


**Non-Linear Vibration**  
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**Module - 5**  
**Numerical Techniques**  
**Lecture - 3**  
**Frequency Response Curves**

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<b>4</b>  <b>Numerical Techniques</b>	<b>28</b>	Time response, Numerical Techniques: Runga-Kutta method,
	<b>29</b>	Wilson- Beta method, FFT analysis, Poincare' section of fixed-point, periodic, quasi-periodic and chaotic responses. Lyapunov exponents
	<b>30</b>	Frequency response curves: solution of polynomial equations, solution of set of algebraic equations, Continuation Algorithm, Basin of attraction: point to point mapping and cell-to-cell mapping.



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So welcome to today class of non-linear vibration. So, today class we are going to study about the frequency response curves, and then some continuation techniques, and Basin of attraction in the non-linear system.


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**Duffing Equation**

$$\ddot{x} + \omega_n^2 x + 2\varepsilon\zeta\omega_n \dot{x} + \varepsilon\alpha x^3 = \varepsilon f \cos\Omega t$$

$$x = a \cos(\Omega t - \gamma) + O(\varepsilon)$$

$$\left[ \zeta^2 + \left( \sigma - \frac{3\alpha}{8\omega_n^2} a^2 \right)^2 \right] a^2 = \frac{f^2}{4\omega_n^2}$$

$$\underline{\Omega = \omega_n}, \quad \underline{\Omega = \omega_n + \varepsilon\delta}$$


So, previous two class in this module, we have discussed about the time response of the system, so how to obtain the time response we have discussed in this last two lecture; and today lecture we are going to study, how to plot the frequency response of the system. So, in this module we are discussing about the numerical techniques, one can use to study the non-linear systems.

For example, let us take the Duffing equation; so in this case of Duffing equation one can write the equation motion in this form, so that is  $x$  double dot plus  $\omega_n^2 x$  plus  $2\varepsilon\zeta\omega_n \dot{x}$  plus  $\varepsilon\alpha x^3$  equal to  $\varepsilon f \cos\Omega t$ . Here  $x$  is the response amplitude,  $\omega_n$  is the natural frequency of systems, and  $\zeta$  is the damping factor or a damping ratio, and this  $\alpha$  is the coefficient of the cubic non-linear term, and  $\varepsilon$  is the book keeping parameter, and  $f$  is the forcing amplitude, and capital  $\Omega$ , so this  $\Omega$  is the forcing frequency of the system.

So in this case already we know, we can use different methods to find the find this solution of the system, so where the solution of the systems can be written in this form, that is  $x$  equal to  $a \cos(\Omega t - \gamma) + O(\varepsilon)$ ; so one can write the solution of this equation in this form by using different methods. So, different methods include this perturbation methods, by method of multiple scale, Lindstedt poicare method, method of averaging, or one can use this harmonic balance method also in this case.

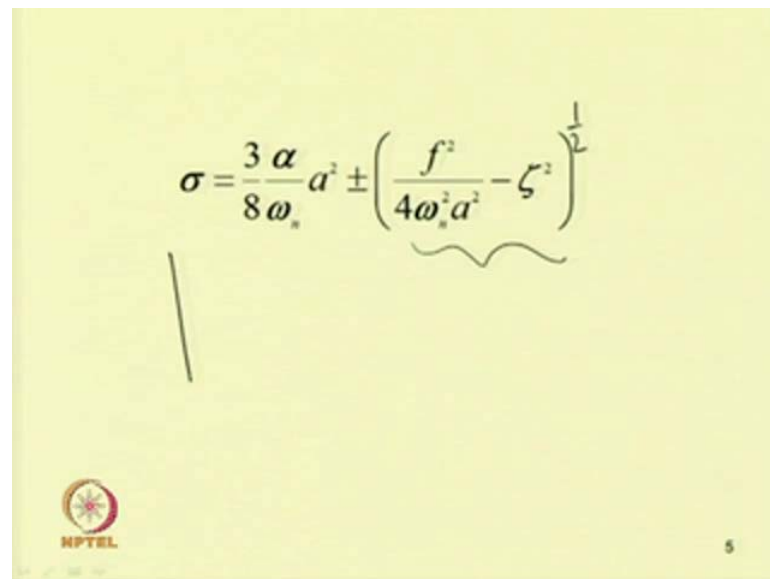
So, the first order solution of this system can be given by this equation,  $x$  equal to  $a \cos(\omega t - \gamma)$ ; so if one consider the primary resonance condition, so that is in case of primary resonance condition, that is when this external frequency is nearly equal to the frequency natural frequency of the system, so this is nearly equal to the natural frequency of the system, or one can write this  $\omega$  equal to  $\omega_n + \epsilon \sigma$ , where  $\sigma$  is the detuning parameter.

So, one can write this external frequency  $\omega$  equal to  $\omega_n + \epsilon \sigma$ , where  $\sigma$  is the detuning parameter, and by using method of multiple scale, so one can obtain, one can obtain a frequency amplitude relation in this form. So where the frequency amplitude relation can be given by, so this  $\zeta^2 + \sigma^2 - 3 \frac{8\alpha}{\omega_n^4} a^2$  equal to  $\frac{f^2}{4\omega_n^4}$ , here in this equation one can find the coefficient, one can find that  $a$  is of the order of  $\epsilon^{1/2}$ ; a square in to 2 a square square then  $a$  to the power fourth, and multiply by outside a square, so in this equation it is written in the form of  $a$  to the power six, the highest order amplitude is six, and but one can see that this detuning parameter is of the quadratic order, that is  $\sigma^2$ .

So this equation one can write, using either  $\sigma^2$ , or one can use the variable, so taking one as the unknown variable either  $\sigma$  or  $a$ , one can write this equation in a quadratic form using  $\sigma$ , or using a sixth order equation in terms of  $a$ . The same equation can be written either in quadratic form in terms of  $\sigma$ , or sixth order equation in terms of  $a$ .

So, now one has to solve this equation to find the response of the system, or one can plot this frequency response, that is amplitude versus  $\sigma$ , that is detuning parameter or amplitude versus  $\omega$ , as  $\omega$  equal to  $\omega_n + \epsilon \sigma$ . So this plot which in, which we can plot  $a$  versus  $\sigma$ , or  $a$  versus  $\omega$  is the frequency response curve of the system. So now so in this, in this particular case, so it is easier to solve this quadratic equation in terms of  $\sigma$ .

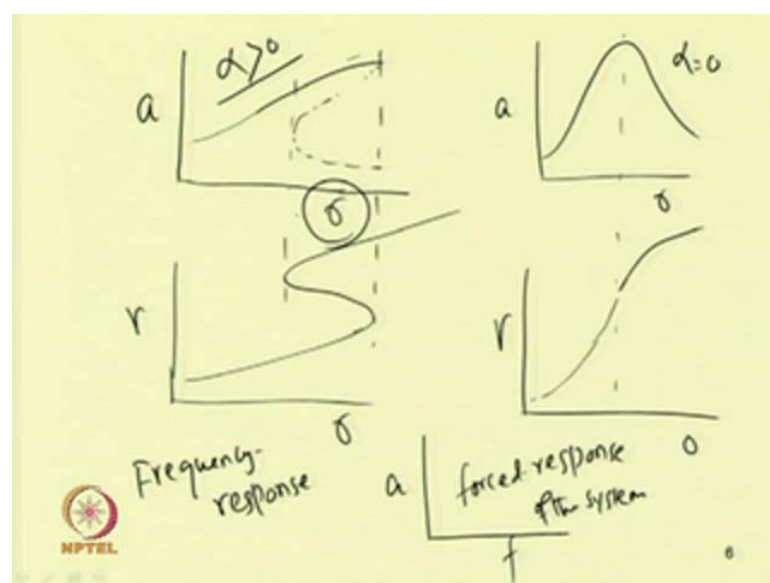
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$$\sigma = \frac{3\alpha}{8\omega_n} a^2 \pm \left( \frac{f^2}{4\omega_n^2 a^2} - \zeta^2 \right)^{\frac{1}{2}}$$


The image shows a handwritten equation for  $\sigma$  in terms of  $a$ ,  $f$ ,  $\alpha$ ,  $\omega_n$ , and  $\zeta$ . Below the equation, there is a vertical line and a small circle with a horizontal line passing through its center, representing a geometric interpretation of the equation.

And if you can write in terms of sigma, one can write this equation in this form, so it will be so to the power 1 by 2, so it will be sigma will be equal to 3 by 8 alpha by omega n a square plus minus f square by 4 omega n square a square minus zeta square to the power 1 by 2. So in this case, first one has to find this term so when this term equal to is positive, then one can find this two roots, and if it is negative, then this will yield a imaginary term; so one has to first check for what value of this forcing parameter one gets the real parameter, now one can plot this response in terms of a and sigma.

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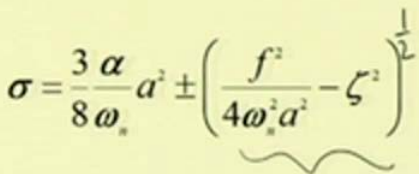
So, if one plot let us plot, so for positive value of sigma or positive value of alpha, so if one plot  $a$  versus sigma, the curve will be so one can one can plot this curve, and one can see that this curve will be similar to this, so this is  $a$  that is the amplitude, one can also plot the face of the system, that is gamma. So, gamma versus sigma also one can write so here, one can see so if it is, so one can plot this gamma versus alpha also. So, in this way one can plot this  $a$  versus gamma,  $a$  versus sigma, or gamma versus sigma, so this for alpha greater than 0.

So, one can plot also for alpha less than 0 or alpha equal to 0, alpha equal 0 is the linear system, and already we know that, for alpha equal to 0 the system response will be like this,  $a$  versus sigma, if one plot then the response will be like this. For in case of  $a$  versus for alpha equal to 0 similarly, one can plot the gamma versus sigma also, so in this case gamma versus sigma, so one can get, so the response will be like this. So gamma is the face, and  $a$  is the amplitude of the system; so this curve  $a$  versus sigma is the frequency response curve of the system.

Similarly, one can plot the force response curve by plotting this  $a$  versus sigma, or  $a$  versus so if one plot, this  $a$  amplitude versus this forcing parameter, then it will be forcing response of the system or force response of the system; and similarly, so this is the frequency response so here we are plotting frequency frequency part, this sigma is the frequency part, this is the detuning parameter, so here for alpha greater than 0, so one can get this curve.

And we can later discuss that in this case, one can have this jump off jump down phenomena, and in this class we are particularly interested to know, how we are going to find this response when we have or what are numerical techniques, we are going to use to solve this type of equation, or this type of algebraic equation or if you have a number of equations, then what is the methods we are going to solve.

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$$\sigma = \frac{3\alpha}{8\omega_n} a^2 \pm \left( \frac{f^2}{4\omega_n^2 a^2} - \zeta^2 \right)^{\frac{1}{2}}$$

The slide shows a handwritten equation for  $\sigma$ . The equation is  $\sigma = \frac{3\alpha}{8\omega_n} a^2 \pm \left( \frac{f^2}{4\omega_n^2 a^2} - \zeta^2 \right)^{\frac{1}{2}}$ . The term  $\frac{f^2}{4\omega_n^2 a^2}$  is underlined with a wavy line. The NPTEL logo is in the bottom left corner, and the number 5 is in the bottom right corner.

So if one interested to solve this sixth order equation instead of this quadratic equation, one can solve, also the equation with sixth order in a, and in that case one can use different methods, different numerical techniques to solve this equation; so the numerical techniques what we have already discussed are method of so already we have discussed several method; method of bisection, method of false position Newton's method, Muller method, and second methods, so one can use these methods to find the solution of this equation.

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**Duffing Equation**

$$\ddot{x} + \omega_n^2 x + 2\varepsilon\zeta\omega_n \dot{x} + \varepsilon\alpha x^3 = \varepsilon f \cos\Omega t$$

$$x = a \cos(\Omega t - \gamma) + O(\varepsilon)$$

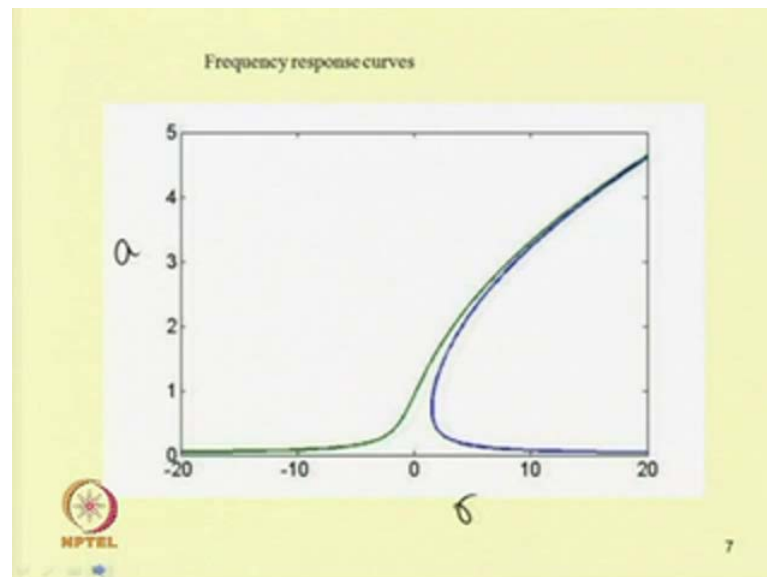
$$\left[ \zeta^2 + \left( \sigma - \frac{3\alpha}{8\omega_n} a^2 \right)^2 \right] a^2 = \frac{f^2}{4\omega_n^2}$$

$\Omega = \omega_n, \quad \Omega = \omega_n + \varepsilon\delta$

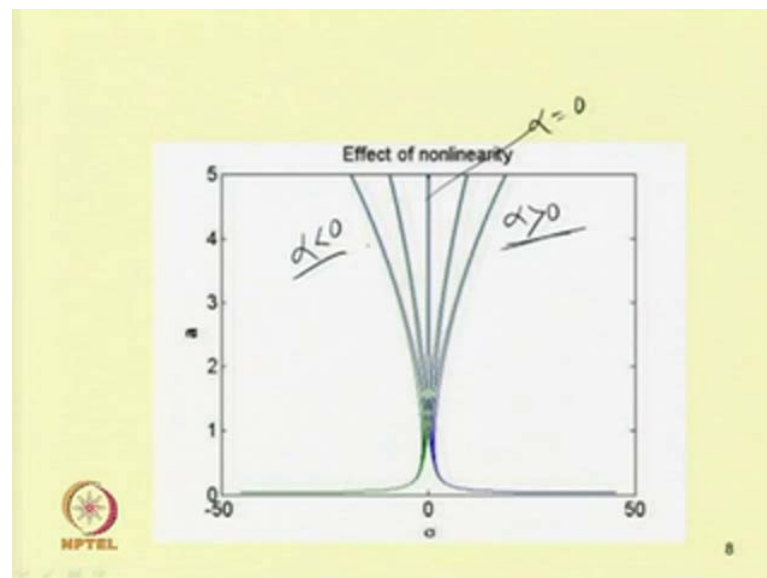
The slide shows the Duffing Equation and its solution. The equation is  $\ddot{x} + \omega_n^2 x + 2\varepsilon\zeta\omega_n \dot{x} + \varepsilon\alpha x^3 = \varepsilon f \cos\Omega t$ . The solution is  $x = a \cos(\Omega t - \gamma) + O(\varepsilon)$ . The equation for  $a$  is  $\left[ \zeta^2 + \left( \sigma - \frac{3\alpha}{8\omega_n} a^2 \right)^2 \right] a^2 = \frac{f^2}{4\omega_n^2}$ . The frequency  $\Omega$  is given by  $\Omega = \omega_n$  and  $\Omega = \omega_n + \varepsilon\delta$ . The NPTEL logo is in the bottom left corner, and the number 4 is in the bottom right corner.

But, in this case we have seen only we have a single equation, and which we have solved to find the response of the system, but sometimes we may have more number of equations, and that time we can we have solve this equation, or we have to solve a system of equations by using Newton's method.

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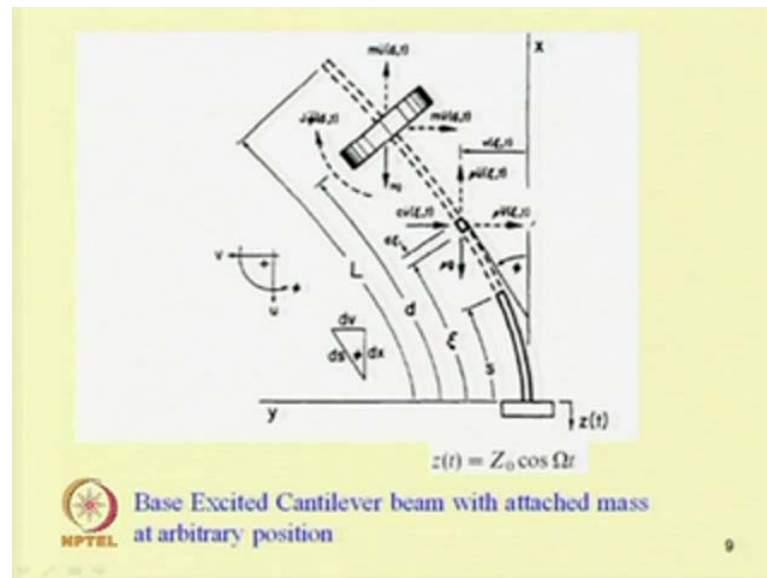
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So, this is the frequency response curve. For this frequency response curve for this Duffing equation, or similar equation, equation similar to Duffing type, and so here the effect of nonlinearity is shown; so this is for alpha equal to 0, so these are for alpha less

than 0, and this is for  $\alpha$  greater than 0; so for  $\alpha$  greater than 0, so which shows hardening type of spring the response tilts towards right, and for  $\alpha$  less than 0, when this system is that of a soft spring, then the response tilt towards left. And for  $\alpha$  equal to 0, this is the linear curve, one can get similar due to the presence of damping, so this response amplitude will decrease, those things in details will be covered in module six.

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So let us take another example, so in this example, this is a base excited cantilever beam with attached mass at arbitrary position, so in this case for different position of the system, one can observe this internal resonance.



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Using generalized Galerkin's procedure governing temporal equation becomes

$$\ddot{u}_n + 2\varepsilon\zeta_n\dot{u}_n + \omega_n^2 u_n - \varepsilon \sum_{m=1}^{\infty} f_{nm} u_m \cos \phi \tau$$


Parametric forcing term

$$+ \varepsilon \sum_{k=1}^{\infty} \sum_{l=1}^{\infty} \sum_{m=1}^{\infty} \{ \alpha_{klm}^n u_k u_l u_m + \beta_{klm}^n u_k \dot{u}_l \dot{u}_m$$

$$+ \gamma_{klm}^n u_k u_l \ddot{u}_m \} = 0, \quad n = 1, 2, \dots, \infty$$

Cubic geometric nonlinearities

Cubic inertial nonlinearities      Cubic inertial nonlinearities



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And instead of a single governing, so instead, so the governing equation of motion can be written in this form. So, this is the covering temporal equation of motion, so in this case this  $u_n$  is the time modulation,  $\zeta_n$  is the damping parameter,  $\omega_n$  is the natural frequency, and  $f_{nm}$  is the forcing term; so here for so here, these two are the cubic geometric nonlinearity, and this is the cubic inertial nonlinearity, so we have two inertial non-linear term  $u \dot{u}$  and  $\dot{u} \dot{u}$ ; here  $u \dot{u}^2$  into  $u_k$  this is the cubic non-linear inertial non-linear term. Also this is  $u \ddot{u}$  this is another cubic inertial non-linear term, so we will study about this system in detail in module six.


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$$\left. \begin{aligned} 2\omega_1(\zeta_1 a_1 + a_1') - \frac{1}{2}\{f_{11} a_1 \sin 2\gamma_1 \\ + f_{12} a_2 \sin(\gamma_1 - \gamma_2)\} \\ + 0.25 Q_{12} a_2 a_1^2 \sin(3\gamma_1 - \gamma_2) = 0, \\ 2\omega_1 a_1(\gamma_1' - \frac{1}{2}\sigma_1) - \frac{1}{2}\{f_{11} a_1 \cos 2\gamma_1 \\ + f_{12} a_2 \cos(\gamma_1 - \gamma_2)\} + \frac{1}{4} \sum_{j=1}^2 \alpha_{e1j} a_j^2 a_1 \\ + \frac{1}{4} Q_{12} a_2 a_1^2 \cos(3\gamma_1 - \gamma_2) = 0, \\ 2\omega_2(\zeta_2 a_2 + a_2') - \frac{1}{2} f_{21} a_1 \sin(\gamma_2 - \gamma_1) \\ + \frac{1}{4} Q_{21} a_1^2 \sin(\gamma_2 - 3\gamma_1) = 0, \\ 2\omega_2 a_2(\gamma_2' + \sigma_2 - 1.5\sigma_1) - \frac{1}{2} f_{21} a_1 \cos(\gamma_2 - \gamma_1) \\ + \frac{1}{4} \sum_{j=1}^2 \alpha_{e2j} a_j^2 a_2 + \frac{1}{4} Q_{21} a_1^2 \cos(\gamma_2 - 3\gamma_1) = 0, \end{aligned} \right\} 1.3$$

Reduced Equations

where

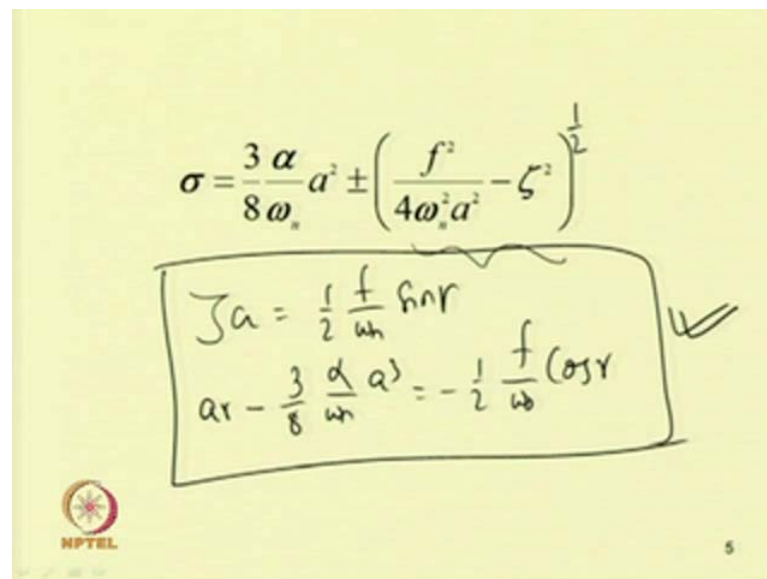
$$\gamma_1 = -\beta_1 + \frac{1}{2}\sigma_1 T_1,$$

$$\gamma_2 = -\beta_2 + (1.5\sigma_1 - \sigma_2) T_1.$$


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But in the present case the objective is to show, that in this case, if we are considering the internal resonance, so one can get a set of equations or one can by using this method of multiple scale. So, one can get a set of equation here considering 1 is to 3 internal resonance case, so here one can obtain four set of equations, so these are the four equations; unlike in case of this duffing equation where one will get two reduced equations only.

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$$\sigma = \frac{3\alpha}{8\omega_n} a^2 \pm \left( \frac{f^2}{4\omega_n^2 a^2} - \zeta^2 \right)^{\frac{1}{2}}$$

$$\zeta a = \frac{1}{2} \frac{f}{\omega_n} \sin \gamma$$

$$a^3 - \frac{3}{8} \frac{\alpha}{\omega_n} a^3 = -\frac{1}{2} \frac{f}{\omega_n} \cos \gamma$$

So, the reduced equation in case of Duffing equation can be written in this form, zeta a equal to 1 by 2 by omega n sin gamma, and this a gamma minus 3 by 8 alpha by omega n a cube equal to minus 1 by 2 f by omega 0 cos gamma; so this equations are written for the steady state, so one has two equations here, one can solve this two equation in case of the Duffing equation.

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$$\begin{aligned}
 & 2\omega_1(\zeta_1 a_1 + a_1') - \frac{1}{2}\{f_{11} a_1 \sin 2\gamma_1 \\
 & + f_{12} a_2 \sin(\gamma_1 - \gamma_2)\} \\
 & + 0.25 Q_{12} a_2 a_1^2 \sin(3\gamma_1 - \gamma_2) = 0, \\
 & 2\omega_1 a_1(\gamma_1' - \frac{1}{2}\sigma_1) - \frac{1}{2}\{f_{11} a_1 \cos 2\gamma_1 \\
 & + f_{12} a_2 \cos(\gamma_1 - \gamma_2)\} + \frac{1}{4} \sum_{j=1}^2 \alpha_{e1j} a_j^2 a_1 \\
 & + \frac{1}{4} Q_{12} a_2 a_1^2 \cos(3\gamma_1 - \gamma_2) = 0, \\
 & 2\omega_2(\zeta_2 a_2 + a_2') - \frac{1}{2} f_{21} a_1 \sin(\gamma_2 - \gamma_1) \\
 & + \frac{1}{4} Q_{21} a_1^3 \sin(\gamma_2 - 3\gamma_1) = 0, \\
 & 2\omega_2 a_2(\gamma_2' + \sigma_2 - 1.5\sigma_1) - \frac{1}{2} f_{21} a_1 \cos(\gamma_2 - \gamma_1) \\
 & + \frac{1}{4} \sum_{j=1}^2 \alpha_{e2j} a_j^2 a_2 + \frac{1}{4} Q_{21} a_1^3 \cos(\gamma_2 - 3\gamma_1) = 0,
 \end{aligned}$$

Reduced Equations

where

$$\begin{aligned}
 \gamma_1 &= -\beta_1 + \frac{1}{2}\sigma_1 T_1, \\
 \gamma_2 &= -\beta_2 + (1.5\sigma_1 - \sigma_2) T_1.
 \end{aligned}$$

But, in the present case, so in this case, one has a set of four equations, so where this a 1 gamma 1 are for the first mod, and a 2 gamma 2 are for the second mod. So considering the two mod interaction, so where the first mod frequency is taken non dimensional, first mod frequency is taken to be 1, the second mod frequency is nearly 3 times the first mod; so here, 1 is to 3 internal resonance condition is considered, so in that case, so one can get a set of four equations.

So for steady state condition, so we can put this a 1 dash, gamma 1 dash, and a 2 dash and gamma 2 dash equal to 0, and by putting these terms equal to 0, so one we obtain four algebraic or transcendental equation, so solving those equations, one can obtain the response of the system.

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Now one may perturb the normalized reduced equation to obtain the Jacobian matrix  $J_c$  to study the stability for both trivial and nontrivial solution


$$\{\Delta p'_1, \Delta q'_1, \Delta p'_2, \Delta q'_2\}^T = [J_c] \{\Delta p_1, \Delta q_1, \Delta p_2, \Delta q_2\}^T$$

The first order steady state solution can be written as

$$\left. \begin{aligned} u_1 &= a_1 \cos\{(\omega_1 + \varepsilon \sigma_1/2)\tau - \gamma_1\}, \\ u_2 &= a_2 \cos\{(\omega_2 + \varepsilon(1.5\sigma_1 - \sigma_2))\tau - \gamma_2\}. \end{aligned} \right\}$$

The first-order solution of the system in terms of  $p_i, q_i$  ( $i = 1, 2$ ) can be given by

$$\left. \begin{aligned} u_1 &= p_1 \cos \bar{\omega}_1 \tau + q_1 \sin \bar{\omega}_1 \tau, \\ u_2 &= p_2 \cos 3\bar{\omega}_1 \tau + q_2 \sin 3\bar{\omega}_1 \tau. \end{aligned} \right\} \quad \bar{\omega}_1 = \omega_1 + \frac{1}{2} \varepsilon \sigma_1$$

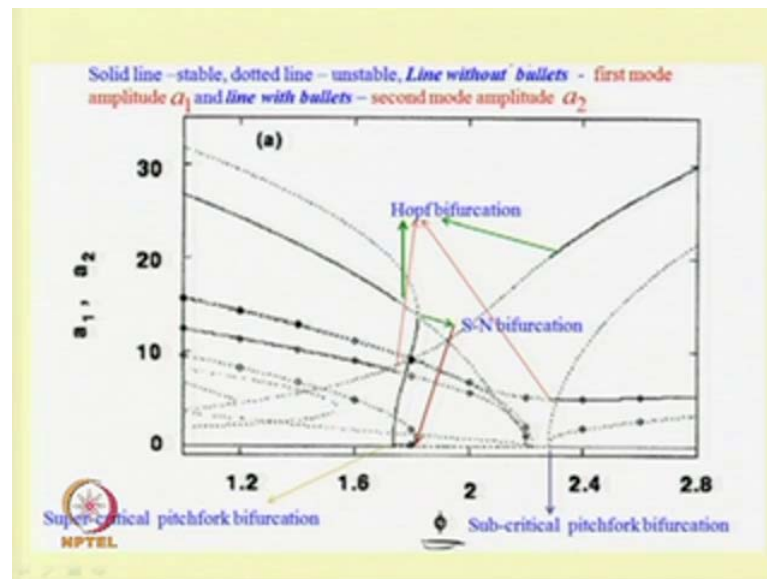
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And while solving this equation, it is required also to find the stability of the system, so to plot this different branches, one should know, so which branch is stable, and which branch is unstable. So, to study the stability of the system, so in this particular case so one can make the transformation, as we have this coupled term  $a_1 \gamma_1$  dash, and  $a_2 \gamma_2$  dash, and for trivial state this perturbation will due to the presence of this coupled term, the perturbation will not be there, and to circumvent that thing so one can use some transformation in terms of  $p$  and  $q$ .

So by using that transformation, one can write the perturbed equation in this form, so here  $p_1$  is taken equal to  $a_1 \cos \gamma_1$ , and  $p_2$  equal to  $a_2 \cos \gamma_2$ , and  $q_1$  equal to  $a_1 \sin \gamma_1$ , and  $q_2$  equal to  $a_2 \sin \gamma_2$ ; so this four reduced equation can be reduce to or can be written in terms of another four normalized reduced equation, and using those normalized equation, and perturbing those equations, one can write this equation where this is the Jacobian matrix, and by finding the Eigen value of the Jacobian matrix, one can find the or study the stability of the system.

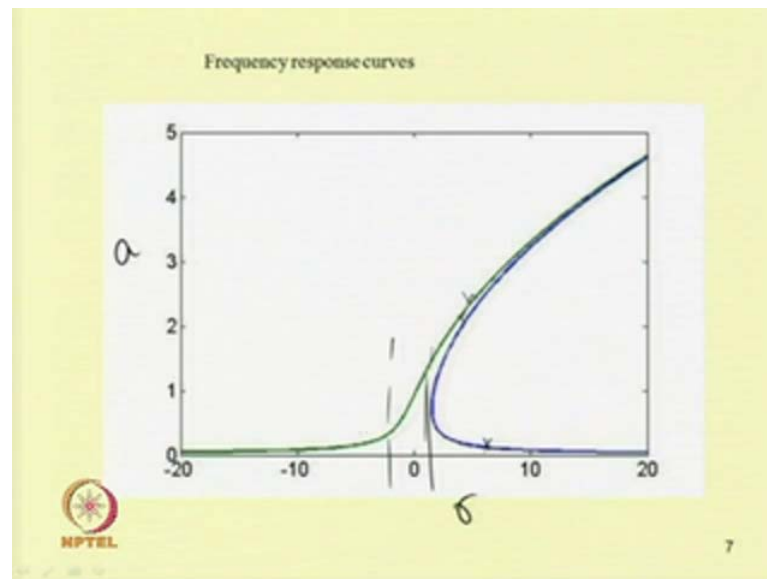
If the real part of the Eigen values of those Jacobian matrix is negative, then the system is stable, otherwise the system is unstable. So in this case, so we are getting this  $u_1$ , so we have four equations. The objective of this lecture is to show that what are numerical techniques we will use in this case to solve these four equations.

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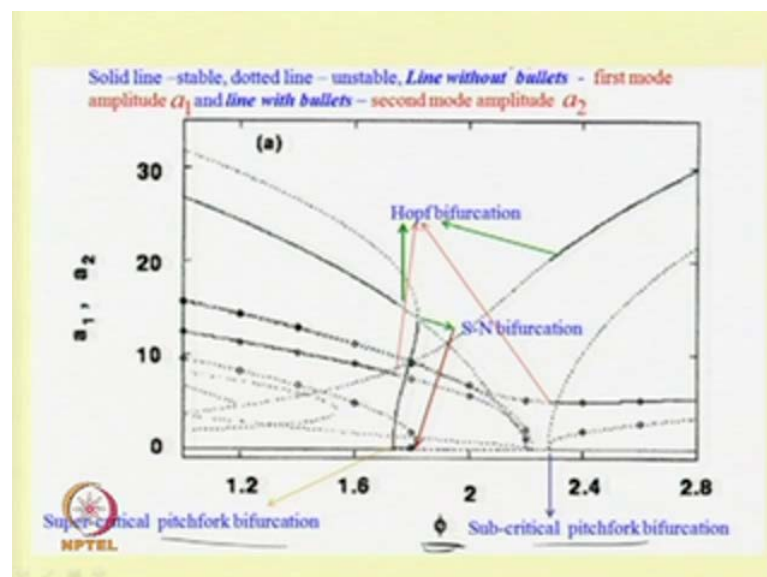
So here one can see, that one can use this Newton's method to solve this equations, so one can see this is the frequency response curve. So in this frequency response curve both  $A_1$  and  $A_2$  are plotted with respect to the forcing parameter, that is  $\phi$  forcing frequency, that is  $\phi$ , and when  $\phi$  is nearly equal to 2, so we have this principle parametric resonance case, and this curve shows the response curve, when it is near to the near to twice the natural frequency of the system. So, the lines with bubbles are for second mod, and the lines without bubbles are the first mod, so one can observe many branches of the solution. So here, the question arise how to find these branches of the solution, or how in case of Duffing equation that frequency response curve what we have seen, so we can observe that for certain parameter.

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So we have only one solution, and for some other parameters so up to this, up to this, we have only single solution, and after that we have one, two, and three solutions. So after this value so we have three solutions, but or three branches. So here we have one, two, and three branch, and before that we have one branch of solution, so the question now arise, how to obtain this multi branch solution in this case of non-linear systems.

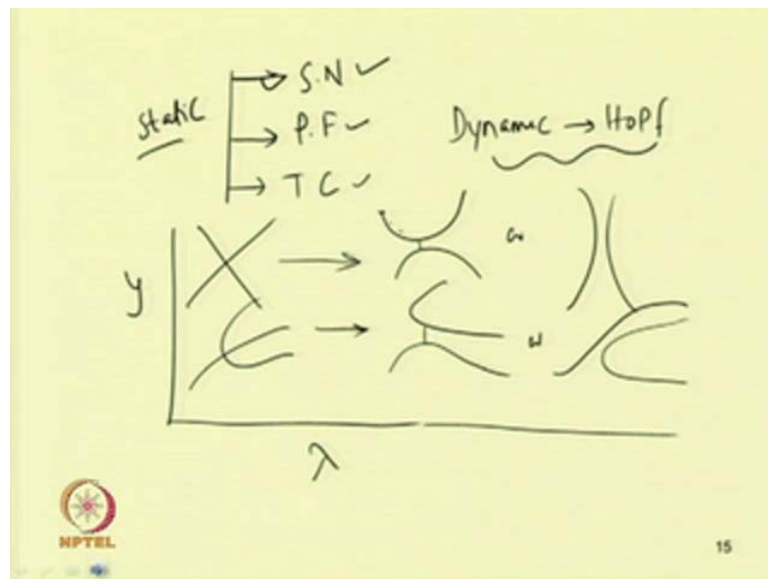
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So, here one can use some continuation techniques, and continuation techniques to find the multi branch solution. So about this continuation techniques, we will discuss to in

today's class, so while studying this branching, also one has to take care of different bifurcation points, so these for example, in this case we have this super critical pitch fork bifurcation; so these points are super critical pitch fork bifurcation, soft critical pitch fork bifurcation here, the saddle node bifurcation, and this Hopf bifurcation, so many different bifurcations occur at these points. And also we know at these bifurcation points, this field vector becomes 0. So one has to take special care at this bifurcation point to know, how the branch will continue at that point.

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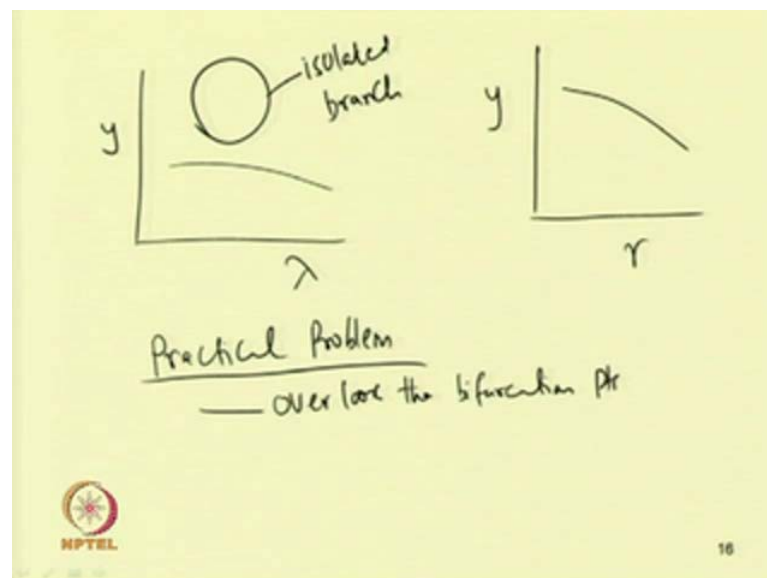
It may be noted that for one parameter, one parameter controls space problem, one parameter controls space problem, so we can have two different types of bifurcation of the fixed points, so one is the static bifurcation. So in case of the static bifurcation, so in case of static bifurcation, already we have discussed in module four.

There are saddle node bifurcation, so we can have this pitch fork bifurcation, also we have this trans critical bifurcation; so this is saddle node, pitch fork, and trans critical bifurcation. And in case of the dynamic bifurcation, so we have Hopf bifurcation, so in this static and dynamic bifurcation of the fixed point response so we know that this saddle node bifurcation and Hopf bifurcation only are the generic bifurcations, which will not change in by changing the control space.

But, the other type of bifurcation for example, so let us take this other bifurcation, so  $y$  versus  $\lambda$  is the bifurcation parameter, so if we have a trans critical type of bifurcation, so it may happen that the branching, so while we will change this parameter  $\lambda$  slightly this may the curve instead of becoming this trans critical, so it may become like this or it may be like this.

Similarly, in case of the pitch fork bifurcation, so the curve may becomes like so one branch so this is one branch so this becomes one branch, and the other branch bifurcate like this, or it may be a single branch. So this upper one, and then one can have this. So, there is some gap between so by changing, by changing slightly the parameter, by changing slightly the critical parameter  $\lambda$ , so one can see there will be some gap generated between different branch; so except the saddle node bifurcation or Hopf bifurcation other in other bifurcation, so we can see by changing the control parameter, one can obtain this gap or this will deform this bifurcation points will deform like this.

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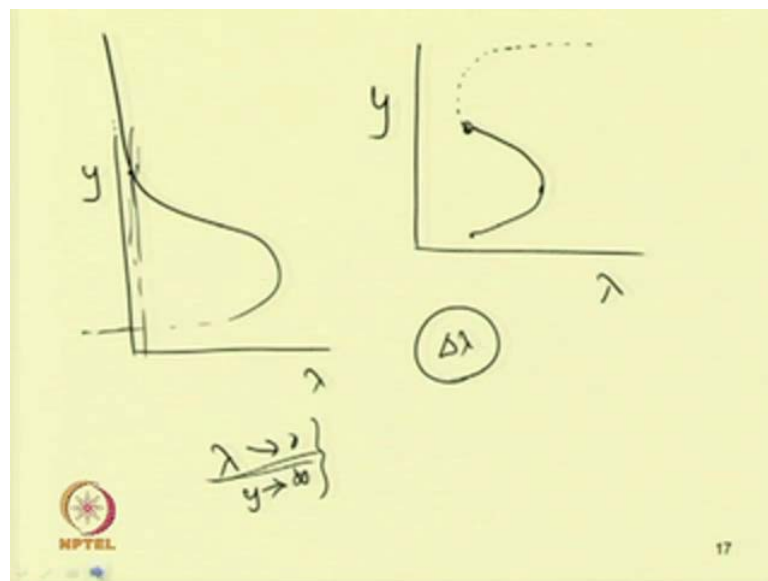


So also we may have some sometimes, we may have in case of two parameter system two parameter control parameter. So, in two parameter one can we may observe that sometimes, we may have some isolated branch; so this is an isolated branch, so this is displacement versus or parameter versus this control parameter.



So this is isolated branch, so we may have some isolated branch, so by changing that parameter so let us take some other parameter, so by changing another parameter, the curve may change. So, one has to take care or one has to note, which control parameter has to be taken for plotting the frequency response type of curve. So the practical problem one can observe, by if I am plotting this type of curves  $r$  so one may overlook the practical problems, one can so this may be, one may overlook the bifurcation point, so this bifurcation point may be overlooked also, sometimes this turning point let us take this example.

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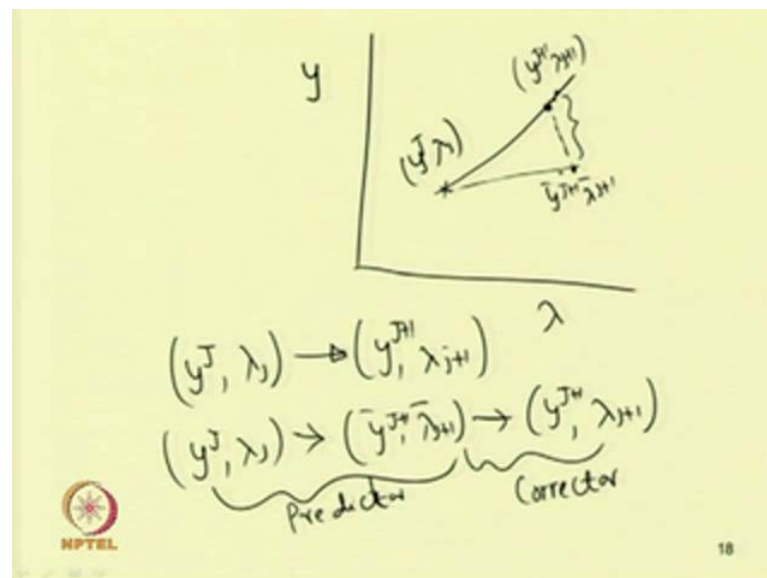
So, we may have some turning point, or some sometimes this turning point may not be the solver, may not find this turning point, so this point, and this point, may not find, or it may overlook these points. Similarly, so we may have this so what is the step size of this control parameter will take, so it may sometimes be too large or too small. So this control so we have to divide this control space into different segments in terms of this  $\Delta \lambda$ , sometimes this  $\Delta \lambda$  may be too small or too large, so that one has one may overlook certain points in this space.

So we have to discuss, or we should take care while, so starting from a particular point, how one has to continue this branch with change in the control parameter, sometimes it may happen, that so let us take this situation. So, in which so we have a branch, so this

branch so for lambda tends to 0, so for lambda tends to 0, so one can see, this y tends to so here, y tends to infinity.

But in actual case the response will be bounded, so one has to truncated the solution, or one should take, or one should start, or one should start the solution, or one should avoid taking this value of this lambda. For which it tends to infinity, so one has to avoid this range or one has to truncated the response up to this; so in that case one will get a finite value of the solution, so one has to so we have to discuss how to continue the solution, and how to switch the solution when this bifurcation points are there.

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So in this case, let us take this response, this is y versus lambda, this parameter so let us see, so this is the solution at jth iteration; let us take that this is the solution y j and lambda j, for the control parameter lambda j let the solution is y j. And actually we want to find what is the solution, that is y j plus 1 j plus 1 at lambda j plus 1 so this is the solution actual solution, we are interested to find, so to find the solution we may have to use or this continuation technique. But we are going to use, should obtain this point in two state, that is one state is the predictor step, so first we have to predicated the solution, and then let us take, so this is the predictor solution.

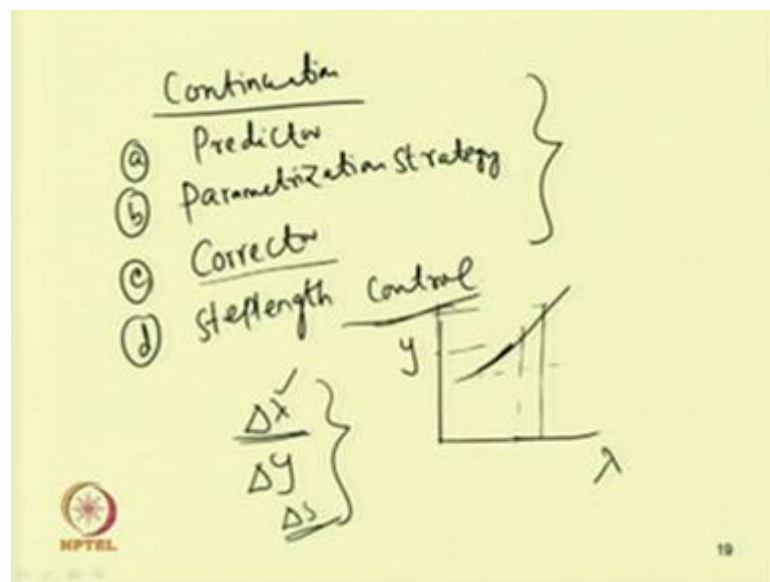
So, y bar j plus 1 lambda bar j plus 1, so this is the predictor point, and after this predictor point, we have to correct the solution by this; so this is the corrector part, and

this is the predictor part. So in this continuation from  $y_j, \lambda_j$  to  $y_{j+1}, \lambda_{j+1}$  we have some intermediate point, that is  $y_j + 1, \lambda_j + 1$  is the control parameter. So this involves two parameter two process, so in the first process so we can go from  $y_j, \lambda_j$  to  $y_j + 1, \lambda_j + 1$ , and then in the next step we will go, from  $y_j + 1, \lambda_j + 1$  to  $y_{j+1}, \lambda_{j+1}$ ; so this step from  $y_j, \lambda_j$  to  $y_{j+1}, \lambda_{j+1}$ , so is known as the predictor step, and this part is known as the corrector step.

So one can use this predictor and corrector method to find the solution, in case of this fix point response while, finding this fix point response solution, with change in control parameter, we may have a single point control parameter like your detuning parameter in case of Duffing equation, or we may have multiple parameters.

So for example, we may use this forcing parameter  $f$  or this detuning parameter  $\sigma$ , in case of the Duffing equation also, in that case it will be two parameter control space, so we may have single parameter control space, we may have two parameter control space or multi parameter control space.

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So our continuation method, so will contain a, so the continuation procedure what we are going to use, so it will have a predictor space, then which would have a parameterization strategy, how will parameterize that thing, so which would have this parameterization strategy, then we should have this corrector. And finally, we should find the step length,

so step length control so which would have this step length control. So this first three we can choose independently, and this last one this step length control depends on this other three parameter. So, in this predictor method, so one can use this ordinary differential equation solver to find the predictor point, and then one can use this parameterization strategy and corrector to solve this thing.

So in case of the corrector, so either we can control so for example, let us have this, so we can control this, we have three different ways we can correct it, so either so this  $y$  versus this  $\lambda$ , so either we can correct by so we have this three parameter, so correction can be done in three ways, so either we can branching by branching the parameter  $\lambda$ .

So, we can change this step length  $\lambda$  by taking  $\Delta \lambda$ , so this is  $\Delta \lambda$ , so this corrector, it can take  $\Delta \lambda$ , second local parameterization we can do, in case of local parameterization we can take this parameter  $\Delta y$ , and or we can take, or we can correct along this curve, along this curve, that is known as arc length parameterization, so  $\Delta s$ . So we can have three different corrector scheme, so in one case we can control this step length  $\Delta \lambda$ , second local parameterization we can do by taking this  $\Delta y$ , and third we can do this arc length parameterization by taking this  $\Delta s$ .


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**CONTINUATION OF FIXED POINTS**

There are essentially two types of continuation methods.  
They are


1. *Predictor-corrector methods* ✓  
In these methods, one approximately follows branch of solutions.
2. *Piece-wise-linear methods*  
In this methods, one exactly follows piecewise linear curve that approximates a branch of solutions.

only predictor-corrector methods are considered here.

 I. Nayfeh and B. Balachandran, Applied Nonlinear Dynamics, Wiley-VCH2004

Now, we will study these different fix. For fix point response, we will see what are the different continuation schemes? So let us see, so two basically, two schemes are there, one is the predictor corrector method which we are going to discuss now, and one may see the other method also, that is piece wise linear method; so the methods what I am going to discuss are taken, or adopted from this book by A H Nayfeh and B Balachandran Applied non-linear dynamics.

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- **Implicit function Theorem:** For a dynamical system  $\dot{x} = F(x, \alpha)$  if the Jacobian matrix  $D_x F(x_0; \alpha_0)$  is not singular, then there exists a neighbourhood around  $(x_0; \alpha_0)$  such that for each  $\alpha$  in the neighbourhood,  $\dot{x} = F(x, \alpha)$  has a unique solution  $x$ .
- At saddle-node, pitchfork and transcritical bifurcation point the Jacobian matrix is singular.

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So in this case, so for the fixed point response, first we should know this implicit function theorem which is used for making this continuation. So for a dynamical system  $\dot{x} = F(x, \alpha)$ , if the Jacobian matrix  $D_x F$  is not singular, then there exist a neighborhood around  $x_0, \alpha_0$ , such that for each  $\alpha$  in the neighborhood, so we can have a unique solution, so that means if in the neighborhood of a initial point  $x_0, \alpha_0$ .

This Jacobian matrix is not singular, then we have a unique solution; so as at the saddle node, pitchfork and transcritical point, Jacobian matrix is singular. So, we have to use different method for the continuation of the branching at those points, so one can use this implicit theorem for continuing the solution, or along a branch of the system.

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### Sequential Continuation

The simplest continuation method is *sequential scheme* and also known as *natural parameter continuation*.

For a dynamical system the equilibrium point can be obtained from the equation

$$F(x, \alpha) = 0 \quad (1)$$

$\alpha$  is used as the continuation parameter.

The interval of  $\alpha$  is divided into closely spaced intervals defined by the grid points  $\alpha_0, \alpha_1, \alpha_2, \dots, \alpha_n$

Then the solution  $x_j$  at  $\alpha_j$  is used as the predicted value or initial guess for the solution  $x_{j+1}$  at  $\alpha_{j+1}$

So in case of this, so we have the sequential continuation, the simplest continuation method is the sequential scheme, also it is known as this natural parameter continuation. So in for the equation  $\dot{x} = F(x, \alpha)$ , so for steady state as  $\dot{x} = 0$ , so we can solve this equation,  $x$  such that  $F(x, \alpha) = 0$ , so where  $\alpha$  is the continuation parameter. So in this case what we have to do, so we have to this  $\alpha$ 's range, we have to divide by  $\alpha_0, \alpha_1, \alpha_2, \dots, \alpha_n$ , and we have to find this  $x_j$  correspond to  $\alpha_j$ , so first we have to predict, and then taking some initial guess we have to predict that thing and we have to find this solution in the next step.

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The predicted value is corrected through a Newton-Raphson iteration scheme. Thus

$$x_{j+1}^{k+1} = x_{j+1}^k + r \Delta x^k \quad (2)$$

Where the subscript  $k$  is the iteration number and

$$x_{j+1}^1 = x_j$$

where  $r$  is called the *relaxation parameter*, such that  $0 < r \leq 1$  and  $\Delta x^k$  is the solution of the  $n$  linear algebraic equations

$$J_F(x_{j+1}^k, \alpha_{j+1}) \Delta x^k = -F(x_{j+1}^k, \alpha_{j+1}) \quad (3)$$

Obtained using Newton-Raphson method



So, it can be done by using this Newton Raphson's iteration scheme, so in this Newton Raphson iteration scheme, so one can take this  $x_{j+1}^{k+1}$  equal to  $x_j^k + r \Delta x^k$ , so where the subscript  $k$  is the iteration number, and  $x_j$  so at one so the first step, so this is the, so this is the, initial guess value, one can take, so here  $r$  is the relaxation parameter, such that  $0 < r \leq 1$ , so this is the relaxation parameter one can take, and  $\Delta x^k$  is the solution of the  $n$  linear algebraic equation. So, this is the equation obtained from the Newton Raphson method, so here  $F_x$  that is the first derivate of  $F$  the Jacobian matrix into  $\Delta x^k$  th iteration will be equal to minus  $f_{j+1}^k$ , so this is, this is obtained from the Newton Raphson method so by solving this equation, so one can find the solution of the system.

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The relaxation parameter  $r$  is chosen such that

$$\|F(x_{j+1}^{k+1}, \alpha_{j+1})\| < \|F(x_{j+1}^k, \alpha_{j+1})\| \quad (4)$$

- If the above relation is satisfied for  $r=1$ , then  $r$  is set equal to 1 otherwise  $r$  is halved until the above equation is satisfied.
- If the grid points  $\alpha_j$  are sufficiently close, few iterations are sufficient for obtaining an accurate solution.
- Sequential continuation will fail at such points where two or more branches meet because the Jacobian  $F_x$  is singular there.

The relaxation parameter  $r$  is chosen such that, this it has to satisfy this equation, so if the above relation is satisfied, then for  $r$  equal to 1, then  $r$  is said to set equal to 1, otherwise  $r$  is halved until the above equation is satisfied, if the grid point  $\alpha_j$  are sufficiently close, new iterations few iterations are sufficient for obtaining the accurate solution sequential continuation will fail, at as the differentiation or the derivate is equal to 0 at the at the singular point, so it will fail at the singular point, such as the saddle node bifurcation point or pitchfork bifurcation points or transcritical bifurcation point.

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**Davidenko-Newton-Raphson continuation**

- the predictor is based on solving a system of ordinary-differential equations, hence it is also called an *ordinary-differential equation predictor*

In this method,  $\alpha$  is used as continuation parameter.

Differentiating  $F(x, \alpha) = 0$  w r to  $\alpha$  yields

$$F_x(x, \alpha) \frac{dx}{d\alpha} = -F_\alpha(x, \alpha) \quad (5) \checkmark$$

Which constitutes a system of linear algebraic equations for the unknowns  $dx/d\alpha$ .

So, in this way one can use this sequential continuation technique to find so or otherwise one can use this Davidenko Newton Raphson continuation; so here the predictor is based on solving a system of ordinary differential equations, hence it is also called ordinary differential equation predictor, so in this method alpha is used as the continuation parameter. So here, differentiating this equation that is your failed equation  $F(x, \alpha) = 0$  with respect to this alpha, the continuation parameter so we can write this  $F_x(x, \alpha) \frac{dx}{d\alpha} = -F_\alpha(x, \alpha)$ , so we obtain this equation. So which constitute as we have n dimensional  $x$   $x$  is n dimensional, so we can have n or will have a set of liner algebraic equation with unknown  $dx/d\alpha$ , so where  $x$  equal to  $x_1, x_2, \dots, x_n$ . So we can with these unknown we can have a set of liner algebraic equations.



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Hence, if the Jacobian  $F_x(x, \alpha)$  is regular in the interval  $[\alpha_0, \alpha_n]$ , then

$$\frac{dx}{d\alpha} = -F_x^{-1}(x, \alpha)F_\alpha(x, \alpha) \quad \checkmark \quad (6)$$

**Solve(6) using RK4 method with initial condition  $x(\alpha_0) = x_0$**

➤ The predicted values obtained from the integration are likely to deviate from the true solutions due to truncated error. Hence, the predicted values are used as initial guesses for a **Newton-Raphson method to obtain corrected values.**

Now, this one can find this Jacobian matrix,  $f_x$   $\alpha$  in this interval  $\alpha_0$  to  $\alpha_n$ ; so one can write in this interval, this  $d x$  by  $d \alpha$  equal to minus  $F_x$  or one by  $F_x$  into  $F_\alpha x \alpha$ , so this is from the Newton's method, then by solving so this differential equation can be solved by using this ordinary differential equation.

For example, one can use this Runge Kutta fourth and Runge Kutta method, by taking this initial guess  $x \alpha_0$  equal to  $x_0$ , by taking this so one can now predict this value obtained from this integration, and this likely to do deviate from the true solution due to this truncated error. Hence, the predicated value are used as the initial guess for a Newton Raphson method to obtain the corrected value, so in this way so in the previous case, so that is simple continuation technique, so we have solved this differential we have solved the field equation.

But in case of this Newton Davidenko Newton's continuation technique so we have differentiated, we have differentiated the field equation with respect to this continuation parameter, and we got a set of system of liner algebraic equation, and also we have then solved this equation in term by using this ordinary differential equation to find the initial guess, and then by solving those equations we obtained the corrected value, so in this way one can get the next iteration points.

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**3 Arclength Continuation**

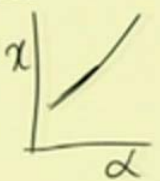
- In this method, the arclength  $s$  along a branch of solutions is used as the continuation parameter.
- $x$  and  $\alpha$  are considered to be function of  $s$ ; that is,  $x=x(s)$  and  $\alpha=\alpha(s)$  such that

$$F[x(s), \alpha(s)] = 0 \quad (7)$$

Differentiating (7) with respect to  $s$  yields

$$F_x(x, \alpha)x' + F_\alpha(x, \alpha)\alpha' = 0$$

where  $x' = dx/ds$  and  $\alpha' = d\alpha/ds$ .



Also one can use this arc length continuation technique already, I told that we have three different methods: so in first method, we have taken this delta lambda continuation, in the second case we have parameterized, so one can parameterize that thing by taking this control parameter, and in the third so we can use this arc length continuation. so in this case so along the curve, so we have to take a arc length, and we to correct it, predict it , and correct it.

So in this case, for this arc length continuation scheme, so the arc length is along the branch, so this is along the branch, so arc length along the branch of the solution is used as a continuation parameter.  $x$  and  $\alpha$ , so this is  $x$ ,  $x$  is the response  $x$  and  $\alpha$ , let me take this continuation parameter  $\alpha$ ,  $x$  and  $\alpha$  are considered to be function of  $s$ , so if they are function of  $s$ , then we can write this  $x$  equal to  $x(s)$  and  $\alpha$  equal to  $\alpha(s)$ , so that our field equation can be written in this form  $F(x(s), \alpha(s)) = 0$ . Now differentiating this equation with respect to  $s$ , we can write this  $F_x(x(s), \alpha(s))x'(s) + F_\alpha(x(s), \alpha(s))\alpha'(s) = 0$ , where  $F_x$  is the where  $x'$  is  $dx/ds$  and  $\alpha'$  is  $d\alpha/ds$ .

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Equation (8) may be rewritten as

$$[F_x | F_\alpha] \begin{Bmatrix} x' \\ \alpha' \end{Bmatrix} = [F_x | F_\alpha] \underline{t} = 0 \quad (9)$$

where the  $(n+1)$  vector  $\underline{t}$  is the tangent vector at  $(x, \alpha)$  on the path.


The system (8) consists of  $n$  linear algebraic equations in the  $(n+1)$  unknowns  $x'$  and  $\alpha'$ . To specify this unknowns uniquely, we supplement (8) with a homogeneous equation specified by Euclidean arclength normalization

$$x'^2 + \alpha'^2 = x_1'^2 + x_2'^2 + \dots + x_n'^2 + \alpha'^2 = 1 \quad (10)$$

Now this equation, now from this equation, so we can write this  $F_x F_\alpha x' \alpha'$  equal to  $F_x F_\alpha t$  equal to 0, where  $t$  so where  $n+1$  vector,  $t$  is the tangent vector, at  $x, \alpha$  on the path, so one can find this tangent vector, so the system, so this equation the system of equation 8 consist of  $n$  liner algebraic equation, in the  $n+1$  unknowns  $x'$  and  $\alpha'$ . To specify this unknown uniquely, we supplement this equation by a homogenous equation specified by this Euclid Eculiden arc length normalization. So, one can do this normalization by using this equation that is  $x'$  transpose into  $x'$  plus  $\alpha'$  square equal to, so by taking  $n$  term in  $x$ , so one can write this is  $x_1'^2 + x_2'^2 + \dots + x_n'^2 + \alpha'^2 = 1$ .

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The initial conditions for (8) and (10) are given by  
 $\underline{x = x_0} \quad \text{and} \quad \underline{\alpha = \alpha_0} \quad \text{at } s=0$   
 If the Jacobian  $F_x$  is nonsingular and  $F_\alpha$  is a zero vector, (8) and (10) yield  
 $[x'^T \alpha'] = \pm [0 \ 0 \ \dots \ 0 \ 1] \quad (11)$   
 If the Jacobian  $F_x$  is non singular and  $F_\alpha$  is a nonzero vector, one can solve (8) and (10) to determine the tangent vector  $t$  as follows.

$$F_x(x, \alpha)z = -F_\alpha(x, \alpha) \quad (12)$$


So, then the initial condition for 8 and 10 are taken, by so initial condition  $x_0$ , we can take  $x_0$  and  $\alpha_0$  at  $s$  equal to 0, so if the Jacobian matrix  $F_x$  is nonsingular and  $F_\alpha$  is a 0 vector, then we can have this equation, that is  $x'^T \alpha' = \pm [0 \ 0 \ \dots \ 0 \ 1]$ , and if the Jacobian  $F_x$  is nonsingular and  $F_\alpha$  is nonzero vector, one can solve equation 8 and 10 to determine the tangent vector  $t$ , so after determining so one can determine the tangent vector  $t$  from this equation, that is  $F_x(x, \alpha)z = -F_\alpha(x, \alpha)$ .

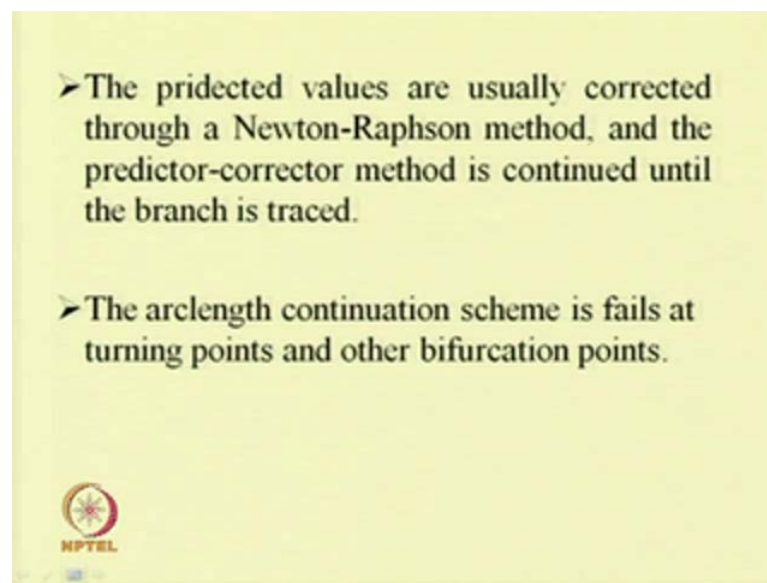
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Then owing to linearity of (8) in  $x'$  and  $\alpha'$ ,  
 $x' = z\alpha' \quad (13)$   
 where  $\alpha'$  is still unknown. Substituting (12) into the arclength condition (10) yields  
 $\alpha' = \pm(1 + z^T z)^{-1/2} \quad (14)$   
 where the plus and minus signs determine the direction of the continuation.  
 The values of  $x$  and  $\alpha$  at  $s + \Delta s$  by taking an Euler step  
 $x = x_0 + x'\Delta s \quad \text{and} \quad \alpha = \alpha_0 + \alpha'\Delta s \quad (15)$



So, then we can have this  $\dot{x}$  equal to linearity, so taking this linearity condition, that is  $\dot{x}$  equal to  $\dot{z}$   $\alpha$ , so where  $\alpha$  is still unknown. So we can substitute this equation 12 into the arc length condition 10, so that we can obtain this  $\alpha$  equation, so where this  $\alpha$  equal to  $\pm \sqrt{1 + \dot{z}^T \dot{z}}$ , where the plus and minus sign determines the direction of the continuation, the values of  $x$  and  $\alpha$  at  $s + \Delta s$  can be the values of  $x$  and  $\alpha$  at  $s$  plus  $\Delta s$ , by taking an Euler step determines, where  $x = x_0 + \dot{x} \Delta s$ , and  $\alpha = \alpha_0 + \dot{\alpha} \Delta s$ .


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So next iteration value, we can obtain in this way and by using this arc length technique one can find the continuation. The predicted values are usually corrected through a Newton-Raphson method, and the predictor corrector method is continued until the branches are traced, the arc length continuation scheme failed at the turning point and other bifurcation points.

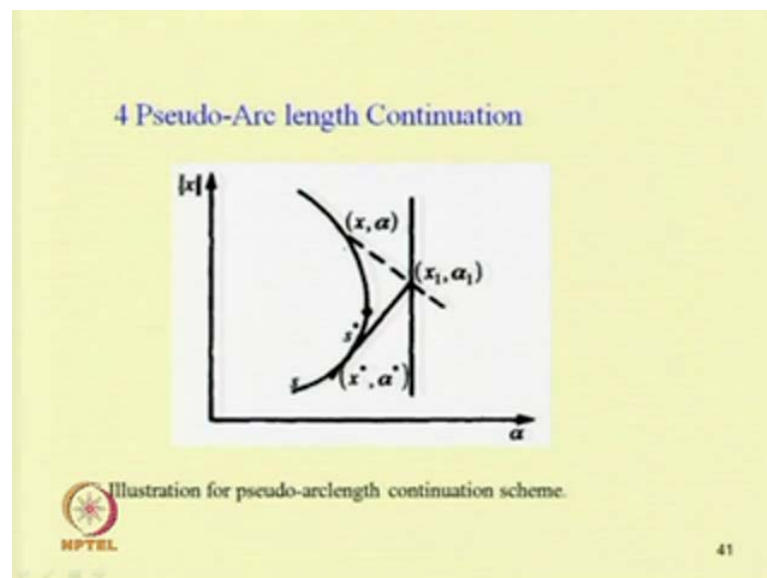
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➤ In this method, it is possible to overshoot past turning points and end up at values of  $\alpha$  where there are no solutions. To overcome this problem, one may use *pseudo-arclength continuation scheme*.



So in this method, it is possible to overshoot past turning points and end off at values of  $\alpha$  where there is no solution. To overcome this problem, so one may use this Pseudo arc length continuation scheme.

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- This procedure also uses arclength parameterization developed by Keller.
- In Figure the turning point is marked by a dot.
- Near the turning point, at  $s=s^*$ , we obtain  $(x^*, \alpha^*)$  by using Eqs.(11), (13), and (14).
- Use tangent predictor to determine the prediction  $(x_1, \alpha_1)$  at  $s^* + \Delta s$ ; that is

$$\alpha_1 = \alpha^* + \alpha^{*'} \Delta s \quad (16)$$

$$x_1 = x^* + x^{*'} \Delta s \quad (17)$$

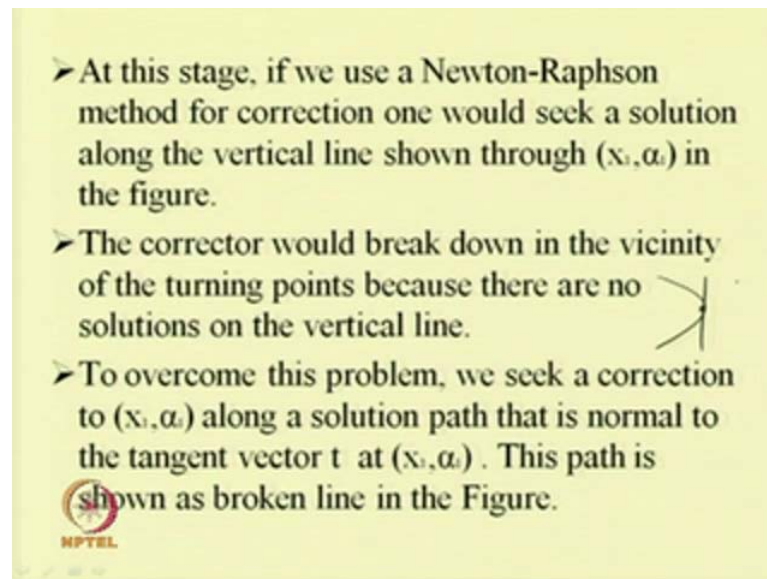
Where the step length  $\Delta s$  can be specified freely.

So one can use a Pseudo arc length instead of so this is the arc length continuation we are taking. So, let we have this saddle node bifurcation point noted by  $s^*$ , so using this arc length technique, so one can find the predictor point, and then one can correct it. And let us see this Pseudo arc length continuation, in which we have to overcome this turning point continuation.

So, this procedure also uses the arc length parameterization, so here we are discussed the method developed by Keller, so that reference I will show few minutes, so already I told that at  $s$  equal to  $s^*$ , we have this turning point. Now, one can get the near the turning point at  $s$  equal to  $s^*$ , we can obtain this  $x^*$   $\alpha^*$  by using our previous equations, so then use the tangent predictor to determine the prediction  $x_1$   $\alpha_1$  at  $s^* + \Delta s$ , so we can get the tangent.

At  $x_1$   $\alpha_1$ , so at  $x_1$   $\alpha_1$ , so this is the point  $x_1$   $\alpha_1$  so use tangent predictor to determine the predication  $x_1$   $\alpha_1$  at  $s^* + \Delta s$ , that is  $\alpha_1$  equal to  $\alpha^* + \alpha^{*'} \Delta s$ , and  $x_1$  equal to  $x^* + x^{*'} \Delta s$ , where the step length  $\Delta s$  can be specified freely.

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- At this stage, if we use a Newton-Raphson method for correction one would seek a solution along the vertical line shown through  $(x_1, \alpha_1)$  in the figure.
- The corrector would break down in the vicinity of the turning points because there are no solutions on the vertical line.
- To overcome this problem, we seek a correction to  $(x_1, \alpha_1)$  along a solution path that is normal to the tangent vector  $t$  at  $(x_1, \alpha_1)$ . This path is shown as broken line in the Figure.

So at this stage, if we use a Newton-Raphson method for correction, one would seek a solution along the vertical line, so one can seek a so this vertical line, along this vertical line one can so the corrector would break down in the vicinity of the turning point, because there are a no solutions on the vertical line. So along the vertical line, as we have the saddle node bifurcation point, so along this vertical line, there will be no solution, so this will break down.

So to overcome this problem, so we seek a solution to  $x_1, \alpha_1$  along a solution part, that is normal to the tangent vector  $t$  at  $x_1, \alpha_1$ ; so these path is shown here, so this is the path, so we can take a normal to these, so this is the, so along this path we can find the solution.



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On the solution path,  $(x, \alpha)$  satisfies

$$F(x, \alpha) = 0 \quad (18)$$


and is such that the vector

$$X = \begin{Bmatrix} x - x_1 \\ \alpha - \alpha_1 \end{Bmatrix} \quad (19) \quad \checkmark$$

is normal to the tangent vector  $t$ ; that is,

$$X^T t = 0 \quad (20)$$

substituting (16) and (17) into (19) and using the definition of  $t$ , we obtain

$$(x - x^*)^T x^{*'} + (\alpha - \alpha^*) \alpha^{*'} - [\alpha^{*2} + (x^{*'})^T x^{*'}] \Delta s = 0$$


So on the solution path,  $x, \alpha$  satisfy this kill equation, so that is  $F(x, \alpha) = 0$  and is such that, this vector  $X$  equal to  $x - x_1$  alpha minus alpha 1 is normal to the tangent vector  $t$ . that is  $X^T t = 0$  substituting this equations 16, so this equation 16 substituting this equation 16 and 17 in this equation, and using the definition of  $t$ , so one can obtain this equation, so that is  $(x - x^*)^T x^{*'} + (\alpha - \alpha^*) \alpha^{*'} - [\alpha^{*2} + (x^{*'})^T x^{*'}] \Delta s = 0$ .

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or

$$g(x, \alpha) = (x - x^*)^T x^{*'} + (\alpha - \alpha^*) \alpha^{*'} - \Delta s = 0 \quad (20)$$

because

$$\alpha^{*2} + (x^{*'})^T x^{*'} = 1$$

Equations (18) and (20) constitute the pseudo-arclength continuation scheme. In this scheme, one solves  $n+1$  nonlinear algebraic equations (18) and (20) for the  $n+1$  unknowns  $(x, \alpha)$ .



So from this or one can get this equation, so as we have this equal to 1 due to this condition, we have taken, so we have this equation, so equation 18 and 20, so this equation 18, so this equation and this  $x$  transpose  $t$  equal to 0, so they constitute this pseudo arc length continuation scheme, so in this scheme one solved  $n$  plus 1, non-linear algebraic equations 18 and 20, so for  $n$  plus one unknowns  $x$  and  $\alpha$ , so after find that thing, then on each continue this scheme.

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If we apply a Newton-Raphson scheme to (18) and (20), then at each iteration of this scheme equations are

$$\underline{x^{k+1}} = x^k + r \Delta x^{k+1} \quad (21)$$

$$\underline{\alpha^{k+1}} = \alpha^k + r \Delta \alpha^{k+1} \quad (22)$$

where  $r$  is a relaxation parameter and  $\Delta x^{k+1}$  and  $\Delta \alpha^{k+1}$  are determined from

$$\left. \begin{aligned} F_x(x^k, \alpha^k) \Delta x^{k+1} + F_\alpha(x^k, \alpha^k) \Delta \alpha^{k+1} &= -F(x^k, \alpha^k) \\ (x^{k*})^T \Delta x^{k+1} + \alpha^{k*} \Delta \alpha^{k+1} &= -g(x^k, \alpha^k) \end{aligned} \right\} \quad (23)$$

$$(24)$$


So, if we apply a Newton-Raphson scheme to 18 and 20, then each iteration of the scheme  $x$   $k$  plus 1 will be  $x$   $k$  plus  $r$  delta  $x$   $k$  plus 1,  $\alpha$   $k$  plus 1 will be  $\alpha$   $k$  plus  $r$  delta  $\alpha$   $k$  plus 1, where  $r$  is the relaxation parameter, delta  $x$   $k$  plus 1 and delta  $\alpha$   $k$  plus 1 are determined from this equation. So this equations are obtained from this Newton-Raphson method, so by solving so if a  $x$  is nonsingular, one can solve 23 equation 23, so this equation.

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If  $F_x$  is nonsingular, one can solve (23) by using bordering algorithm, which is based on the method of superposition. First, one solves the systems

$$F_x(x^k, \alpha^k)z_2 = -F_\alpha(x^k, \alpha^k) \quad (25)$$

and

$$F_x(x^k, \alpha^k)z_1 = -F(x^k, \alpha^k) \quad (26)$$

Then, it follows from (23) that

$$\Delta x^{k+1} = z_1 + z_2 \Delta \alpha^{k+1} \quad (27)$$



One can solve this equation by using this bordering algorithm which is based on the method of super position, first one solve this system  $F_x z_2 = -F_\alpha$  and  $F_x z_1 = -F$ ; so by solving this then follow, then it follows from equation 23 that  $x^{k+1}$  will be equal to  $z_1 + z_2 \Delta \alpha^{k+1}$ .

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substituting (27) into (24) yields

$$\Delta \alpha^{k+1} = -\frac{[g(x^k, \alpha^k) + z_1^T x^{*'}]}{[\alpha^{*'} + z_2^T x^{*'}]} \quad (28)$$

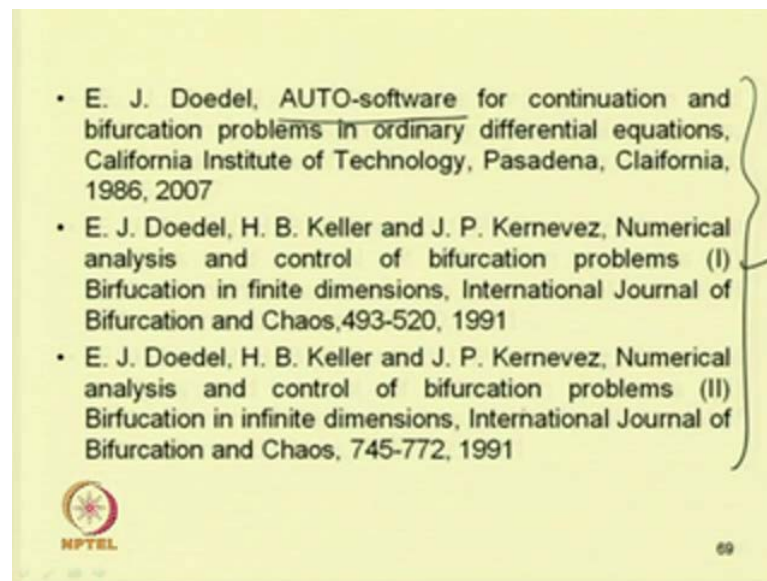
once  $\Delta \alpha^{k+1}$  is known,  $\Delta x^{k+1}$  can be determined from (27), and the iterations are continued until the required convergence is achieved.



So substituting this equation, so one obtain this equation, so after  $\Delta \alpha^{k+1}$  is known, then  $\Delta x^{k+1}$  can be determined, and then this iteration are continued

until one converge the solution. So, in this way by using different continuation scheme, so one can obtain this solutions, or one can continue the, or one can plot different branches of the solution, different branches of a multi parameter, or single parameter multi solution, or the response of a multi valued system. So, in the system when we have multiple solutions, where we can have different branches, and by using different continuation schemes, so one can obtain different branches of the solution, particularly by using this pseudo arc length continuation scheme, we can overcome this turning point. So, for more detail study on this continuation scheme, one can refer different books or the book by this Nayfeh and Balachandran, so one can use this for periodic response one can use this shooting technique or this continuation arc length continuation technique, or pseudo arc length continuation technique.

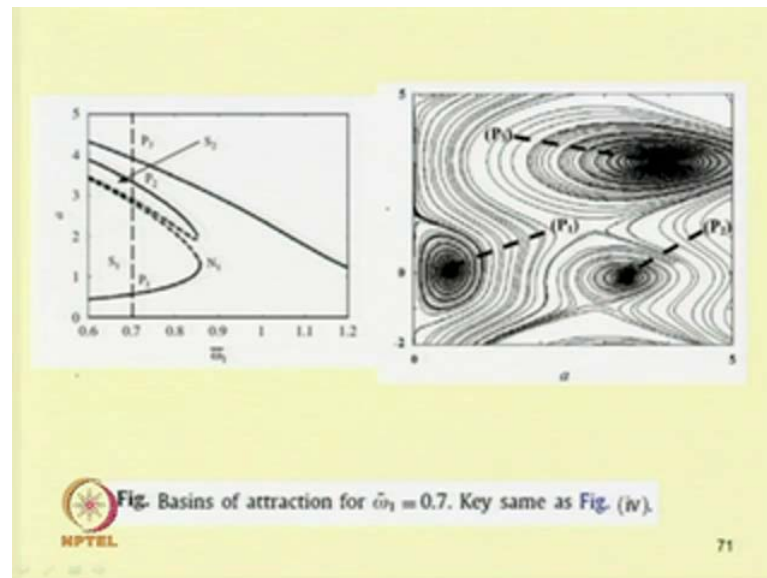
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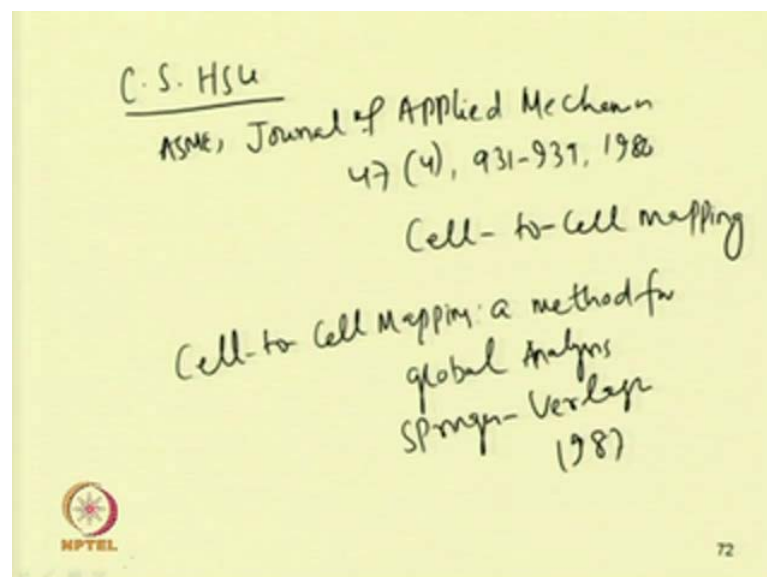
So this schemes are described in detail in the book by non-linear dynamics by Nayfeh and Balachandran, so one can refer these papers also, by Doedel, so this is the software developed by E J Doedel for plotting different branches of the fix point response, so E J Doedel, so this paper auto, so this software auto software for continuation, and bifurcation problems in ordinary differential equations California Institute of Technology.

Also one can refer this paper numerical analysis and control of bifurcation problems, So which is published in international Journal of bifurcation, and Chaos by the same author, and another paper also by this numerical analysis, and control of bifurcation problems bifurcation in infinite dimensions, which is published in international journal of bifurcation and Chaos.

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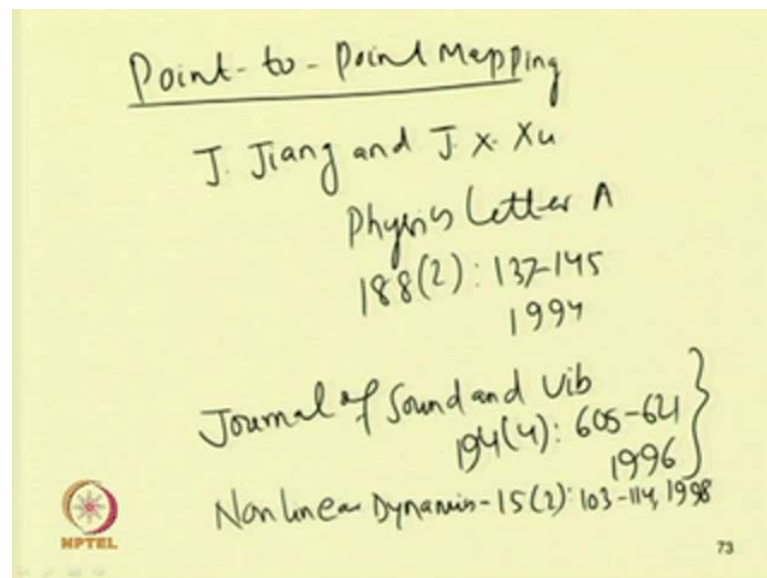


So already we have discussed that, when we have multiple solutions, one has to plot the basin of attraction; so this basin of attraction can be obtained by taking different roots, so

one can refer the so for more information, one can refer the paper by so there are two basic method, one is cell to cell mapping. So one can refer the paper by C S Hsu which is published in this journal of journal of applied mechanics; journal of applied mechanics, that is transaction of ASME, so 47 volume 47 number 4 page number 931 to 939 in 1980.

So, this is on cell to cell mapping, so one can use this cell to cell mapping for plotting the basin of attraction, also one can refer a book by the same author C S Hsu, that is cell to cell mapping, the book name is cell to cell mapping a method for global analysis, so this is published by the Springer and 1987.

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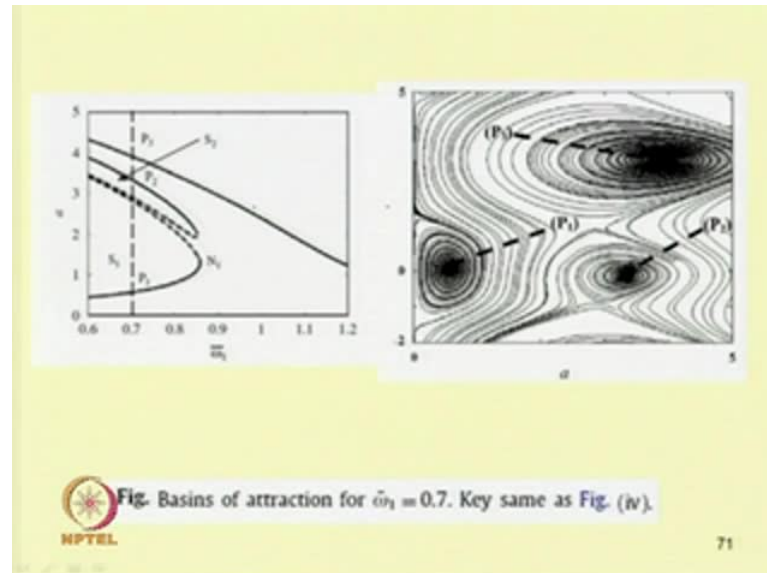


Also, one can use point to point mapping technique. Point to point mapping technique so this point to point mapping technique is developed by J Jiang and J X Xu, so this published in physics letter, physics letter A, volume 188 issue 2 137 to 145 in 1994. So, one can see another paper also, by this same author on this; so this is published in journal of sound and vibration, so in this paper, so this is journal of sound and vibration 194 4 so this 605 to 621 in 1996 it is published.

So this is on point to point mapping, so another paper also by the same author can be found in this journal of non-linear dynamics, non-linear dynamics so it is volume 15 issue 2, so this is 103 to 114 1998. So one can use this cell to cell mapping, or point to

point mapping method for finding the basin of attraction, or one can directly use by taking different initial conditions.

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By taking different initial conditions, one can find the basin of attraction, when multiple solutions are present in the system. So, in this module, we have discussed about different numerical techniques for finding the time response, and the frequency response of the system. And in the next module, we will study about different applications of the non-linear methods, and the numerical techniques, what we have studied in this course.

Thank you. .