

Nonlinear Control Design

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Alright, so I am going to go over quickly again this example of feedback passivation that we did. This is on the standard Euler Lagrange model for a robotic manipulator. So this is a very general model if you remember we talked about this. You can use any kind of coordinates that's why they are called the cues are called generalized coordinates they could be the angle coordinates or they could be the linear coordinates. Yeah, so your robot could have this motion or it could have you know sort of elongation and you know you can have a pneumatic actuator which sort of elongates and gets bigger and so on and so forth or you could have them or you could have spherical joints whatever you can have different kinds of variables and that's why it's called generalized coordinates it's not just Cartesian coordinates it's also maybe angle coordinates and it is very much possible to write all of them in this form yeah no problem yeah the only cases where you cannot write them in this form the robot dynamics in this form is typically the non-holonomic cases yeah where you have some non-holonomic constraints we are we have not talked about those so do not worry about it in those cases the model looks different yeah because there is some you have to have redundant variables because there are non-holonomic constraints so that that is the only case where you will have different kind of models than this one but otherwise most robotic manipulators can be modeled in this in fact even mobile robots can be modeled in this if the wheels are of only if it's an only directional robot yeah if you have only directional mobile robot that can also be modeled like this no problem okay so that's sort of the nice thing this encapsulates a lot of different systems okay the control is on the right hand side typically you will see the control as being motors mounted on the joints for angular motion for linear motion also you can have linear actuators okay so that is the control typically like a torque or a force okay alright if you remember I mentioned that this M matrix is the inertia matrix it is symmetric and positive definite always okay C is the damping well C is not the damping C is the centrifugal and Coriolis courses okay and D is the viscous damping yeah we are not a modeling course otherwise we would have talked about how to arrive at these matrices so we are not going to talk about how to arrive at these we just give you some of these matrices alright G is of course the gravity term yeah if you are if gravity is a factor then you have to add the gravity terms also alright you one of the facts that is known about this model is that $m \ddot{q} - 2C\dot{q}$ is symmetric okay what's the value of this it means that any quadratic form that you construct with any vector η on this on a skew symmetric matrix that is 0 okay quadratic form of a skew symmetric matrix is always 0 okay this is again standard result alright suppose the aim is to track a constant

reference yeah I was careful we discussed this if it's a time varying reference then you have to do a little bit more jugglery it's not this simple so if you have a constant reference Q_R okay then your error model yeah error is Q minus Q_R the error model actually looks exactly similar okay again because I chose a constant reference R that's it if you chose time varying you'll have to slightly modify how you work with this problem yeah we may look at it later but not right now so constant reference model would mean that it's a what we call set point regulation problem yeah it means I started some configuration and I ended some configuration okay I give a start confusion and an end so whatever you folks if you work with quadrotors typically you give waypoints right it's this you go from one waypoint to the other you are not giving a trajectory in between sometimes but but more often than not you would also want to specify the trajectory in between so that you are not following very very bad trajectories to reach from one point to the other that is not covered here we are only going from one set point to another set point okay so that's what this Q_R is you construct an error you get the error dynamics yeah and we want E equal to 0 to be globally asymptotically stable here all right okay yeah for some K_P equal to K_P^T positive we consider this control law for feedback passivation okay what were we doing in feedback passivation we were saying that we will specify the control so that the resulting system becomes feedback passive in the new control okay that's what we are sort of doing yeah I'm already saying what U is yeah because I know this will work so this is GQ minus $K_P E$ plus V which is the new control and I am going to claim that the system is feedback passive with this control and some output we have not yet decided the output either all right output is not decided either if I plug in this control what happens if I plug this in here what happens this and this cancel out right and this $K_P E$ goes to the left hand side becomes a positive term okay that's it that's what I've written here okay so now once I have this structure and I know this is a very nice structure even for you it should be evident it's a very nice structure why first of all M is positive definite yeah always the term on the highest derivative should be positive definite symmetric yeah it's already nice think about the Routh criteria the all generalization of that way because it's almost a linear looking system not very nonlinear actually it's almost a linear looking system right because this is E \dot{E} and again \dot{E} and then you have an \ddot{E} and the second order almost linear looking system yeah and also the term in the connecting to the highest derivative is positive yeah again as generalization of positive yeah so if you think Routh-Herwitz criteria also it's nice yeah because the coefficient on the highest power should be positive right so that's already something nice that's happening okay but we since we are in the world of Lyapunov and energy functions and so on and so forth we are going to actually construct a storage function right for passivity we need a storage function okay what is the storage function this guy yeah and in the context of what Antonio talked about this is the energy of the system okay why because by introducing this element okay this element is somehow a spring element I don't know if you understand this see this or not yeah this is like a spring yeah so this is sort of a spring energy yeah and spring energy is what it's like $\frac{1}{2} K X^2$ right this is spring energy type of a term and what is the spring energy it's potential energy always potential energy spring energy seen as potential energy so we sort of created a fake spring where is this spring connected yeah it is very interesting this spring

is sort of if you have this initial state I am just going to draw this kind of a revolute joints only to make my life easy and say this is the final state yeah the set point right and so what am I trying to do I want to go from this angle to this angle right and this angle say I measure from horizontal so I want to go from this angle to well actually maybe better to measure it from this guy suppose I measure from this guy no I should measure from horizontal that was easier I apologize because this is also measured from horizontal I am measuring all angles from the horizontal okay so this angle I want to go to I draw a parallel here so I want this to go to this guy yeah make sense yeah I am just trying to go to fine that's okay yeah so I want to change these angles in this way the first angle goes here second angle goes here alright now what is this spring this spring is an artificial spring that is pulling me there is one spring between these and one spring this way you can think of it as two torsional springs fake torsional springs or pseudo torsional springs which are making me move from here to here and here to here yeah it's so this is a very standard thing in robotics just like you know you think you give waypoint to quadrotors and then the quadrotor moves from one waypoint to the other then when you design a control in reality not in reality but in pseudo terms or energy terms what you are actually doing is you are creating a spring with Center at that waypoint and then the control is sort of pulling it towards that waypoint you can just think of it in your mind in your head if you think like it makes so much more sense that all I am doing is giving it up there is a spring connected to my waypoint and then to my quadrotor body and it's just pulling it so you know it will get to that point or you can think of the dam spring so obviously it stays there yeah you pull it then the next waypoint next waypoint pulls it and then the next waypoint pulls it okay so this is exactly like that I am creating an artificial spring yeah and that is the spring energy this term is just the spring energy it is a potential energy okay and this term is obviously the kinetic energy right anything with the velocities is the kinetic energy so I constructed a potential energy so in terms of what Antonio was saying the storage function is actually an energy function yeah just that I have created some fake pseudo energies yeah it is should not be so worrisome for you because that's how we design Lyapunov functions yeah we are creating some pseudo energies anyway that's the whole idea yeah so great once I have this constructed I am just going to take the derivative because I want to claim that \dot{V} is less than equal to some $u^T y$ and so on and so forth so basically the same deal as energy gained is less than equal to $u^T y$ okay great so what is the derivative $\dot{e}^T m \ddot{e}$ that's the first term yeah because the half goes away because it's quadratic similarly I get $e^T K_p \dot{e}$ the second term but I have an additional term yeah which you should not forget as you can see I also had forgotten it very easy to forget so I wrote it later on yeah m is time varying m is a m has variables in it it's not constant yeah if it's constant great for you but usually never will it be constant for any robot yeah just think about it this arm is moving in a fixed frame okay but the second arm is moving in the frame of the first term okay so you have it will never be a fixed m matrix it will so if you think of inertia now nothing inertia if I want to write the inertia in a fixed frame I mean you have to choose some frame to write the inertia if I choose to write the inertia in this frame then this is okay will be fixed well this will also not be fixed actually because as this moves there is a problem but suppose I choose this frame to write my inertia the rotating frame but then this guy is still rotating

with respect to that frame so if your object is moving in the frame then inertia is changing just like you think of this fan yeah well if it's on yeah right now I will put a frame on that the thing that is the beam that is hanging that with which it's hanging inertia is constant right because the mass distribution is constant fan is not moving I turn on the fan it's not constant anymore right no yeah you seem confused how really mass distribution remains the same even if it's a fan is rotating where is the mass in the fan on the fins yeah the center object yes it's a it's a symmetric object what you are thinking is symmetry correct if it's a symmetric object which is the center disk sure that inertia does mass distribution doesn't change with rotation because all directions are the same doesn't matter but the fins they are they have mass right and their orientation their location keeps changing with respect to the axis and inertia is nothing but mass distribution your mass distribution is time varying okay so if I write the inertia with respect to that fixed frame my inertia is time varying or state varying yeah it's not actually time being it's state varying just like that you will have for more often than not you will have you know state varying inertia okay very obvious but it will not depend on so that it will not depend on \dot{Q} it will depend on only the Q okay this the not the velocity states depend on the position states only yeah so this is there is also an $\dot{m} \cdot Q$ okay which is the time derivative of m by the way yeah you can think of this a little bit of abuse of notation this \dot{m} is actually $\frac{dm}{dt}$ the total derivative so it's actually partial of m with respect to Q times \dot{Q} okay so remember that it's just yeah I have just written it like this and now I am claiming this is less than equal to $V^T Y$ okay this is what you have to prove yeah you have to find the output yeah notice I already use the new input I am using the new input I am not using the old input anymore I am claiming that this is less than equal to $V^T Y$ what you have to do is you have to use this fact that $\dot{m} - 2c$ is Q symmetric that is any quadratic form with $\dot{m} - 2c$ is 0 you have to use this and you will get a very nice Y you will get a very nice Y if you remember I don't know it's like not in this example it was somewhere energy shaping yeah and this energy shaping whatever this example this was interesting energy shaping stuff he had passivity with respect to \dot{Q} in this case if you remember he got passivity with respect to the \dot{Q} variable okay so accordingly you have to I don't know if you remember or not but in this case the passivity was always with respect to the \dot{Q} variable see if you yeah you had something like this okay so anyway so basically in this case also what I need you to do is complete the \dot{V} expression and you should get something like a $V^T Y$ for some Y okay you have to come back and tell me what is the Y okay and you have to of course construct a feedback yeah this is pretty easy once you have a Y your feedback is just V equal to minus $\Phi^T Y$ such that $Y^T \Phi$ is positive definite yeah pretty easy actually I mean if you feel yeah if you if you get a Y the simplest feedback is minus KY itself as you can imagine right we already did this in this example yeah right because it's $V^T Y$ right so if you if you're if you know the Y then you construct Y is minus KY then $V^T Y$ is minus $K^T Y^T Y$ negative definite in Y okay so that's already done yeah you can of course construct you see these saturated controls also like this minus $K \tanh$ hyperbolic Y yeah this just ensures that your control remains within some range like a saturated control alright but otherwise yeah once you identify a Y doing this is very easy however you have to also ensure that or show in this case that with this particular output Y

you get zero state observability this was a little bit more work yeah so basically what is the zero state observability it is that if your if the output you chose is zero then the state also has to be zero there's no other way about it or if you want to define it the way I defined it the set of outputs equal the set containing output equal to zero cannot contain anything but the trivial solution that is X equal to zero okay you have to also show zero state observability because only with these two conditions does this control work yeah you need two conditions not just passivity you also need the zero state observability alright okay. you