

Course Name: Design of Electric Motors

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Title: Design of Induction Machine- Rotor Design -5 (Resistance of Rotor Winding)

Greetings to all, in this lecture we will discuss the equations for bar resistance and end ring resistance, because the slip ring induction motor is nothing, but the cage right. So, for cage how to find the resistance value we will discuss in this lecture. Let us take the resistance for a single bar, which we have already discussed. Resistance of the single bar that is R_b is equals to resistivity of the bar material, whether it may be aluminum or copper that is resistivity of the bar material, length of a single bar divided by area of the area cross sectional area of the each bar. This is in the ohms equation number 1 to find the bar resistance, single bar we have discussed. Now, in the last lecture we have discussed the skewing of the rotor bar, right.

This is the actual bar length that is l_e without any skewing. Now, if you will skew the rotor bar, then the length of the bar will definitely will increase, right. If you will consider it as a right angle triangle and skewing angle will be α , where α is equals to skew angle, which is equals to 2π by Q_s is nothing, but slot angle in the, in with respect to the mechanical aspect into P by 2 will give the electrical angle into S s q will give the how many slots we are short skewing. So, α equals to this one and l_e we know and length of the actual bar with skewing we have to calculate.

Then as per the trigonometric equations, length of the skewed bar is equals to l_e divided by $\cos \alpha$. α we know that is 2π by Q_s into P by 2 into S s q by substituting the α value and l_e value, then we can find the length of a bar, skewed bar. After knowing the length of skewed bar, we have to find the end ring resistance also. If we will see the rotor mesh is nothing, but combination of resistance and inductance values like this it will be n number of bars are there and end ring also there, 2 end rings will be there, circular end rings. We can see here this is one end ring, one side and other side one more end ring is there, the rotor structure I am showing here.

This is the resistance of the bar will be R_b , inductance of the bar will be l_b , these things are the end rings one R_e and L_e and resistance of the bar with after skewing it will be R

b and inductance will be L_b . Current flowing through the branch 1, let us consider this is the branch 1 that is I_{b1} and branch 2 is I_{b2} and current flowing here is I_{e1} in the end ring. In this branch also I_{e1} and this is $I_{e\text{ naught}}$. In order to find the equivalent resistance for the rotor mesh, first we have to know the value of the resistance of the each skewed bar and resistance of the each end ring. So, we will calculate the resistance of the end ring first, that is R_e .

Resistance of the end ring R_e is equals to resistivity of the end ring material into length of the end ring divided by area of cross section of the end ring. In the previous lectures, we have discussed and we have calculated the cross sectional area of the end ring also we know and length of the end ring we can calculate it by doing the mean length. Let us consider this is the end ring. The depth will be d_e and thickness will be t_{er} . In order to find the mean length of the end ring, we have to take the outer diameter of the rotor that is $D_{\text{naught } r}$ and inner diameter with respect to the end ring by considering d_c .

So, inner diameter by considering d_c will be $D_{\text{naught } R} - 2d_c$. From here, we can calculate the mean length of the end ring $l_e R$ equals to π into $D_{\text{naught } r} - 2d_c$ plus π into outer diameter of the rotor, that is $D_{\text{naught } R}$ by 2. It will result in π into $D_{\text{naught } R} - d_c$, $d_c R$, depth of the back iron. So, this equation will give the length of the mean length of the end ring by substituting mean length here and resistivity as well as cross sectional area of the end ring. Then we can get the end ring resistance.

Already we have calculated the bar resistance and now we have calculated the end ring resistance also by utilizing this equation. By substituting R_b value and R_e here and from this network, we have to find the effective resistance for the rotor mesh and effective inductance for the rotor mesh. For that, apply a KVL for this loop. This is the loop we can consider. For this loop, apply a KVL equation.

Take the voltage e_1 back EMF with respect to the branch 1, that is, $e_{b1} - e_{b2}$, which is equal to R_b into $I_{b1} - I_{b2}$, other branch resistance current also I am considering plus 2 into, 2 times the end ring resistance are there, right, this side and this side, $2R_e$ into I_{e1} plus L_{di} by dt terms should come, right, L_b into $di_{b1} - I_{b2}$ divided by dt plus 2 times inductance with respect to the end ring into dI_{e1} by dt . This is equation number 4.

Just apply a KVL with respect to the mesh, which I have represented here with blue color. Apply that KVL equation and then, we will see this equation and $I_{b1} + I_{e\text{ naught}}$ is equals to I_{e1} from the above figure. In steady state, the phasor form of the voltages and currents, how we can represent the phasor form of the voltages and currents like e_{b1} , e_{b2} and I_{b1} and I_{b2} are, ok.

So, the e_{b1} is nothing but induced EMF with respect to the bar 2 and e_{b2} is nothing but induced EMF with respect to the bar 2 and e_{b1} is the induced EMF with respect to

the bar 1, ok. e_{b2} , we can represent in terms of e_{b1} that is e_{b1} into some phase shift $e^{j\theta}$, right. Here θ is nothing but phase or bar angle that is equals to 2π by Q or with respect to the mechanical displacement into P by 2 will give the electrical angle conversion, ok. So, $e^{j\theta}$, we can mention here E_{b1} into $e^{j\pi}$ into P by Q r. This is the E_{b2} equation, equation number 5 and in the same manner, if we will represent the I_{b2} is equals to I_{b1} into some phase shift with respect to the phasor form $e^{j\pi}$ into P by q r.

This is equation number 6. Same way the current in N rings I_{e1} is equals to $I_{e\text{ naught}}$, I_{e1} is equals to $I_{e\text{ naught}}$ into $e^{j\pi}$ into P divided by q r. This is the phase shift. In these three equations, what I have done is I am representing the voltages and currents in a phasor form where the phase shift angle between one value to other value like E_{b1} and E_{b2} difference is the angle θ in phasor form $e^{j\theta}$. I am adding for E_{b1} to get the E_{b2} value.

So, by substituting all these equations in the above KVL equation that is equation number 4, $E_{b1} - E_{b2}$, $I_{e1} - I_{e2}$, we have to calculate first. First we will calculate the $E_{b1} - E_{b2}$ is equals to E_{b1} into $1 - e^{j\pi}$ into P by Q r. Similarly, $I_{b1} - I_{b2}$ is equals to I_{b1} into $1 - e^{j\pi}$ into number of poles by Q r.

This is equation number 8, equation number 9 and with respect to the entering currents I_{e1} is equals to $I_{e\text{ naught}}$ plus I_{b1} . Here I_{b1} is equals to $I_{e1} - I_{e\text{ naught}}$ that is equals to I_{e1} current in entering currents I_{e1} into $1 - e^{j\pi}$ into P by Q r.

So, from this equation we can find I_{e1} is equals to I_{b1} divided by $1 - e^{j\pi}$ into P by Q r.

This is equation number 10. By substituting equation number 8, 9, 10 in the KVL equation, we can get the e_{b1} equation like e_{b1} is equals to e_{b1} into $1 - e^{j\pi}$ into P by Q r is equals to I_{b1} into $1 - e^{j\pi}$ into P by Q r. The term will be there into $r + R_b + j\omega l$ into b plus 2 into I_{b1} divided by $1 - e^{j\pi}$ into P by Q s into r plus $j\omega l$ e. In the entering current waveform, sorry in the entering current equation I_{e1} is equals to I_{b1} divided by $1 - e^{j\pi}$ into P by Q r should come.

Here itself it will be minus because $I_{e1} - I_{e\text{ naught}}$ we are doing, right because of that thing it will come I_{e1} into $1 - e^{j\pi}$ into P by Q r. By substituting all equations 8, 9, 10 in the equation number 3, then we will get this equation number 11. After solving this equation by rearranging the terms, then we will get e_{b1} is equals to in the form of I_{b1} into $R_b + j\omega l$ into b plus I_{b1} into r plus $j\omega l$ e divided by 2 into $\sin^2 \pi$ into P divided by Q r $\sin^2 \pi$ by 2 into

$\sin^2 \pi \frac{P}{Qr}$ we will get it. I am not deriving in between steps, you just rearrange the terms here and then find the equation in this fashion.

Then by equating the real and imaginary terms R_b effective resistance of the bar is equals to R_b plus R_e divided by 2 into $\sin^2 \pi \frac{P}{Qr}$. This is the effective resistance of a bar. Now, to find the equivalent resistance per rotor mesh that is R_r is equals to 2 into R_b 2 times the effective resistance of the each bar of the rotor we will consider and we can find the rotor resistance per mesh. This is the final equation to calculate the rotor resistance.

Similarly, inductance terms also we can calculate it. While discussing the inductance equations, we can recall the same equations and we can find the inductance values at that time.

In this lecture, we will focus only with related to the rotor resistance. That resistance equation is the equation number 12. After knowing the rotor resistance, we will find the weight of the rotor cage with respect to the winding. So, weight is equals to density into volume. Here, density with respect to the aluminum we have to calculate or copper we can consider that is density into volume is equals to n or the number of rotor bars into length of each bar into area of cross section of each bar plus 2 into length of end rings into area of cross section of each end ring because 2 end rings are there and n number of rotor bars are there because of that reason N_r into l into area of cross section.

Here, 2 end rings are there because of that reason 2 into l_e into a_{er} we are doing. The total thing we can get it the weight of the rotor cage winding that is equation number 13.

Now, in order to calculate the inner diameter of the rotor, D_{Ir} is equals to we know the outer diameter minus 2 into the slot opening height that is $D_{naught r}$ plus radius at the slot upper side and slot depth d_{sr} and radius at the bottom side of the rotor slot and the back iron width. This equation will give the rotor inner diameter. This rotor inner diameter we can calculate from the output function equations also where we have to calculate the λ_2 is equals to D_{Ir} divided by $D_{naught r}$ where the function f of copper function f of λ_2 f_r of λ_2 and f_{naught} of λ_2 has to be maximized based on this thing.

We can find the λ_2 value. Once we know the λ_2 , then we can find the d_{Ir} value also. Otherwise, we have to follow this equation number 14.

If we will follow the sizing equations, then we have to utilize the copper function with respect to the rotor geometry and output function with respect to the rotor geometry, we can calculate and then associated λ value take it and calculate the inner diameter of the rotor. Similarly, the area of the rotor slot should be greater than the bar area or cross sectional area of the each bar.

If it is winding like slip ring induction motor is there where the windings are there, A_r should be greater than the number of turns per slot into cross sectional area of the each conductor.

With this equation, we can verify the window area with respect to the each slot of the rotor. So, with this, I am concluding this lecture. In this lecture, we have discussed the bar resistance with respect to the skewed rotor and entering resistance and final cage structure of the rotor mesh resistance also equivalent resistance we have calculated. The rotor inner diameter and window check equations we have discussed with this complete rotor geometry with respect to the dimensions with respect to the windings like rotor bars resistance, weight, volume and everything we have calculated. Thank you.