pi^4 = 0 \quad \text{quadratic}$$

$$\gamma_{1,2} = \frac{-(-2\pi^2) \pm \sqrt{(-2\pi^2)^2 - 4 \times 1 \times \pi^4}}{2 \times 1}$$

$$\gamma_{1,2} = \frac{2\pi^2 \pm \sqrt{4\pi^4 - 4\pi^4}}{2}$$

$$\gamma_1 = \pi^2$$

$$\gamma_2 = \pi^2$$

$\gamma_1 \rightarrow b \pm \sqrt{b^2 - 4ac}$

So you substitute it there. In that equation homogenous equation so it becomes a fourth order root, $\lambda^4 - 2\pi^2 \lambda^2 + \pi^4$. So this is $= 0$. This cannot be so one has to be zero. So from here you substitute some terms. If you have a this kind of equation you can directly if you would have a program or something you can evaluate that a fourth order equation at 4 root or you come out $\lambda^2 = r$ and it becomes to a quadratic equation.

So everyone knows that roots of a quadratic equation is $-b \pm \sqrt{b^2 - 4ac}/2a$ where a is the coefficient of r square, b is the coefficient of r , c is the coefficient of constant just c is a constant so in this way one can evaluate so I am writing that $r_{1,2}$ is nothing but $-b \pm \sqrt{b^2 - 4ac}/2a$. So you see that for isotropic plate this term becomes 0. You take any n combination. You say $n = 1, n = 2, n = 3$ and 4 and so on always this will be in same order. So it is becoming γ_1 and γ_2 π^2 .

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Tut-4 (Levy solution)

$$\lambda_1, \lambda_2 = \pm \pi \quad \lambda_1 = \lambda_3 = \pi$$

$$\lambda_3, \lambda_4 = \pm \pi, \quad \lambda_2 = \lambda_4 = -\pi$$

Solution:

if roots are real and equal,

$$W_n^h = (A_n + B_n x) \cosh \lambda_n x + (C_n + D_n x) \sinh \lambda_n x$$

Unknown constant

You have now roots λ_1, λ_2 is $+\pi$. λ_3 and λ_4 is $-\pi$. So now you have 4 roots; 2 roots are same, π and 2 roots are $-\pi$. So already these things I have discussed in the course during the course that if my roots are real and same then the solution wnn would be look like this. We can write a solution like this that W and homogenous can be 2 roots that if roots are equal because we are writing for just for 4 roots if you have multiple then this shape will be slightly more different.

So $(A_n + B_n \text{ of } x) * \cosh * \lambda_n x + (C_n + D_n x) \sin \text{ hyperbolic } \lambda_n x$. So this is the form of my homogenous solution where λ_n is π again and A_n, B_n, C_n, D_n are the unknown constant. Why are saying A_n and B_n basically if you say that my n is 1 then it will be A_1, B_1, C_1, D_1 . If you see n is 2, A_2, B_2, C_2 for case of a plate uniformly distributed loading then you will at least require no number of constant. If you say that is sine loading, then first term is sufficient enough.

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Tut-4 (Levy solution)

Now

$$\boxed{W_n^p} = \sum_{m=1}^{\infty} W_{mn} \sin \frac{m\pi x}{a}$$

$$\underline{q_n(x)} = \sum_{m=1}^{\infty} q_{mn} \sin \frac{m\pi x}{a}$$

$$\bar{m}^4 W_{mn}^p + 2\bar{m}^2 \bar{n}^2 W_{mn}^p + \bar{n}^4 W_{mn}^p = \frac{q_{mn}^p}{D}$$

$$\boxed{W_{mn}^p = \frac{q_{mn}}{(\bar{m}^4 + 2\bar{m}^2 \bar{n}^2 + \bar{n}^4) D}}$$

Then the next step, evaluation of a particular solution. So we are assuming that W_n^p in this form $W_{mn} * \sin * m * \pi * x/a$ and similarly q_n can be represented like this and finally I would like to say that particular solution will be q_{mn}/D for a case of isotropic plate like this $\bar{m}$ and $\bar{m}$ square and so on. So this q_{mn} will depend upon the type of flow if it is UDL or side loading and so on.

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Tut-4 (Levy solution)

Now

$$q_{mn} = \frac{2}{a} \int_0^a \underline{q_n(x)} \sin \frac{m\pi x}{a} dx$$

$$q_{mn} = \frac{2}{a} \frac{2}{b} \int_0^a \int_0^b q(x,y) \sin \frac{m\pi x}{a} \sin \frac{n\pi y}{b} dx dy$$

So q_{mn} can be evaluated like this. Already, I have told you that q_n is 0 to b so ultimately it can be represented like this.

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Tut -4 (Levy solution)

$$W = \sum_{n=1}^{\infty} (W_n^h + W_n^p) \sin \frac{n\pi y}{b}$$

$$W_0 = \left[(A_n + B_n x) \cosh h x + (C_n + D_n x) \sinh h x + \sum_{m=1}^{\infty} W_{mn}^p \left(\frac{\sinh m \pi x}{a} \right) \right] \sin \frac{n\pi y}{b}$$

Here A_n, B_n, C_n and D_n are constants.

Now you write the final solution. $W_n^h + W_n^p$ and sum $n = 1$ to infinity * sine * n * π * y/b so W_0 is finally written in this form. This was homogenous and particular solution sine m * π * x/a and sine * n * π * y/b . So here A_n, B_n, C_n, D_n are the constants which we need to evaluate and further this also C here is a function of sine. If you assume UDL then it will be a constant. It is a function of hydrostatic or some kind of variation then it will be a function like this.

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Tut -4 (Levy solution)

First case: A, B, C, D

$x=0$ clamped $x=a$ clamped	$x=0$ clamped $x=a$ free
$x=0$ clamped $x=a$ simply supported	$x=0$ free $x=a$ Free
$x=0$ SS $x=b$ SS	

So now I am going to a special case that first what type of boundary conditions. So this is your the main form of deflection where A_n, B_n, C_n and D_n are the unknowns which you have to evaluate. So there these are depend upon the boundary conditions. If I say that my plate $x = 0, x = a$ both are clamped so you will get some A_n, B_n, D_n . If I say that clamped and free different

kind of that clamped and simply supported free and free. So any kind of boundary conditions one may assume and can solve for that even though simply supported one.

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Tut -4 (Levy solution)

Now very special case

$m=1, n=1, a=1, b=1$

Load is constant.

Then

$$w_0 = (A_n + B_n x) \cosh hx + (C_n + D_n x) \sinh hx + \hat{q} \left] \sin \frac{\pi y}{b} \right.$$

$$\hat{q} = \frac{q_{mn}}{d_{mn}} = \frac{P}{w_{mn}}$$

So now I am talking to a very special case where m is 1, n is 1, a is 1, b is 1 and load is constant. So in that case let us say q is q hat not sine, cos nothing. The solution can be represented like this. So again qmn is written as wmn of p.

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Tut -4 (Levy solution)

Let say - $x=0$ clamped and $x=a$ clamped

$w_0 = 0$ $w_{0,x} = 0$ <u>Put $x=0$ / $w_0=0$</u>	$w_0 = 0$ $w_{0,x} = 0$
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$(A_n + \underline{0}) \cosh h(\underline{0}) + (C_n + \underline{0}) \sinh(\underline{0}) + \hat{q} = 0$

$\Rightarrow \boxed{A_n + \hat{q} = 0} \Rightarrow \boxed{A_n = -\hat{q}}$

So let us say $x=0$ clamped and $x=a$ is also clamped that both of the edges $x=0$ as well as $x=a$ are clamped. So you put $x=0$ for that case, deflection must vanish. So put $x=0$ in that form.

Then from there you come to know that $A_n + q \text{ hat} = A_n - q \text{ hat}$. So your first constant will be the negative of your load vector.

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Tut -4 (Levy solution)

$$\begin{aligned} \omega_{0,x} &= (A_n + B_n x) \lambda \sinh \lambda x + B_n \cosh \lambda x \\ &+ (C_n + D_n x) \lambda \cosh \lambda x + D_n \sinh \lambda x \\ &= 0 \end{aligned}$$

$$\boxed{B_n + C_n \lambda = 0} \Rightarrow \boxed{B_n = -C_n \lambda}$$

$x = a \quad \lambda a = 1$

$$(A_n + B_n) \cosh \lambda + (C_n + D_n) \sinh \lambda + \hat{q} = 0$$

Now $\boxed{A_n = -\hat{q}}$, $\boxed{B_n = -\lambda C_n}$

Then slope w, x at $x = 0$. So if you put here $x = 0$, 0 it becomes 1, it becomes 1, it becomes 0, it becomes 0. So from this equation $B_n + C_n * \lambda$ tells you that the coefficient of $B_n = -\lambda * \text{coefficient of } C_n$. Then $x = a$. Put x is a and we know that $a = 1$. So I have just simplified this expression that $(A_n + B_n) * \cosh \lambda + (C_n + D_n) \sinh \lambda + \hat{q} = 0$ and substitute this. $A_n = -\hat{q}$ and $B_n = -\lambda C_n$. If you substitute these values.

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Tut -4 (Levy solution)

$$(-\hat{q} - \lambda C_n) \cosh \lambda + (C_n + D_n) \sinh \lambda + \hat{q} = 0$$

$$C_n [\sinh \lambda - \lambda \cosh \lambda] + D_n [\sinh \lambda] = \hat{q} - \hat{q} \cosh \lambda$$

$$\Omega_1 = \sinh \lambda - \lambda \cosh \lambda, \quad \Omega_2 = \sinh \lambda$$

$$C_n \Omega_1 + D_n \Omega_2 = \hat{q}_1$$

Now $x = 0, w_{0,x} = 0$

$$(A_n + B_n) \lambda \sinh \lambda + B_n \cosh \lambda + (C_n + D_n) \lambda \cosh \lambda + D_n \sinh \lambda = 0$$

$$(-\hat{q} - \lambda C_n) \lambda \sinh \lambda - \lambda C_n \cosh \lambda + (C_n + D_n) \lambda \cosh \lambda + D_n \sinh \lambda = 0$$

So it becomes $C_n \times$ some constants or some high sine D_n something and some loading constant. So I am saying so let us say these coefficients are noted as capital omega 1 and these coefficients are known as capital omega 2. So this is a load term and this loading is denoted as $\hat{q}_1$. So you got this equation C_n and D_n 1 equation. Then at $x = a$, $w, x = 0$ slopes so put that A value in the slope equation and from there substitute the value of A_n and B_n wherever is B_n so it reduces to.

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Tut -4 (Levy solution)

$$C_n [\cancel{\lambda \cosh \lambda} - \cancel{\lambda \cosh \lambda} - \lambda^2 \sinh \lambda] + D_n [\lambda \cosh \lambda + \sinh \lambda] = + \hat{q}_1 \lambda \sinh \lambda$$

$$\boxed{C_n [-\lambda^2 \sinh \lambda] + D_n [\sinh \lambda + \lambda \cosh \lambda] = \hat{q}_1}$$

$$C_n \Omega_3 + D_n \Omega_4 = \hat{q}_2$$

An equation like this where we say this is omega 3 and this is omega 4 and this is also $\hat{q}_2$ hat.

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Tut -4 (Levy solution)

$$\boxed{C_n \Omega_1 + D_n \Omega_2 = \hat{q}_1}$$

$$\boxed{C_n \Omega_3 + D_n \Omega_4 = \hat{q}_2}$$

Now
Free

$x=0$ $x=a$

$M_{xx}=0$
 $V_{xx}=0$

$$D_n (\Omega_2 \Omega_3 - \Omega_4 \Omega_1) = \hat{q}_1 - \hat{q}_2$$

$$-D_n = \frac{-\hat{q}_1 + \hat{q}_2 \cosh \lambda - \hat{q}_2 \lambda \sinh \lambda}{\Omega_2 \Omega_3 - \Omega_4 \Omega_1}$$

$$\boxed{C_n = \frac{\hat{q}_1 - D_n \Omega_2}{\Omega_1}}$$

Similarly, C_n can be evaluated. Now we have evaluated all the constants. For a particular boundary condition that $x = \text{clamped}$ and $x_a = \text{clamped}$. Suppose if I ask $x = 0$ is clamped, but $x = a$ is free or simply supported free so for this case here moment and V_{xx} needs to be specified. So there are boundary conditions so there are some different kind of variation may come, but the procedure remains same.

Tut -4 (Levy solution)

$$w_0 = (A_n + B_n x) \cosh \frac{\pi x}{b} + (C_n + D_n x) \sinh \frac{\pi x}{b} + \frac{q}{2} \int \frac{\sinh \pi y}{b}$$

$n = 9/2$ $\cosh(kn)$ radian

$$\frac{M_{xx}}{M_{yy}} = -\frac{D_{11} w_{0,xx}}{D_{22} \left(\frac{\pi^2}{b^2}\right)} - \frac{D_{12} w_{0,yy}}{D_{22} \left(\frac{\pi^2}{b^2}\right)}$$

So wrong deflection so all these things are in radiant. So accordingly one has to evaluate. So first I had given this thing to one of my M. Tech student and they said okay everything evaluated by just assuming that degree, degree and that deflection and moment all things were coming along.

so then I realized this you must remember this thing whenever we do things in the plate so cos hyperbolic or sine $x * \sinh \phi$ all these if things has to reevaluate in terms of a radian.

So, now if somebody is interested in terms of a moment or this plate it will be - D_{11} of W, xx - D_{12} of W, yy . So w, yy (FL) (16:23-16:25) only $\phi^2/b D_{12}$ and the same term similarly you take double derivative of this substitute those values and evaluate that similarly evaluate M_{yy} and so on. So now by going through this tutorial 4 you have learned that how to solve a Levy plate. How to solve the different constants?

So one may write a program very simple program in Matlab that $\lambda_1, \lambda_2, \lambda_3$, all are given evaluated B_n , evaluate q_n for a different material may be isotropic, may be for a steel and then you change the material to aluminum and if you are very much interested go for a orthotropic one may try for that. So with this our tutorial 4 ends here.