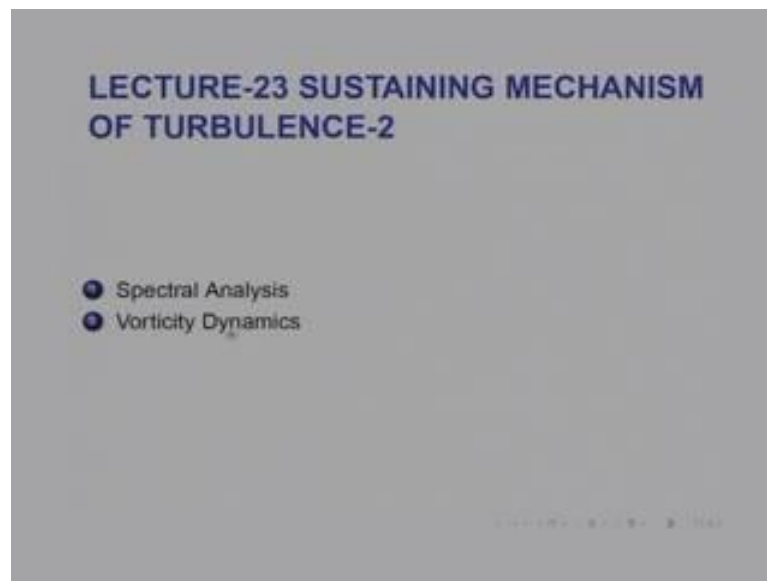


Convective Heat and Mass Transfer
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Module No. # 01
Lecture No. # 23
Sustaining Mechanism of Turbulence-2

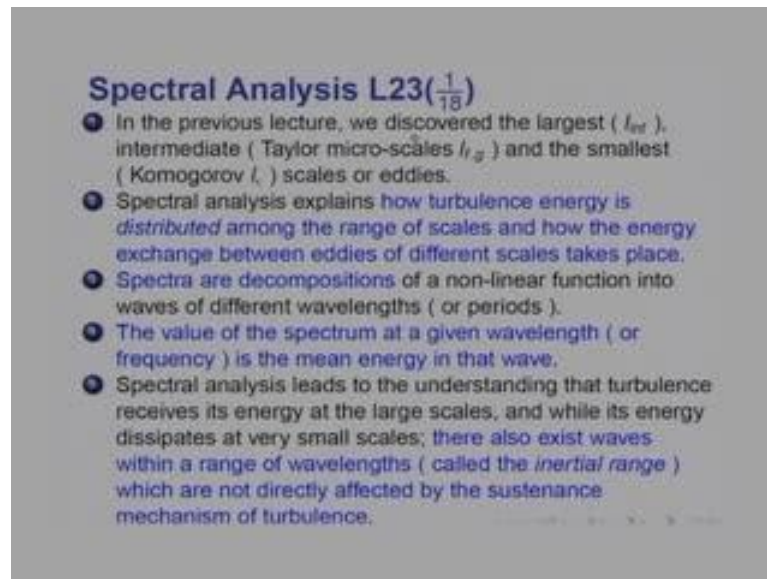
In this lecture, we shall continue with our discussion of the Sustaining Mechanism of Turbulence, but by employing Spectral Analysis and Vorticity Dynamics.

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Both these terms need explanation. In the course of this lecture, you will understand what they mean. I miss one that the subject matter is somewhat mathematical. Therefore, a very close attention would be required.

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Spectral Analysis L23(1/18)

- 1 In the previous lecture, we discovered the largest (l_{int}), intermediate (Taylor micro-scales l_{fg}) and the smallest (Komogorov l_{ϵ}) scales or eddies.
- 2 Spectral analysis explains how turbulence energy is distributed among the range of scales and how the energy exchange between eddies of different scales takes place.
- 3 Spectra are decompositions of a non-linear function into waves of different wavelengths (or periods).
- 4 The value of the spectrum at a given wavelength (or frequency) is the mean energy in that wave.
- 5 Spectral analysis leads to the understanding that turbulence receives its energy at the large scales, and while its energy dissipates at very small scales; there also exist waves within a range of wavelengths (called the *inertial range*) which are not directly affected by the sustenance mechanism of turbulence.

We recall that in the previous lecture, we discovered three characteristic length scales of turbulence. One was the largest - the integral length scale, which was obtained by integrating spatial correlation coefficient l_{int} , intermediate Taylor micro-scale l_{fg} ; f being longitudinal and g being transverse length scale. Then, the very smallest scales, which we call Kolmogorov scales; l_{ϵ} , where energy dissipation takes place because of the strong influence of viscosity. Spectral analysis goes little further. It explains how turbulence energy is distributed among the range of wave scales and how the energy exchange between eddies of different scales takes place.

In this sense, it is a much more continuous description of energy transfer from largest scale to the smallest scale. To do this, we use the notion of spectra. The spectra are decompositions of any non-linear function into waves of different wavelengths; or they can even be periods.

The value of the spectrum at a given wavelength or frequency in case of time-dependent function is the mean energy in that wave. Spectral analysis leads to the understanding that turbulence receives its energy at large scales. While its energy dissipates at very small scales, there also exists waves within a range of wavelengths called the inertial sub range, which are not directly affected by the sustenance mechanism of turbulence. That is the overall story that we wish to narrate by going through somewhat tedious mathematics.

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Main Postulate - 1 - L23($\frac{2}{18}$)

- The spatial correlation tensor $B_{ij}(\vec{r} = \Delta x_1, \Delta x_2, \Delta x_3)$ is related to the spectral tensor $\Phi_{ij}(k = k_1, k_2, k_3)$ via the 3D Fourier transform as:

$$B_{ij}(\vec{r}) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \Phi_{ij}(\vec{k}) \exp(i \vec{k} \cdot \vec{r}) d\vec{k}$$

and its inverse transform

$$\Phi_{ij}(\vec{k}) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} B_{ij}(\vec{r}) \exp(-i \vec{k} \cdot \vec{r}) d\vec{r}$$
- Therefore, spectral interpretation of the Reynolds stress (one-point correlation) tensor $-\rho \overline{u_i' u_j'}$ is

$$-\rho \overline{u_i' u_j'} = -\rho B_{ij}(\vec{r} = 0) = -\rho \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \Phi_{ij}(\vec{k}) d\vec{k}$$
- Now, since $\overline{u_i' u_j'}$ determine the energy in the various velocity components, the value of $\Phi_{ij}(\vec{k})$ gives the division of this energy in different eddy sizes or wave numbers¹. Consequently, $\Phi_{ij}(\vec{k})$ is called the **energy spectrum tensor**.

¹Small values of wave numbers correspond to large eddies or wavelengths and vice versa.

You will recall the spatial correlation tensor B_{ij} at a vector position \vec{r} equal to $\Delta x_1, \Delta x_2, \Delta x_3$ is related to the spectral tensor Φ_{ij} as a function of wavelength vector \vec{k} via the 3D Fourier transform. The Fourier transform is defined as B_{ij} at vector \vec{r} equal to **integral from** minus infinity to plus infinity 3 times over $\Phi_{ij}(\vec{k}) \exp(i \vec{k} \cdot \vec{r}) d\vec{k}$; i is the complex number under root minus 1. The inverse transform of this is given by $\Phi_{ij}(\vec{k})$ equal to **integral from** minus infinity to plus infinity 3 times $B_{ij}(\vec{r}) \exp(-i \vec{k} \cdot \vec{r}) d\vec{r}$.

Therefore, spectral interpretation of the Reynolds stress, which is of the one-point correlation tensor $-\rho \overline{u_i' u_j'}$; both u_i' and u_j' are measured at the same point. Therefore, $-\rho \overline{u_i' u_j'}$ will become $-\rho B_{ij}(\vec{r} = 0)$ equal to **minus rho integral from** minus infinity to plus infinity 3 times over. Since \vec{r} is 0, exponential of that would be 1 and you get $\Phi_{ij}(\vec{k}) d\vec{k}$. Now, since $\overline{u_i' u_j'}$ time average determine the energy in the various velocity components of the fluctuations, the value of $\Phi_{ij}(\vec{k})$ gives the division of this energy in different eddy sizes or wave numbers. The small value of wave number corresponds to a large eddy and vice versa.

A large wave number or wavelength corresponds to very small eddies and very small wavelength corresponds to large eddies. So, what the Fourier transform does is - it gives

you the division of the energy of the fluctuations in different eddy sizes. Consequently, ϕ_{ij} vector k is called the energy spectrum tensor.

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Main Postulate - 2 - L23($\frac{3}{18}$)

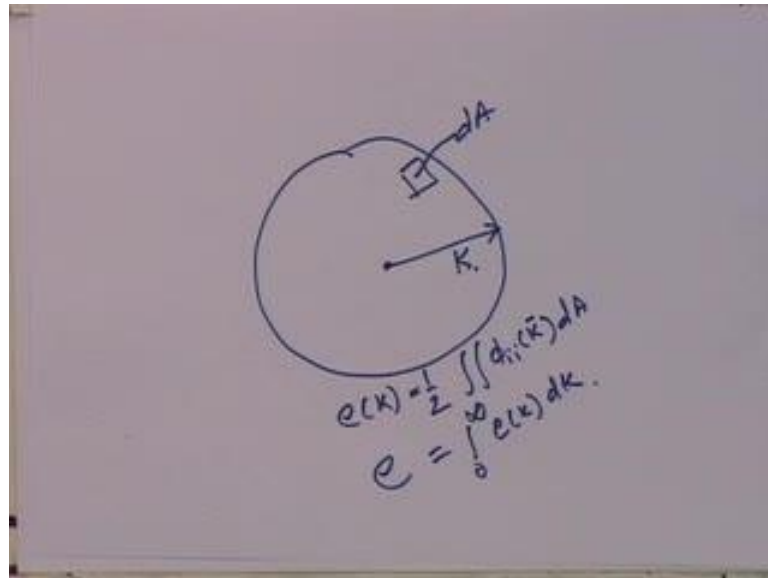
- Further, the sum of the diagonal components of the tensor gives the turbulent kinetic energy at a given wavenumber.
 $B_{ii}(\vec{r} = 0) = \overline{u_i u_i} = 2e = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \phi_{ii}(\vec{k}) d\vec{k}$
- The spectral tensor $\phi_{ij}(\vec{k})$ is a function of 3 wavenumber components. In order that physical interpretation becomes easier, it is customary to remove directional dependence by integrating $\phi_{ij}(\vec{k})$ over a spherical shell of radius k (scalar) where $k = \sqrt{k_1^2 + k_2^2 + k_3^2}$.
- If dA is the area of an element on the surface of the spherical shell of radius k then

$$e(k) = \frac{1}{2} \int \int \phi_{ii}(\vec{k}) dA \quad \rightarrow \quad e = \int_0^{\infty} e(k) dk$$
- The function $e(k)$ is called the *scalar kinetic energy spectrum*.

Further, if we take the sum of the diagonal components of the tensor, gives the turbulent kinetic energy spectrum at a given wave number. So, B_{ii} is equal to 0 ; $\overline{u_i u_i}$ will be 2 times the kinetic energy e equal to integral from minus infinity to plus infinity 3 times over $\phi_{ii}(\vec{k}) dk$; here, e is the turbulent kinetic energy.

The spectral tensor $\phi_{ij}(\vec{k})$ is a function of three wave number components k_1, k_2 and k_3 because k is a vector. This makes interpretation of this expression (Refer Slide Time: 06:19) somewhat difficult. Therefore, in order that physical interpretation becomes easier, it is customary to remove directional dependence by integrating $\phi_{ij}(\vec{k})$ over a spherical shell of radius k ; where k is square root of $k_1^2 + k_2^2 + k_3^2$ square. In other words, **the total magnitude** of the vector k is taken as the radius.

(Refer Slide Time: 06:53)



On this spherical shell, we form a sphere of radius k . If we take an element dA on this sphere, then the energy spectrum of $e(k)$ is half times integral $\phi_{ii}(k) dA$. e would be equal to integral 0 to infinity $e(k) dk$.

This is what I have shown here (Refer Slide Time: 07:37). Energy at wavelength k is half area integral of $\phi_{ii}(k) dA$. That gives e equal to integral from 0 to infinity $e(k) dk$, which is the kinetic energy e . The function $e(k)$ is called the scalar kinetic energy spectrum.

(Refer Slide Time: 08:00)

TKE Eqn in k-Space - 1 - L23($\frac{4}{18}$)

To derive the transport eqn for $e(k)$, an equation for B_i is first derived for a non-homogeneous, anisotropic and steady turbulent flow. Thus, the instantaneous ($\hat{u} = u + u'$) form of the NS equations (with $\partial u'_k / \partial x_k = \partial u_k / \partial x_k = 0$) is

$$\frac{\partial \hat{u}_i}{\partial t} + \hat{u}_k \frac{\partial \hat{u}_i}{\partial x_k} = -\frac{1}{\rho} \frac{\partial \hat{p}}{\partial x_i} + \nu \frac{\partial^2 \hat{u}_i}{\partial x_j \partial x_j}$$

$$\frac{\partial u'_i}{\partial t} + (u_k + u'_k) \frac{\partial u'_i}{\partial x_k} + u'_k \frac{\partial u'_i}{\partial x_k} + \frac{\partial u'_k u'_i}{\partial x_k}$$

$$= -\frac{1}{\rho} \frac{\partial (\hat{p} + p')}{\partial x_i} + \nu \frac{\partial^2 (u_i + u'_i)}{\partial x_j \partial x_j}$$

We now subtract the RANS momentum eqn from this eqn (next slide)

To derive the transport equation for ϵ_k , an equation for B_{ijk} is first derived for a non-homogeneous, anisotropic and steady turbulent flow. As you know that in a steady turbulent flow, $u_k \frac{du_k}{dx_k}$ is 0 from continuity. The instantaneous form of the Navier-Stokes equations would be given by $\frac{du_i}{dt} + u_k \frac{du_i}{dx_k}$ equal to the pressure gradient term and the diffusion term.

(Refer Slide Time: 08:50)

The image shows a hand pointing to a whiteboard with the following handwritten derivation:

$$\begin{aligned}
 & u_k \frac{\partial u_i}{\partial x_k} \\
 &= (u_k + u'_k) \frac{\partial (u_i + u'_i)}{\partial x_k} \\
 &= (u_k + u'_k) \frac{\partial u_i}{\partial x_k} + (u_k + u'_k) \frac{\partial u'_i}{\partial x_k} \\
 &= u_k \frac{\partial u_i}{\partial x_k} + u'_k \frac{\partial u_i}{\partial x_k} + u_k \frac{\partial u'_i}{\partial x_k} + u'_k \frac{\partial u'_i}{\partial x_k}
 \end{aligned}$$

The final line shows the expansion of the convective term into four terms, with the last term $u'_k \frac{\partial u'_i}{\partial x_k}$ being crossed out with a diagonal line.

Now, what I am going to do is explain how the second term is modified. $u_k \frac{du_i}{dx_k}$ is written as $u_k + u'_k \frac{d}{dx_k} (u_i + u'_i)$. That gives me the first term as $u_k + u'_k \frac{d}{dx_k} (u_i + u'_i)$. So, this term remains as it is; plus $u_k \frac{du'_i}{dx_k} + u'_k \frac{du_i}{dx_k}$. This equals $u_k \frac{du'_i}{dx_k} + u'_k \frac{du_i}{dx_k} + u'_k \frac{du'_i}{dx_k}$. Now, that term is 0 because of continuity and you will see this is what I have written here. So, you have three terms $u_k + u'_k \frac{d}{dx_k} (u_i + u'_i)$ plus $u_k \frac{du'_i}{dx_k} + u'_k \frac{du_i}{dx_k}$ equal to all that.

If I subtract from this equation (Refer Slide Time: 10:52), the RANS equation. You will recall - what is the RANS equation?

(Refer Slide Time: 10:58)

The RANS equation is $u_k \frac{du_i}{dx_k}$ equal to minus 1 over rho dp by dx i plus d by dx k into nu minus $du_{dash i} u_{dash k}$ by dx k.

If I subtract this equation from this equation (Refer Slide Time: 11:46) that you see here, then you will notice that I would get the following equation:

(Refer Slide Time: 11:53)

TKE Eqn in k-Space - 2 - L23($\frac{5}{18}$)

Subtraction results in eqn for position r_1^i

$$\frac{\partial u_i^j}{\partial t} + u_k^j \frac{\partial u_i^j}{\partial x_k} + u_k^j \frac{\partial u_i^j}{\partial x_k} + \frac{\partial}{\partial x_k} (u_k^j u_i^j - \overline{u_k^j u_i^j}) = -\frac{1}{\rho} \frac{\partial p^j}{\partial x_i} + \nu \frac{\partial^2 u_i^j}{\partial x_k^2}$$

and a similar equation for u_j^i at position r_2^j

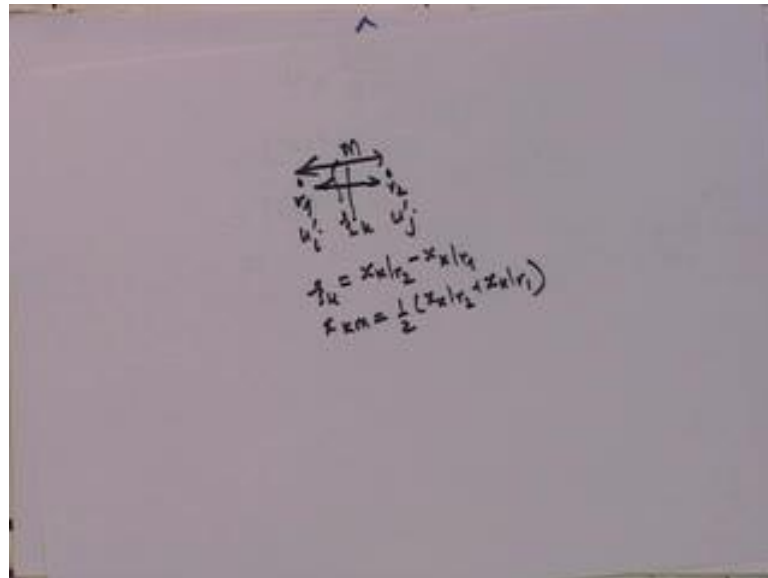
$$\frac{\partial u_j^i}{\partial t} + u_k^i \frac{\partial u_j^i}{\partial x_k} + u_k^i \frac{\partial u_j^i}{\partial x_k} + \frac{\partial}{\partial x_k} (u_k^i u_j^i - \overline{u_k^i u_j^i}) = -\frac{1}{\rho} \frac{\partial p^i}{\partial x_j} + \nu \frac{\partial^2 u_j^i}{\partial x_k^2}$$

Now, multiplying first equation by u_j^i at r_2^j and second equation by u_i^j at r_1^i and, adding and time-averaging, yields the **required equation for B_{ij}** (next slide) in terms of two (in fact, six) independent variables namely: $x_k|_{r_2} - x_k|_{r_1}$ (separation) and $x_k|_m = \frac{1}{2} (x_k|_{r_1} + x_k|_{r_2})$ (mid-point)

$du_i \text{ dash } i \text{ by } dt$ plus $u \text{ dash } k \text{ } du_i \text{ by } dx_k$ plus $u_k \text{ } du \text{ dash } i \text{ by } dx_k$ plus $d \text{ by } dx_k$ into $u \text{ dash } k \text{ } u \text{ dash } i$ minus $u \text{ dash } k \text{ } u \text{ dash } i$; time average is equal to minus 1 over rho dp

dash by dx i plus nu d 2 u dash i by dx l dx l. So, this is simply subtracting the mean RANS equation from the instantaneous form of the momentum equation. If I say this is the equation for u dash i at position r 1, I could also write a similar equation for u dash j at another position r 2.

(Refer Slide Time: 12:50)



That would read as let say position r 1, where I wrote an equation for u dash i and position r 2, where I wrote an equation for u dash j.

(Refer Slide Time: 13:00)

TKE Eqn in k-Space - 2 - L23($\frac{5}{18}$)

Subtraction results in eqn for position r_1

$$\frac{\partial u_i}{\partial t} + u_k \frac{\partial u_i}{\partial x_k} + u_k \frac{\partial u_i}{\partial x_k} + \frac{\partial}{\partial x_k} (u_k u_i - \overline{u_k u_i}) = -\frac{1}{\rho} \frac{\partial p}{\partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_k \partial x_k}$$

and a similar equation for u_j at position r_2

$$\frac{\partial u_j}{\partial t} + u_k \frac{\partial u_j}{\partial x_k} + u_k \frac{\partial u_j}{\partial x_k} + \frac{\partial}{\partial x_k} (u_k u_j - \overline{u_k u_j}) = -\frac{1}{\rho} \frac{\partial p}{\partial x_j} + \nu \frac{\partial^2 u_j}{\partial x_k \partial x_k}$$

Now, multiplying first equation by u_j at r_2 and second equation by u_i at r_1 and, adding and time-averaging, yields the required equation for B_2 (next slide) in terms of two (in fact, six) independent variables namely: $\xi_k = x_k|r_2 - x_k|r_1$ (separation) and $x_k|m = \frac{1}{2} (x_k|r_1 + x_k|r_2)$ (mid-point)

That equation would again read very much like the first one with the \overline{dp} dash by dx_j here and these terms. To do further development, we multiply the first equation; this equation at position r_1 by u_j at r_2 and the second equation by u_i at r_1 . Then, we add the two equations and time average, which would yield the required equation for B_{ij} , which I will show on the right hand side with 2 independent variables x_k ; which is the difference between these (Refer Slide Time: 13:44). So, x_k equal to x_k at r_2 minus x_k at r_1 and x_k mean equal to half of x_k at r_2 plus x_k at r_1 . So, you have the midpoint m and the difference xi . So, we have two independent variables in this equation. This may be little bit unfamiliar to you, but it is a straightforward algebra to show that this is indeed the case.

(Refer Slide Time: 14:37)

TKE Eqn in k-Space - 3 - L23($\frac{6}{18}$)

$$\begin{aligned} \frac{\partial B_{ij}}{\partial t^2} &+ \left[B_{ij} \left(\frac{\partial u_i}{\partial x_k} \right)_{r_1} + B_{ij} \left(\frac{\partial u_i}{\partial x_k} \right)_{r_2} \right] \\ &+ \frac{1}{2} (u_{k,r_1} + u_{k,r_2}) \left. \frac{\partial B_{ij}}{\partial x_k} \right|_m + (u_{k,r_2} - u_{k,r_1}) \frac{\partial B_{ij}}{\partial \xi_k} \\ &- \frac{1}{2} \frac{\partial}{\partial x_k} (T_{ikj} + T_{kij})_m - \frac{\partial}{\partial \xi_k} (T_{ikj} - T_{kij}) \\ &- \frac{1}{2\rho} \left[\left. \frac{\partial C_{p,j}}{\partial x_i} \right|_m + \left. \frac{\partial C_{p,i}}{\partial x_j} \right|_m \right] + \frac{1}{\rho} \left[\frac{\partial C_{p,j}}{\partial \xi_i} - \frac{\partial C_{p,i}}{\partial \xi_j} \right] \\ &+ \nu \left[\frac{1}{2} \left. \frac{\partial^2 B_{ij}}{\partial x_i \partial x_j} \right|_m + 2 \frac{\partial^2 B_{ij}}{\partial \xi_i \partial \xi_j} \right] \end{aligned}$$

$$\begin{aligned} T_{ikj} &= \overline{(u_i)_{r_1} (u_j)_{r_2} (u_k)_{r_2}} & T_{kij} &= \overline{(u_i)_{r_1} (u_k)_{r_1} (u_j)_{r_2}} \\ C_{p,j} &= \overline{(p')_{r_1} (u_j)_{r_2}} & C_{p,i} &= \overline{(p')_{r_2} (u_i)_{r_1}} & B_{ij} &= \overline{(u_i)_{r_1} (u_j)_{r_2}} \end{aligned}$$

The total equation for non-homogeneous anisotropic turbulence would read like this. $\frac{dB_{ij}}{dt}$ plus $B_{kj} \frac{du_i}{dx_k}$ at r_1 plus $B_{ik} \frac{du_j}{dx_k}$ at r_2 plus half of u_{k,r_1} by u_{k,r_2} into $\frac{dB_{ij}}{dx_k}$ at mean point plus u_{k,r_2} minus u_{k,r_1} into $\frac{dB_{ij}}{d\xi_k}$; equal to minus half of T_{ikj} plus T_{kij} ; T_{ikj} here is defined as u_i dash i at r_1 multiplied by u_j dash j at r_2 multiplied by u_k dash k at r_2 ; T_{kij} the second term is defined as u_i dash i at r_1 multiplied by u_k dash k at r_1 multiplied by u_j dash j at r_2 . So, you get that transfer term minus $\frac{d}{d\xi_k}$ based on the difference between the two points. Then, minus $\frac{1}{2\rho} \frac{dC_{p,j}}{dx_i}$ at m ; $C_{p,j}$ is the product of pressure fluctuation at r_1 multiplied by u_j dash j at r_2 . That is the $C_{p,j}$. Likewise, $C_{p,i}$ is the

pressure fluctuation at r_2 multiplied by u_i at r_1 ; B_{ij} is u_i at r_1 into u_j at r_2 ; is the tensor B_{ij} plus ν times $\frac{1}{2} \frac{\partial^2 B_{ij}}{\partial x_k \partial x_k}$. These are the diffusion terms.

(Refer Slide Time: 16:28)

TKE Eqn in k-Space - 4 - L23($\frac{7}{18}$)

- The eqn of the previous slide represents complete eqn for non-homogeneous non-isotropic turbulent flow. The eqn is not tractable.
- For *homogeneous turbulence*, however, all derivatives of the correlations with x_k vanish but are finite w.r.t. ξ_k .

$$\begin{aligned} \frac{\partial B_{ij}}{\partial t} &= \xi_j \frac{\partial u_k}{\partial x_l} \Big|_m \frac{\partial B_{ij}}{\partial \xi_k} \quad (\text{mean convection}) \\ &- \left[B_{ij} \left(\frac{\partial u_j}{\partial x_k} \right)_{r_1} + B_{ik} \left(\frac{\partial u_j}{\partial x_k} \right)_{r_2} \right] \quad (\text{production}) \\ &- \frac{\partial}{\partial \xi_k} (T_{ikj} - T_{kij}) \quad (\text{v-diffu}) \\ &- \frac{1}{\rho} \left[\frac{\partial C_{p,ij}}{\partial \xi_j} - \frac{\partial C_{p,ji}}{\partial \xi_i} \right] \quad (\text{p-diffu}) + 2\nu \frac{\partial^2 B_{ij}}{\partial \xi_k \partial \xi_k} \quad (\text{diss}) \end{aligned}$$

To make further progress, we postulate - the equation of the previous slide represents complete equation for non-homogeneous non-isotropic turbulent flow. The equation is not tractable because it has two types of independent variables; as you can see, x_i and x_k (Refer Slide Time: 16:49). So, midpoint and the difference between the two points.

It is not tractable, (Refer Slide Time: 16:58) but we can make it tractable somewhat by postulating homogeneous turbulence. As we will recall, in homogeneous turbulence, derivatives of correlations with x_k vanish, but are finite with respect to x_i , the difference.

(Refer Slide Time: 17:21)

TKE Eqn in k-Space - 3 - L23($\frac{6}{18}$)

$$\begin{aligned} \frac{\partial B_k}{\partial t} + \left[B_{k_l} \left(\frac{\partial u_l}{\partial x_k} \right)_{r_1} + B_{k_r} \left(\frac{\partial u_l}{\partial x_k} \right)_{r_2} \right] \\ + \frac{1}{2} (u_{k,r_1} + u_{k,r_2}) \frac{\partial B_k}{\partial x_k} \Big|_m + (u_{k,r_2} - u_{k,r_1}) \frac{\partial B_k}{\partial \xi_k} = \\ = - \frac{1}{2} \frac{\partial}{\partial x_k} (T_{i,k} + T_{k,i}) \Big|_m - \frac{\partial}{\partial \xi_k} (T_{i,k} - T_{k,i}) \\ - \frac{1}{2\rho} \left[\frac{\partial C_{p,l}}{\partial x_l} \Big|_m + \frac{\partial C_{p,l}}{\partial x_l} \Big|_m \right] + \frac{1}{\rho} \left[\frac{\partial C_{p,l}}{\partial \xi_l} - \frac{\partial C_{p,l}}{\partial \xi_l} \right] \\ + \nu \left[\frac{1}{2} \frac{\partial^2 B_k}{\partial x_l \partial x_l} \Big|_m + 2 \frac{\partial^2 B_k}{\partial \xi_l \partial \xi_l} \right] \end{aligned}$$

$$\begin{aligned} T_{i,k} &= \overline{(u'_i)_{r_1} (u'_k)_{r_2} (u'_k)_{r_2}} & T_{k,i} &= \overline{(u'_i)_{r_1} (u'_k)_{r_1} (u'_i)_{r_2}} \\ C_{p,l} &= \overline{(\rho')_{r_1} (u'_l)_{r_2}} & C_{p,l} &= \overline{(\rho')_{r_2} (u'_l)_{r_1}} & B_k &= \overline{(u'_i)_{r_1} (u'_i)_{r_2}} \end{aligned}$$

Therefore, you will get all these terms. So, this would vanish and you would get this equation (Refer Slide Time: 17:32) - $\frac{dB_k}{dt} = \xi_l \frac{\partial u_l}{\partial x_k} \frac{dB_k}{\partial \xi_k}$ (mean convection term; this term (Refer Slide Time: 17:46). Because this is already 0, it is this term $u_{k,r_2} - u_{k,r_1}$ into $\frac{dB_k}{d\xi_k}$. That mean convection (Refer Slide Time: 17:56) plus production. Remember: The product of stress multiplied by rate of strain means strain; gives you the production term. So, that becomes the production term.

(Refer Slide Time: 18:09)

TKE Eqn in k-Space - 4 - L23($\frac{7}{18}$)

- 1 The eqn of the previous slide represents complete eqn for non-homogeneous non-isotropic turbulent flow. The eqn is not tractable.
- 2 For *homogeneous turbulence*, however, all derivatives of the correlations with x_k vanish but are finite w.r.t. ξ_k .

$$\begin{aligned} \frac{\partial B_k}{\partial t} &= \xi_l \frac{\partial u_l}{\partial x_k} \Big|_m \frac{\partial B_k}{\partial \xi_k} \quad (\text{mean convection}) \\ &- \left[B_{k_l} \left(\frac{\partial u_l}{\partial x_k} \right)_{r_1} + B_{k_r} \left(\frac{\partial u_l}{\partial x_k} \right)_{r_2} \right] \quad (\text{production}) \\ &- \frac{\partial}{\partial \xi_k} (T_{i,k} - T_{k,i}) \quad (\nu\text{-diffu}) \\ &- \frac{1}{\rho} \left[\frac{\partial C_{p,l}}{\partial \xi_l} - \frac{\partial C_{p,l}}{\partial \xi_l} \right] \quad (\rho\text{-diffu}) + 2\nu \frac{\partial^2 B_k}{\partial \xi_l \partial \xi_l} \quad (\text{diss}) \end{aligned}$$

d by $\frac{d}{dx_i} (u_{k,j} - u_{k,i})$ is this term (Refer Slide Time: 18:20). That is the diffusion of B_{ij} due to velocity fluctuation. So, we say that is v diffusion. Then, the pressure diffusion terms, which are given by these (Refer Slide Time: 18:37) are the pressure diffusion terms. These vanish, but these survive because these are the derivatives with respect to x_i .

Then finally, this term (Refer Slide Time: 18:48) survives because it is the derivative with respect to x_l . That is, $2\nu \frac{d^2 B_{ij}}{dx_l^2}$ by $\frac{d}{dx_l} \frac{d}{dx_l}$, which is really the dissipation due to viscosity. So, you have fairly complex equation.

(Refer Slide Time: 19:13)

TKE Eqn in k-Space - 5 - L23($\frac{8}{18}$)

- 1 The mean convection term is really $(u_{k,j_2} - u_{k,j_1}) \partial B_{ij} / \partial x_k$. However, $(u_{k,j_2} - u_{k,j_1}) = \zeta_j \partial u_k / \partial x_l$. The v -diffu and p -diffu terms represent diffusion of energy due to velocity and pressure fluctuations respectively.
- 2 In order to study the transfer process, each term is Fourier transformed so as to yield an equation for $\Phi_{ij}(k)$.
- 3 Then, setting $i = j$, the equation for $\Phi_{ii}(k)$ results.
- 4 Further, to achieve directional independence, each term is integrated over a spherical shell of radius k to yield

$$\frac{\partial \theta(k)}{\partial t} = P(k) - \frac{\partial T_i(k)}{\partial k} - D(k)$$

where, $P(k)$ is production, $D(k)$ is dissipation and $T_i(k) = T_{conv}(k) + T_{v-diff}(k) + T_{p-diff}(k)$

Now, the mean convection terms x_l times du_k by dx_l into $\frac{dB_{ij}}{dx_k}$ by $\frac{d}{dx_k}$ is really the $u_{k,r_2} - u_{k,r_1} \frac{dB_{ij}}{dx_k}$ as I explained. However, $u_{k,r_2} - u_{k,r_1}$ will be $x_l \frac{du_k}{dx_l}$ at m . Therefore, we have written that as that. This is (Refer Slide Time: 19:30) $u_{k,r_2} - u_{k,r_1}$.

The v diffusion and p diffusion terms represent diffusion of energy due to velocity and pressure fluctuations respectively. In order to study the transfer process, each term of this equation is Fourier transformed so as to yield an equation for $\Phi_{ij}(k)$. So, we will have a differential equation in Fourier space of $\Phi_{ij}(k)$. If you then set i equal to j , we would get an equation $\Phi_{ii}(k)$.

Further, to achieve directional independence, each term is integrated over a spherical shell. I left out all the algebra here to yield $\frac{de}{dt} = P(k) - T(k) - D(k)$, where $P(k)$ is production; $D(k)$ is dissipation and $T(k)$ is the transfer term due to convection due to v diffusion and due to p diffusion. That is, the diffusion due to pressure fluctuation; diffusion due to velocity fluctuation and this is diffusion due to mean convection.

Essentially, then we get an equation in scalar k space. It is a one-dimensional equation because there is only one independent variable in wave number space k ; dk . It is a transient equation $\frac{de}{dt} = P(k) - T(k) - D(k)$, which is the dissipation.

(Refer Slide Time: 21:26)

TKE Eqn in k-Space - 6 - L23($\frac{9}{18}$)

- This is spectral form of the TKE eqn for homogeneous turbulence. It can be regarded as a 1D eqn representing energy balance over CV (dk) in the wavenumber space.
- The $P(k)$ term comprises of spectral functions (arising out of B_{ij} and B_{ik}) and mean velocity gradients, is not expected to be large at high wave numbers (small scale motions) but significant at small wave numbers.
- The gradient transport of $T_i(k)$ vanishes when integrated from $k = 0$ to $k = \infty$ giving

$$\frac{de}{dt} = \frac{d}{dt} \int_0^\infty e(k) dk = \int_0^\infty (P(k) - D(k)) dk$$
 This transfer term simply redistributes energy both directionally and among the different wave numbers.
- Dissipation $D(k) = 2\nu k^2 e(k)$. The presence of k^2 confirms that it is significant only at high wave numbers.

We can look up on this equation, which is the spectral form of the turbulent kinetic energy equation for homogeneous turbulence. It is nothing but a one-dimensional equation representing the energy balance over a control volume dk in the wave number space.

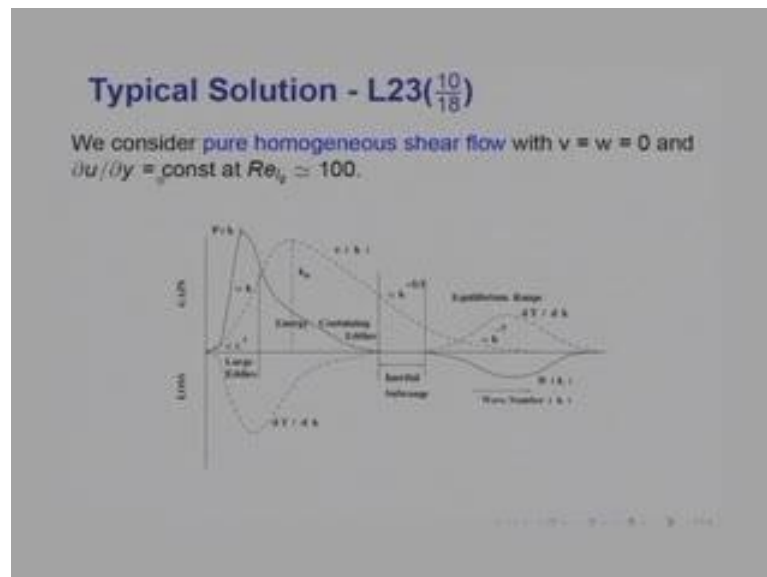
The $P(k)$ term comprises spectral functions arising out of B_{kj} and B_{ik} and multiplied by the mean velocity gradients, is not expected to be large at high wave numbers; where the velocity fluctuations have almost died down and viscosity has taken over. So, the $P(k)$ term would largely dominate at small wave number.

The gradient $T_t k$ term would vanish when integrated from k equal to 0 to k equal to infinity giving de by dt equal to d by dt integral 0 to infinity $e k dk$ equal to integral 0 to infinity $P k$ minus $D k$ $d k$. This transfer term simply redistributes energy both directionally in the components as well as along the wave numbers. That is, along the sizes. Therefore, T_t means total transfer term.

The dissipation term after Fourier transforming of this term (Refer Slide Time: 22:53) would be written as $2 \nu k^2 e k$. The presence of k^2 confirm that it would be significant only at very high wave numbers; k^2 suggests that it would be significant at very high wave numbers.

As I said, I have left out the algebra because it is considerably long. However, the essential ideas that we had seen in RANS equations from which we derived the turbulent kinetic energy in physical space and the equation we have now derived in the wave number space have very similar characteristics is that a rate of change of energy is equal to the rate of its production minus net rate of its transfer to smaller scales and minus dissipation.

(Refer Slide Time: 23:52)



If you consider a flow in which homogeneous shear flow in which v and w are 0, the mean velocities are 0 and du by dy is a constant, then here are the results computed at the turbulence Reynolds number based on **transfers Taylor micro-scale** of about 100. Looks

something like this. You see that loss means negative contribution to energy balance; gain means positive contribution to energy balance. You see that the production term is indeed very high at small wave numbers. This is the wave number access at small wave numbers. In fact, it peaks at very small wave numbers. Therefore, it is called large eddies; as I said, very large eddies at which the production dominates. However, it declines as the wave number increases. In this range, the transfer term is negative, which means energy is being sucked out from large eddies and being push towards smaller eddies; energy is continuously being fed to smaller eddies.

A point is reached where the production almost dies down and so does the transfer almost died down. There can be a region called the inertial sub range about which I will talk in a minute. However, dissipation takes over. As you can see, it is shown as negative dissipation, which occurs at very large wave numbers. The transfer term becomes positive at large wave numbers and again dies down. As we would expect the area under the negative sign here (Refer Slide Time: 25:49) of the transfer term must equal the area under the positive part of $\frac{dT_i}{dk}$ so that the net area is 0 in this.

The energy itself raises to very large value $e(k)$ and peaks at some wave number, which is designated by k_{e} and then begins to decline;. energy itself is goes on declining. Then, it falls here at the rate proportional to k to the power of minus phi by 3 and finally, keep very rapidly to k to the power of minus 7.

(Refer Slide Time: 26:31)

Discussion -1 - L23($\frac{11}{18}$)

- 1. $D(k)$ term dominates at high k (Kolmogorov small eddies, say $(0.1/L) < k < (1/L)$). Energy is mainly supplied by transfer term $\partial T_i(k)/\partial k$ and energy extraction from mean motion is minimal $P(k) \approx 0$.
- 2. $\partial T_i(k)/\partial k$ is negative at small k and positive at higher k indicating that the energy is indeed transferred out of low- k region and into high- k region. $\int_0^\infty (\partial T_i(k)/\partial k) dk = 0$
- 3. The dominance of $P(k)$ in low- k region indicates that most of the production is brought about by large eddies.
- 4. As $k \rightarrow 0$, very large eddies dominate and the $e(k)$ spectrum is not expected to be universal being influenced by mean velocity gradients. Also $\partial e(k)/\partial t$ is small and $\partial T_i(k)/\partial k = P(k)$. This is region of *rapid distortion*.
- 5. The $e(k)$ is maximum near k_e which characterises the *most energetic eddies*. l_{ov} is largely determined by these eddies.

What does all these indicate? The D_k term dominates at very high k , which means large wavelengths or Kolmogorov small eddies; say of the order of $0.1 \text{ divided by } l \text{ sub } \epsilon \text{ k}$ to $1 \text{ divided by } l \text{ sub } \epsilon$. That is the range of wave numbers in this part here (Refer Slide Time: 26:52) $0.1 \text{ divided by } l \text{ over } l \text{ epsilon}$ to $1 \text{ over } l \text{ epsilon}$.

Energy is mainly supplied by the transfer term $dT_t k \text{ by } dk$ and the energy extraction from the mean motion is minimal as we saw here (Refer Slide Time: 27:07). The energy for dissipation is essentially supplied by the transfer term and the production term itself contributes nothing to energy dissipation.

The transfer term is negative at small k and positive at high k indicating that energy is indeed transferred out of low- k region into high- k region. Therefore, the integral of $dT_t k \text{ by } dk$ into dk is 0.

The dominance of P_k in the low k region indicates that most of the energy production is brought about by large eddies. As you saw here (Refer Slide Time: 27:44), most of the production is brought about by large eddies. That is why I have said large eddies here. As k tends to 0, very large eddies dominate and the e_k spectrum is not expected to be universal at all, being influenced by the mean velocity gradients. Also $de_k \text{ by } dt$ is small and $dT_t k \text{ by } dk$ equals production. This means all the energy produced simply goes into its transfer to smaller and smaller eddies or bigger and bigger wavelengths. Therefore, this region (Refer Slide Time: 28:29) is called the region of rapid distortion.

The e_k is maximum near $k \text{ sub } e$ which characterizes the most energy-containing eddies. The l integral where we saw in the previous lecture is largely determined by these eddies. The characteristic eddies of this region (Refer Slide Time: 28:52) recall the energy containing eddies this is where the l integral corresponds somewhere to $k \text{ sub } e$.

(Refer Slide Time: 29:01)

Discussion - 2 - L23(12/18)

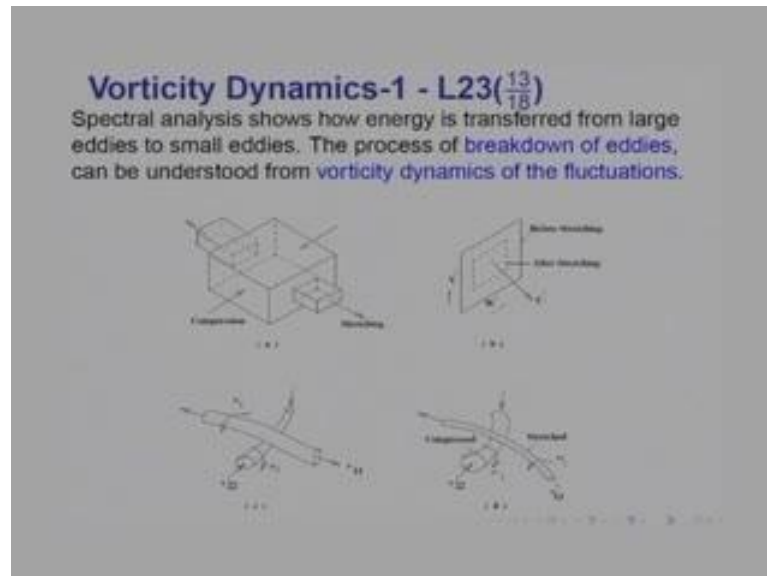
- 1 If $k_{diss} \gg k_e$, then an *inertial equilibrium range* ($k < (0.1/l)$) identified with Taylor micro-scale exists in which the conditions for isotropy of the small scale eddies and of independence of the turbulence structure from energy containing eddies are simultaneously satisfied. For this region $e(k) \propto k^{-5/3}$.
- 2 The existence, or otherwise, of the inertial range has considerable significance for the *near-wall turbulence*.
- 3 Finally, at very high wave numbers, where $k > (1/l)$, the energy spectrum varies as $e(k) \propto k^{-7}$. At this point, $D(k)$ is maximum.

If k dissipation is much greater than the energy containing wave number k sub e , then an inertial sub range exists at k less than 0.1 divided by l sub ϵ . As you can see (Refer Slide Time: 29:20), if k dissipation is much bigger than K sub e , then a range exists. As you can see here, (Refer Slide Time: 29:31) k less than 0.1 divided by l ϵ identified with Taylor micro-scale exists in which the conditions of the isotropy of the small scale eddies and of independence of turbulence structure from energy containing eddies are simultaneously satisfied.

In other words, this range of wave number (Refer Slide Time: 29:53) is small enough for isotropy to prevail; is a range in which the isotropy of the large scale and the independence of the turbulence structure from energy containing eddies are simultaneously satisfied. In this range, $e(k)$ is proportional to **k to the power of minus 5 by 3**. This is very important. Many experiments always want to ensure that they are turbulent **and** sufficiently vigorous so that they can take it as fully turbulent or not. This means they are the large wave numbers, where dissipation takes place and the small wave numbers; the energy containing wave numbers, where the production takes place. Are they sufficiently separated or not? Because if they are separated, then an inertial sub range must exist with k raised to minus 5 by 3 as the energy spectrum. If it exists, they would declare such turbulence as being truly representative of vigorous turbulence.

The existence, or otherwise, of the inertial sub range has considerable significance for the near-wall turbulence. This is the matter, which is employed in turbulence modeling, which may be used a little later. Finally, at very high wave numbers, where k is greater than 1 over l epsilon, the energy spectrum varies as e_k is proportional to k raised to minus 1 . At this point, $D k$ is maximum as we saw earlier.

(Refer Slide Time: 31:38)



Spectral analysis gives you how continuously the energy is transferred from large eddies to small eddies or from small wave numbers to large wave numbers. Vorticity dynamics is another way of explaining the same phenomenon. That is, by the process of breakdown of eddies. For example, consider a three-dimensional cubic element here. This is direction 1, direction 2 and direction 3. Imagine that this element is being stretched because of the strain rate in direction 1. If the turbulence was very high where viscosity would have very little influence, then you will see that the plane of cross-section must shrink as I have shown here. Because of this stretching in x direction, the cross-section in y and z direction or the length scales associated with y and z direction must decrease.

(Refer Slide Time: 32:50)

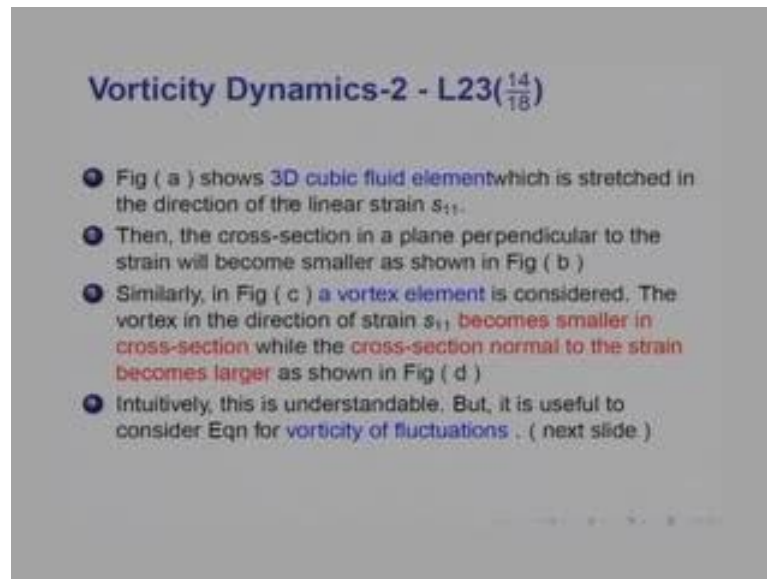


Figure a shows 3D cubic fluid element, which is stretched in the direction of the linear strain s_{11} . Then, the cross-section in a plane perpendicular to the strain will become smaller as shown in figure b.

Similarly in figure c, I now consider a vortex element rather than a cubic element. The vortex in the direction of strain s_{11} becomes smaller in cross-section as you can see here (Refer Slide Time: 33:19). This is s_{11} and the vortex is being stretched. So, it becomes smaller in cross-section while the cross-section normal to the strain becomes larger as shown in figure d. So, the cross-section in this direction (Refer Slide Time: 33:39) would become larger while in the stretch direction, it would become smaller from this to there.

Now, intuitively, this is understandable, but it is useful to consider equation for vorticity of fluctuations on the next slide. I will return to 3D cubic element after this explanation.

(Refer Slide Time: 34:05)

Vorticity Dynamics-3 - L23(¹⁵/₁₈)

- Consider large eddy structure where effects of viscosity are small. Then vorticity eqn is $\partial \omega_i / \partial t = \omega_i s_{ij}$
- Now, for simplicity, consider a 2D strain field with $s_{11} = -s_{22} = s$ (a constant) for all times $t > 0$ and, $s_{12} = 0$. Then, if ω_0 is the vorticity at $t = 0$,

$$\frac{\partial \omega_1}{\partial t} = \omega_1 s \rightarrow \frac{\omega_1}{\omega_0} = \exp(st), \quad \frac{\partial \omega_2}{\partial t} = -\omega_2 s \rightarrow \frac{\omega_2}{\omega_0} = \exp(-st)$$

Hence, $(\omega_1)^2 + (\omega_2)^2 = (\omega_0)^2 (\exp(2st) + \exp(-2st))$

- The total vorticity thus increases with $s \times t$. At large values of $s \times t$, ω_1 in the direction of stretching increases rapidly and ω_2 in the direction of compression decreases slowly. Eddies are thus stretched at a rapid rate into smaller eddies. Their growth to larger sizes occurs at a much slower rate resulting in net reduction in their size.

Consider large eddy structure, where effects of viscosity are small. Then vorticity equation will read as $d\omega_i / dt = \omega_i s_{ij}$. Again, vorticity equation is simple; I have not derived here the full form of it. However, when viscosity goes to 0, you could very well take it as that at the moment for the purpose of discussion.

Now, for simplicity, consider a 2D strain field in which only s_{11} is equal to $-s_{22}$; s_{11} being stretching, tensile; s_{22} being compressive; is equal to s and that is equal to constant. These are strain fields for all times t greater than 0 and s_{12} is equal to 0. That is, the strain rate. If ω_0 is the vorticity at time $t = 0$, then from this equation (Refer Slide Time: 35:07), we say that $d\omega_1 / dt$ would be equal to $\omega_1 s$. This is because s_{11} is positive, which would give the solution $\omega_1 / \omega_0 = \exp(st)$. Likewise, $d\omega_2 / dt$ will be equal to $-\omega_2 s$ equal to $\omega_2 / \omega_0 = \exp(-st)$. Therefore, if I were to consider $\omega_1^2 + \omega_2^2$ as the total vorticity; that would be equal to $\omega_0^2 (\exp(2st) + \exp(-2st))$.

Therefore, the total vorticity increases with s multiplied by t at large values of s multiplied by t . ω_1 in the direction of stretching increases very rapidly because of the plus. ω_2 in the direction of compression decreases slowly because of

the minus. What does it tell us? This tells us that the eddies are thus stretched at a rapid rate into smaller eddies. However, their growth to larger eddies occurs at a much smaller rate resulting in the net reduction in their size. This is a very important observation to make from vorticity dynamics.

(Refer Slide Time: 36:32)

Vorticity Dynamics-4 - L23($\frac{16}{22}$)

- When effect of μ is small, angular momentum is conserved. $(\omega')^2 r = \text{const.}$
- In Fig (b), element is stretched in x dirn. Then, KE of rotation in the y-z plane increases at the expense of the KE of velocity component u' which does the stretching.
- Length scales of motion in y-z plane decrease and hence, v' and w' increase.

v' and w' bring about further stretching in y and z directions and, so on. At each stretching, however, the length scale of the element decreases. This is called the breaking down of the eddies.

Now, for the same case when effect of μ is small, then the angular momentum must be conserved or $\omega^2 r = \text{constant}$.

(Refer Slide Time: 36:46)

Vorticity Dynamics-1 - L23($\frac{13}{18}$)

Spectral analysis shows how energy is transferred from large eddies to small eddies. The process of breakdown of eddies, can be understood from vorticity dynamics of the fluctuations.

If we now go back to cubic element, I am stretching it in x 1 direction. Therefore, it shrinks in the y-z plane. However, since angular momentum must reduce length scale, which means increase intensity of vorticity. This would mean v dash and w dash must now increase compared to the state before stretching, whereas u dash is doing the stretching.

(Refer Slide Time: 37:15)

Vorticity Dynamics-4 - L23(¹⁶/₂₂)

- 1 When effect of μ is small, angular momentum is conserved. $(\omega')^2 r = \text{const.}$
- 2 In Fig (b), element is stretched in x dirn. Then, KE of rotation in the y-z plane increases at the expense of the KE of velocity component u' which does the stretching.
- 3 Length scales of motion in y-z plane decrease and hence, v' and w' increase.

v' and w' bring about further stretching in y and z directions and, so on. At each stretching, however, the length scale of the element decreases. This is called the breaking down of the eddies.

Say in figure b, element is stretched in x direction. Then, the kinetic energy of rotation in the y-z plane increases at the expense of the kinetic energy of the velocity component u dash, which does the stretching. Therefore, the length scales of motion in y-z plane decrease and hence, v dash and w dash increase.

Now, this increased v dash and w dash will bring about further stretching in y and z directions and so on. So, you can see that stretching in x direction brings about intensification of velocities in y and z directions, which do further stretching. So, intensification in y will do stretching, which will increase the intensity in z and x direction while reducing the scale. Similarly, intensified w dash would bring about reduction in size in x and y directions and so on and so forth. However, at each stretching, the length scale of the element will go on decreasing. This is called the breakdown of the eddies.

(Refer Slide Time: 38:25)

Summary -1 - L23(17/18)

The tree demonstrates that stretching in x direction (say) intensifies motions in y and z directions; producing smaller scale stretching in these directions and intensifying motions in x, y and, z directions at the end of the second stage and, so on to further stages. As the length scales are progressively reduced, the effects of mean motion are weakened and the small eddies tend towards a universal structure that is homogeneous and isotropic despite the fact that the mean flow and the large scale structure are anisotropic and inhomogeneous.

The breaking down of the eddies would continue indefinitely if it were not for the action of viscosity which kills all fluctuations and maintains the fluid continuum²

²P. Bardshaw, *An Introduction to Turbulence and Its Measurement*, Pergamon Press, Oxford. (1971)

In summary, I can say the tree demonstrates that the stretching in x direction intensifies motions in y and z directions; producing smaller scale stretching in these directions and intensifying motions in x y and z directions at the end of the second stage and so on to the further stages. As the length scales are progressively reduced, the effects of mean motion are weakened and small eddies tend towards a universal structure that is homogeneous and isotropic despite the fact that the mean flow and large scale structure are anisotropic and inhomogeneous.

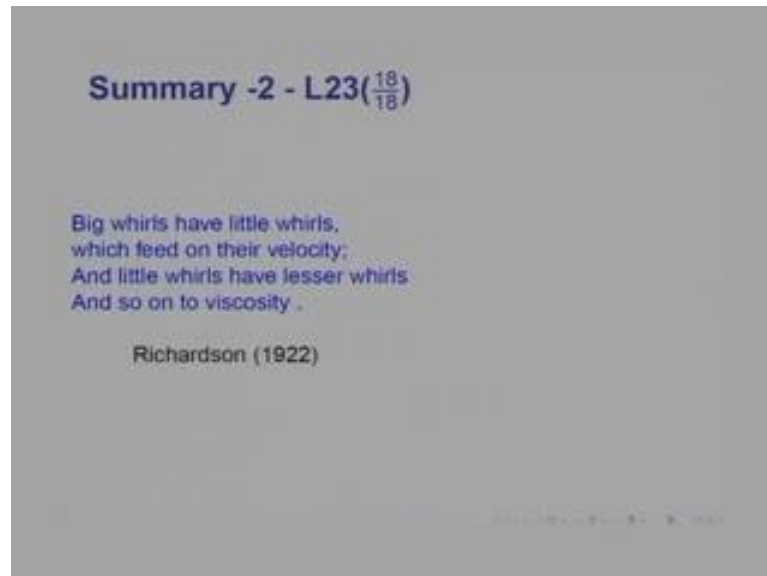
The breakdown of eddies would continue indefinitely if it were not for the action of viscosity, which finally, kills the fluctuations and maintains the fluid continuum. This is the notion, which we started with; we questioned - whether the fluid continuum survives?

In our previous lecture, the first slide - whether the fluid actually spiked up? By observing that the scales at the molecular levels and the scales at the turbulence level being so far separate, we concluded there that the turbulence in no way influences the molecular motions and vice versa. Therefore, there is no question of continuum being brought under question.

As the analysis shows, continuum indeed prevails at small in turbulence. Therefore, as we showed here, (Refer Slide Time: 40:14) the breaking down of the eddies would

continue indefinitely if it were not for the action of viscosity, which kills all fluctuations and maintains the fluid continuum.

(Refer Slide Time: 40:32)



Now, this idea is very well captured in a beautiful poem by Richardson. Big whirrs have little whirrs, which feed on their velocity; and little whirrs have lesser whirrs and so on to viscosity. This poem was written in 1922. The turbulence modules while appreciating the poem very much because it explains to the layman how turbulence sustains itself, they often point out that the existence of the inertial sub range is not revealed in this poem.

However, this was the poem and not science. The existence of inertial sub range in which you have independence from energy containing eddies and the isotropy of the dissipating eddies is not made explicit in this poem. That is well taken, but nonetheless to a layman at least. It is a good take-home message to remember that big whirrs have little whirrs, which feed on their velocity; and the little whirrs have lesser whirrs and so on to viscosity. So, big whirrs indicating large-scale eddies, which creates small-scale eddies and small-scale eddies creates smaller-scale eddies and so on to viscosity.