

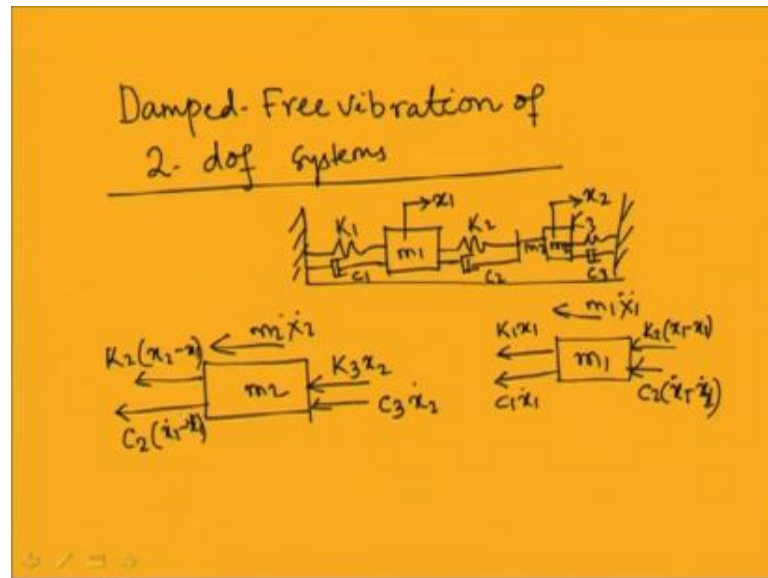
Mechanical Vibrations
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Module – 5
2 DOF Free Vibrations
Lecture - 4
Forced Harmonic Vibration

Last three classes, we were studying about the 2 degree of freedom systems and we have studied the free vibration response of 2 degree of freedom system. And in this case of 2 degree freedom system we were finding 2 natural frequency and 2 normal modes of the system. Unlike the single degree of freedom system; here you have two natural frequency and already I told you how to derive this equation motion. Equation motion can be derived using Newton's method or D'Alembert principle or by using this Lagrange method or extended Hamilton principle. So, after deriving this equation motion you can find the free vibration response of the system by assuming normal modes of the system. And by assuming this normal mode you can find the natural frequencies of the system.

So, after finding the natural frequencies then you can find the normal mode of the system or you can study the free vibration response of the system. In case of free vibration you can assume that this free vibration of a system is the summation of the normal mode of the systems. So, in this case of 2 degree of freedom system already you have seen for a double pendulum; how to determine the normal modes of the system. And from the normal modes also how to determine the free vibration response of the system; also we have studied the damped free vibration of 2 degree of freedom system; last class we have studied about this.

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And, I can draw a spring mass damper system with damping. And today class we will study about this will see an example of this damped free vibration of 2 degree of freedom system. And also will study semi definite systems and force vibration of 2 degree of freedom system. So, to start with this damped free vibration of 2 degree freedom system; let us see the example we have taken in the last class. So, I am drawing a spring mass damper system with 3 springs and 2 mass. So, this is mass 1 this is mass 2 and already you have seen. So, this is mass 1, this is mass 2, this is k_1 , k_2 , k_3 and also we have put some damper here also; so this is damper 1.

So, I have put damper 2 and this is the third damper. So, let me draw it clearly; so this is the second mass and spring and I will put a damper also; so this is damper. So, this is c_1 , c_2 and c_3 . So, in this case you have found the equation of motion by assuming the general generalized coordinate x_1 and x_2 ; x_1 is the generalized coordinate for mass m_1 and x_2 is the generalized coordinate for mass m_2 . So, by taking this you can write the equation of motion. So, already you have seen that equation of motion I have derived using either Lagrange principle or Newton's method. So, you can use the Newton's method for simplicity here. So, you can draw the free body diagram of the system. So, for this mass m_1 ; if you draw the free body diagram so it will have inertia force of $m_1\ddot{x}_1$; then this is the spring force k_1x_1 and damping force $c_1\dot{x}_1$. And similarly, for this k_2 and c_2 elements so it will be k_2 . So, this spring will have a relative

motion of x_1 minus x_2 ; so it will be $k_2 x_1$ minus x_2 and this is $c_2 x_2$ dot minus x_1 dot minus x_2 dot. So, in this way you can find the equation motion for the first mass.

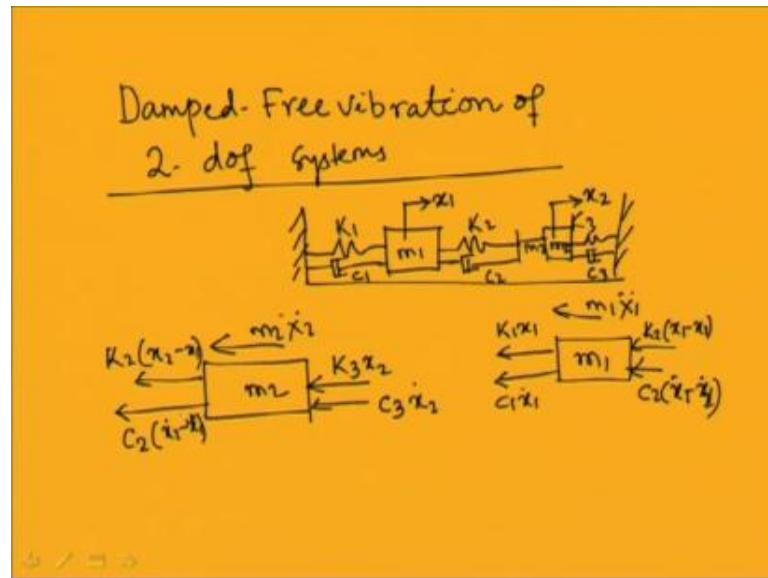
So, this will become $m_1 x_1$ double dot plus k_1 plus $k_2 x_1$ minus $k_2 x_2$ plus $c_1 x_1$ dot plus $c_2 x_1$ dot minus $c_2 x_2$ dot. Similarly, for mass 2 also you can draw the free body diagram. So, for mass two, if will draw the free body diagram. So, this is mass m_2 ; so the free body diagram. So, this is x_2 . So, inertia force $m_2 x_2$ acting in this direction and this spring force I can write it equal to k_2 into x_2 minus x_1 and damping force equal to c_2 into x_2 dot minus x_1 dot. And this side you have spring force of $k_3 x_3$ $k_3 x_2$ and damping force of c_3 into x_2 dot. So, your equation motion will become $m_2 x_2$ double dot plus k_2 plus $k_3 x_2$ minus $k_2 x_1$ plus c_2 plus $c_3 x_2$ dot minus $c_2 x_1$ dot will be equal to 0. So, you have already written the equation motion.

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$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} k_1+k_2 & -k_2 \\ -k_2 & k_2+k_3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} c_1+c_2 & -c_2 \\ -c_2 & c_2+c_3 \end{bmatrix} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

And, you know that equation motion is nothing but so this equation becomes $m_1 x_1$ m_1 0. So, this becomes m_1 0 0 $m_2 x_1$ double dot x_2 double dot plus k_1 plus k_2 minus k_2 minus k_2 k_2 plus $k_3 x_1 x_2$ plus C_1 plus C_2 minus C_2 minus C_2 C_2 plus C_3 into x_1 dot x_2 dot equal to 0 0.

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So, from this free body diagram of the system we have determined the equation motion by applying the Newton's method here; also you may apply Lagrange principle to find the this equation motion in that case you can write the kinetic energy of the system. So, kinetic energy of the system equal to half $m_1 \dot{x}_1^2$ and kinetic energy of the second mass equal to half $m_2 \dot{x}_2^2$. So, total kinetic energy of the system becomes half $m_1 \dot{x}_1^2$ plus half $m_2 \dot{x}_2^2$ and potential energy of the system is due to the springs. So, it becomes half $k_1 x_1^2$ plus half $k_2 (x_1 - x_2)^2$ plus half $k_3 x_2^2$.

And, the dissipation energy you can write equal to half $c_1 \dot{x}_1^2$ plus half $c_2 (\dot{x}_1 - \dot{x}_2)^2$ plus half $c_3 \dot{x}_2^2$. So, by writing this 3 energy that is the kinetic energy, potential energy and dissipation energy and then applying the Lagrange principle also you will get the same equation of motion.

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$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} k_1+k_2 & -k_2 \\ -k_2 & k_2+k_3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} c_1+c_2 & -c_2 \\ -c_2 & c_2+c_3 \end{bmatrix} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\left. \begin{aligned} x_1 &= A_1 e^{\delta t} \\ x_2 &= A_2 e^{\delta t} \end{aligned} \right\}$$

So, after getting this equation motion; so you can assume a solution in this form. So, you can assume a x_1 equal to... So you can write x_1 equal to $A_1 e$ to the power $s t$ and x_2 equal to $A_2 e$ to the power $s t$. And last class we have seen by applying this equation in this equation in this original equation motion you can reduce this equation to this form.

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$$\begin{bmatrix} m_1 s^2 + (c_1+c_2)s + k_1+k_2 & -c_2s - k_2 \\ -c_2s - k_2 & m_2 s^2 + (c_2+c_3)s + k_2+k_3 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\left. \begin{aligned} x_1 &= A_{11} e^{\delta_1 t} + A_{12} e^{\delta_2 t} + A_{13} e^{\delta_3 t} + A_{14} e^{\delta_4 t} \\ x_2 &= A_{21} e^{\delta_1 t} + A_{22} e^{\delta_2 t} + A_{23} e^{\delta_3 t} + A_{24} e^{\delta_4 t} \end{aligned} \right\}$$

$$\frac{A_{1i}}{A_{2i}} = \frac{c_2 \delta_i + k_2}{m_1 \delta_i^2 + (c_1+c_2)\delta_i + k_1+k_2}$$

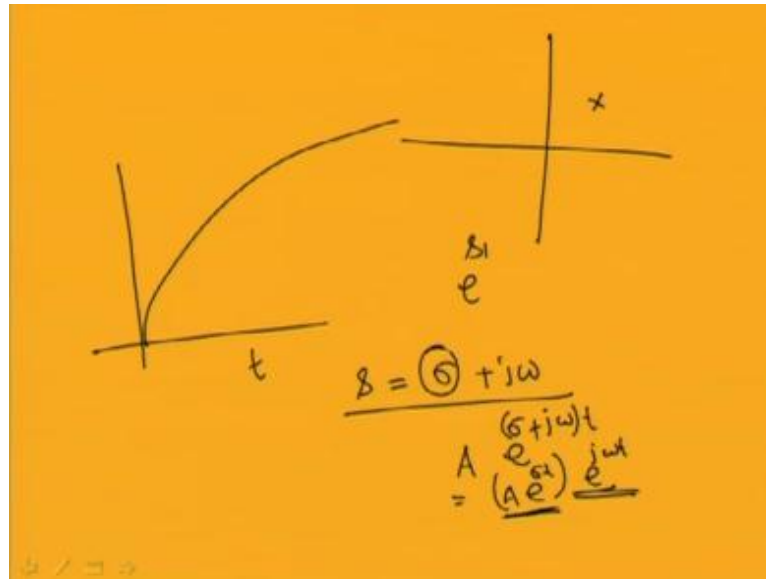
So, this becomes $m_1 s^2$ plus C_1 plus $C_2 s$ plus k_1 plus k_2 then minus $C_2 s$ minus k_2 then minus $C_2 s$ minus k_2 . And this becomes $m_2 s^2$ plus C_2 plus C_3 into s plus k_2 plus k_3 into $A_1 A_2$ equal to $0 0$. So, for non trivial solution A_1, A_2 you

can write or you can find the determinant of this matrix will be equal to 0. And from this you can find 4 value of s and after finding this roots you can write the expression for x_1 and x_2 . So, x_1 and x_2 will become; so x_1 will becomes $A_{11} e^{s_1 t}$ plus $A_{12} e^{s_2 t}$ plus $A_{13} e^{s_3 t}$ plus $A_{14} e^{s_4 t}$. Similarly, you can write x_2 will be equal to $A_{21} e^{s_1 t}$ plus $A_{22} e^{s_2 t}$ plus $A_{23} e^{s_3 t}$ and plus $A_{24} e^{s_4 t}$.

So, you can obtain the solution of this damped free vibration system by after finding these roots of this characteristic equation. So, this is the characteristic equation which you got by finding the determinant of this matrix. So, after finding this determinant you can find 4 roots of this and by substituting these roots you can find the equation in this form. So, you can observe that out of this 4 roots some roots may be real or some may be complex also or complex conjugates you can find these roots. So, after finding these roots you can find x_1 and x_2 ; you may note that this A_{1i} and A_{2i} are not independent So, they are dependent on each other or linearly dependent. So, after finding this 4 roots from this equation you can write that A_{1i} ; so if you substitute this thing.

So, this into so for half set of roots. So, you can write A_{1i} by A_{2i} . So, this into A_{1i} into this into A_{2i} will becomes 0. So, from this you can write A_{1i} by A_{2i} is nothing but this is equal to $C_2 s + k_2$ by $m_1 s^2 + m_1 s + C_1$ plus $C_2 s + k_2$. So, for a stable system all the 4 roots must be either real negative number or complex number with negative real parts. So, you know for a stable system.

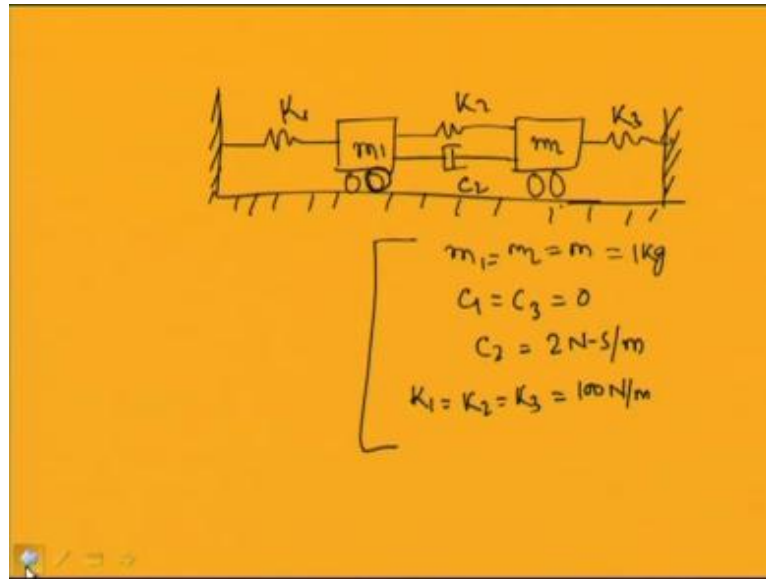
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So, for a stable system all roots should be all the roots should have a negative real part; if they have a positive real part then the solution will contain e to the power s 1 t. So, this s let me write this s equal to sigma 1 plus j omega for so as s is a complex number you can write in this form sigma plus j omega. So, if I am writing this s equal to sigma plus j omega if I have a root here so the solution will be in this form. So, it will contain A into e to the power sigma plus j omega t.

So, this will becomes A into e to the power sigma t into e to the power j omega t. So, this part will give the oscillatory motion but the part containing A into e to the power sigma t if sigma is positive will exponentially grow with time t. So, with exponentially it grow; so this part will grow exponential. So, the system will have a unbounded solution. So, for a stable system this sigma should be sigma should be negative. So, for a stable system the root should have negative real parts or a complex conjugate yes a complex conjugate with negative real part or a real number with or a negative real number. So, after finding this roots. So, you can find the solutions.

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And, let us take another physical example to find the response of a system. So, let us take a similar system similar spring mass damper system but here I will reduce the number of damper. So, let me put a damper only in the middle to simplify the calculation I can do it. And so this is the system; let us take the system. So, this is m_1 , m_2 let me take this in this case. So, let us study the free vibration of the system. Here, m_1 equal to m_2 equal to m ; let me take it equal to 1 kg and then let me this k_1 . So, this is k_1 , this is k_2 , this is c_2 , this is k_3 .

So, I am taking this c_1 equal to c_3 equal to 0 in the previous example; here I am taking c_2 , c_2 equal to 2 Newton's second per meter let me take. And this k_1 equal to k_2 equal to k_3 equal to 100 Newton per meter. So, for simplicity this data I have taken. So, you may take any other data to find the 3 vibration response of the system. So, in this case already you know the equation motion which can be written in this form $m_1 \ddot{x}_1$ or the equation motion is written in this form $m_1 \ddot{x}_1 + k_1 x_1 - k_2 (x_2 - x_1) - c_2 (\dot{x}_2 - \dot{x}_1) + k_2 x_2 + k_3 x_2 = 0$, and for damping this. So, this equation is reduced to; so I can write this equation is this form.

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$$\begin{bmatrix} m & 0 \\ 0 & m \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} 2K & -K \\ -K & 2K \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} C & -C \\ -C & C \end{bmatrix} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

So, for this case I can write the equation; so this is equal to $m \ddot{x}_1$ and $m \ddot{x}_2$. So, $m \ddot{x}_1 + m \ddot{x}_2$ plus; so this becomes k_1 plus k_2 . So, k_1 plus k_2 this becomes $2k$ and this is minus k_2 . So, minus k and this is minus k and k_2 plus k_3 becomes $2k$ and so this becomes $x_1 - x_2$ and for damping case. So, this becomes $C \dot{x}_1$ plus $C \dot{x}_2$. So, as $C \dot{x}_1$ equal to 0. So, this becomes C I can write it equal to C . And this becomes minus C and this is minus C and this is C and this becomes \dot{x}_1 and \dot{x}_2 equal to 0. So, the equation motion for the system you can write in this form. So, without referring the previous case also you can directly write the equation motion by drawing the free body diagram of the system. So, if you draw the free body diagram for this mass m_1 . So, the inertia force is $m_1 \ddot{x}_1$. So, spring force equal to $k_1 x_1$ damping force there is no damping force this side and this side you have the spring force $k_2 (x_1 - x_2)$.

And, the damping force equal to $C \dot{x}_1$ so $C \dot{x}_2$. So, this becomes C . So, it will have a displacement of $x_1 - x_2$. So, velocity difference will be $\dot{x}_1 - \dot{x}_2$. So, the damping force equal to $C (\dot{x}_1 - \dot{x}_2)$. Similarly, for this mass m_2 . So, second mass you can draw the free body diagram and you can write the equation motion. So, this is $m_2 \ddot{x}_2$ and you have a spring force $k_2 (x_2 - x_1)$ and damping force equal to $C (\dot{x}_2 - \dot{x}_1)$ and this side you have a spring force of $k_3 x_2$. So, using these forces you can draw using these forces you can write the equation motion of the system.

So, first equation becomes as $m \ddot{x}_1 = -kx_1 + kx_2$. So, $m \ddot{x}_1 + kx_1 = kx_2$. So, here $kx_1 = kx_2$. So, $kx_1 + kx_2 = kx_1 + kx_2$. So, you can write $2kx_2 = kx_1 + kx_2$ and minus kx_2 minus kx_2 equal to $kx_1 - kx_2$. So, minus kx_2 into x_2 then for damping you can write this is equal to $C \dot{x}_1 - C \dot{x}_2 = 0$. So, into $C \dot{x}_1 - C \dot{x}_2 = 0$. So, this is the first equation. And the second equation becomes $m \ddot{x}_2 = -kx_2 + kx_1 - c \dot{x}_2 + c \dot{x}_1$. So, $m \ddot{x}_2 + c \dot{x}_2 + kx_2 = kx_1 + c \dot{x}_1$. So, this becomes $kx_2 + kx_1 = kx_1 + kx_2$ and for $kx_1 - kx_2 = kx_1 - kx_2$. So, this becomes minus kx_2 . So, this becomes minus kx_2 . So, this becomes minus kx_2 and $kx_2 + kx_1 = kx_1 + kx_2$. And for damping this becomes $C \dot{x}_1 - C \dot{x}_2 = 0$. So, minus $C \dot{x}_2 + C \dot{x}_1 = 0$. So, in this way you can write the equation motion.

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$$\left. \begin{aligned} x_1 &= A_1 e^{\delta t} \\ x_2 &= A_2 e^{\delta t} \end{aligned} \right\}$$

$$(m\delta^2 + C\delta + 2k)(m\delta^2 + C\delta + k) - (C\delta + k)^2 = 0$$

$$(m\delta^2 + k)(m\delta^2 + 2C\delta + 3k) = 0$$

$$\delta_{1,2} = \pm i \sqrt{\frac{k}{m}}$$

$$\delta_{3,4} = -\frac{C}{m} \pm \sqrt{\left(\frac{C}{m}\right)^2 - \frac{3k}{m}}$$

Now, you can substitute $x_1 = A_1 e^{\delta t}$ and $x_2 = A_2 e^{\delta t}$ to the power $s t$. So, if you substitute this equation in the equation motion your equation motion will reduce to this form. So, it becomes $m s^2 + C s + 2k$ into $m s^2 + C s + k$ minus $(C s + k)^2 = 0$. So, you will get this characteristic equation. So, now you have to find the solution of this characteristic equation to find all the 4 roots. So, this equation you can write in this form. So, if you multiply this thing and you can write this equation in this form. So, it will reduce to $m s^2 + k$ into $m s^2 + 2 C s + 3 k = 0$. So, you multiply this write this equation and then you can write the same equation in this form.

So, this becomes so you can do this thing by following 2, 3 steps. So, you just first multiply this equation with this equation and minus C s plus k square you expand this terms. And after expanding this thing you can rewrite this equation in this form. So, from this you can find at s 1, 2 from this. So, this will be equal to 0 when this first part either this first part equal to 0 or this second part equal to 0. So, s 1, 2 you can find will be equal to plus minus i root over K by m and from this you can see that s 3, 4 will be equal to so this will becomes minus C by m plus minus root over C by m whole square minus 3 K m. So, in the present case by substituting this value, so I can write this s 1, 2.

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The image shows handwritten mathematical work on a yellow background. It includes the following equations:

$$s_{1,2} = \pm \sqrt{\frac{100}{1}} = \pm 10i$$

$$s_{3,4} = -2 \pm \sqrt{296}i$$

$$= -2 \pm 17.2i$$

$$x_1 = A_{11} e^{10it} + A_{12} e^{-10it} + A_{13} e^{(-2+17.2i)t} + A_{14} e^{(-2-17.2i)t}$$

$$x_2 = A_{21} e^{10it} + A_{22} e^{-10it} + A_{23} e^{(-2+17.2i)t} + A_{24} e^{(-2-17.2i)t}$$

So, s 1, 2 becomes root over k by m k I have taken equal to 100 Newton per meter and m equal to 1; so this becomes 10. So, plus minus 10 I am getting 2 roots, those are plus minus 10 plus minus i into 10.

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$$\left. \begin{aligned} x_1 &= A_1 e^{s_1 t} \\ x_2 &= A_2 e^{s_2 t} \end{aligned} \right\}$$

$$(m s^2 + c s + 2k)(m s^2 + c s + k) - (c s + k)^2 = 0$$

$$(m s^2 + k)(m s^2 + 2c s + 3k) = 0$$

$$s_{1,2} = \pm i \sqrt{\frac{k}{m}}$$

$$s_{3,4} = -\frac{c}{m} \pm \sqrt{\left(\frac{c}{m}\right)^2 - \frac{3k}{m}}$$

So, this is plus minus $10 i$ and previously I have written s plus I into root over K by m . So, because this s square equal to minus K by m . So, root over minus root over K by m equal to plus minus i into root over K by m . So, $s_{1,2}$ you can find this and $s_{3,4}$ becomes; so if I substitute those values. So, it becomes minus 2 plus minus root over 296 i . And this equal to minus 2 plus minus $17.2 i$. So, after getting this 4 roots now you got 4 roots this s_1 equal to plus $10 i$, s_2 equal to minus $10 i$, s_3 equal to minus 2 plus $17.2 i$. And s_4 becomes minus 2 minus $17.2 i$. So, here you just note that you got 4 complex numbers out of these 2 are imaginary, purely imaginary and other 2 are complex conjugates. So, this imaginary roots will give oscillatory motions and you can write your x_1 in this form already you know you can write $x_1 = A_{11} e^{10 i t} + A_{12} e^{-10 i t} + A_{13} e^{(-2 + 17.2 i) t} + A_{14} e^{(-2 - 17.2 i) t}$.

Similarly, x_2 can write in this form $A_{21} e^{10 i t} + A_{22} e^{-10 i t} + A_{23} e^{(-2 + 17.2 i) t} + A_{24} e^{(-2 - 17.2 i) t}$. So, here you can observe that the system have 2 frequency; one frequency is 10 and the other frequency is 17.2 . So, this 2 degree of freedom system will have 2 frequencies you obtain those 2 frequencies; and you can simplify these 2 expression to write the expression for x_1 and x_2 . Also you may note that this $A_{11}, A_{12}, A_{13}, A_{14}$ and $A_{21}, A_{22}, A_{23}, A_{24}$ can be obtained from the initial conditions.

So, you know you have 4 initial conditions these are the displacement and velocity of mass 1 and 2; so but you have 8 unknowns. So, out of this 8 unknowns and you have 4 equations and also you know that A_{1i} and A_{2i} are related. So, if you find some of this A either A_{1i} or A_{2i} then you can find the other 4 unknowns.

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Semidefinite systems

$$x_1 = B_{11}(\sin 10t + \phi_{11}) + B_{12}(\sin 17.2t + \phi_{12})$$

$$x_2 = B_{21}(\sin 10t + \phi_{21}) + B_{22}(\sin 17.2t + \phi_{22})$$

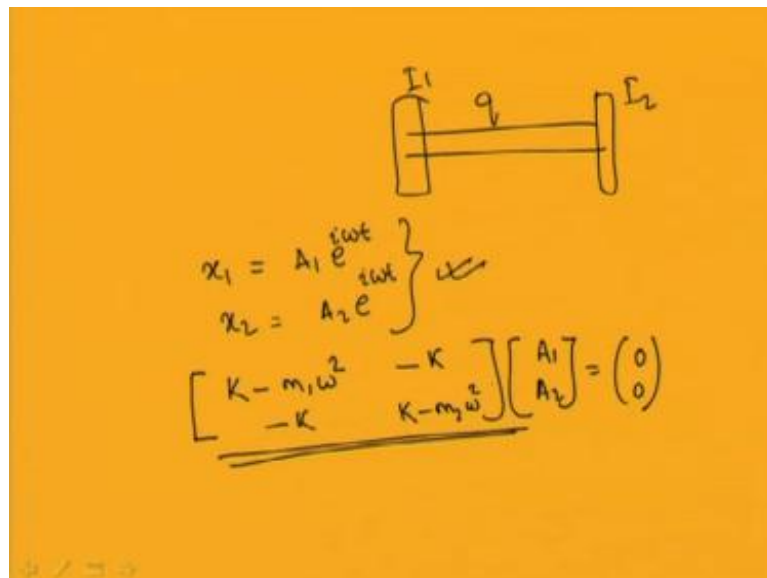
$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} K & -K \\ -K & K \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

So, you can simplify this equations and you can write this equation also in this form. So, by using this property $e^{i\theta} = \cos \theta + i \sin \theta$ if you use that property then you can write this equation in this form. So, you can write this x_1 equal to $B_{11} \sin 10t + \phi_{11} + B_{12} \sin 17.2t + \phi_{12}$. And x_2 also you can write equal to $B_{21} \sin 10t + \phi_{21} + B_{22} \sin 17.2t + \phi_{22}$. So, in this case you have this $B_{11} \phi_{11}$ and $B_{12} \phi_{12}$. So, B_{11} this is the magnitude and ϕ_{11} is the phase difference. So, this is the first mode and this is the second mode. So, already you know by using this normal modes how to write this equation motion. So, these are the normal modes. So, $\sin 10t$ and $\sin 17.2t$. So, 17.2 is the second frequency and 10 is the first frequency of the system.

So, in this way you can find the response of a 2 degree of freedom system with damping. So, let us see some other system, which are known as semi definite system; semi definite system or degenerate system; there are class of system for which out of this 2 natural frequency you can find that 1 natural frequency equal to 0. So, the system for which at least 1 natural frequency is 0 are known as the degenerate system or semi definite

systems. So, let us take the system simple spring mass damper system in which the sides are not constant. So, this is m_1 and m_2 ; so you have 2 systems or 2 bogies they are connected by the spring k . So, in this case you can derive this equation motion. So, for this case the equation motion you can derive by using Lagrange principle. So, by using Lagrange principle you can write the equation motion; so this is x_1 and this is generalized coordinate x_2 . So, kinetic energy equal to half $m_1 \dot{x}_1^2$ plus half $m_2 \dot{x}_2^2$ and potential energy equal to half $k(x_2 - x_1)^2$. So, you can find the equation motion of the system this form. So, it will leads to $m_1 \ddot{x}_1 - k(x_2 - x_1) = 0$ and $m_2 \ddot{x}_2 + k(x_2 - x_1) = 0$.

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So, you can take a 2 rotor system also which will have similar equation motion. So, this is a 2 rotor system with inertia i_1 and i_2 and let q is the stiffness of the system. So, in this case also you can have a similar equation motion. So, for this case I can write now this x_1 equal to I can assume a solution x_1 equal to $A_1 e^{i\omega t}$ and x_2 equal to $A_2 e^{i\omega t}$. So, I am taking the normal modes. So, already you know in case of normal modes all the masses will vibrate with same frequency. So, I have taken the frequency to be same in both the cases; in case of x_1 I have taken it ω and in case of x_2 also I have taken it ω but the amplitudes are different. In case of normal modes the systems or the masses of the system are vibrating with same frequency and passing through the equilibrium position at the same time. So, I can assume the solution like this and after assuming the solution I can find and substituting in

this equation motion I can write this in this form. So, the equation motion will reduce to $k - m_1 \omega^2$ into $k - m_2 \omega^2$ minus k^2 equal to 0. So, for non trivial response; so the determinant will be equal to 0 to find the determinant. So, determinant will be $k - m_1 \omega^2$ into $k - m_2 \omega^2$ minus k^2 equal to 0.

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The image shows a handwritten derivation on a yellow background. The steps are as follows:

$$(k - m_1 \omega^2)(k - m_2 \omega^2) - k^2 = 0$$

$$\cancel{k^2} - k(m_1 + m_2)\omega^2 + m_1 m_2 \omega^4 - \cancel{k^2} = 0$$

$$\omega^2 (m_1 m_2 \omega^2 - k(m_1 + m_2)) = 0$$

$$\omega = 0$$

$$\omega^2 = \frac{k(m_1 + m_2)}{m_1 m_2}$$

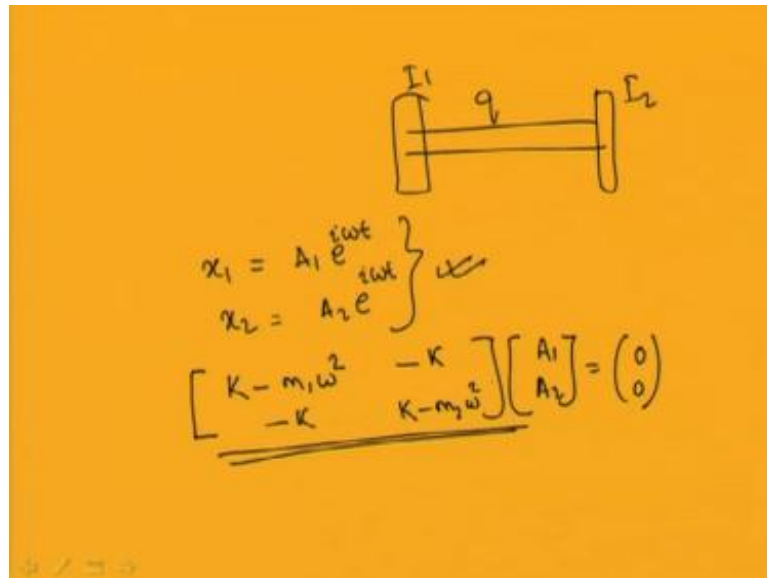
$$\omega_2 = \sqrt{\frac{k(m_1 + m_2)}{m_1 m_2}}$$

So, I can write the determinant in this form. So, the determinant becomes $k - m_1 \omega^2$ into $k - m_2 \omega^2$ minus k^2 equal to 0. So, I will multiply this; so I can write this equation in this form k into k . So, this becomes k^2 minus k into $m_1 + m_2$ omega square plus $m_1 m_2$ omega fourth minus k^2 equal to 0 or I can write this equation in this form omega square. So, I can take omega square common from these 2. So, this becomes omega square into $m_1 m_2$ omega square minus k into $m_1 + m_2$ equal to 0. So, this as this k^2 minus k^2 cancel. So, this equation becomes $m_1 m_2$ omega square minus k into $m_1 + m_2$ equal to 0. So, I can take omega square and this becomes $m_1 m_2$ omega square minus k into $m_1 + m_2$ equal to 0. So, from this equation you can observe that either this omega equal to 0 or this part will be equal to 0.

So, you are getting a frequency omega equal to 0. So, the other frequency can be obtained from this. So, this will give omega square equal to K into $m_1 + m_2$ by $m_1 m_2$ or you can write. So, this is your omega 1 equal to 0 and omega 2 you can

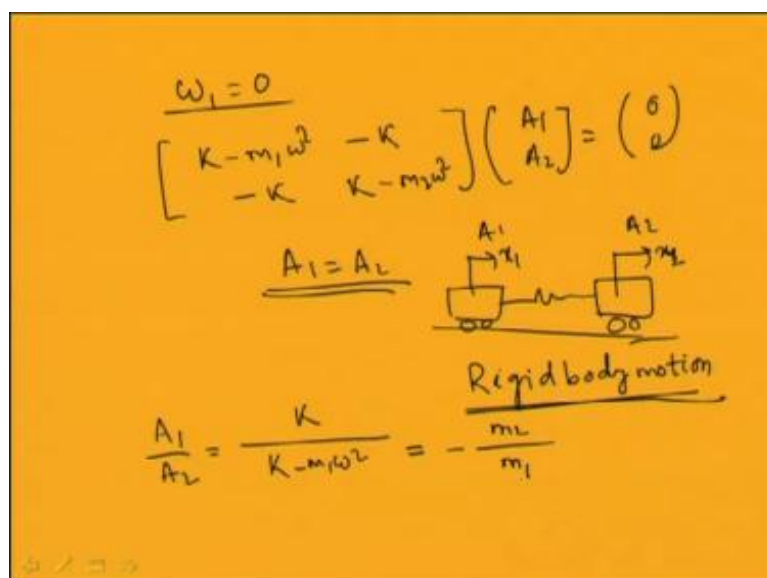
write equal to root over K into m 1 plus m 2 by m 1 m 2. So, you have seen you have 2 frequency out of which one frequency equal to 0. So, this is A degenerate system and for which you have this omega 1 equal to 0. So, if I substitute this omega 1 equal to 0 in this equation.

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So, let omega equal to 0. So, if omega equal to 0; so you can see that K into A 1 minus K into A 2 equal to 0 that means A 1 equal to 0 A 1 equal to A 2.

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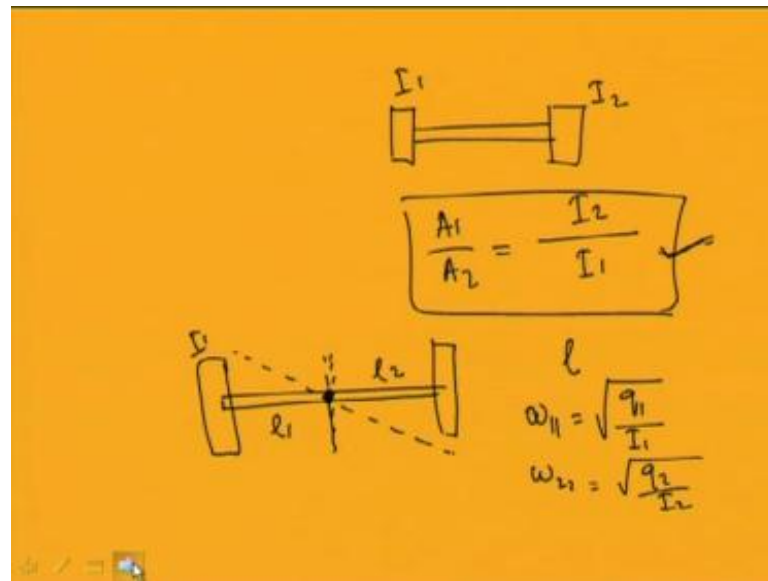
So, for omega 1 equal to 0 you have observed that from this equation. So, your equation is $m_1 \omega^2 - K - K - m_2 \omega^2 = 0$. So, from this equation if you substitute omega equal to 0 omega equal to omega 1 equal to 0. So, you are getting $A_1 = A_2$. So, $A_1 = A_2$ means both the springs or both the mass; so this is x_1 this is x_2 x_1 this is x_2 . So, amplitude $A_1 = A_2$ that means both the mass will move in the same direction with same amplitude. That means, there will be a rigid body motion in the system. So, the body may have a rigid body motion in this case of degenerate system and in the second case it will have a frequency. So, you can you can find in case of second mode.

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$$\begin{aligned}
 (K - m_1 \omega^2)(K - m_2 \omega^2) - K^2 &= 0 \\
 K^2 - K(m_1 + m_2)\omega^2 + m_1 m_2 \omega^4 - K^2 &= 0 \\
 \omega^2 (m_1 m_2 \omega^2 - K(m_1 + m_2)) &= 0 \\
 \omega &= 0 \\
 \omega^2 &= \frac{K(m_1 + m_2)}{m_1 m_2} \\
 \omega &= \sqrt{\frac{K(m_1 + m_2)}{m_1 m_2}}
 \end{aligned}$$

So, this $A_1 = A_2$ if you substitute $A_1 = A_2$ if you substitute this value of omega 2, then you can find to omega square will be equal to $K(m_1 + m_2) / m_1 m_2$; if you substitute in this equation $A_1 = A_2$ equal to... So this becomes k by so this equation gives $k - m_1 \omega^2 = A_1$ equal to $k - m_2 \omega^2 = A_2$. So, $A_1 = A_2$ becomes $K - K - m_1 \omega^2 = K - K - m_2 \omega^2$ you substitute the value of omega square that is equal to $k(m_1 + m_2) / m_1 m_2$. So, if I will substitute it here in this equation. So, this reduces to $-m_2 \omega^2 = -m_1 \omega^2$. So, this becomes $-m_2 \omega^2 = -m_1 \omega^2$. So, in this case you can observe that this amplitude ratio is inversely proportional to the mass ratio of the system $A_1 = A_2$ equal to m_2 / m_1 .

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So, in case of a 2 rotor system similarly you can write. So, this is a 2 rotor system. So, in this case of 2 rotator system also you can write if the inertia is I_1 and this inertia I_2 . So, you can write this A_1 by A_2 that is the amplitude of rotation of this mass by amplitude of rotation of this mass will be equal to I_2 by I_1 . So, it will inversely proportional to the inertia ratio in case of this 2 mass or 2 rotor system you can proceed in this way also in another way also. So, in this case I can write when they are moving with same frequency ω , let me find the same relation by another method. So, this is the system; so in this system when it is rotating with frequency. So, already you know that 1 frequency equal to 0 the other frequency you have to find.

So, let we have given that this system will have a length of this rod equal to l and when it is rotating with the other frequency; so there will be node point here; this node point means this point will have no vibration. So, you can assume that this 2 rotor system is equivalent to a cantilever beam or rotating cantilever beam. So, in which it is fixed at this point. So, at this point it is fixed. So, let this length is l_1 this length is l_2 . So, this natural frequency of this part you can write equal to; so ω_{n1} or ω_{n1} you can write natural frequency of this part it is equal to root over stiffness of this part by. So, let stiffness is q_1 .

So, stiffness of this part by inertia of this part q_1 by I_1 . Similarly, you can write this ω_{n2} you can write or this part you can write it is equal to q_2 by I_2 .

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$$\begin{aligned} \frac{T}{J} &= \frac{G\theta}{L} \\ q &= \frac{T}{\theta} = \frac{GJ}{L} \\ q_1 &= \frac{GJ}{L_1} \\ q_2 &= \frac{GJ}{L_2} \\ \omega_1 = \omega_2 &\Rightarrow \sqrt{\frac{q_1}{I_1}} = \sqrt{\frac{q_2}{I_2}} \end{aligned}$$

But this q_1 is nothing but so q_1 . So, already you know this formula for torsional vibration of this system T by J equal to $G\theta$ by L you know this formula. So, from this you know T by θ equal to GJ by L . So, T by θ is nothing but the stiffness of the system so q . So, you can have q_1 equal to GJ or as I am taking the same system or same rod. So, I can write GJ by L_1 ; similarly, I can write q_2 equal to GJ by L_2 . So, the as the natural frequency is same for both the parts I can write ω_1 equal to ω_2 . So, this implies that root over q_1 by I_1 ; that means GJ by $L_1 I_1$ will be equal to root over GJ by $L_2 I_2$.

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$$\begin{aligned} \frac{1}{L_1 I_1} &= \frac{1}{L_2 I_2} \\ \boxed{\frac{L_1}{L_2} &= \frac{I_2}{I_1}} \\ \boxed{\frac{A_1}{A_2} &= \frac{I_2}{I_1}} \end{aligned}$$

So, from this you can find that I_1 by L_1 I_1 equal to I_2 by L_2 I_2 . So, from this you can see that this L_1 by L_2 L_1 by L_1 by L_2 equal to I_2 I_1 . And from this you can see from this figure so the amplitude ratio is amplitude ratio will proportional to this L_1 L_2 . So, this amplitude ratio A_1 by A_2 will be equal to so amplitude ratio will be equal to I_2 by I_1 . So, in this way you can show also that this amplitude ratio is inversely proportional to the inertia ratio.

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$$\frac{I}{J} = \frac{G\theta}{L}$$

$$q = \frac{I}{\theta} = \frac{GJ}{L}$$

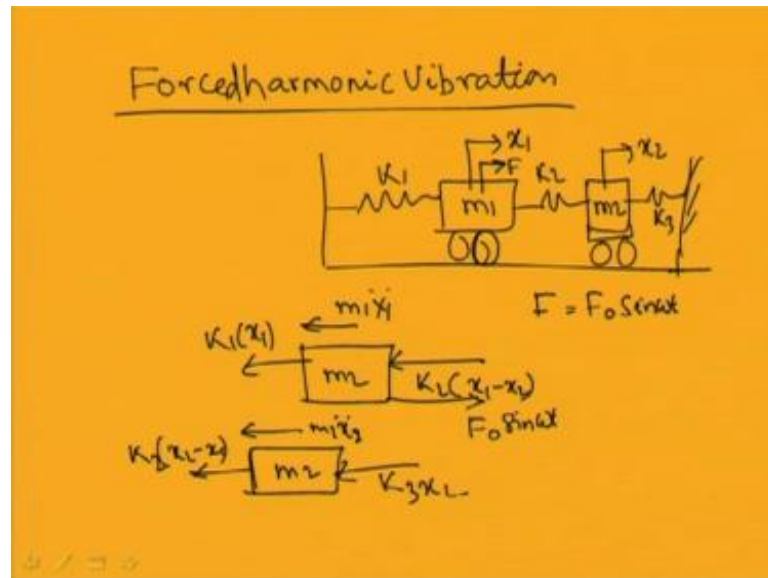
$$q_1 = \frac{GJ}{L_1}$$

$$q_2 = \frac{GJ}{L_2}$$

$$\omega_1 = \omega_2 \Rightarrow \sqrt{\frac{GJ}{L_1 I_1}} = \sqrt{\frac{GJ}{L_2 I_2}}$$

And, you can find for a given system parameters GJ and length of the system. So, you can find the natural frequency ω also. So, one natural frequency in this 2 rotor system equal to 0 and the other method frequency will be equal to GJ by $L_1 I_1$. And this node point you can find by using this relation. So, you know the inertia of the system. So, by using that inertia ratio you can find L_1 , L_2 and also you know L equal to L_1 plus L_2 . So, by using that you can find the node point. So, after finding this node point you can find this amplitude ratio. So, in this way you can find the response of a degenerated system or semi definite system. So, till now we have studied about the free vibration response of 2 degrees of freedom system.

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So, let us see the forced harmonic vibration of a 2 degree of freedom system, forced force harmonic vibration. So, in case of force harmonic vibration the system is subjected to a harmonic force. So, for simplicity we can take the same system what we have studied before and we can write the equation motion. So, let us take the system. So, this is a spring mass damper system. So, this K_1 this is K_2 and I will take another spring also this is K_3 . So, this is mass m_1 this is mass m_2 and so this mass m_1 is moving with displacement x_1 . So, this x_1 and x_2 are the generalized coordinate of the system. So, in this case you know that the equation motion equal to $m_1 \ddot{x}_1 = 0$ $m_2 \ddot{x}_2 = 0$. So, for free vibration case you have already studied this equation motion. So, let me give a force or let me assume that this mass m_1 is subjected to a force.

So, this is F and this force F is nothing but this is equal to $F_0 \sin$ or $F_0 \sin \omega t$. So, I can write the equation motion by drawing the free body diagram of the system. So, by drawing the free body diagram of the system you can see. So, let me draw the free body diagram of this mass m_1 . So, in this case it will have a inertia force in this direction that is equal to $m_1 \ddot{x}_1$ and spring force $k_1 x_1$ and this side we have a spring force $k_2 (x_1 - x_2)$. And in addition to this it is subjected to an external force that is equal to F and this external force equal to $F_0 \sin \omega t$ for this mass m_2 . So, the free body diagram of this mass m_2 is same as before. So, this is equal to $m_2 \ddot{x}_2$ then this is equal to $k_2 (x_2 - x_1)$ and this side it is equal to $k_3 x_2$.

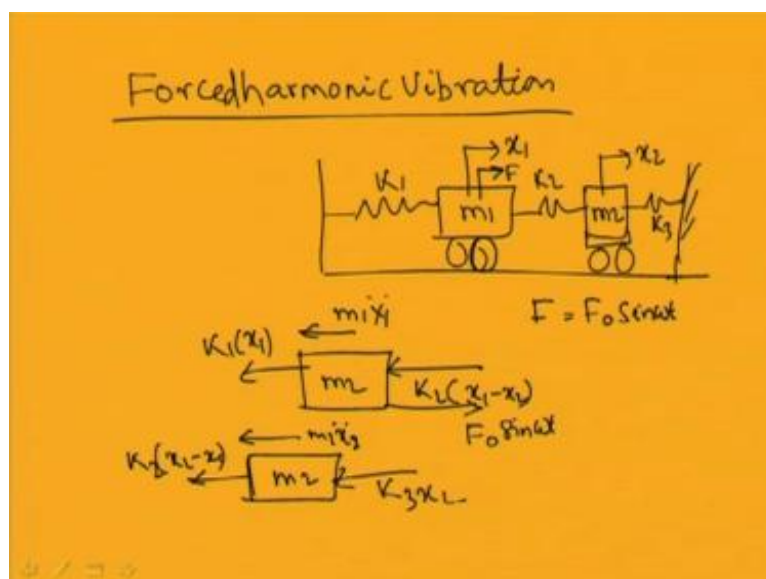
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$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} k_1+k_2 & -k_2 \\ -k_2 & k_2+k_3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F \sin \omega t \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} k_{11} & k_{12} \\ k_{21} & k_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F_0 \\ 0 \end{bmatrix} \sin \omega t$$

So, the equation motion you can write in this form. So, this is equal to $m_{11} \ddot{x}_1 + m_{12} \ddot{x}_2 + k_{11}x_1 + k_{12}x_2 = F_0 \sin \omega t$ and $m_{21} \ddot{x}_1 + m_{22} \ddot{x}_2 + k_{21}x_1 + k_{22}x_2 = 0$. So, in this way you can write the equation motion of the system. So, let us first take a general system. So, in a general system your mass matrix may be coupled and stiffness matrix may be coupled. So, for a general system I can write this equation in this form. So, it will become $m_{11} \ddot{x}_1 + m_{12} \ddot{x}_2 + m_{21} \ddot{x}_1 + m_{22} \ddot{x}_2 + k_{11}x_1 + k_{12}x_2 + k_{21}x_1 + k_{22}x_2 = F_0 \sin \omega t$. So, this is equal to $F_0 \sin \omega t$.

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So, instead of applying a force in first mass if I will apply a force in second mass I can write this equation in this form. So, it becomes 0 and this becomes $F \sin \omega t$; already you know in case of a single degree of freedom system when a system is subjected to a harmonic force of $F \sin \omega t$ the system will oscillate with the same frequency. But with and different with different magnitude and with a phase difference. So, you can assume for this case that both x_1 and x_2 are moving or oscillating with same frequency ω . So, you can assume a solution in this form $x_1 x_2$.

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The image shows handwritten mathematical work on a yellow background. It starts with the assumption of a harmonic solution:
$$\begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{pmatrix} X_1 \\ X_2 \end{pmatrix} \sin \omega t$$
 This is substituted into a matrix equation representing the system's dynamics. The resulting equation is:
$$\begin{bmatrix} K_{11} - m_1 \omega^2 & K_{12} - m_{12} \omega^2 \\ K_{21} - m_{21} \omega^2 & K_{22} - m_{22} \omega^2 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} \sin \omega t = \begin{bmatrix} F_0 \\ 0 \end{bmatrix} \sin \omega t$$
 The $\sin \omega t$ terms are cancelled out, leading to the final matrix equation:
$$\begin{bmatrix} K_{11} - m_1 \omega^2 & K_{12} - m_{12} \omega^2 \\ K_{21} - m_{21} \omega^2 & K_{22} - m_{22} \omega^2 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} F_0 \\ 0 \end{bmatrix}$$
 The matrix is labeled with the letter 'A' underneath it.

So, for steady state; so this for steady state. So, you can assume x_1 and x_2 equal to $X_1 X_2 \sin \omega t$. So, you can substitute this equation in this equation motion then it will reduce to this form. So, it will become $K_{11} - m_1 \omega^2$ $K_{21} - m_{21} \omega^2$ $K_{12} - m_{12} \omega^2$ $K_{22} - m_{22} \omega^2$ into $X_1 X_2 \sin \omega t$ equal to $F_0 0 \sin \omega t$ or I can write this equation in this form. So, this will become $K_{11} - m_1 \omega^2$ $K_{21} - m_{21} \omega^2$ $k_{12} - m_{12} \omega^2$ $k_{22} - m_{22} \omega^2$ into $X_1 X_2$ equal to $F_0 0$. So, all this is a 2 degree of freedom system or you have only 2 equations you can solve this equation to find this X_1 and X_2 by using a number of methods.

So, directly you can solve this equation like this $K_{11} - m_1 \omega^2$ into X_1 plus $K_{12} - m_{12} \omega^2$ into X_2 equal to F_0 . And the second equation

you can write $K_{21} - m_{21}\omega^2 X_1 + K_{22} - m_{22}\omega^2 X_2 = 0$. So, you can solve these 2 equations to find this X_1 and X_2 . So, these equations will be written in terms of $K_{11} - m_{11}\omega^2$ and $K_{12} - m_{12}\omega^2$ or you may use the Cramer's rule to find the equation motion or you can write this X_1 X_2 if I write this matrix. So, let this matrix I am writing it as A matrix.

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$$\begin{pmatrix} X_1 \\ X_2 \end{pmatrix} = A^{-1} \begin{pmatrix} F_0 \\ 0 \end{pmatrix} = \frac{\begin{bmatrix} K_{22} - m_{22}\omega^2 & -K_{12} + m_{12}\omega^2 \\ -K_{21} + m_{21}\omega^2 & K_{11} - m_{11}\omega^2 \end{bmatrix} \begin{pmatrix} F_0 \\ 0 \end{pmatrix}}{\begin{vmatrix} K_{11} - m_{11}\omega^2 & K_{12} - m_{12}\omega^2 \\ K_{21} - m_{21}\omega^2 & K_{22} - m_{22}\omega^2 \end{vmatrix}}$$

$Z(\omega) \rightarrow \swarrow$

So, X_1 X_2 I can write also in this form. So, X_1 X_2 will be equal to A inverse into F_1 0. So, this way also you can write. So, in this case; so you can write this equal to so it will be equal to so if you find the inverse of this matrix. So, inverse of this matrix can be obtained by finding the adjoint matrix and divided it by the determinant of this matrix. So, if you write in this way; so you can find this will becomes $K_{22} - m_{22}\omega^2$ minus $K_{21} + m_{21}\omega^2$ minus $K_{12} + m_{12}\omega^2$ plus $K_{11} - m_{11}\omega^2$ into F_0 0 by determinant of this. So, determinant equal to $K_{11} - m_{11}\omega^2$ $K_{21} - m_{21}\omega^2$ minus $K_{12} - m_{12}\omega^2$ $K_{22} - m_{22}\omega^2$. So, this side it is $K_{12} - m_{12}\omega^2$ and this $K_{22} - m_{22}\omega^2$. So, if this determinant part I can write it equal to Z omega determinant of this.

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$$x_1 = \frac{(k_{22} - m_2 \omega^2) F_0}{|Z(\omega)|}$$

$$x_2 = \frac{(k_{21} - m_1 \omega^2) F_0}{|Z(\omega)|}$$

So, if this equal to Z omega; so I can write this X 1 equal to K 2 2 minus m 2 2 omega square by determinant Z omega into F 0 and X 2 equal to k 2 1 minus m 2 1 omega square F 0 by determinant Z omega. So, in this way you can find this X 1 X 2 or in this or you may find this by using Cramer's rule also in this equation.

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$$\begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = A^{-1} \begin{pmatrix} F \\ 0 \end{pmatrix}$$

$$= \frac{\begin{bmatrix} k_{22} - m_2 \omega^2 & -k_{12} + m_{12} \omega^2 \\ -k_{21} + m_{21} \omega^2 & k_{11} - m_1 \omega^2 \end{bmatrix} \begin{bmatrix} F_0 \\ 0 \end{bmatrix}}{\begin{vmatrix} k_{11} - m_1 \omega^2 & k_{12} - m_{12} \omega^2 \\ k_{21} - m_{21} \omega^2 & k_{22} - m_2 \omega^2 \end{vmatrix}}$$

$Z(\omega) \rightarrow \leftarrow$

So, when you are using Cramer's rule then this x 1 will be will becomes. So, in this place you just replace it by F 0 0. So, it will becomes determinant of F 0 0 then this 2 terms will remain same by the determinant of A. And similarly X 2 will becomes K 1 1 minus

$m_1 \omega^2 - K_1 - K_2$ minus $m_2 \omega^2$; this part this part you may replace by F_0 by 0 F_0 0 . So, in that way by using this Cramer's rule also you can find the solution X_1 and X_2 of the system.

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$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} K_1 + K_2 & -K_2 \\ -K_2 & K_2 + K_3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F \sin \omega t \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F_0 \\ 0 \end{bmatrix} \sin \omega t$$

So, for the system we have taken before. So, in this case this mass matrix becomes m_1 0 zero m_2 and the stiffness matrix equal to K_1 K_2 minus K_2 minus K_2 K_2 plus K_3 .

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$K_1 = K_2 = K_3 = 100 \text{ N/m}$
 $m = 1 \text{ Kg}$

$$\begin{bmatrix} m & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} 2K & -K \\ -K & 2K \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F \sin \omega t \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} \sin \omega t$$

So, let me take this example same example in which I will take this K_1 equal to K_2 equal to K_3 . So, let this becomes 100 Newton per meter and then let me take m equal to

1 kg. So, in this case I can write already you have seen that the equation motion can be written in this form. So, $m \ddot{x} + \dots$; so I am taking the system. So, I have taken the system for which already I have derived the equation motion. So, I have taken this is K , this is K , this is K and I have taken this m_1 equal to m_2 equal to m . And I have to find this is x_1 x_2 and this mass m_1 is subjected to a force F . So, in this case I have already derived this equation motion $m \ddot{x}_1 + \dots$ or $m \ddot{x}_2 + \dots$ I can write $m \ddot{x}_1 + \dots$ $m \ddot{x}_2 + \dots$ plus. So, this becomes $2K - m\omega^2$ minus K minus K $2K - m\omega^2$ x_1 x_2 equal to $F \sin \omega t$. So, now I will assume a solution in this form x_1 x_2 equal to X_1 $X_2 \sin \omega t$ I can assume and find the steady state response.

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$$|Z(\omega)| = \begin{vmatrix} 2K - m\omega^2 & -K \\ -K & 2K - m\omega^2 \end{vmatrix}$$

$$= m^2 \left(\omega^4 - 4 \frac{K}{m} \omega^2 + 3 \frac{K^2}{m^2} \right)$$

$$= m^2 \left(\omega^2 - \frac{K}{m} \right) \left(\omega^2 - 3 \frac{K}{m} \right)$$

$$\omega_1^2 = \frac{K}{m}, \quad \omega_2^2 = 3 \frac{K}{m}$$

So, by assuming this thing so I can first find this $Z(\omega)$. So, $Z(\omega)$ is nothing but this becomes $2K$ determinant of this matrix $2K - m\omega^2$ minus K minus K . So, this becomes $2K - m\omega^2$; so determinant of this matrix. So, the determinant of this matrix you can expand this. So, this multiplied with this minus this multiplied with this. So, you can find the determinant becomes equal to m^2 into ω^4 minus $4K$ by m ω^2 plus $3K^2$ by m^2 . So, you can simplify this thing. So, this becomes m^2 into ω^2 minus K by m into ω^2 minus $3K$ by m . Let me write this ω_1^2 equal to ω_1^2 equal to K by m and ω_2^2 equal to $3K$ by m .

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$$|Z(\omega)| = m^2 (\omega^2 - \omega_1^2) (\omega^2 - \omega_2^2)$$
$$\omega_1 = \sqrt{\frac{K}{m}} = \sqrt{\frac{100}{1}} = 10 \text{ rad/s}$$
$$\omega_2 = \sqrt{3 \frac{K}{m}} = 17.32 \text{ rad/s}$$
$$|Z(\omega)| = 20625$$
$$X_1 = \frac{(2K - m\omega^2)F}{|Z(\omega)|} = \frac{(2 \times 100 - 25)}{20625} = 0.0848 \text{ m}$$
$$X_2 = \frac{KF}{|Z(\omega)|} = 0.0484$$

So, this equation becomes; so this determinant of Z omega becomes m square into omega square minus omega 1 square into omega square minus omega 2 square. So, here you can find your omega 1 equal to root over k by m. So, this becomes root over hundred by one. So, this becomes 10 radian per second. And similarly omega 2 becomes root 3 into K by m or so this becomes 17.32 radian per second. So, you got omega 1 and omega 2 now you can find this X 1. So, X 1 equal to from this expression you can find. So, by substituting this equation in this equation you can find X 1, X 2 already you have found that expression. So, this becomes 2 k minus m omega square into F by this determinant of this determinant Z omega. So, this determinant of Z omega you can find this equal to; so determinant of Z omega I have found it equal to 20625. So, I can substitute it is in this expression. So, this becomes 2 into 100 minus 25.

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$$\begin{aligned} |Z(\omega)| &= \left| \begin{bmatrix} 2K - m\omega^2 & -K \\ -K & 2K - m\omega^2 \end{bmatrix} \right| \\ &= m^2 \left(\omega^4 - 4\frac{K}{m}\omega^2 + 3\frac{K^2}{m^2} \right) \\ &= m^2 \left(\omega^2 - \frac{K}{m} \right) \left(\omega^2 - 3\frac{K}{m} \right) \\ \omega_1^2 &= \frac{K}{m}, \quad \omega_2^2 = 3\frac{K}{m} \\ F &= 10 \sin \omega t \\ \omega &= 5 \text{ rad/s} \end{aligned}$$

So, let me take a force F equal to 10 sin omega t; this omega also I can assume. So, let I am assuming this omega equal to 5 radian per second. So, if I am assuming this equal to 5 radian per second. So, in this case I can write this omega square equal to 25 and this becomes 20625. So, this becomes 0.0848 meter. And similarly you can find X 2 equal to K F by Z omega. So, this gives rise to 0.0484.

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$$\begin{aligned} X_1 &= \frac{(2K - m\omega^2)F}{m^2 (\omega^2 - \omega_1^2)(\omega^2 - \omega_2^2)} \\ X_2 &= \frac{KF}{m^2 (\omega^2 - \omega_1^2)(\omega^2 - \omega_2^2)} \end{aligned}$$

So, from this expression you can see all right I can write this X 1 equal to 2 K minus m omega square F by m square into omega square minus omega 1 square into omega

square minus ω_2^2 . And x_2 equal to $\frac{K F}{m(\omega_1^2 - \omega^2)}$. So, you can observe that when ω equal to ω_1 or when ω equal to ω_2 this X_1 or X_2 tends to infinity. And when ω^2 equal to $\frac{2K}{m}$ ω^2 equal to $\frac{2K}{m}$ X_1 becomes 0. So, in this class we have studied or in this module we have studied the free and forced vibration of damped and undamped system. And we have studied this semi definite system; we have derived the equation motion by using different principles. And today class we have studied about the force vibration of damped system. Next class will study about using this force vibration will study the vibration absorber or principle of vibration absorber. And will apply this vibration absorber principle to suppress the vibration or absorb the vibration for different mechanical systems.