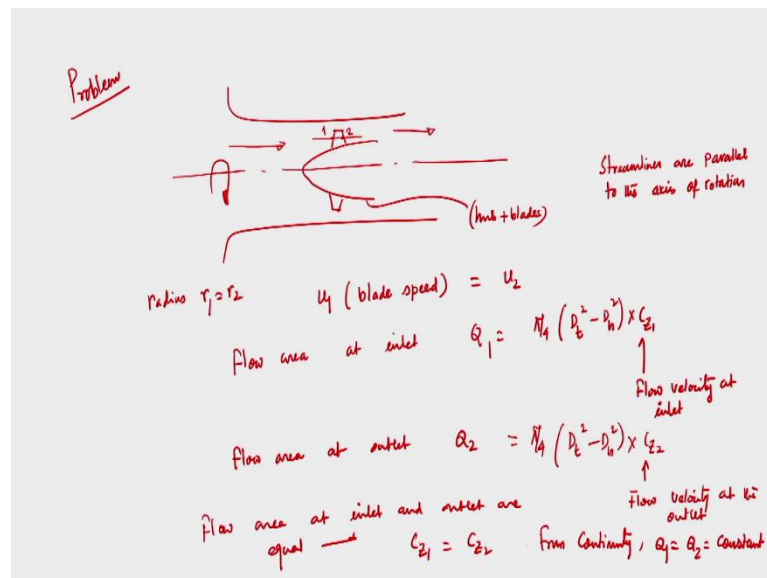


Principle of Hydraulic Machines and System Design
Dr. Pranab K. Mondal
Department of Mechanical Engineering
Indian Institute of Technology, Guwahati

Lecture – 15
Pumps Operation: Series and Parallel, Problems – II

So, today we will solve a few problems that we could not solve in my last lectures. So, I will solve one problem for axial flow machines. So, before I go to solve the problems on axial flow machines I will briefly discuss about a few important features whenever fluid is inclined axial flow machines.

(Refer Slide Time: 00:44)



So, I am writing problem it is very important on axial flow machines. So, if I draw the schematic of axial flow machines again. So, this is the hub plus blades that is impeller of an axial flow machines, fluid is flowing in the axial direction and machine is rotating in this direction.

And if I take a streamline; so this is 2 and this point is 1; so 1 and 2. So, you know here stream lines are parallel you know to the axis of rotation, to the axis of rotation. So, here streamlines are parallel axis rotation. So, before I go to solve the problem here, I will discuss that now radius $r_1 = r_2$. So, you know half and tips; So, radius $r_1 = r_2$ therefore, the blade speed u_1 blade speed at the inlet will be equal to blade speed u_2 blade speed outlet since you know RPM is same.

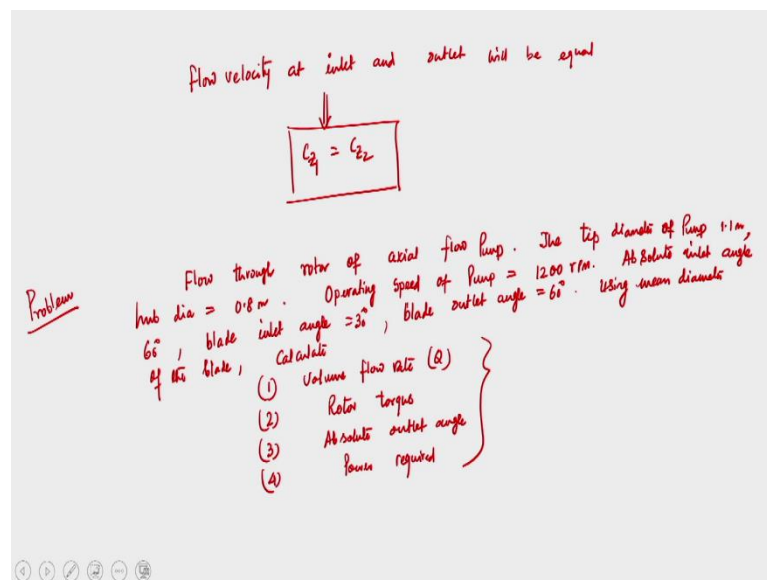
$$\text{Flow area at inlet } Q_1 = \frac{\pi}{4} (D_t^2 - D_h^2) C_{z1}$$

$$\text{Flow area at outlet} = \frac{\pi}{4} (D_t^2 - D_h^2) C_{z2}$$

So, now flow area at the inlet; flow area at inlet and outlet are equal; that means, flow area at inlet and outlet are equal; that means, it will give $C_{z1} = C_{z2}$ So, why? Because flow area at the inlet and outlet are equal this will give $C_{z1} = C_{z2}$ this is from the continuity equation.

Because from continuity $Q_1 = Q_2$ is equal to constant right. So, from continuity $Q_1 = Q_2 = K$.

(Refer Slide Time: 05:23)



So; that means, if I go to the next slides; so, the flow velocity that means flow velocity at inlet and outlet will be equal; will be equal that is in implying $C_{z1} = C_{z2}$. So, this is the condition we get from this you know analysis.

That means, if we talk about flow through axial flow machines then since the flow area at inlet and outlet are constant and from the continuity $Q_1 = Q_2$. So, it will imply that the flow velocity at the inlet and outlet has to be equal that is $C_{z1} = C_{z2}$. So, this is the condition rather this is the conclusion what we get from this analysis this will be important while you are solving a problem for the axial flow machines.

Now, we will discuss one problem one axial flow machines and that is very important. So, will discuss one problem I will write the problem; so, flow through rotor, flow through

rotor of axial flow fan right. The tip diameter tip diameter of fan is 1.1 meter; half diameter is equal to 0.8 meter.

It is given operating speed sorry it will be axial flow pump; it is axial flow pump at tip diameter of the pump is 1.1-meter half diameter is given operating speed of the pump is equal to 1200 rpm. Absolute inlet angle is given 60-degree, blade inlet angle is equal to given 30-degree, blade outlet angle is equal to given 60 degree.

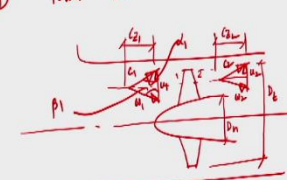
Use mean diameter of the blade; use mean diameter of the blade rather using mean diameter of the blade; we have to calculate one volume flow rate; volume flow rate Q, number 2 rotor torque, number 3 absolute outlet angle, number 4 power required. So, these 4 quantities we have to calculate based on the data given. So, we need to solve the problem; so, we will solve the problem, now we will solve that solution.

(Refer Slide Time: 09:46)

Sol: 1) Volume flow rate $Q_1 = Q_2 = Q = \frac{\pi}{4} (D_t^2 - D_h^2) \times C_{z2} / c_{z2}$

2) Rotor torque $T = \dot{m} (C_{\theta 2} - C_{\theta 1}) \times R_m$
↓ mean radius

① Power $P = T \times \omega$



$\alpha_1 = 60^\circ$
 $\beta_1 = 30^\circ$
 $\beta_2 = 60^\circ$

$u = u_1 = u_2 = \frac{\pi D_m N}{60} = \frac{\pi \times 0.95 \times 1200}{60} = 59.7 \text{ m/s}$

from inlet velocity triangle

$$\frac{C_{z1}}{\omega R_1} = \tan \beta_1 \quad \left| \quad C_{\theta 1} = C_{z1} \cot \beta_1 \right.$$

$$\omega R_1 = C_{z1} \cot \beta_1 \quad \left| \quad \frac{u}{\cot \beta_1 + \cot \beta_2} = \frac{59.7}{\cot 60^\circ + \cot 30^\circ} = 25.9 \text{ m/s} \right.$$

$$u = \omega R_1 + C_{\theta 1} = C_{z1} (\cot \beta_1 + \cot \beta_2) \Rightarrow C_{z1} = \frac{u}{(\cot \beta_1 + \cot \beta_2)} = 25.9 \text{ m/s}$$

So, volume flow rate volume flow rate $Q_1 = Q_2 = Q$ whatever it is will be $\frac{\pi}{4} (D_t^2 - D_h^2) C_{z2}$ whatever we can calculate.

Rotor torque $T = \dot{m} (C_{\theta 2} - C_{\theta 1}) R_m$

So, R_m is the mean radius because it is given that we have to consider mean radius. So, this will be the rotor torque and finally, if we calculate power then power P will be torque

into omega. So, that the answer of 4 that will get Newton meter per second what whatever will that that will obtain that is the power.

Now, we have to solve the problem by drawing the velocity angles. So, now, am drawing the velocity angles of inlets and outlets. So, if it is an axial flow machines or axial flow pump.

So, we have obtained, and this is the half diameter D h and tip diameter will be like this. So, this is the tip diameter Dt; so, you have obtained Dt and Dh, but what is given? We have given flow angle absolute angle absolute flow angle $\alpha_1 = 60$ degree is given, $\beta_1 = 30$ -degree, $\beta_2 = 60$ degree.

$$U_1=U_2 = \frac{\pi D_m N}{60} = \frac{\pi * 0.95 * 1200}{60} = 59.7$$

So, to obtain flow rate we know Dt we know Dh only thing we need to know either Cz1 or Cz2. So, if take the inlet velocity angle; so which one is the alpha 1 is the 60 degree. So, this angle is 60 degree; so, from inlet velocity triangle from inlet velocity triangle we obtain Cz 1. So, this is the Cz1 and this is this is Cz2.

$$\frac{C_{z1}}{W_{\theta 1}} = \tan \beta_1$$

$$W_{\theta 1} = C_{z1} \cot \beta_1$$

$$C_{\theta 1} = C_{z1} \cot \alpha_1$$

$$U = W_{\theta 1} + C_{\theta 1} = (C_{z1} \cot \beta_1 + \cot \alpha_1) C_{z1}$$

So, from here we can calculate c z 1 is equal to u divide by cot alpha 1 plus cot beta 1 and it will give a value of because u = 59.7 and if I put the value of cot alpha 1 and cot beta 1 cot 60 degree plus cot 30 degree will obtain the value of 25.9 meter per second. So, we will obtain at flow velocity at the inlet will is 25.9 meter per second, knowing the value of this continuity we can go to calculate Q; Q 1.

(Refer Slide Time: 15:42)

flow rate $Q = \pi/4 (D_t^2 - D_h^2) \times C_{z1}$
 $= \pi/4 (1.1^2 - 0.8^2) \times 25.9 = 11.6 \text{ m}^3/\text{s}$

Sketch velocity triangle 1

$C_{z1} = C_1 \sin 60^\circ \Rightarrow C_1 = C_{z1} / \sin 60^\circ = 29.9 \text{ m/s}$
 $C_{\theta 1} = C_1 \cos 60^\circ = 29.9 \times \cos 60^\circ = 15 \text{ m/s}$
 $C_{z1} = C_{z2} = 25.9 \text{ m/s}$

Outlet velocity triangle

$\tan \alpha_2 = \frac{C_{z2}}{C_{\theta 2}} = \frac{C_{z2}}{u_2 - w_{\theta 2}} = \frac{25.9}{59.7 - C_{z2} \cot \beta_2}$
 $C_{\theta 2} = u_2 - w_{\theta 2}$
 $\frac{w_{\theta 2}}{C_{z2}} = \cot \beta_2; w_{\theta 2} = C_{z2} \cot \beta_2$

$$Q = \frac{\pi}{4} (D_t^2 - D_h^2) C_{z2} = \frac{\pi}{4} (1.1^2 - 0.8^2) \times 25.9 = 11.6 \text{ m}^3/\text{s}$$

So, this is the answer for the flow rate we will obtain now we need to calculate another a few quantities that is a torque. To calculate torque what we need to know you know we need to know the value of $C_{\theta 2}$ and $C_{\theta 1}$ that is the very important.

$$\frac{C_{z1}}{C_1} = \sin 60$$

$$C_1 = \frac{C_{z1}}{\sin 60} = 29.9 \text{ m/s}$$

$$C_{\theta 1} = C_1 \cos 60 = 15 \text{ m/s}$$

$$C_{z1} = C_{z2} = 25.9 \text{ m/s}$$

$$\tan \alpha_2 = \frac{C_{z2}}{C_{\theta 2}} = \frac{C_{z2}}{u_2 - w_{\theta 2}} = \frac{25.9}{59.7 - C_{z2} \cot \beta_2}$$

$$\left\{ \frac{C_{\theta 2}}{C_{z2}} = \cot \alpha_2 \right\}$$

$$C_{\theta 2} = 44.6$$

$$T = m \cdot (C_{\theta 2} - C_{\theta 1}) \cdot R_m = 201 \text{ Nm}$$

$$\text{Power } P = T \cdot \omega = 25.3 \text{ kW}$$

(Refer Slide Time: 22:05)

$$\frac{C_{02}}{C_{22}} = \omega r_{02} \rightarrow C_{02} = C_{22} \omega r_{02} = 44.6 \text{ m/s}$$
$$T_2 = \dot{m} r_{02} (C_{02} - C_{01}) = \rho A (0.95 \frac{r_{02}}{r_{01}}) (44.6 - 15)$$
$$= 201 \text{ N-m}$$
$$\text{Power } P = T \omega = 201 \times \frac{2\pi \times 1000}{60} = 25.3 \text{ kW}$$

So, essentially what we have to calculate? For the key is for axial flow machine flow area at the inlet and outlet are equal which will give that flow velocity at the inlet and outlet are equal. And from the given data we have to calculate different components of you know velocity right component of axial velocity in the tangential direction at the inlet and outlet, component of electricity at the tangential direction at inlet and outlet; from there we can calculate all other quantities and we have to solve the problem.

With this, I stop here, and we will continue in the next lecture.

Thank you.